

**Microbial Effects on Ni and Cd  
Sorption and Transport in Volcanic Tuff**

by

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I dedicate this work to my mother and deceased father who have provided love and support throughout my life.



# Chapter 1

## Introduction

## INTRODUCTION

This thesis consists of a submitted journal article and supporting appendices. The purpose of the project was to determine the effect of microbes on cationic transition-metal sorption and transport. The project findings can be applied to land-based metal storage plans and to heavy-metal waste remediation. The methods, results, and discussion of this work are presented in the journal article titled *Microbial Effects on Ni and Cd Sorption and Transport in Volcanic Tuff*, which was submitted to the Journal of Environmental Quality in June, 1993. The objective of the study was to quantify the sorption effects of microbes on  $\text{Cd}^{2+}$  and  $\text{Ni}^{2+}$  to crushed volcanic tuff; then determine what effect the microbe which most influenced  $\text{Ni}^{2+}$  sorption had on  $\text{Ni}^{2+}$  transport in the tuff. Batch equilibrium experiments were performed with aqueous metal solutions. Transport studies were performed by pumping aqueous solution through packed columns. In both sorption and transport experiments, I compared the microbial effects in sterile media to the effects in inoculated media.

Appendix A relates the biological classification of each microbial strain studied to the identification number used to identify strains in other appendices, in my laboratory notebooks, in the frozen cultures at the NMIMT microbiology laboratory, and other persons or groups who collected or stored the strains.

Appendix B contains results from  $\text{Ni}^{2+}$  batch equilibration experiments. Eight experiments were performed to determine the effect of freshly-washed microbes on  $\text{Ni}^{2+}$  sorption to crushed volcanic tuff. Other experiments quantify the effect of  $\text{NaN}_3$  and of freeze-dried *Bacillus megaterium* on  $\text{Ni}^{2+}$  sorption to

tuff. The appendix also displays results from an experiment performed to determine sorption of  $\text{Ni}^{2+}$  to crushed tuff in a buffered system for both sterile samples and for samples inoculated with freshly-washed *B. megaterium*.

Appendix C contains the results of two batch equilibrium experiments performed to quantify  $\text{Cd}^{2+}$  sorption to the crushed volcanic tuff and the results of a kinetic study to determine when sorbed  $\text{Cd}^{2+}$  reaches an equilibrium with  $\text{Cd}^{2+}$  in solution.

Appendix D contains results from the transport study performed using four columns. The appendix includes effluent concentrations from a  $\text{Br}^-$  tracer study,  $\text{Ni}^{2+}$  effluent concentration, results from liquid scintillation counts of samples from each bottle of influent solution, and information on the effluent flux, the water volume in the apparatus, the bulk density, and the influent and effluent pH.

Appendix E contains data on microbial numbers determined by direct microscopic count and by plate counts. I performed direct microscopic cell counts on suspensions used in batch equilibration studies and plate counts on microbes in batch equilibrium samples and in media contained in the columns.

Appendix F contains information on how the autoclave affects the moisture content of tuff.

## Chapter 2

Paper Titled "Effect of Microbes on Ni and Cd Sorption  
and Transport in Volcanic Tuff"

by R. L. Brown, R. S. Bowman, and T. L. Kieft

## ABSTRACT

We performed sorption and transport experiments to determine how vadose-zone microbes affect sorption of  $\text{Ni}^{2+}$  and  $\text{Cd}^{2+}$  on crushed volcanic tuff and transport of  $\text{Ni}^{2+}$  in the same medium. Sorption of  $\text{Ni}^{2+}$  and  $\text{Cd}^{2+}$  to the tuff was less in samples inoculated with microbes than in sterile samples. Since Ni sorption was the same both in the presence and absence of microbes when a buffer was used, microbes appear to decrease sorption by decreasing solution pH. Samples with *Bacillus megaterium* decreased  $\text{Ni}^{2+}$  sorption the most of the 14 subsurface microbial strains tested. Nickel isotherms were linear up to initial concentrations of  $10 \text{ mg L}^{-1}$  with an average distribution coefficient ( $k_d$ ) of  $7.4 \text{ L kg}^{-1}$  for samples with freeze-dried *B. megaterium* and  $50 \text{ L kg}^{-1}$  for sterile samples containing  $1 \text{ g L}^{-1} \text{ NaN}_3$ . Sterile samples without  $\text{NaN}_3$  had a higher  $k_d$  (184 to  $265 \text{ L kg}^{-1}$ ). We therefore predicted that the retardation of Ni in inoculated columns would be lower than in sterile columns. A transport experiment with both inoculated (inoculum consisted of freeze-dried *B. megaterium*) and sterile (solutions contained  $\text{NaN}_3$ ) columns indicated that retardation (R) of Ni was less for columns with microbes (R = 205) than for sterile columns (R = 307), but retardation was higher than predicted by batch sorption experiments in both groups of columns. Dispersion was lower in inoculated columns, possibly due to microbial clogging of secondary pores. The results indicate that microbes can increase the mobility of cationic metals in subsurface environments.

## INTRODUCTION

Preventing hazardous wastes from reaching sensitive environments and remediating waste that is already in the environment requires understanding of microbiological effects on hazardous waste fate and transport. Microbes may significantly influence metal contaminant transport by either increasing or decreasing sorption of metals to surfaces in porous media. Francis (1990) summarized microbial influences on metal solubility as (1) changes in the pH of the solution, (2) redox reactions which affect metal valence states and solubility, (3) chelation, solubilization, and leaching by microbial metabolites and decomposition products, (4) biomethylation and production of volatile and/or toxic alkylated metal compounds, and (5) biodegradation of metal-organic complexes. Microbes are also capable of sorbing metals (Kelly et al., 1979; Beveridge, 1986). This could lead to increased proportions of metals in the solid phase, but also to increased colloidal transport of the metals. These effects need to be considered for remediation efforts and for prediction of contaminant fate.

Several studies have shown that microbes can decrease sorption of  $\text{Cd}^{2+}$  and  $\text{Ni}^{2+}$  to a medium. Chanmugathas and Bollag (1987) determined that mobilization of strongly bound Cd is microbially mediated. For some but not all soils in their study, the release of Cd was accompanied by a decrease in the soil suspension pH. Burke et al. (1991) determined that sediments containing microbes sorb less Cd than sediments that are autoclaved. In a study by Gerringa (1990) many metals, including Cd, increased in mobility concomitant with aerobic degradation of organic matter. Wildung et al. (1979) found that many metal-tolerant microbes produce metabolites that complex with

Ni and increase Ni transport through soil.

The objective of this study was to determine the effects of vadose-zone microbes on the sorption of  $\text{Ni}^{2+}$  and  $\text{Cd}^{2+}$  and transport of  $\text{Ni}^{2+}$  in crushed volcanic tuff. The tuff we used is similar to that which underlies the proposed high-level radioactive waste repository at Yucca Mountain, Nevada, and low-level radioactive waste disposal sites at Los Alamos National Laboratory, New Mexico. Both Ni and Cd, as well as other heavy metals, may occur in industrial waste, in sewage sludge, and in long-term waste storage facilities.  $\text{Ni}^{2+}$  served as a model of other heavy metals in the +2 valence state.  $\text{Ni}^{2+}$  is stable in aqueous solutions over a wide range of Eh and pH (Deltombe et al., 1974). Although high Ni concentrations are toxic (Drake, 1988), Ni is an essential trace element for bacteria, plants, and animals (Ankel-Fuchs and Thauer, 1988). Many bacteria require Ni for the synthesis of nickel hydrogenase. Nickel toxicity in microorganisms depends on the type of organism and on the growth medium (Kaltwasser and Frings, 1980). We performed sorption experiments with  $\text{Cd}^{2+}$  for comparison with the Ni data. Cd has been implicated in health problems in humans and animals (Friberg et al., 1971).

## MATERIALS AND METHODS

### Porous Medium

The porous medium was Bandelier tuff which was crushed and sieved to less than 250  $\mu\text{m}$ . The tuff was obtained from a rock quarry along Jemez Road across from the Meson Center SE of the city of Los Alamos, NM. Twenty-nine percent of the crushed tuff was between 149 and 250  $\mu\text{m}$ , 49% was between 44 and 149  $\mu\text{m}$  and 22% was less than 44  $\mu\text{m}$  in diameter. X-ray fluorescence analysis indicated that the tuff was composed primarily of  $\text{SiO}_2$ , with significant portions of Al, K, Na, and Fe oxides (Table 1). X-ray diffraction analysis indicated that the tuff contained much quartz, minor anorthoclase, and either cristobalite or opal, but no clay minerals.

### Microbes

We investigated sorption effects of 14 microbial strains that were isolated from the vadose zone of the Pajarito Plateau at Los Alamos National Laboratory (LANL) in July, 1987. The microbes were present in tuffaceous cores collected using a continuous auger drilling technique and sterile split-spoon samplers (Hersman et al., 1988). Depths of sampling ranged from 15.2 to 53.3 m. The core samples contained 10 to 100 culturable microbes or colony forming units (CFU)  $\text{g}^{-1}$  dry weight soil and  $2.0$  to  $9.5 \times 10^6$  total cells  $\text{g}^{-1}$  based on direct microscopic counts. Microbial cultures were supplied by W. C. Ghiorse, Cornell University. To preserve the cultures, a mixture consisting of 50% glycerol and 50% cells suspended in a complex growth medium was frozen at  $-80^\circ\text{C}$ . The microbes, identified by fatty-acid methyl ester profiles (Microbial ID, Inc., Newark, DE), consisted of yeasts and both Gram-negative and Gram-positive



Table 1. Composition of tuff as determined by X-Ray fluorescence.

| Oxide                              | Weight % |
|------------------------------------|----------|
| SiO <sub>2</sub>                   | 79.5     |
| TiO <sub>2</sub>                   | 0.09     |
| Al <sub>2</sub> O <sub>3</sub>     | 11.9     |
| Fe <sub>2</sub> O <sub>3</sub> -T* | 1.37     |
| MgO                                | 0.04     |
| CaO                                | 0.15     |
| K <sub>2</sub> O                   | 3.97     |
| Na <sub>2</sub> O                  | 3.97     |
| MnO                                | 0.05     |
| P <sub>2</sub> O <sub>5</sub>      | 0.01     |
| S                                  | 0.007    |
| LOI**                              | 0.45     |
| Total                              | 100.51   |

\*Fe<sub>2</sub>O<sub>3</sub>-T = Total iron calculated as Fe<sub>2</sub>O<sub>3</sub>

\*\*LOI = Loss on ignition

bacillus and coccoid bacteria (Table 2). One unidentified yeast from 15.2 m had a profile that was similar to both *Cryptococcus* and *Candida*.

### Sorption Experiments

Prior to the batch equilibration experiments, we acid-washed 250-mL polypropylene flat-bottom centrifuge bottles and 50-mL polyallomer Oak Ridge-Type centrifuge tubes in 5% HCl solution. We made all solutions using NANOpure water (Barnstead, Dubuque, IA). All solutions, centrifuge bottles (used for washing microbes), and glass pipettes were sterilized by autoclaving at 121°C for 20 min. To prepare the sterile tuff, we first measured 10 g of the crushed tuff into the centrifuge tubes, then autoclaved the tubes for 1 h at 121°C for three successive days. To produce sufficient quantities of microbes for the experiments, we inoculated a broth consisting of 1.0 g glucose, 1.0 g Difco yeast extract (Difco Laboratories, Detroit, MI), 0.5 g Difco bactopectone, 0.6 g  $\text{MgSO}_4 \cdot \text{H}_2\text{O}$ , and 0.07 g  $\text{CaCl}_2 \cdot 2\text{H}_2\text{O}$  in 1 L distilled water. This is a modification of a growth medium developed by Balkwill and Ghiorse (1985). The incubating microbes were shaken on a rotary shaker at 150 rpm at room temperature (about 25°C) for two days. We washed the cells by centrifuging at 19000 x g, pouring off the supernatant, and resuspending the pellet in 0.005 M  $\text{CaCl}_2$  solution. The washing procedure was repeated twice. The optical density of the final suspension averaged 0.76 with a standard deviation (sd) of 0.18) for all experiments performed with freshly washed microbes.

We performed all batch equilibrium experiments in triplicate. We mixed 10 g of sterile tuff with 10 mL of 0.005 M  $\text{CaCl}_2$  solution for sterile samples or 10 mL of the microbial suspension for inoculated samples. Each sample was vortex-mixed for 30 s and then placed on a reciprocal shaker at 100 rpm for about 16 h, allowing the microbes to adjust to new conditions. We then added

Table 2. Microbes identified by fatty-acid methyl ester profiles and depths from which they were obtained.

| Classification                             | Depth (m) | # of strains |
|--|-----------|--------------|
| Bacteria: <i>Arthrobacter oxydans</i>      | 45.7      | 1            |
|  | 53.3      | 3            |
| <i>Bacillus megaterium</i>                 | 53.3      | 1            |
| <i>Clavibacter michiganense insidiosum</i> | 15.2      | 1            |
| <i>Pseudomonas</i> (species not known)     | 15.2      | 4            |
| <i>Rhodococcus fascians</i>                | 15.2      | 1            |
| Yeast: <i>Candida famata</i>               | 53.3      | 1            |
| <i>Cryptococcus albidus</i>                | 15.2      | 1            |
| Unidentified yeast                         | 15.2      | 1            |

10 mL of NiCl<sub>2</sub> spiked with <sup>63</sup>Ni or 10 mL CdCl<sub>2</sub> solution at double the desired initial concentrations. We used initial Ni<sup>2+</sup> concentrations of 0.01 to 20 mg L<sup>-1</sup> and initial Cd<sup>2+</sup> concentrations from 5 to 125 mg L<sup>-1</sup>. To determine the relative effects of each microbial strain on Ni sorption, we used initial concentrations of 10 mg L<sup>-1</sup>. All solutions were added under a HEPA filter sterile hood (Environmental Air Control, Inc., Hagerstown, MD). The samples were shaken for an additional 24 h (determined in preliminary Cd<sup>2+</sup> experiments to be sufficient time to attain sorption equilibrium). Then we centrifuged them at 27000 x g for 15 min and analyzed the supernatant for metal concentrations. We used inductively coupled plasma emission spectroscopy to analyze Cd. We quantified <sup>63</sup>Ni concentration using a Packard Tri-Carb 460 CD liquid scintillation counter (Packard Instrument Co., Downers Grove, IL). The samples for most of the Ni<sup>2+</sup> batch experiments were prepared by adding 1 mL of aqueous sample to 20 mL of Universol scintillation cocktail (ICN Biomedical, Irvine, CA). The samples for the transport study and the latter batch studies were prepared by adding 1 mL of aqueous sample to 14 mL of either Universol or ScintiVerse I scintillation cocktail (Fisher Scientific, Pittsburgh, PA). There was no statistically significant difference between the counts from the two cocktail types. The quench factor was the same for all samples. We subtracted the background counts from all sample counts.

We performed other batch experiments to determine the effects of (1) using freeze-dried *Bacillus megaterium* instead of freshly grown microbes, (2) pH, and (3) NaN<sub>3</sub> on Ni<sup>2+</sup> sorption to crushed tuff. All of these experiments

were performed concurrently with sterile samples not containing  $\text{NaN}_3$ . To determine if the microbes decreased sorption by changing the solution pH, some isotherms were prepared in buffered systems. The buffer consisted of 0.57 g  $\text{KH}_2\text{PO}_4$  and 6.24 g  $\text{K}_2\text{HPO}_4$  mixed with 100 mL of NANOpure water to make a 0.4 M solution. We did not use  $\text{CaCl}_2$  as an electrolyte in samples with buffer because a precipitate formed when  $\text{CaCl}_2$  and  $\text{K}_2\text{HPO}_4$  were mixed together. We first added 5 mL of buffered solution and 5 mL of suspension for the inoculated group of samples or 5 mL of buffered solution and 5 mL of distilled water for the sterile group of samples to 10 g of the tuff. We used an initial  $\text{Ni}^{2+}$  concentration of  $10 \text{ mg L}^{-1}$ . At the end of the experiment, the pH of the supernatant was measured using a gel-filled polymer-body combination pH electrode with an Ag/AgCl reference. To determine the  $\text{NaN}_3$  effect on  $\text{Ni}^{2+}$  sorption, we added a 10-mL mixture of  $2 \text{ g L}^{-1} \text{ NaN}_3$  and  $0.005 \text{ M CaCl}_2$  solution to 10 g of tuff. Brock (1978) showed that  $1 \text{ g L}^{-1} \text{ NaN}_3$  (the final solution concentration in our experiments) effectively inhibits microbial activity. To determine the effect of freeze-dried *B. megaterium* on  $\text{Ni}^{2+}$  sorption, we first froze a suspension of washed microbes in  $0.005 \text{ M CaCl}_2$  solution at  $-50^\circ\text{C}$  in a shell freezer (Labconco, Kansas City, MO) and dried them with a lyophilizer (Labconco). Prior to performing experiments, the freeze-dried cells were suspended in a  $0.005 \text{ M CaCl}_2$  solution. Mixing the suspension with the tuff resulted in about 2.4 mg of freeze-dried microbes per g of tuff or  $5.2 \times 10^8 \text{ cells g}^{-1}$  determined by direct count. The initial  $\text{Ni}^{2+}$  concentrations for experiments with both freeze-dried microbes and with  $\text{NaN}_3$  were 1, 4, 7, and  $10 \text{ mg L}^{-1}$ .

## Transport Experiment

The transport experiments were performed in 5-cm tall by 5-cm diameter Plexiglas columns. These columns were made from 30-cm columns purchased from Soil Measurement Systems (Tucson, AZ). The stainless steel porous endplates had air entry values of 25 kPa and pore diameters of 0.5  $\mu\text{m}$ . Rubber O-rings were placed next to the porous endplates for sealing purposes. In addition we used 3.2-mm I.D. silicone tubing, polypropylene dual check valves (Manostat, New York, NY), 3-mL plastic luer-lok tip syringes, low-density polyethylene connectors, and glass influent bottles and sampling tubes.

Prior to the transport experiment, we sterilized all apparatus, solutions, and crushed tuff. We sterilized the columns, connectors, check valves, and O-rings by placing them over boiling water for 10 min on three successive days (tyndallization). Solutions, tubing, and other labware were autoclaved at 121°C for 20 min. The tuff was divided into two containers, each with 400 g, then autoclaved at 121°C for 1 h for 3 consecutive days. We dried the sterile tuff at 100°C for 24 h, then cooled it to room temperature ( $\sim 25^\circ\text{C}$ ). Packing was done in the sterile hood using sterile gloves. The freeze-dried microbes were mixed thoroughly with one container of tuff (1.3 mg freeze-dried microbes  $\text{g}^{-1}$  tuff) prior to packing the columns. Two columns were packed with sterile tuff and two with inoculated tuff. To pack the columns, we transferred the tuff into a funnel with the bottom of the funnel placed directly on the bottom of the column. We lifted the funnel slightly so the tuff slid into the column, then moved the funnel around the bottom to distribute the tuff. After about 0.5 cm of tuff had accumulated, the column was vibrated for about 10 s to settle the tuff. Then the process was repeated until the column was full. This resulted in an average dry

bulk density of  $1390 \text{ kg m}^{-3}$  for the four columns. When the packing was complete, we cleared the top of the column using a sterile pipette attached to a vacuum, then inserted the sterile rubber O-ring and placed the end plate and top on the column. The average saturated hydraulic conductivity was  $2.3 \times 10^{-6} \text{ m s}^{-1}$  (sd =  $7.1 \times 10^{-7}$ ) for two columns packed in this manner, determined using the falling-head permeameter method (Todd, 1959).

After packing, we filled the columns from the bottom with sterile  $0.005 \text{ M CaCl}_2$  solution at a rate of  $605 \text{ mL/day}$ . Solutions were pumped into the columns using a multichannel syringe pump (Soil Measurement Systems). To maintain sterile conditions, all solutions entering the sterile columns contained  $1 \text{ g L}^{-1} \text{ NaN}_3$ . Approximately 30 pore volumes (PVs) were pumped through each column prior to adding a constant supply of  $0.005 \text{ M CaCl}_2$ ,  $9.3 \text{ mg L}^{-1} \text{ Ni}^{2+}$  solution. After about 270 PVs ( $\sim 11 \text{ L}$ ) of Ni solution had passed through each column, we pumped a solution containing  $8.5 \text{ mg L}^{-1} \text{ Br}^-$  (sterile columns) or  $7.45 \text{ mg L}^{-1} \text{ Br}^-$  (inoculated columns) in addition to  $9.3 \text{ mg L}^{-1} \text{ Ni}^{2+}$  for about 30 PVs to determine the characteristics of nonreactive tracer flow through the columns. Then we continued adding Ni solution without Br.  $\text{Br}^-$  was analyzed using high performance liquid chromatography. The total volume of Ni solution pumped was about 530 PVs ( $\sim 21 \text{ L}$ ) for the sterile columns and 850 PV ( $\sim 34 \text{ L}$ ) for inoculated columns. Column pore volumes were determined from the weight of water present in each column at the end of the experiment and corrected for the volume of water in the apparatus (endplates and connecting tubing).

## Microbe Enumeration

To determine the number of culturable bacteria, we performed plate counts as described by Kieft and Rosacker (1991). We used growth medium consisting of 0.1 g glucose, 0.1 g Difco yeast extract, 0.05 g Difco bacto-peptone, 0.6 g  $\text{MgSO}_4 \cdot \text{H}_2\text{O}$ , 0.07 g  $\text{CaCl}_2 \cdot 2\text{H}_2\text{O}$ , 15 g Difco Bacto-agar, and 1 L distilled water (another modification of the medium developed by Balkwill and Ghiorse, 1985). To determine how  $\text{Ni}^{2+}$  affected the viability of microbes in the saturated crushed tuff during the batch equilibrium experiment, we performed plate counts for batch equilibration experiments with both freshly cultured microbes and freeze-dried microbes on the microbe suspension, the tuff-suspension mixture immediately prior to adding Ni solution, and the tuff-suspension mixture after adding Ni and shaking for 24 h. We also performed plate counts on the crushed tuff used for column experiments. We sampled both the tuff used to pack the columns and the tuff taken from the center of each column at the end of the transport experiment. We performed direct counts using a Petroff-Hausser counting chamber (Hausser Scientific Partnership, Horsham, PA) and phase contrast microscopy to determine the number of cells in relation to culturable cells. When the samples could not be counted immediately, we preserved the 10 mL suspension with 200  $\mu\text{L}$  of glutaraldehyde.



## RESULTS AND DISCUSSION

### Microbial Numbers

The number of culturable microbes remained approximately  $10^6$  to  $10^7$  CFU  $g^{-1}$  tuff during batch experiments using either freshly grown or freeze-dried *B. megaterium* (Table 3). We conclude that *B. megaterium* mixed with crushed tuff and aqueous solution is not susceptible to the toxic effects of  $Ni^{2+}$  for the concentration range of 0 to 100 mg  $L^{-1}$  and that the microbes continue to be metabolically active in the presence of  $Ni^{2+}$  and crushed tuff.

The dry tuff used to pack the columns contained  $1.5 \times 10^3$  CFU  $g^{-1}$  tuff. After unpacking the columns, one inoculated column contained  $1.0 \times 10^5$  CFU  $g^{-1}$  tuff and the other contained  $1.3 \times 10^5$  CFU  $g^{-1}$ . No culturable cells were detected in the sterile columns at the end of the experiment. Assuming that the number of cells was 20 x the cultured number (as indicated by comparing plate counts of the microbial suspensions to direct counts), the volume of each microbe was  $1 \mu m^3$ , and the bulk density of the tuff was  $1390 \text{ kg } m^{-3}$ , the volume occupied by the microbes in the inoculated columns was  $3.2 \text{ cm}^3 m^{-3}$  of porous medium. Assuming the area of each microbe is  $0.7 \mu m^2$ , the surface area covered was  $2.2 \text{ mm}^2 \text{ cm}^{-3}$ .

### Ni Sorption Experiments

We prepared sorption isotherms with initial Ni concentrations of 1, 4, 7, and 10 mg  $L^{-1}$  to determine the effect of  $NaN_3$  and of freeze-dried *B.*

Table 3. Culturable microbe numbers from batch sorption experiments using *B. megaterium*. Each sample was taken from a separate tube.

| Stage sample was taken  | Freshly Washed<br>Microbes<br>(CFU g <sup>-1</sup> tuff) | Lyophilized<br>Microbes<br>(CFU g <sup>-1</sup> tuff) |
|---|--|---|
| Immediately following inoculation:                                | 4.7 x 10 <sup>7</sup>                                    | 2.9 x 10 <sup>7</sup>                                 |
| After shaking slurry for 16 hours,<br>but prior to adding Ni ion: | 1.1 x 10 <sup>7</sup>                                    | 1.1 x 10 <sup>7</sup>                                 |
| After adding Ni ion and shaking<br>an additional 24 hours:        |  |   |
| Ni <sup>2+</sup> concentration = 0 mg L <sup>-1</sup>             | 7.9 x 10 <sup>6</sup>                                    | -   |
| Ni <sup>2+</sup> concentration = 0.01 mg L <sup>-1</sup>          | 9.3 x 10 <sup>6</sup>                                    | -   |
| Ni <sup>2+</sup> concentration = 1.0 mg L <sup>-1</sup>           | 8.0 x 10 <sup>7</sup>                                    | -   |
| Ni <sup>2+</sup> concentration = 10.0 mg L <sup>-1</sup>          | -  | 1.4 x 10 <sup>7</sup>                                 |
| Ni <sup>2+</sup> concentration = 100 mg L <sup>-1</sup>           | 1.3 x 10 <sup>7</sup>                                    | -   |

*megaterium* on Ni sorption (Fig. 1). For this concentration range, the isotherms were linear and could be characterized by a distribution coefficient ( $k_d$ ) where:

$$S = k_d C$$

S is the sorbed concentration and C is the solution concentration. The average  $k_d$  for sterile samples without  $\text{NaN}_3$  was  $158 \text{ L kg}^{-1}$  (sd =  $50 \text{ L kg}^{-1}$ , the number of samples (n) = 10). Sodium azide decreased  $\text{Ni}^{2+}$  sorption ( $k_d = 49.9 \text{ L kg}^{-1}$ , sd = 1.7, n = 2); however sorption in the presence of  $\text{NaN}_3$  was significantly higher than sorption in two experiments using samples inoculated with freeze-dried *B. megaterium* ( $k_d = 7.4 \text{ L kg}^{-1}$ , sd = 0.5). A factor that may lend support to these findings is that the  $\text{Ni}^{2+}$  sorption for samples inoculated with *B.*

*megaterium* was similar to sorption of  $\text{Ni}^{2+}$  to nonsterile crushed tuff ( $k_d = 8.2 \text{ L kg}^{-1}$ ) in a study by Bowman et al. (1981). However, the tuff they used probably had different chemical and physical properties since it was not autoclaved and consisted of larger diameter grains.

Isotherms were also linear for initial  $\text{Ni}^{2+}$  concentrations less than  $10 \text{ mg L}^{-1}$  for other microbes including *Candida famata*, *Rhodococcus fascians*, and an *Arthrobacter oxydans* strain. We thus assumed the isotherms were linear for all microbes tested at an initial concentration of  $10 \text{ mg L}^{-1}$ . All of the microbes caused decreased sorption of  $\text{Ni}^{2+}$ ; however, the degree of the effect varied among microorganisms (Fig. 2). *B. megaterium* consistently decreased sorption of  $\text{Ni}^{2+}$  more than other microorganisms. For experiments with an initial  $\text{Ni}^{2+}$  concentration of  $10 \text{ mg L}^{-1}$ , the average  $k_d$  for all 14 microbial strains tested

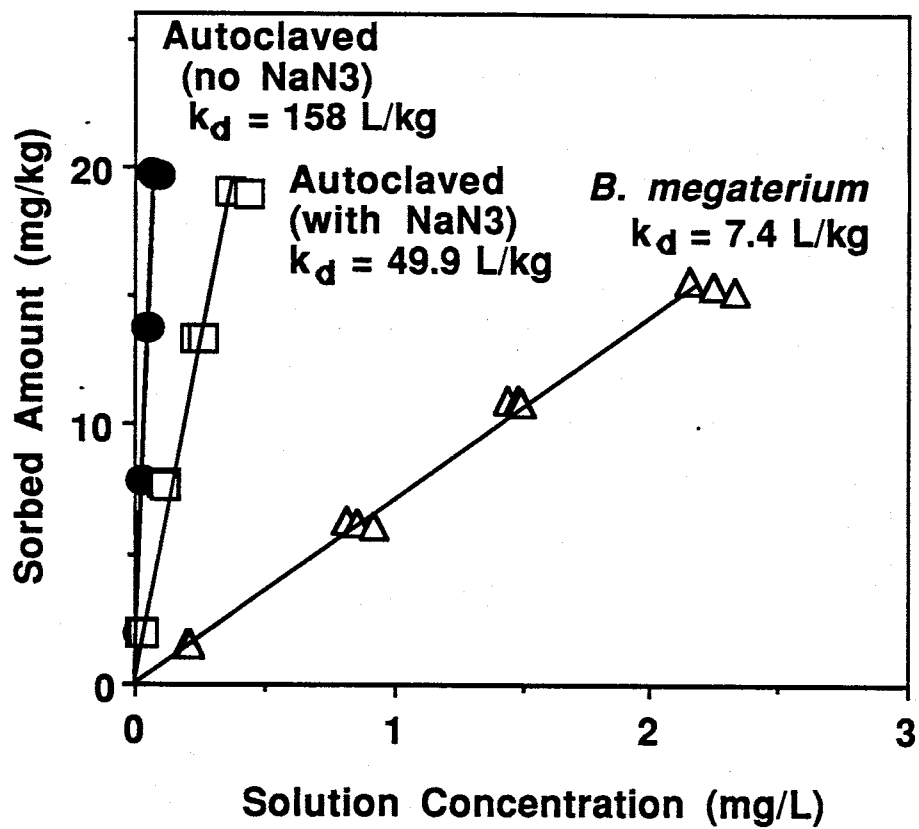


Fig. 1. Linear Ni isotherms for autoclaved tuff with and without  $\text{NaN}_3$ , and for tuff inoculated with freeze-dried *B. megaterium*.

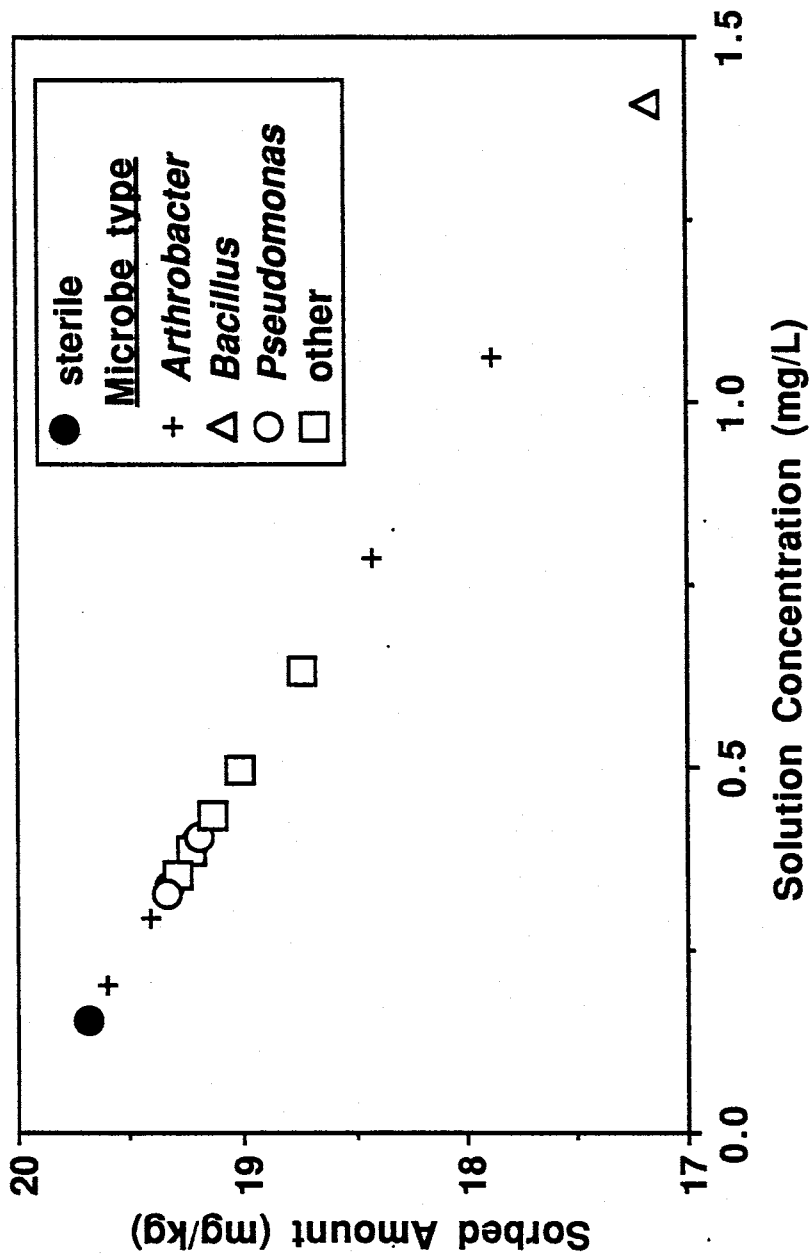


Fig. 2. The effect of each microbial strain on Ni sorption to tuff. Initial  $Ni^{2+}$  concentration was  $10 \text{ mg L}^{-1}$ . Data points are averages of experiments with each microbial strain. For most microbes, the results are from averages of triplicates from one experiment. For *B. megaterium* and *C. famata*, the results are from an average of three experiments.

was  $44.5 \text{ L kg}^{-1}$  (sd = 22.7, n = 14). All *Pseudomonas* strains affected sorption to a similar degree with an average  $k_d$  of  $52.1 \text{ L kg}^{-1}$  (sd = 5.7, n = 4); however, different strains of *Arthrobacter* exhibited varying sorption with an average  $k_d$  of  $52.0 \text{ L kg}^{-1}$ , but a standard deviation of 35.4 (n = 4). Inconsistencies between isotherms from different experiments using either sterile samples or samples inoculated with a specific microbial strain may be explained by the bacteria being in different growth phases, by different quantities of microbes being added to the sample, or by different temperatures for different experiments. Temperatures ranged from 24 to 30°C.

Although bacteria may decrease sorption of metals by decreasing the pH, producing chelating agents, or by influencing the oxidation state of the metals through redox reactions, the decreased sorption of  $\text{Ni}^{2+}$  to the crushed tuff in our experiments appears to be caused mostly by microbially produced acid (Fig. 3). For an initial concentration of  $10 \text{ mg L}^{-1}$ , supernatant pH was 1.1 units less in inoculated samples than in sterile samples. For samples buffered to pH 7.8 - 7.9, the  $\text{Ni}^{2+}$  sorption was equal in sterile samples and samples inoculated with *B. megaterium*. The supernatant resulting from washing the microbes did not affect sorption.

#### Cd Sorption Experiments

To determine if microbes had a similar effect on sorption of other divalent transition metals, we prepared  $\text{Cd}^{2+}$  isotherms using an initial concentration range of 6 to  $126 \text{ mg L}^{-1}$  (Figs. 4 and 5). The isotherms were logarithmic as has been previously observed in studies with  $\text{Ni}^{2+}$  and  $\text{Cd}^{2+}$  sorption on soils for

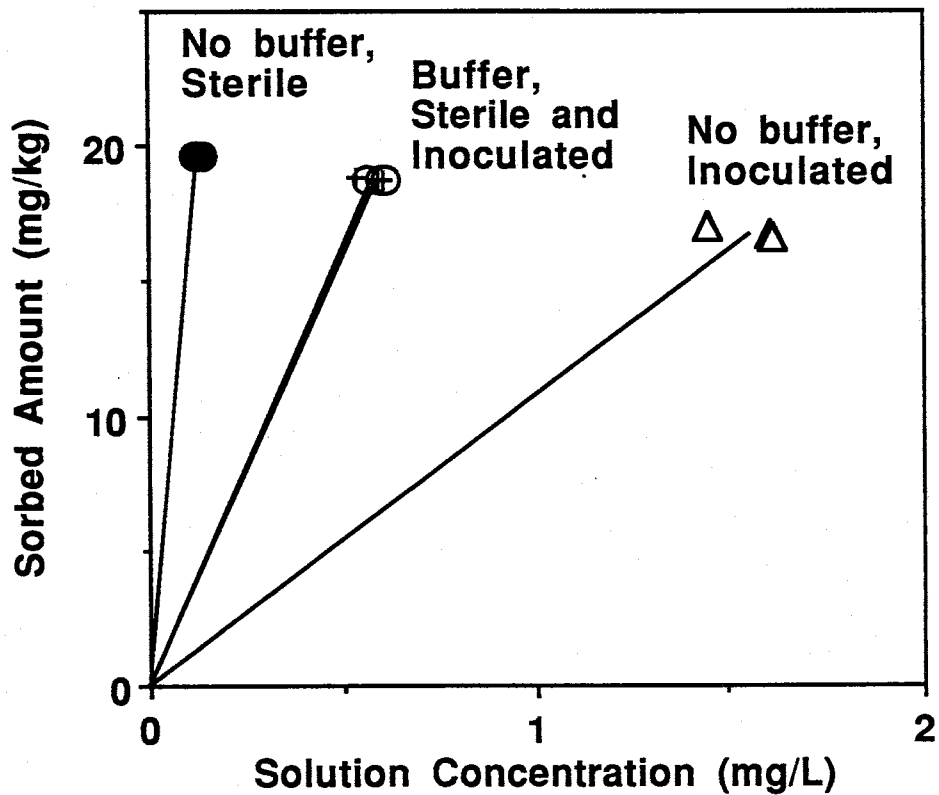


Fig. 3. Ni sorption isotherms showing the pH effect on samples inoculated with *B. megaterium*. ● = sterile samples without buffer (pH = 8.2), ○ = sterile samples with buffer (pH = 7.9), + = inoculated samples with buffer (pH = 7.8), △ = inoculated samples without buffer (pH = 7.1)

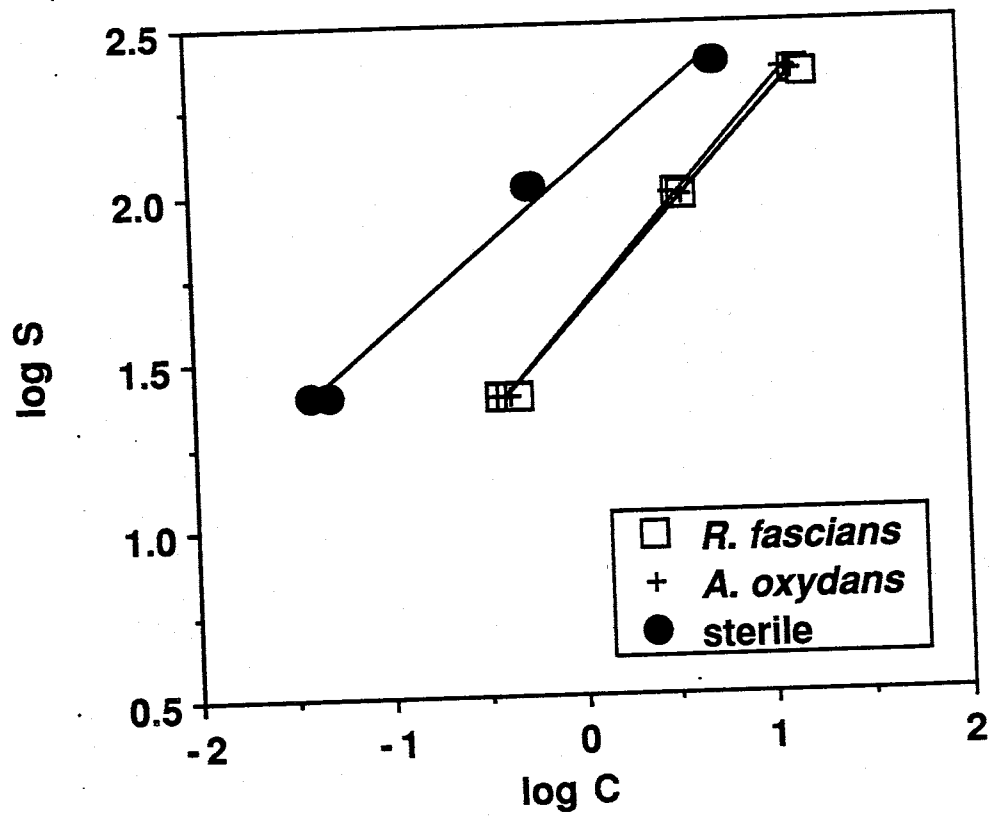


Fig. 4. Logarithmic Cd sorption isotherms for initial Cd concentrations of 13 to 120 mg L<sup>-1</sup> on sterile and inoculated tuff.



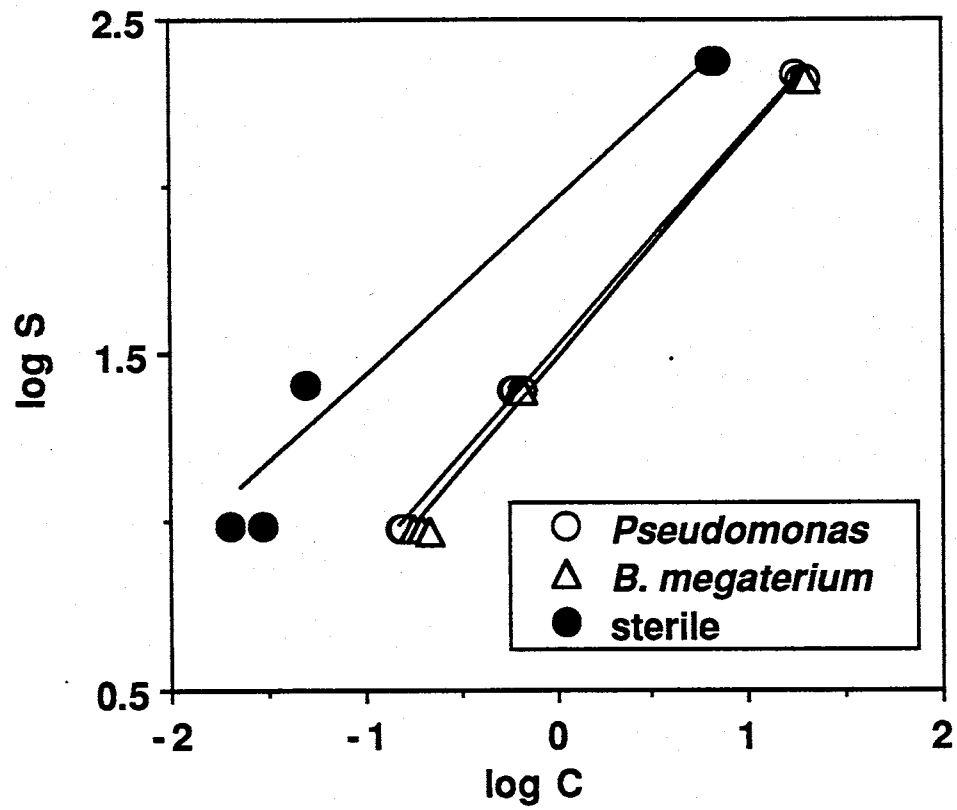


Fig. 5. Logarithmic Cd sorption isotherms for initial  $\text{Cd}^{2+}$  concentrations of 13 to 120  $\text{mg L}^{-1}$  on sterile and inoculated tuff.

initial concentrations above 10 mg L<sup>-1</sup> (Bowman et al., 1981; O'Connor et al., 1984) and can be described for both metals by the Freundlich sorption equation:

$$\log S = \log k_f + N \log C$$

where N is the Freundlich isotherm exponent and  $k_f$  is the Freundlich isotherm constant. If S is expressed in units of mg kg<sup>-1</sup> and C is in units of mg L<sup>-1</sup>, then N for sterile samples ranged from 0.52 and 0.62 and  $k_f$  ranged from 89 to 115. Variability may have been caused by performing experiments at different temperatures. For isotherms resulting from inoculating samples with *R. fascians*, an *A. oxydans* strain, *B. megaterium*, or a *Pseudomonas* strain, N was similar to the values for sterile treatments, ranging from 0.62 to 0.66;  $k_f$  was lower, ranging from 30 to 43. For all experiments, sorption of Cd<sup>2+</sup> to tuff decreased when microbes were present. The difference in sorption may have been caused by the microbes lowering the pH of the solution; however, we did not measure the supernatant pH or perform any Cd<sup>2+</sup> experiments with buffer.

#### Transport Experiment

Br<sup>-</sup> and Ni<sup>2+</sup> BTCs are shown in Figs. 6 and 7. We used the curve-fitting program CXTFIT (Parker and van Genuchten, 1984) to fit the parameters of the 1-dimensional advection-dispersion equation to the experimental BTCs.

Assuming that R is unity for Br<sup>-</sup> BTCs, we fitted the pore-water velocity (v), the dispersion coefficient (D), and the pulse to all four columns in the time domain, using the one-region, flux concentration model (Table 4). We used the fitted parameters from the Br<sup>-</sup> BTCs to calculate R for Ni<sup>2+</sup> BTCs (Table 5).

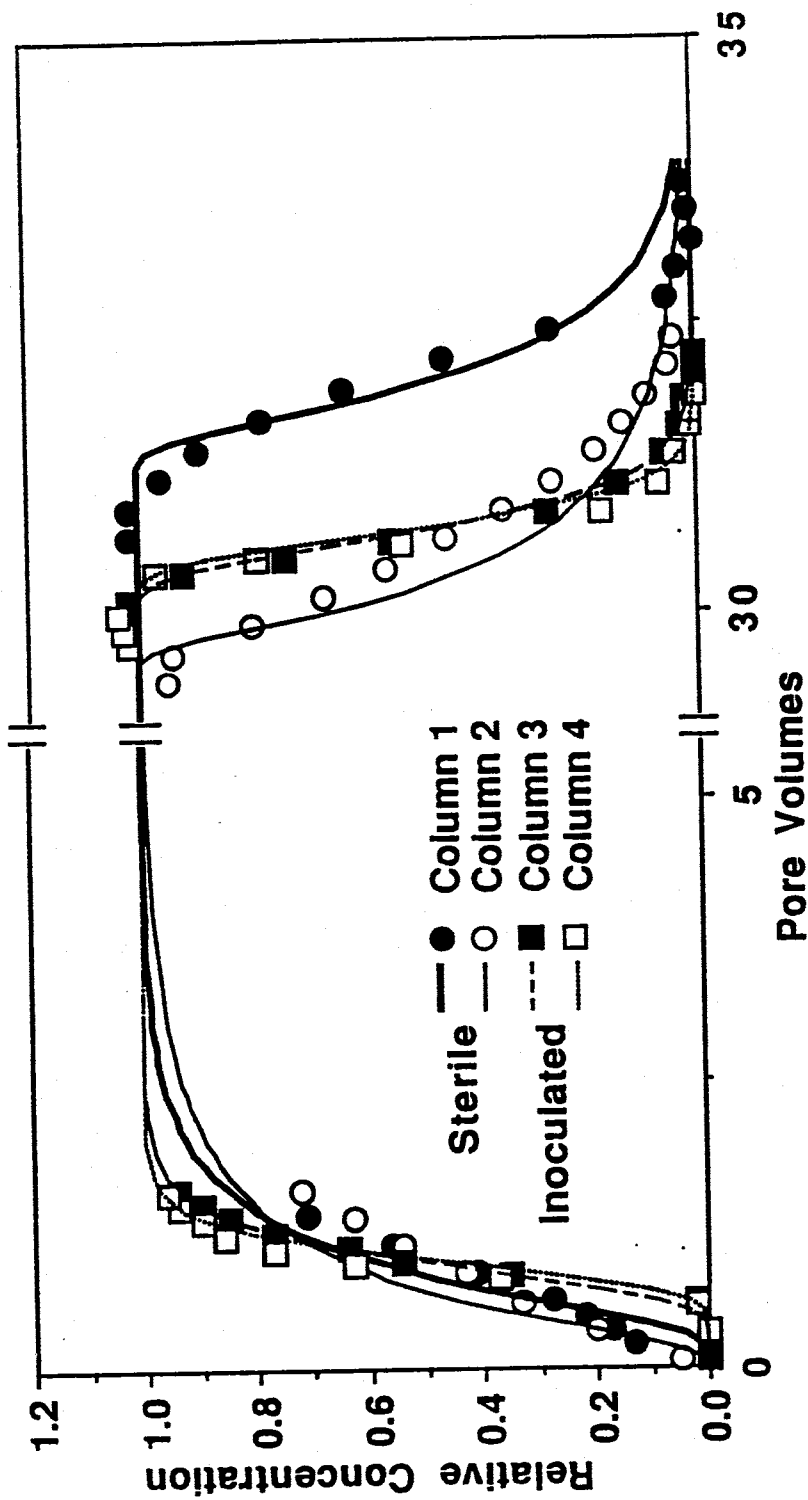


Fig. 6.  $\text{Br}^-$  breakthrough curves. We did not measure  $\text{Br}^-$  concentrations of sample effluent between 2 and 22 pore volumes. Curves were fitted using CXTFIT.

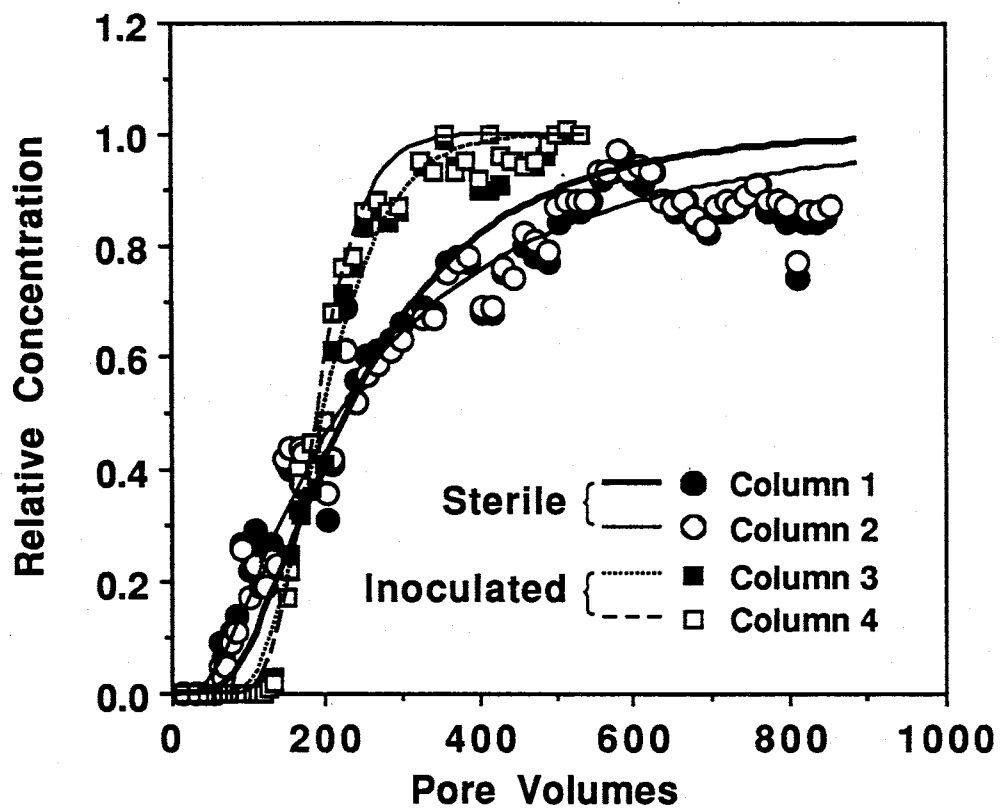


Fig. 7.  $Ni^{2+}$  breakthrough curves. Curves were fitted using CXTFIT.

Table 4. CXTFIT parameters for Br<sup>-</sup> BTCs (one-region model). 95% confidence intervals are given.

|  | Sterile Columns |              | Inoculated Columns |              |
|--|-----------------|--------------|--------------------|--------------|
| Column number                          | 1               | 2            | 3                  | 4            |
| Input parameter:                       |                 |              |                    |              |
| R                                      | 1               | 1            | 1                  | 1            |
| Fitted parameters:                     |                 |              |                    |              |
| $v_{Br}$ (cm day <sup>-1</sup> )       | 73.4 ± 10.9     | 56.5 ± 7.6   | 77.7 ± 2.5         | 84.8 ± 3.1   |
| D (cm <sup>2</sup> day <sup>-1</sup> ) | 78.8 ± 34.2     | 133.7 ± 47.5 | 23.2 ± 4.8         | 14.3 ± 4.3   |
| Pulse (day)                            | 2.03 ± 0.01     | 1.99 ± 0.01  | 2.01 ± 0.003       | 1.99 ± 0.003 |
| R <sup>2</sup>                         | 0.96            | 0.97         | 0.99               | 0.99         |

Table 5. CXTFIT parameters for Ni<sup>2+</sup> BTCs (one region model). 95% confidence intervals are given.

| Column number                            | Sterile Columns |          | Inoculated Columns |         |
|--|-----------------|----------|--------------------|---------|
|  | 1               | 2        | 3                  | 4       |
| Input parameters:                        |                 |          |                    |         |
| $v_{Ni}$ (cm day <sup>-1</sup> )         | 61.1            | 48.8     | 66.8               | 71.1    |
| $D$ (cm <sup>2</sup> day <sup>-1</sup> ) | 65.6            | 115      | 19.9               | 12.0    |
| Fitted parameter:                        |                 |          |                    |         |
| $R$                                      | 276 ± 18        | 318 ± 14 | 210 ± 5            | 195 ± 4 |
| $R^2$                                    | 0.90            | 0.97     | 0.99               | 0.99    |

Differences in water flow rates for the Br<sup>-</sup> and Ni<sup>2+</sup> BTCs were accounted for by assuming a linear relationship between velocity and flow rate. Also, D was calculated for the Ni<sup>2+</sup> BTCs assuming a linear relationship between D and v (van Genuchten and Wierenga, 1986)

Using the the average  $k_d$  from the experiments with NaN<sub>3</sub> for sterile samples and with freeze-dried *B. megaterium* for inoculated samples, we predicted that for sterile samples, the retardation factor (R) would be 170 and for inoculated samples R would be 25, assuming that:

$$R = 1 + \frac{\rho k_d}{\theta}$$

where  $\rho$  is the bulk density of the columns and  $\theta$  is the porosity of the saturated column. The average  $\rho$  of the four columns was 1390 kg m<sup>-3</sup> (sd = 0.01) and the average  $\theta$  was 0.405 (sd = 0.05).

The optimized values for R (Table 5) indicate that the retardation in inoculated columns was less than in sterile columns; however, all values for R are much higher than predicted from the batch isotherm data. The reasons for the greater sorption are not certain. One possible explanation is that in the dynamic system the tuff buffers the solution to a higher pH causing higher sorption. This is not supported by measurements taken of the column effluent pH because the average pH of the column effluent was between the pH of the sterile and inoculated samples in batch experiments. The pH of the sterile column effluent was 7.65 (sd = 0.35, n = 12) and of the inoculated columns was 7.77 (sd = 0.17, n = 8). This compares with the pH measurements of the

nonbuffered samples of 8.18 (sd = 0.08, n = 3) for sterile samples and 7.09 (sd = 0.04, n = 3) for the inoculated samples for initial  $\text{Ni}^{2+}$  concentrations of  $10 \text{ mg L}^{-1}$ . The pH of the influent solution was 7.2. The lack of microbial effect on the pH of the columns may have been caused by the flux of solution through the material, and also there may not have been enough microbes to acidify the solution. Inoculated samples in the batch equilibrium experiments contained approximately  $100 \times$  more CFU  $\text{g}^{-1}$  than the media used for the column experiments.

The difference in R between the two sets of columns may have been caused by differences in the physical properties instead of by microbially produced acid. For example, if bacteria clogged secondary pores and if some sorption sites were located in the clogged secondary pores, then retardation would have been less in inoculated media. Since *B. megaterium* forms flocs when grown in liquid culture, it may also have formed flocs within the porous medium and thus clogged pores that were bigger than the actual size of the bacteria. Another factor suggesting that secondary pores may be present in sterile columns and not in inoculated columns is that dispersion of both  $\text{Ni}^{2+}$  and  $\text{Br}^-$  BTCs was much greater in the sterile columns than in inoculated columns. Since the values of D within each treatment were similar, we conclude that the method used in packing did not cause the dispersion difference. We believe that microbial blockage of pores may be the main explanation for decreased D and may also explain increased R; however, other factors are probably involved. One argument against secondary porosity explaining the differences in R and D is that the surface area covered by the



microbes appears to be insignificant. Perhaps the surface area per microbe was greater than assumed; or alternatively, microbes may have clogged pores by producing extracellular polymeric substances.

#### Overall Significance

We have determined that microbes can decrease the sorption of  $\text{Ni}^{2+}$  and  $\text{Cd}^{2+}$  to crushed volcanic tuff. Microbes increased the mobility of  $\text{Ni}^{2+}$  in the crushed tuff, but not to the extent predicted by the batch equilibration studies. The findings of decreased sorption and increased transport confirm studies by Chanmugathas and Bollag (1989), Burke et al. (1991), Gerringa (1990), and Wildung (1979). Our findings that microbes decrease dispersion are contrary to past studies showing that microbes increase dispersion as well as clogging pores (Taylor and Jaffé, 1990).

All of the observed effects may be of significance to prediction and management of cationic transition-metal fate and transport. For example, the rate of transport of metals from waste storage areas may be increased if microbial populations are present. Decreased dispersion caused by the presence of microbes may result in solutes occupying a smaller, more concentrated region.

The presence of microbes may also result in increased availability of metals to plants and other organisms in the soil. Although some metals in the solution may be used by organisms, increased concentrations of toxic metals may cause decreased growth and increased mortality. The ability of microbes to increase the availability of metals may be much greater than would be predicted by the results of this study, since the microbes may affect microenvironments surrounding the cells to a greater extent than they affect the

bulk solution.

Although we did not study the phenomenon, we suspect that microbial effects on metal sorption may be more pronounced in nutrient-amended systems. Thus care should be taken that bioremediation of organic contaminants does not cause increased metal mobility.

Unlike Wildung (1979), who determined that  $\text{Ni}^{2+}$  transport was increased by microbial chelators, decreased sorption in our batch experiments was probably caused by a microbially influenced pH decrease. Thus, in stagnant systems or systems with a small water flux, as in many ground-water and vadose-zone systems, microbes that are present in the soils have the ability to change soil-water chemistry sufficiently to affect the transport of metals. The effect of microbes on metal retardation may be of less concern in systems with high fluid flux or low numbers of microbes because the natural buffering capacity of the soil may overcome the acid-producing capability of the microbes.

Our study has particular significance for waste sites located in volcanic tuff. We determined that the buffering capacity of volcanic tuff does not always exceed the acid-producing capability of the microbes and thus the microbially produced acid may affect the fate and transport of contaminants within the tuff. The microbes may also have had a greater affect on dispersion in the tuff than in other media that do not contain secondary porosity.

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**Appendix A**  
**Microbe Identification**

APPENDIX A  
MICROBE IDENTIFICATION

This appendix contains information on microbial identification including (1) the classification, (2) the identification number used in appendices B, D, and F, (3) the color, and (4) the gram stain type. The color and Gram Stain were described by Colette Kubichan in her laboratory notebook. The identification number is also used to identify cultures in the NMIMT microbiology laboratory (originally isolated by W. C. Ghiorse at Cornell University). The first part of the identification number refers to the depth in m from which the microbes were obtained. The following identifies each strain:

| <u>Microbe Number</u> | <u>Identity</u>                                 | <u>Color</u> | <u>Gram Stain</u> |
|-----------------------|---|--------------|-------------------|
| 50 T#2                | <i>Pseudomonas</i>                              | Yellow       | -                 |
| 50 T#6                | <i>Cryptococcus albidus</i> var. <i>albidus</i> | Pink         | +                 |
| 50 T#7                | <i>Rhodococcus fascians</i> GC subgroup B       | Pale yellow  | +                 |
| 50 T#8                | <i>Pseudomonas</i>                              | Yellow       | +                 |
| 50 T#9                | <i>Clavibacter michiganense insidiosum</i>      | White        | +                 |
| 50 T#11               | Unidentified yeast                              | White        | +                 |
| 50 T#12               | <i>Pseudomonas</i>                              | Yellow       | -                 |
| 50 T#13               | <i>Pseudomonas</i>                              | Yellow       | -                 |
| 150 T#3               | <i>Arthrobacter oxydans</i>                     | White        | -                 |
| 175 T#1               | <i>Arthrobacter oxydans</i>                     | White        | -                 |
| 175 T#2               | <i>Arthrobacter oxydans</i>                     | White        | -                 |
| 175 T#3               | <i>Bacillus megaterium</i>                      | White        | +                 |
| 175 T#6               | <i>Arthrobacter oxydans</i>                     | White        | -                 |
| 175 T#7               | <i>Candida famata</i>                           | Pink         | +                 |
| 175 T#8               | <i>Candida famata</i>                           | Pink         | +                 |

In addition to the classification given above, information that Microbial ID, Inc., provided is summarized below:

1. 175 T#7 and 175 T#8 are the same species and probably the same strain.

2. All *Pseudomonas* strains belong to the same species; this species was not in the MIDI data base at the time of identification. 50 T#2, 50 T#8 are the same subspecies, 50 T#12 and 50 T#13 are the same subspecies. All four *Pseudomonas* are different strains.
3. All *Arthrobacter oxydans* (150 T#3, 175 T#1, 175 T#2, and 175 T#6) belong to the same species. 175 T#6 belongs to a different subspecies. All are different strains.
4. 50 T#11 may be a *Cryptococcus* or *Candida* strain.

Microbes designated 125 T#1, a designation not used in the original samples from Ghiorse, were used in some of the experiments. This designation may have resulted from mislabeling a culture of 175 T#2, since the fatty-acid profile was identical to 175 T#2.



## Appendix B

### Ni Batch Equilibrium Experiments

## APPENDIX B

### NICKEL BATCH EQUILIBRIUM EXPERIMENTS

This appendix consists of data for experiments performed to determine  $\text{Ni}^{2+}$  sorption to crushed tuff under a variety of conditions. Most experiments presented in this appendix contain both  $\text{Ni}^{2+}$  concentrations and optical densities of the microbial suspension used to inoculate the batch equilibrium samples. The concentrations of the standards are given under the heading 'initial concentration'. The standard concentrations were double the sample 'initial concentrations' since half of the solution in the samples consisted of the  $\text{Ni}^{2+}$  standard. The other half of the solution consisted of microbial suspension or sterile  $\text{CaCl}_2$  solution. Experiments designated with an 'L' (L2 and L3Az7) were performed to determine the effect of freeze-dried *B. megaterium*. Experiments designated with 'Az' (L3Az7 and Az8) were performed to determine the  $\text{NaN}_3$  effect. Experiments designated with an 'N' (N1 to N8) were performed to determine the effect of a variety of freshly washed microbes. The experiment designated 'B1' was used to show the effect of buffered system on  $\text{Ni}^{2+}$  sorption in the presence and absence of microbes.

The results from these experiments are summarized in the Results and Discussion section of Chapter 2 under the subheading 'Ni Sorption Experiments'. Results from L3Az7 were used for Figure 1. Experiments Az8 and L3Az7 were used to determine the average  $k_d$  for  $\text{NaN}_3$ . Experiments L2 and L3Az7 were used to determine  $k_d$  for freeze-dried *B. megaterium*. Experiments N1 and N7 were used to find isotherms for *Candida famata* (175 T#7), *Rhodococcus facsiens* (50 T#7), and an *Arthrobacter oxydans* (175 T#1).

Experiments N2 to N5 were used to obtain data points for Figure 2; data from samples with initial  $\text{Ni}^{2+}$  concentrations of  $10 \text{ mg L}^{-1}$  were used. Experiments N2, N5, N7, N8, L2, and L3Az7 were used to determine the average  $k_d$  for *B. megaterium*; only samples with initial  $\text{Ni}^{2+}$  concentrations of 10 to  $11 \text{ mg L}^{-1}$  were used. Experiments N2 to N7, L2, L3, and B1 were used to find to find average  $k_d$  for all 14 strains and to find the  $k_d$ 's for *Arthrobacter* and *Pseudomonas* strains. Experiments N8 and L2 contain pH data that were not reported in Chapter 2. In experiment N8, I also performed a test in which I determined that  $\text{Ni}^{2+}$  sorption to tuff in sterile samples is similar to sorption in samples containing supernatant used to wash microbes. These results indicate that the supernatant resulting from washing the microbes does not include chelators or microbially produced acid that changes the sorption. The sample used to run this test is designated as 'supn 175 T#3' in the table. Experiment B1 was used to produce Figure 3 in Chapter 2.

In addition to information reported in Chapter 2, experiment N1 contains information showing that results from filtered supernatant were the same as unfiltered supernatant. Also, for most experiments, initial solution liquid scintillation counts were taken from both the original Pyrex mixing flask (Standard) and from solutions which were shaken in centrifuge tubes for 24 hours (CT Standard). Results obtained using the two types of solution counts resulted in the same  $k_d$  to two significant figures.

Experiment: L3Az7  
 Experiment Dates: 2/8/93 to 2/10/93

Objective: Determine Ni isotherms for samples inoculated with freeze-dried  
 B. megaterium (175 T#3), and sterile samples with and  
 and without NaN3.

No optical density readings taken.

| #  | Sample Type      | CPM/mL   | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|------------------|----------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile, azide   | 2784.9   | 2751.8              | 1.0                  | 2.66E-02            | 1.93E+00              |
| 2  | sterile, azide   | 2593.5   | 2560.4              | 1.0                  | 2.47E-02            | 1.94E+00              |
| 3  | sterile, azide   | 2630.5   | 2597.4              | 1.0                  | 2.51E-02            | 1.94E+00              |
| 4  | sterile, azide   | 3271.5   | 3238.4              | 4.0                  | 1.20E-01            | 7.71E+00              |
| 5  | sterile, azide   | 3010.7   | 2977.6              | 4.0                  | 1.11E-01            | 7.73E+00              |
| 6  | sterile, azide   | 2880.1   | 2847.0              | 4.0                  | 1.06E-01            | 7.74E+00              |
| 7  | sterile, azide   | 3835.9   | 3802.8              | 7.0                  | 2.34E-01            | 1.34E+01              |
| 8  | sterile, azide   | 3847.7   | 3814.6              | 7.0                  | 2.34E-01            | 1.34E+01              |
| 9  | sterile, azide   | 4267.2   | 4234.1              | 7.0                  | 2.60E-01            | 1.34E+01              |
| 10 | sterile, azide   | 2329.9   | 2296.8              | 10.0                 | 3.67E-01            | 1.91E+01              |
| 11 | sterile, azide   | 2332.6   | 2299.5              | 10.0                 | 3.67E-01            | 1.91E+01              |
| 12 | sterile, azide   | 2811.4   | 2778.3              | 10.0                 | 4.44E-01            | 1.90E+01              |
| 13 | Lyoph 175 T3     | 20719.2  | 20686.1             | 1.0                  | 2.00E-01            | 1.59E+00              |
| 14 | Lyoph 175 T3     | 20838.5  | 20805.4             | 1.0                  | 2.01E-01            | 1.59E+00              |
| 15 | Lyoph 175 T3     | 21193.7  | 21160.6             | 1.0                  | 2.04E-01            | 1.58E+00              |
| 16 | Lyoph 175 T3     | 23107.0  | 23073.9             | 4.0                  | 8.57E-01            | 6.24E+00              |
| 17 | Lyoph 175 T3     | 24924.5  | 24891.4             | 4.0                  | 9.24E-01            | 6.10E+00              |
| 18 | Lyoph 175 T3     | 22047.9  | 22014.8             | 4.0                  | 8.17E-01            | 6.32E+00              |
| 19 | Lyoph 175 T3     | 24048.4  | 24015.3             | 7.0                  | 1.48E+00            | 1.10E+01              |
| 20 | Lyoph 175 T3     | 23452.3  | 23419.2             | 7.0                  | 1.44E+00            | 1.10E+01              |
| 21 | Lyoph 175 T3     | 24346.1  | 24313.0             | 7.0                  | 1.49E+00            | 1.09E+01              |
| 22 | Lyoph 175 T3     | 13501.5  | 13468.4             | 10.0                 | 2.15E+00            | 1.56E+01              |
| 23 | Lyoph 175 T3     | 14139.3  | 14106.2             | 10.0                 | 2.25E+00            | 1.54E+01              |
| 24 | Lyoph 175 T3     | 14599.6  | 14566.5             | 10.0                 | 2.33E+00            | 1.52E+01              |
| 25 | sterile, nonazid | 851.2    | 818.1               | 1.0                  | 7.90E-03            | 1.97E+00              |
| 26 | sterile, nonazid | 744.0    | 710.9               | 1.0                  | 6.87E-03            | 1.97E+00              |
| 27 | sterile, nonazid | 704.8    | 671.7               | 1.0                  | 6.49E-03            | 1.98E+00              |
| 28 | sterile, nonazid | 797.5    | 764.4               | 4.0                  | 2.84E-02            | 7.90E+00              |
| 29 | sterile, nonazid | 893.1    | 860.0               | 4.0                  | 3.19E-02            | 7.89E+00              |
| 30 | sterile, nonazid | 720.7    | 687.6               | 4.0                  | 2.55E-02            | 7.90E+00              |
| 31 | sterile, nonazid | 864.2    | 831.1               | 7.0                  | 5.11E-02            | 1.38E+01              |
| 32 | sterile, nonazid | 788.2    | 755.1               | 7.0                  | 4.64E-02            | 1.38E+01              |
| 33 | sterile, nonazid | 784.8    | 751.7               | 7.0                  | 4.62E-02            | 1.38E+01              |
| 34 | sterile, nonazid | 405.9    | 372.8               | 10.0                 | 5.96E-02            | 1.98E+01              |
| 35 | sterile, nonazid | 590.2    | 557.1               | 10.0                 | 8.90E-02            | 1.97E+01              |
| 36 | sterile, nonazid | 499.0    | 465.9               | 10.0                 | 7.44E-02            | 1.97E+01              |
| 37 | Standard         | 205260.0 | 205226.9            | 2.0                  |                     |                       |
| 38 | Standard         | 207904.0 | 207870.9            | 2.0                  |                     |                       |
| 39 | Standard         | 207950.0 | 207916.9            | 2.0                  |                     |                       |
| 40 | Standard         | 214016.0 | 213982.9            | 8.0                  |                     |                       |
| 41 | Standard         | 215625.0 | 215591.9            | 8.0                  |                     |                       |

Experiment: L3Az7  
Experiment Dates: 2/8/93 to 2/10/93

Objective: Determine Ni isotherms for samples inoculated with freeze-dried  
B. megaterium (175 T#3), and sterile samples with and  
and without NaN<sub>3</sub>.

No optical density readings taken.

| #  | Sample Type | CPM/mL   | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|----------|---------------------|----------------------|---------------------|-----------------------|
| 42 | Standard    | 216991.0 | 216957.9            | 8.0                  |                     |                       |
| 43 | Standard    | 225937.0 | 225903.9            | 14.0                 |                     |                       |
| 44 | Standard    | 228946.0 | 228912.9            | 14.0                 |                     |                       |
| 45 | Standard    | 228826.0 | 228792.9            | 14.0                 |                     |                       |
| 46 | Standard    | 124182.0 | 124148.9            | 20.0                 |                     |                       |
| 47 | Standard    | 125405.0 | 125371.9            | 20.0                 |                     |                       |
| 48 | Standard    | 126072.0 | 126038.9            | 20.0                 |                     |                       |

Experiment: L2  
 Experiment Dates: 9/16/92 to 9/18/92

Objective: Determine Ni isotherms for samples inoculated with freeze-dried 175 T#3  
 We also have plate counts and direct counts of this experiment.

Optical Density of Lyophilized 175 T#3: 0.78

| #  | Sample Type  | CPM/mL - |            | pH   | Initial      | Sample       | Sorbed         |
|----|--------------|----------|------------|------|--------------|--------------|----------------|
|    |              | CPM/mL   | Background |      | Conc. (mg/L) | Conc. (mg/L) | Amount (mg/kg) |
| 1  | sterile      | 259.0    | 225.9      | 8.45 | 1.0          | 1.19E-02     | 1.89E+00       |
| 2  | sterile      | 222.6    | 189.5      |      | 1.0          | 9.99E-03     | 1.90E+00       |
| 3  | sterile      | 243.3    | 210.2      |      | 1.0          | 1.11E-02     | 1.89E+00       |
| 4  | sterile      | 238.0    | 204.9      | 8.52 | 4.0          | 4.25E-02     | 7.85E+00       |
| 5  | sterile      | 272.4    | 239.3      |      | 4.0          | 4.97E-02     | 7.84E+00       |
| 6  | sterile      | 266.0    | 232.9      |      | 4.0          | 4.83E-02     | 7.84E+00       |
| 7  | sterile      | 231.8    | 198.7      | 8.55 | 7.0          | 8.08E-02     | 1.46E+01       |
| 8  | sterile      | 231.6    | 198.5      |      | 7.0          | 8.08E-02     | 1.46E+01       |
| 9  | sterile      | 227.3    | 194.2      |      | 7.0          | 7.90E-02     | 1.46E+01       |
| 10 | sterile      | 219.6    | 186.5      | 8.52 | 10.0         | 1.03E-01     | 1.97E+01       |
| 11 | sterile      | 214.0    | 180.9      |      | 10.0         | 1.00E-01     | 1.97E+01       |
| 12 | sterile      | 231.7    | 198.6      |      | 10.0         | 1.10E-01     | 1.96E+01       |
| 13 | Lyoph175 T#3 | 3861.8   | 3828.7     | 7.26 | 1.0          | 2.02E-01     | 1.51E+00       |
| 14 | Lyoph175 T#3 | 3597.9   | 3564.8     |      | 1.0          | 1.88E-01     | 1.54E+00       |
| 15 | Lyoph175 T#3 | 3589.6   | 3556.5     |      | 1.0          | 1.87E-01     | 1.54E+00       |
| 16 | Lyoph175 T#3 | 3834.3   | 3801.2     | 7.10 | 4.0          | 7.89E-01     | 6.36E+00       |
| 17 | Lyoph175 T#3 | 3983.2   | 3950.1     |      | 4.0          | 8.20E-01     | 6.30E+00       |
| 18 | Lyoph175 T#3 | 5649.0   | 5615.9     |      | 4.0          | 1.17E+00     | 5.60E+00       |
| 19 | Lyoph175 T#3 | 3019.4   | 2986.3     | 7.45 | 7.0          | 1.21E+00     | 1.24E+01       |
| 20 | Lyoph175 T#3 | 4729.6   | 4696.5     |      | 7.0          | 1.91E+00     | 1.10E+01       |
| 21 | Lyoph175 T#3 | 3625.9   | 4696.5     |      | 7.0          | 1.91E+00     | 1.10E+01       |
| 22 | Lyoph175 T#3 | 2977.8   | 2944.7     | 7.45 | 10.0         | 1.63E+00     | 1.66E+01       |
| 23 | Lyoph175 T#3 | 2778.5   | 2745.4     |      | 10.0         | 1.52E+00     | 1.68E+01       |
| 24 | Lyoph175 T#3 | 3634.4   | 3601.3     |      | 10.0         | 2.00E+00     | 1.59E+01       |
| 25 | CT Standard  | 35911.9  | 35878.8    |      | 2.0          |              |                |
| 26 | CT Standard  | 36863.8  | 36830.7    |      | 2.0          |              |                |
| 27 | CT Standard  | 38433.0  | 38399.9    |      | 8.0          |              |                |
| 28 | CT Standard  | 38103.2  | 38070.1    |      | 8.0          |              |                |
| 29 | CT Standard  | 36282.8  | 36249.7    |      | 14.0         |              |                |
| 30 | CT Standard  | 36556.2  | 36523.1    |      | 14.0         |              |                |
| 31 | CT Standard  | 35720.2  | 35687.1    |      | 20.0         |              |                |
| 32 | CT Standard  | 35941.9  | 35908.8    |      | 20.0         |              |                |
| 33 | Standard     | 37982.5  | 37949.4    |      | 2.0          |              |                |
| 34 | Standard     | 37989.2  | 37956.1    |      | 2.0          |              |                |
| 35 | Standard     | 38451.2  | 38418.1    |      | 8.0          |              |                |
| 36 | Standard     | 38705.2  | 38672.1    |      | 8.0          |              |                |
| 37 | Standard     | 34523.3  | 34490.2    |      | 14.0         |              |                |
| 38 | Standard     | 34368.6  | 34335.5    |      | 14.0         |              |                |
| 39 | Standard     | 36093.6  | 36060.5    |      | 20.0         |              |                |
| 40 | Standard     | 36078.0  | 36044.9    |      | 20.0         |              |                |

Experiment: Az8

Experiment Dates: 2/17/93 to 2/19/93

Objective: Determine Ni isotherms for samples containing NaN<sub>3</sub>.

Optical Density: N/A

| #  | Sample Type       | CPM/mL   | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------------|----------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile, azide    | 2436.4   | 2401.1              | 1.02                 | 2.32E-02            | 1.98E+00              |
| 2  | sterile, azide    | 2870.4   | 2835.1              | 1.02                 | 2.74E-02            | 1.97E+00              |
| 3  | sterile, azide    | 2975.6   | 2940.3              | 1.02                 | 2.84E-02            | 1.97E+00              |
| 4  | sterile, azide    | 3186.5   | 3151.2              | 3.98                 | 1.17E-01            | 7.68E+00              |
| 5  | sterile, azide    | 3007.9   | 2972.6              | 3.98                 | 1.10E-01            | 7.70E+00              |
| 6  | sterile, azide    | 3311.8   | 3276.5              | 3.98                 | 1.22E-01            | 7.67E+00              |
| 7  | sterile, azide    | 4281.6   | 4246.3              | 7.05                 | 2.61E-01            | 1.35E+01              |
| 8  | sterile, azide    | 4393.2   | 4357.9              | 7.05                 | 2.68E-01            | 1.35E+01              |
| 9  | sterile, azide    | 4145.6   | 4110.3              | 7.05                 | 2.53E-01            | 1.35E+01              |
| 10 | sterile, azide    | 2674.1   | 2638.8              | 9.97                 | 4.22E-01            | 1.90E+01              |
| 11 | sterile, azide    | 2609.2   | 2573.9              | 9.97                 | 4.11E-01            | 1.90E+01              |
| 12 | sterile, azide    | 2639.3   | 2604.0              | 9.97                 | 4.16E-01            | 1.90E+01              |
| 13 | sterile, no azide | 902.8    | 867.5               | 1.02                 | 8.38E-03            | 2.01E+00              |
| 14 | sterile, no azide | 794.4    | 759.1               | 1.02                 | 7.33E-03            | 2.01E+00              |
| 15 | sterile, no azide | 774.8    | 739.5               | 1.02                 | 7.14E-03            | 2.02E+00              |
| 16 | sterile, no azide | 812.9    | 777.6               | 3.98                 | 2.89E-02            | 7.86E+00              |
| 17 | sterile, no azide | 876.0    | 840.7               | 3.98                 | 3.12E-02            | 7.86E+00              |
| 18 | sterile, no azide | 809.8    | 774.5               | 3.98                 | 2.87E-02            | 7.86E+00              |
| 19 | sterile, no azide | 820.7    | 785.4               | 7.05                 | 4.83E-02            | 1.39E+01              |
| 20 | sterile, no azide | 943.3    | 908.0               | 7.05                 | 5.58E-02            | 1.39E+01              |
| 21 | sterile, no azide | 979.2    | 943.9               | 7.05                 | 5.80E-02            | 1.39E+01              |
| 22 | sterile, no azide | 605.7    | 570.4               | 9.97                 | 9.11E-02            | 1.96E+01              |
| 23 | sterile, no azide | 636.9    | 601.6               | 9.97                 | 9.61E-02            | 1.96E+01              |
| 24 | sterile, no azide | 624.3    | 589.0               | 9.97                 | 9.41E-02            | 1.96E+01              |
| 25 | Standard          | 210030.0 | 209994.7            | 2.04                 |                     |                       |
| 26 | Standard          | 212305.0 | 212269.7            | 2.04                 |                     |                       |
| 27 | Standard          | 211758.0 | 211722.7            | 2.04                 |                     |                       |
| 28 | Standard          | 214386.0 | 214350.7            | 7.97                 |                     |                       |
| 29 | Standard          | 214148.0 | 214112.7            | 7.97                 |                     |                       |
| 30 | Standard          | 215353.0 | 215317.7            | 7.97                 |                     |                       |
| 31 | Standard          | 229202.0 | 229166.7            | 14.11                |                     |                       |
| 32 | Standard          | 228386.0 | 228350.7            | 14.11                |                     |                       |
| 33 | Standard          | 231379.0 | 231343.7            | 14.11                |                     |                       |
| 34 | Standard          | 124521.0 | 124485.7            | 19.95                |                     |                       |
| 35 | Standard          | 124404.0 | 124368.7            | 19.95                |                     |                       |
| 36 | Standard          | 125751.0 | 125715.7            | 19.95                |                     |                       |

Batch Experiment: N1  
 Experiment Dates: 10/23/91 to 10/25/91

Objective: Determine Ni isotherms for samples inoculated with 50 T#7 and 175 T#1.

Optical Densities: 50 T#7: 0.80  
 175 T#1: 0.80

| #  | Sample Type | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 1  | CT Standard | 35903.0 | 35869.9             | 0.04                 |                     |                       |
| 2  | CT Standard | 35530.8 | 35497.7             | 0.04                 |                     |                       |
| 3  | CT Standard | 34937.9 | 34904.8             | 0.04                 |                     |                       |
| 4  | CT Standard | 37216.3 | 37183.2             | 0.4                  |                     |                       |
| 5  | CT Standard | 36595.5 | 36562.4             | 0.4                  |                     |                       |
| 6  | CT Standard | 35559.5 | 35526.4             | 0.4                  |                     |                       |
| 7  | CT Standard | 35159.9 | 35126.8             | 4.0                  |                     |                       |
| 8  | CT Standard | 35695.7 | 35662.6             | 4.0                  |                     |                       |
| 9  | CT Standard | 35402.8 | 35369.7             | 4.0                  |                     |                       |
| 10 | CT Standard | 35723.7 | 35690.6             | 40.0                 |                     |                       |
| 11 | CT Standard | 36096.6 | 36063.5             | 40.0                 |                     |                       |
| 12 | CT Standard | 35858.3 | 35825.2             | 40.0                 |                     |                       |
| 13 | CT Standard | 37499.4 | 37466.3             | 400.0                |                     |                       |
| 14 | CT Standard | 37149.1 | 37116.0             | 400.0                |                     |                       |
| 15 | CT Standard | 37179.2 | 37146.1             | 400.0                |                     |                       |
| 16 | 50 T#7      | 774.7   | 741.6               | 0.02                 | 8.37E-04            | 3.83E-02              |
| 17 | 50 T#7      | 744.2   | 711.1               | 0.02                 | 8.03E-04            | 3.84E-02              |
| 18 | 50 T#7      | 716.4   | 683.3               | 0.02                 | 7.72E-04            | 3.85E-02              |
| 19 | 50 T#7      | 768.8   | 735.7               | 0.2                  | 8.08E-03            | 3.84E-01              |
| 20 | 50 T#7      | 692.6   | 659.5               | 0.2                  | 7.24E-03            | 3.86E-01              |
| 21 | 50 T#7      | 610.2   | 577.1               | 0.2                  | 6.34E-03            | 3.87E-01              |
| 22 | 50 T#7      | 573.2   | 540.1               | 2.0                  | 6.11E-02            | 3.88E+00              |
| 23 | 50 T#7      | 590.7   | 557.6               | 2.0                  | 6.30E-02            | 3.87E+00              |
| 24 | 50 T#7      | 621.4   | 588.3               | 2.0                  | 6.65E-02            | 3.87E+00              |
| 25 | 50 T#7      | 1171.8  | 1138.7              | 20.0                 | 1.27E+00            | 3.75E+01              |
| 26 | 50 T#7      | 1164.4  | 1131.3              | 20.0                 | 1.26E+00            | 3.75E+01              |
| 27 | 50 T#7      | 1138.5  | 1105.4              | 20.0                 | 1.23E+00            | 3.75E+01              |
| 28 | 50 T#7      | 2759.9  | 2726.8              | 200.0                | 2.93E+01            | 3.41E+02              |
| 29 | 50 T#7      | 2838.3  | 2805.2              | 200.0                | 3.01E+01            | 3.40E+02              |
| 30 | 50 T#7      | 2861.0  | 2827.9              | 200.0                | 3.04E+01            | 3.39E+02              |
| 31 | 175 T#1     | 1167.3  | 1134.2              | 0.02                 | 1.28E-03            | 3.74E-02              |
| 32 | 175 T#1     | 1067.5  | 1034.4              | 0.02                 | 1.17E-03            | 3.77E-02              |
| 33 | 175 T#1     | 1031.9  | 998.8               | 0.02                 | 1.13E-03            | 3.77E-02              |
| 34 | 175 T#1     | 1152.4  | 1119.3              | 0.2                  | 1.23E-02            | 3.75E-01              |
| 35 | 175 T#1     | 1197.2  | 1164.1              | 0.2                  | 1.28E-02            | 3.74E-01              |
| 36 | 175 T#1     | 1207.6  | 1174.5              | 0.2                  | 1.29E-02            | 3.74E-01              |
| 37 | 175 T#1     | 1075.7  | 1042.6              | 2.0                  | 1.18E-01            | 3.76E+00              |
| 38 | 175 T#1     | 949.5   | 916.4               | 2.0                  | 1.04E-01            | 3.79E+00              |
| 39 | 175 T#1     | 1089.5  | 1056.4              | 2.0                  | 1.19E-01            | 3.76E+00              |
| 40 | 175 T#1     | 1601.7  | 1568.6              | 20.0                 | 1.75E+00            | 3.65E+01              |
| 41 | 175 T#1     | 1648.3  | 1615.2              | 20.0                 | 1.80E+00            | 3.64E+01              |
| 42 | 175 T#1     | 1708.6  | 1675.5              | 20.0                 | 1.87E+00            | 3.63E+01              |
| 43 | 175 T#1     | 3254.9  | 3221.8              | 200.0                | 3.46E+01            | 3.31E+02              |



Batch Experiment: N1  
 Experiment Dates: 10/23/91 to 10/25/91

Objective: Determine Ni isotherms for samples inoculated with 50 T#7 and 175 T#1.

Optical Densities: 50 T#7: 0.80  
 175 T#1: 0.80

| #  | Sample Type  | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|--------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 44 | 175 T#1      | 3127.4  | 3094.3              | 200.0                | 3.32E+01            | 3.34E+02              |
| 45 | 175 T#1      | 3062.4  | 3029.3              | 200.0                | 3.25E+01            | 3.35E+02              |
| 46 | sterile      | 232.1   | 199.0               | 0.02                 | 2.25E-04            | 3.96E-02              |
| 47 | sterile      | 272.3   | 239.2               | 0.02                 | 2.70E-04            | 3.95E-02              |
| 48 | sterile      | 266.2   | 233.1               | 0.02                 | 2.63E-04            | 3.95E-02              |
| 49 | sterile      | 265.0   | 231.9               | 0.2                  | 2.55E-03            | 3.95E-01              |
| 50 | sterile      | 249.0   | 215.9               | 0.2                  | 2.37E-03            | 3.95E-01              |
| 51 | sterile      | 260.2   | 227.1               | 0.2                  | 2.49E-03            | 3.95E-01              |
| 52 | sterile      | 221.1   | 188.0               | 2.0                  | 2.13E-02            | 3.96E+00              |
| 53 | sterile      | 224.6   | 191.5               | 2.0                  | 2.17E-02            | 3.96E+00              |
| 54 | sterile      | 236.0   | 202.9               | 2.0                  | 2.29E-02            | 3.95E+00              |
| 55 | sterile      | 307.7   | 274.6               | 20.0                 | 3.06E-01            | 3.94E+01              |
| 56 | sterile      | 294.4   | 261.3               | 20.0                 | 2.92E-01            | 3.94E+01              |
| 57 | sterile      | 280.4   | 247.3               | 20.0                 | 2.76E-01            | 3.94E+01              |
| 58 | sterile      | 1495.2  | 1462.1              | 200.0                | 1.57E+01            | 3.69E+02              |
| 59 | sterile      | 1685.5  | 1652.4              | 200.0                | 1.77E+01            | 3.65E+02              |
| 60 | sterile      | 1728.5  | 1695.4              | 200.0                | 1.82E+01            | 3.64E+02              |
| 61 | bkgd w/ tuff | 36.0    | 2.9                 |                      |                     |                       |
| 62 | bkgd w/ tuff | 34.1    | 1.0                 |                      |                     |                       |
| 63 | bkgd w/ tuff | 30.3    | -2.8                |                      |                     |                       |
| 64 | Standard     | 36227.0 | 36193.9             | 0.04                 |                     |                       |
| 65 | Standard     | 36349.6 | 36316.5             | 0.04                 |                     |                       |
| 66 | Standard     | 36518.0 | 36484.9             | 0.04                 |                     |                       |
| 67 | Standard     | 37698.1 | 37665.0             | 0.4                  |                     |                       |
| 68 | Standard     | 37845.7 | 37812.6             | 0.4                  |                     |                       |
| 69 | Standard     | 37826.9 | 37793.8             | 0.4                  |                     |                       |
| 70 | Standard     | 35705.6 | 35672.5             | 4.0                  |                     |                       |
| 71 | Standard     | 35643.1 | 35610.0             | 4.0                  |                     |                       |
| 72 | Standard     | 35472.8 | 35439.7             | 4.0                  |                     |                       |
| 73 | Standard     | 35760.4 | 35727.3             | 40.0                 |                     |                       |
| 74 | Standard     | 35836.7 | 35803.6             | 40.0                 |                     |                       |
| 75 | Standard     | 35735.3 | 35702.2             | 40.0                 |                     |                       |
| 76 | Standard     | 36885.0 | 36851.9             | 400.0                |                     |                       |
| 77 | Standard     | 36868.0 | 36834.9             | 400.0                |                     |                       |
| 78 | Standard     | 36767.5 | 36734.4             | 400.0                |                     |                       |
| 79 | filtered 16  | 808.0   | 774.9               |                      |                     |                       |
| 80 | filtered 17  | 762.1   | 729.0               |                      |                     |                       |
| 81 | filtered 18  | 744.2   | 711.1               |                      |                     |                       |
| 82 | filtered 28  | 2716.9  | 2683.8              |                      |                     |                       |
| 83 | filtered 29  | 2897.2  | 2864.1              |                      |                     |                       |
| 84 | filtered 30  | 2987.4  | 2954.3              |                      |                     |                       |
| 85 | filtered 31  | 1195.0  | 1161.9              |                      |                     |                       |
| 86 | filtered 32  | 1076.2  | 1043.1              |                      |                     |                       |

Batch Experiment: N1

Experiment Dates: 10/23/91 to 10/25/91

Objective: Determine Ni isotherms for samples inoculated with 50 T#7 and 175 T#1.

Optical Densities: 50 T#7: 0.80  
175 T#1: 0.80

| #  | Sample Type   | CPM/mL | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|---------------|--------|---------------------|----------------------|---------------------|-----------------------|
| 87 | filtered 33   | 1056.3 | 1023.2              |                      |                     |                       |
| 88 | air/no Sc. C. | 28.4   |                     |                      |                     |                       |
| 89 | bkgr          | 34.3   |                     |                      |                     |                       |
| 90 | bkgr          | 30.5   |                     |                      |                     |                       |
| 91 | bkgr          | 33.2   |                     |                      |                     |                       |

Batch Experiment: N2

Experiment Dates: 11/20/91 to 11/22/91

Objective: Find the effects of 50 T#2, 50 T#6, 50 T#7, 50 T#9, 50 T#12, 50 T#13, 175 T#3, and 175 T#7 on Ni sorption to crushed tuff.

|                    |         |      |          |      |
|--------------------|---------|------|----------|------|
| Optical Densities: | 50 T#2: | 0.56 | 50 T#12: | 0.80 |
|                    | 50 T#6: | 0.46 | 50 T#13: | 0.80 |
|                    | 50 T#7: | 1.30 | 175 T#3: | 0.75 |
|                    | 50 T#9: | 1.00 | 175 T#7: | 0.75 |

| #  | Sample Type | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile     | 339.0   | 305.9               | 10.00                | 1.82E-01            | 1.96E+01              |
| 2  | sterile     | 313.3   | 280.2               | 10.00                | 1.67E-01            | 1.97E+01              |
| 3  | sterile     | 315.5   | 282.4               | 10.00                | 1.68E-01            | 1.97E+01              |
| 4  | 50 T#2      | 704.3   | 671.2               | 10.00                | 4.00E-01            | 1.92E+01              |
| 5  | 50 T#2      | 688.9   | 655.8               | 10.00                | 3.91E-01            | 1.92E+01              |
| 6  | 50 T#2      | 717.3   | 684.2               | 10.00                | 4.08E-01            | 1.92E+01              |
| 7  | 50 T#6      | 925.3   | 892.2               | 10.00                | 5.31E-01            | 1.89E+01              |
| 8  | 50 T#6      | 850.0   | 816.9               | 10.00                | 4.87E-01            | 1.90E+01              |
| 9  | 50 T#6      | 820.8   | 787.7               | 10.00                | 4.69E-01            | 1.91E+01              |
| 10 | 50 T#7      | 777.4   | 744.3               | 10.00                | 4.43E-01            | 1.91E+01              |
| 11 | 50 T#7      | 588.4   | 555.3               | 10.00                | 3.31E-01            | 1.93E+01              |
| 12 | 50 T#7      | 680.2   | 647.1               | 10.00                | 3.85E-01            | 1.92E+01              |
| 13 | 50 T#9      | 603.9   | 570.8               | 10.00                | 3.40E-01            | 1.93E+01              |
| 14 | 50 T#9      | 552.8   | 519.7               | 10.00                | 3.10E-01            | 1.94E+01              |
| 15 | 50 T#9      | 717.4   | 684.3               | 10.00                | 4.08E-01            | 1.92E+01              |
| 16 | 50 T#12     | 577.6   | 544.5               | 10.00                | 3.24E-01            | 1.94E+01              |
| 17 | 50 T#12     | 617.2   | 584.1               | 10.00                | 3.48E-01            | 1.93E+01              |
| 18 | 50 T#12     | 563.6   | 530.5               | 10.00                | 3.16E-01            | 1.94E+01              |
| 19 | 50 T#13     | 706.6   | 673.5               | 10.00                | 4.01E-01            | 1.92E+01              |
| 20 | 50 T#13     | 697.3   | 664.2               | 10.00                | 3.96E-01            | 1.92E+01              |
| 21 | 50 T#13     | 726.8   | 693.7               | 10.00                | 4.13E-01            | 1.92E+01              |
| 22 | 175 T#3     | 1176.0  | 1142.9              | 10.00                | 6.81E-01            | 1.86E+01              |
| 23 | 175 T#3     | 1196.1  | 1163.0              | 10.00                | 6.93E-01            | 1.86E+01              |
| 24 | 175 T#3     | 1125.4  | 1092.3              | 10.00                | 6.51E-01            | 1.87E+01              |
| 25 | 175 T#7     | 1113.0  | 1079.9              | 10.00                | 6.43E-01            | 1.87E+01              |
| 26 | 175 T#7     | 1100.3  | 1067.2              | 10.00                | 6.36E-01            | 1.87E+01              |
| 27 | 175 T#7     | 1077.5  | 1044.4              | 10.00                | 6.22E-01            | 1.88E+01              |
| 28 | CT Standard | 33814.1 | 33781.0             | 20.00                |                     |                       |
| 29 | CT Standard | 33571.3 | 33538.2             | 20.00                |                     |                       |
| 30 | CT Standard | 33444.6 | 33411.5             | 20.00                |                     |                       |
| 31 | Standard    | 33427.7 | 33394.6             | 20.00                |                     |                       |
| 32 | Standard    | 33589.6 | 33556.5             | 20.00                |                     |                       |
| 33 | Standard    | 33519.0 | 33485.9             | 20.00                |                     |                       |

Batch Experiment: N3  
 Experiment Dates: 12/2/91 to 12/4/91

Objective: Find the effects of 50 T#8, 150 T#3, 175 T#2, and 175 T#8  
 on Ni sorption to crushed tuff.

Optical Densities: 50 T#8: 0.85      175 T#2: 0.85  
                          150 T#3: 0.75      175 T#8: 0.80

| #  | Sample Type | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile     | 248.4   | 215.3               | 10.00                | 1.29E-01            | 1.97E+01              |
| 2  | sterile     | 259.9   | 226.8               | 10.00                | 1.36E-01            | 1.97E+01              |
| 3  | sterile     | 309.1   | 276.0               | 10.00                | 1.66E-01            | 1.97E+01              |
| 4  | 50 T#8      | 506.9   | 473.8               | 10.00                | 2.85E-01            | 1.94E+01              |
| 5  | 50 T#8      | 610.9   | 577.8               | 10.00                | 3.47E-01            | 1.93E+01              |
| 6  | 50 T#8      | 667.4   | 634.3               | 10.00                | 3.81E-01            | 1.92E+01              |
| 7  | 150 T#3     | 366.8   | 333.7               | 10.00                | 2.01E-01            | 1.96E+01              |
| 8  | 150 T#3     | 364.0   | 330.9               | 10.00                | 1.99E-01            | 1.96E+01              |
| 9  | 150 T#3     | 370.5   | 337.4               | 10.00                | 2.03E-01            | 1.96E+01              |
| 10 | 175 T#2     | 532.4   | 499.3               | 10.00                | 3.00E-01            | 1.94E+01              |
| 11 | 175 T#2     | 481.5   | 448.4               | 10.00                | 2.70E-01            | 1.95E+01              |
| 12 | 175 T#2     | 545.1   | 512.0               | 10.00                | 3.08E-01            | 1.94E+01              |
| 13 | 175 T#8     | 768.2   | 735.1               | 10.00                | 4.42E-01            | 1.91E+01              |
| 14 | 175 T#8     | 721.7   | 688.6               | 10.00                | 4.14E-01            | 1.92E+01              |
| 15 | 175 T#8     | 779.6   | 746.5               | 10.00                | 4.49E-01            | 1.91E+01              |
| 16 | CT Standard | 32918.9 | 32885.8             | 20.00                |                     |                       |
| 17 | CT Standard | 33997.1 | 33964.0             | 20.00                |                     |                       |
| 18 | CT Standard | 32950.9 | 32917.8             | 20.00                |                     |                       |
| 19 | Standard    | 33350.8 | 33317.7             | 20.00                |                     |                       |
| 20 | Standard    | 33352.9 | 33319.8             | 20.00                |                     |                       |
| 21 | Standard    | 33264.8 | 33231.7             | 20.00                |                     |                       |

Batch Experiment: N4  
 Experiment Dates: 12/12/91 to 12/14/91

Objective: Find the effect of 175 T#1 and 175 T#6 on Ni sorption to crushed tuff.

Optical Densities: 175 T#1: 0.80  
 175 T#6: 0.75

| #  | Sample Type | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile     | 371.1   | 338.0               | 10.00                | 1.92E-01            | 1.96E+01              |
| 2  | sterile     | 379.6   | 346.5               | 10.00                | 1.97E-01            | 1.96E+01              |
| 3  | sterile     | 377.8   | 344.7               | 10.00                | 1.96E-01            | 1.96E+01              |
| 4  | 175 T#1     | 1556.3  | 1523.2              | 10.00                | 8.66E-01            | 1.83E+01              |
| 5  | 175 T#1     | 1829.0  | 1795.9              | 10.00                | 1.02E+00            | 1.80E+01              |
| 6  | 175 T#1     | 1277.4  | 1244.3              | 10.00                | 7.08E-01            | 1.86E+01              |
| 7  | 175 T#6     | 1405.0  | 1371.9              | 10.00                | 7.80E-01            | 1.84E+01              |
| 8  | 175 T#6     | 1448.1  | 1415.0              | 10.00                | 8.05E-01            | 1.84E+01              |
| 9  | 175 T#6     | 1442.2  | 1409.1              | 10.00                | 8.01E-01            | 1.84E+01              |
| 10 | CT Standard | 35518.8 | 35485.7             | 20.00                |                     |                       |
| 11 | CT Standard | 33765.8 | 33732.7             | 20.00                |                     |                       |
| 12 | CT Standard | 36301.6 | 36268.5             | 20.00                |                     |                       |
| 13 | Standard    | 32222.6 | 32189.5             | 20.00                |                     |                       |
| 14 | Standard    | 32138.1 | 32105.0             | 20.00                |                     |                       |
| 15 | Standard    | 30969.2 | 30936.1             | 20.00                |                     |                       |

Batch Experiment: N5

Experiment Dates: 12/22/91 to 12/24/91

Objective: Find the effect of 125 T#1 and 175 T#1, 175 T#3, and 175 T#6 on Ni sorption to crushed tuff.

Optical Densities: 125 T#1: 0.80                      175 T#3: 0.75  
                          175 T#1: 0.85                      175 T#6: 0.80

| #  | Sample Type | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile     | 294.4   | 261.3               | 10.00                | 1.42E-01            | 1.97E+01              |
| 2  | sterile     | 188.2   | 155.1               | 10.00                | 8.40E-02            | 1.98E+01              |
| 3  | sterile     | 220.7   | 187.6               | 10.00                | 1.02E-01            | 1.98E+01              |
| 4  | 125 T#1     | 1100.8  | 1067.7              | 10.00                | 5.78E-01            | 1.88E+01              |
| 5  | 125 T#1     | 1039.5  | 1006.4              | 10.00                | 5.45E-01            | 1.89E+01              |
| 6  | 125 T#1     | 1209.3  | 1176.2              | 10.00                | 6.37E-01            | 1.87E+01              |
| 7  | 175 T#1     | 1371.2  | 1338.1              | 10.00                | 7.25E-01            | 1.86E+01              |
| 8  | 175 T#1     | 1278.4  | 1245.3              | 10.00                | 6.75E-01            | 1.87E+01              |
| 9  | 175 T#1     | 1367.1  | 1334.0              | 10.00                | 7.23E-01            | 1.86E+01              |
| 10 | 175 T#3     | 4053.3  | 4020.2              | 10.00                | 2.18E+00            | 1.56E+01              |
| 11 | 175 T#3     | 4047.5  | 4014.4              | 10.00                | 2.17E+00            | 1.57E+01              |
| 12 | 175 T#3     | 3868.8  | 3835.7              | 10.00                | 2.08E+00            | 1.58E+01              |
| 13 | 175 T#6     | 2136.0  | 2102.9              | 10.00                | 1.14E+00            | 1.77E+01              |
| 14 | 175 T#6     | 2918.4  | 2885.3              | 10.00                | 1.56E+00            | 1.69E+01              |
| 15 | 175 T#6     | 2407.3  | 2374.2              | 10.00                | 1.29E+00            | 1.74E+01              |
| 16 | CT Standard | 38153.5 | 38120.4             | 20.00                |                     |                       |
| 17 | CT Standard | 36587.3 | 36554.2             | 20.00                |                     |                       |
| 18 | CT Standard | 36105.6 | 36072.5             | 20.00                |                     |                       |
| 19 | Standard    | 37275.5 | 37242.4             | 20.00                |                     |                       |
| 20 | Standard    | 36759.3 | 36726.2             | 20.00                |                     |                       |
| 21 | Standard    | 36142.2 | 36109.1             | 20.00                |                     |                       |

Batch Experiment: N6  
 Experiment Dates: 12/27/91 to 12/29/91

Objective: Find the effect of 50 T#11 and 175 T#7 on Ni sorption to crushed tuff.

Optical Densities: 50 T#11: 0.36  
 175 T#7: 0.80

| #  | Sample Type | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile     | 290.4   | 257.3               | 11.25                | 1.64E-01            | 2.22E+01              |
| 2  | sterile     | 301.1   | 268.0               | 11.25                | 1.71E-01            | 2.22E+01              |
| 3  | sterile     | 288.6   | 255.5               | 11.25                | 1.63E-01            | 2.22E+01              |
| 4  | 50 T#11     | 1490.4  | 1457.3              | 11.25                | 9.32E-01            | 2.06E+01              |
| 5  | 50 T#11     | 1235.7  | 1202.6              | 11.25                | 7.69E-01            | 2.10E+01              |
| 6  | 50 T#11     | 1119.1  | 1086.0              | 11.25                | 6.94E-01            | 2.11E+01              |
| 7  | 175 T#7     | 2200.5  | 2167.4              | 11.25                | 1.39E+00            | 1.97E+01              |
| 8  | 175 T#7     | 3125.8  | 3092.7              | 11.25                | 1.98E+00            | 1.85E+01              |
| 9  | 175 T#7     | 2115.0  | 2081.9              | 11.25                | 1.33E+00            | 1.98E+01              |
| 10 | CT Standard | 34736.0 | 34702.9             | 22.50                |                     |                       |
| 11 | CT Standard | 35747.5 | 35714.4             | 22.50                |                     |                       |
| 12 | CT Standard | 35195.0 | 35161.9             | 22.50                |                     |                       |
| 13 | Standard    | 35303.0 | 35269.9             | 22.50                |                     |                       |
| 14 | Standard    | 35421.5 | 35388.4             | 22.50                |                     |                       |
| 15 | Standard    | 35901.3 | 35868.2             | 22.50                |                     |                       |

Batch Experiment: N7  
 Experiment Dates: 1/13/92 to 1/15/92

Objective: Determine Ni isotherms for samples inoculated with 175 T#3 and 175 T#7.

Optical Densities: 175 T#3: 0.80  
 175 T#7: 0.80

| #  | Sample type | CPM/mL | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|--------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile     | 254.0  | 220.9               | 0.01                 | 1.18E-04            | 2.23E-02              |
| 2  | sterile     | 278.0  | 244.9               | 0.01                 | 1.31E-04            | 2.22E-02              |
| 3  | sterile     | 300.0  | 266.9               | 0.01                 | 1.42E-04            | 2.22E-02              |
| 4  | sterile     | 286.0  | 252.9               | 0.11                 | 1.32E-03            | 2.22E-01              |
| 5  | sterile     | 286.0  | 252.9               | 0.11                 | 1.32E-03            | 2.22E-01              |
| 6  | sterile     | 285.0  | 251.9               | 0.11                 | 1.31E-03            | 2.22E-01              |
| 7  | sterile     | 272.0  | 238.9               | 1.13                 | 1.32E-02            | 2.22E+00              |
| 8  | sterile     | 292.0  | 258.9               | 1.13                 | 1.43E-02            | 2.22E+00              |
| 9  | sterile     | 283.0  | 249.9               | 1.13                 | 1.38E-02            | 2.22E+00              |
| 10 | sterile     | 319.0  | 285.9               | 11.25                | 1.55E-01            | 2.22E+01              |
| 11 | sterile     | 362.0  | 328.9               | 11.25                | 1.78E-01            | 2.21E+01              |
| 12 | sterile     | 437.0  | 403.9               | 11.25                | 2.19E-01            | 2.21E+01              |
| 13 | sterile     | 971.0  | 937.9               | 112.50               | 4.61E+00            | 2.16E+02              |
| 14 | sterile     | 1064.0 | 1030.9              | 112.50               | 5.07E+00            | 2.15E+02              |
| 15 | sterile     | 848.0  | 814.9               | 112.50               | 4.01E+00            | 2.17E+02              |
| 16 | 175 T#3     | 3870.0 | 3836.9              | 0.01                 | 2.05E-03            | 1.84E-02              |
| 17 | 175 T#3     | 4116.0 | 4082.9              | 0.01                 | 2.18E-03            | 1.81E-02              |
| 18 | 175 T#3     | 4291.0 | 4257.9              | 0.01                 | 2.27E-03            | 1.80E-02              |
| 19 | 175 T#3     | 3864.0 | 3830.9              | 0.11                 | 2.00E-02            | 1.85E-01              |
| 20 | 175 T#3     | 4053.0 | 4019.9              | 0.11                 | 2.09E-02            | 1.83E-01              |
| 21 | 175 T#3     | 4130.0 | 4096.9              | 0.11                 | 2.13E-02            | 1.82E-01              |
| 22 | 175 T#3     | 4475.0 | 4441.9              | 1.13                 | 2.45E-01            | 1.76E+00              |
| 23 | 175 T#3     | 4615.0 | 4581.9              | 1.13                 | 2.53E-01            | 1.74E+00              |
| 24 | 175 T#3     | 4391.0 | 4357.9              | 1.13                 | 2.40E-01            | 1.77E+00              |
| 25 | 175 T#3     | 4382.0 | 4348.9              | 11.25                | 2.35E+00            | 1.78E+01              |
| 26 | 175 T#3     | 3911.0 | 3877.9              | 11.25                | 2.10E+00            | 1.83E+01              |
| 27 | 175 T#3     | 4103.0 | 4069.9              | 11.25                | 2.20E+00            | 1.81E+01              |
| 28 | 175 T#3     | 6927.0 | 6893.9              | 112.50               | 3.39E+01            | 1.57E+02              |
| 29 | 175 T#3     | 7086.0 | 7052.9              | 112.50               | 3.47E+01            | 1.56E+02              |
| 30 | 175 T#3     | 6708.0 | 6674.9              | 112.50               | 3.28E+01            | 1.59E+02              |
| 31 | 175 T#7     | 1962.0 | 1928.9              | 0.01                 | 1.03E-03            | 2.04E-02              |
| 32 | 175 T#7     | 1957.0 | 1923.9              | 0.01                 | 1.03E-03            | 2.04E-02              |
| 33 | 175 T#7     | 2028.0 | 1994.9              | 0.01                 | 1.06E-03            | 2.04E-02              |
| 34 | 175 T#7     | 2237.0 | 2203.9              | 0.11                 | 1.15E-02            | 2.02E-01              |
| 35 | 175 T#7     | 2239.0 | 2205.9              | 0.11                 | 1.15E-02            | 2.02E-01              |
| 36 | 175 T#7     | 2263.0 | 2229.9              | 0.11                 | 1.16E-02            | 2.02E-01              |
| 37 | 175 T#7     | 1992.0 | 1958.9              | 1.13                 | 1.08E-01            | 2.03E+00              |
| 38 | 175 T#7     | 2041.0 | 2007.9              | 1.13                 | 1.11E-01            | 2.03E+00              |
| 39 | 175 T#7     | 2102.0 | 2068.9              | 1.13                 | 1.14E-01            | 2.02E+00              |
| 40 | 175 T#7     | 2251.0 | 2217.9              | 11.25                | 1.20E+00            | 2.01E+01              |
| 41 | 175 T#7     | 2310.0 | 2276.9              | 11.25                | 1.23E+00            | 2.00E+01              |
| 42 | 175 T#7     | 2632.0 | 2598.9              | 11.25                | 1.41E+00            | 1.97E+01              |
| 43 | 175 T#7     | 5426.0 | 5392.9              | 112.50               | 2.65E+01            | 1.72E+02              |



Batch Experiment: N7  
 Experiment Dates: 1/13/92 to 1/15/92

Objective: Determine Ni isotherms for samples inoculated with 175 T#3 and 175 T#7.

Optical Densities: 175 T#3: 0.80  
 175 T#7: 0.80

| #  | Sample type | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|---------|---------------------|----------------------|---------------------|-----------------------|
| 44 | 175 T#7     | 4858.0  | 4824.9              | 112.50               | 2.37E+01            | 1.78E+02              |
| 45 | 175 T#7     | 6463.0  | 6429.9              | 112.50               | 3.16E+01            | 1.62E+02              |
| 46 | CT Standard | 42130.0 | 42096.9             | 0.02                 |                     |                       |
| 47 | CT Standard | 42133.0 | 42099.9             | 0.02                 |                     |                       |
| 48 | CT Standard | 42358.0 | 42324.9             | 0.02                 |                     |                       |
| 49 | CT Standard | 43747.0 | 43713.9             | 0.23                 |                     |                       |
| 50 | CT Standard | 42715.0 | 42681.9             | 0.23                 |                     |                       |
| 51 | CT Standard | 43207.9 | 43174.8             | 0.23                 |                     |                       |
| 52 | CT Standard | 40828.0 | 40794.9             | 2.25                 |                     |                       |
| 53 | CT Standard | 40911.0 | 40877.9             | 2.25                 |                     |                       |
| 54 | CT Standard | 40698.0 | 40664.9             | 2.25                 |                     |                       |
| 55 | CT Standard | 41876.0 | 41842.9             | 22.50                |                     |                       |
| 56 | CT Standard | 41209.0 | 41175.9             | 22.50                |                     |                       |
| 57 | CT Standard | 41673.0 | 41639.9             | 22.50                |                     |                       |
| 58 | CT Standard | 45701.0 | 45667.9             | 225.00               |                     |                       |
| 59 | CT Standard | 46101.0 | 46067.9             | 225.00               |                     |                       |
| 60 | CT Standard | 45577.0 | 45543.9             | 225.00               |                     |                       |
| 61 | Standard    | 42614.0 | 42580.9             | 0.02                 |                     |                       |
| 62 | Standard    | 42798.0 | 42764.9             | 0.02                 |                     |                       |
| 63 | Standard    | 41444.0 | 41410.9             | 0.02                 |                     |                       |
| 64 | Standard    | 43179.0 | 43145.9             | 0.23                 |                     |                       |
| 65 | Standard    | 13306.0 | 13272.9             | 0.23                 |                     |                       |
| 66 | Standard    | 43287.0 | 43253.9             | 0.23                 |                     |                       |
| 67 | Standard    | 41536.0 | 41502.9             | 2.25                 |                     |                       |
| 68 | Standard    | 41103.0 | 41069.9             | 2.25                 |                     |                       |
| 69 | Standard    | 40857.0 | 40823.9             | 2.25                 |                     |                       |
| 70 | Standard    | 41780.0 | 41746.9             | 22.50                |                     |                       |
| 71 | Standard    | 41755.0 | 41721.9             | 22.50                |                     |                       |
| 72 | Standard    | 41702.0 | 41668.9             | 22.50                |                     |                       |
| 73 | Standard    | 46006.9 | 45973.8             | 225.00               |                     |                       |
| 74 | Standard    | 46732.0 | 46698.9             | 225.00               |                     |                       |
| 75 | Standard    | 46181.0 | 46147.9             | 225.00               |                     |                       |

Batch Experiment: N8  
 Experiment Dates: 2/3/92 to 2/5/92

Objective: Find the effect of 175 T#3 and 175 T#1, 175 T#6, and 175 T#7  
 on Ni Sorption to crushed tuff.

Optical Densities: 175 T#3: 0.80      175 T#6 0.72  
 175 T#1: 0.81      175 T#7 0.24

| #  | Sample Type   | pH          | CPM/mL | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|---------------|-------------|--------|---------------------|----------------------|---------------------|-----------------------|
| 1  | sterile       | 7.69        | 240.0  | 215.0               | 0.02                 | 2.88E-04            | 4.47E-02              |
| 2  | sterile       | 7.71        | 225.0  | 200.0               | 0.02                 | 2.68E-04            | 4.48E-02              |
| 3  | sterile       | 7.69        | 214.0  | 189.0               | 0.02                 | 2.54E-04            | 4.48E-02              |
| 4  | sterile       | 7.68        | 234.0  | 209.0               | 0.23                 | 2.48E-03            | 4.48E-01              |
| 5  | sterile       | 7.82        | 235.0  | 210.0               | 0.23                 | 2.49E-03            | 4.48E-01              |
| 6  | sterile       | 7.67        | 233.0  | 208.0               | 0.23                 | 2.47E-03            | 4.48E-01              |
| 7  | sterile       | 7.66        | 248.0  | 223.0               | 2.27                 | 2.61E-02            | 4.48E+00              |
| 8  | sterile       | 7.63        | 223.0  | 198.0               | 2.27                 | 2.32E-02            | 4.48E+00              |
| 9  | sterile       | 7.80        | 237.0  | 212.0               | 2.27                 | 2.48E-02            | 4.48E+00              |
| 10 | sterile       | 7.84        | 329.0  | 304.0               | 22.65                | 3.05E-01            | 4.47E+01              |
| 11 | sterile       | 7.72        | 366.0  | 341.0               | 22.65                | 3.43E-01            | 4.46E+01              |
| 12 | sterile       | 7.72        | 365.0  | 340.0               | 22.65                | 3.42E-01            | 4.46E+01              |
| 13 | sterile       | 7.07        | 2906.0 | 2881.0              | 226.50               | 3.54E+01            | 3.82E+02              |
| 14 | sterile       | 7.02        | 3095.0 | 3070.0              | 226.50               | 3.77E+01            | 3.78E+02              |
| 15 | sterile       | 6.97        | 3326.0 | 3301.0              | 226.50               | 4.06E+01            | 3.72E+02              |
| 16 | 175 T#3       | 7.05        | 3085.0 | 3060.0              | 0.02                 | 4.10E-03            | 3.71E-02              |
| 17 | 175 T#3       | 6.79        | 3056.0 | 3031.0              | 0.02                 | 4.07E-03            | 3.72E-02              |
| 18 | 175 T#3       | 6.83        | 3396.0 | 3371.0              | 0.02                 | 4.52E-03            | 3.63E-02              |
| 19 | 175 T#3       | 6.79        | 3949.0 | 3924.0              | 0.23                 | 4.66E-02            | 3.60E-01              |
| 20 | 175 T#3       | 6.80        | 3994.0 | 3969.0              | 0.23                 | 4.71E-02            | 3.59E-01              |
| 21 | 175 T#3       | 6.79        | 4134.0 | 4109.0              | 0.23                 | 4.88E-02            | 3.55E-01              |
| 22 | 175 T#3       | 6.87        | 3717.0 | 3692.0              | 2.27                 | 4.32E-01            | 3.67E+00              |
| 23 | 175 T#3       | 6.86        | 3771.0 | 3746.0              | 2.27                 | 4.38E-01            | 3.65E+00              |
| 24 | 175 T#3       | 6.85        | 3526.0 | 3501.0              | 2.27                 | 4.10E-01            | 3.71E+00              |
| 25 | 175 T#3       | 6.85        | 3502.0 | 3477.0              | 22.65                | 3.49E+00            | 3.83E+01              |
| 26 | 175 T#3       | 6.87        | 3403.0 | 3378.0              | 22.65                | 3.39E+00            | 3.85E+01              |
| 27 | 175 T#3       | 6.92        | 3698.0 | 3673.0              | 22.65                | 3.69E+00            | 3.79E+01              |
| 28 | 175 T#3       | 6.55        | 5946.0 | 5921.0              | 226.50               | 7.27E+01            | 3.08E+02              |
| 29 | 175 T#3       | 6.58        | 6744.0 | 6719.0              | 226.50               | 8.26E+01            | 2.88E+02              |
| 30 | 175 T#3       | 6.58        | 6552.0 | 6527.0              | 226.50               | 8.02E+01            | 2.93E+02              |
| 31 | 175 T#1       | 7.26        | 1947.0 | 1922.0              | 22.65                | 1.93E+00            | 4.14E+01              |
| 32 | 175 T#1       | 7.33        | 988.0  | 963.0               | 22.65                | 9.67E-01            | 4.34E+01              |
| 33 | 175 T#1       | 7.25        | 1134.0 | 1109.0              | 22.65                | 1.11E+00            | 4.31E+01              |
| 34 | 175 T#6       | 7.43        | 1045.0 | 1020.0              | 22.65                | 1.02E+00            | 4.33E+01              |
| 35 | 175 T#6       | 7.34        | 1221.0 | 1196.0              | 22.65                | 1.20E+00            | 4.29E+01              |
| 36 | 175 T#6       | 7.44        | 1346.0 | 1321.0              | 22.65                | 1.33E+00            | 4.26E+01              |
| 37 | 175 T#7       | 7.53        | 901.0  | 876.0               | 22.65                | 8.80E-01            | 4.35E+01              |
| 38 | 175 T#7       | 7.40        | 1154.0 | 1129.0              | 22.65                | 1.13E+00            | 4.30E+01              |
| 39 | 175 T#7       | Not sampled |        | -                   | -                    | -                   | -                     |
| 40 | supn. 175 T#3 | 7.54        | 424.0  | 399.0               | 22.65                | 4.01E-01            | 4.45E+01              |
| 41 | supn. 175 T#3 | 7.62        | 373.0  | 348.0               | 22.65                | 3.50E-01            | 4.46E+01              |

Batch Experiment: N8  
 Experiment Dates: 2/3/92 to 2/5/92

Objective: Find the effect of 175 T#3 and 175 T#1, 175 T#6, and 175 T#7  
 on Ni Sorption to crushed tuff.

Optical Densities: 175 T#3: 0.80      175 T#6 0.72  
 175 T#1: 0.81      175 T#7 0.24

| #  | Sample Type   | pH   | CPM/mL  | CPM/mL - Background | Initial Conc. (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|---------------|------|---------|---------------------|----------------------|---------------------|-----------------------|
| 42 | supn. 175 T#3 | 7.60 | 360.0   | 335.0               | 22.65                | 3.36E-01            | 4.46E+01              |
| 43 | supn. 175 T#3 | 7.62 | 271.0   | 246.0               | 22.65                | 2.47E-01            | 4.48E+01              |
| 44 | supn. 175 T#3 | 7.60 | 274.0   | 249.0               | 22.65                | 2.50E-01            | 4.48E+01              |
| 45 | supn. 175 T#3 | 7.60 | 217.0   | 192.0               | 22.65                | 1.93E-01            | 4.49E+01              |
| 46 | CT Standard   |      | 33626.0 | 33601.0             | 0.05                 |                     |                       |
| 47 | CT Standard   |      | 33751.0 | 33726.0             | 0.05                 |                     |                       |
| 48 | CT Standard   |      | 34008.0 | 33983.0             | 0.05                 |                     |                       |
| 49 | CT Standard   |      | 37859.0 | 37834.0             | 0.45                 |                     |                       |
| 50 | CT Standard   |      | 38368.0 | 38343.0             | 0.45                 |                     |                       |
| 51 | CT Standard   |      | 38364.0 | 38339.0             | 0.45                 |                     |                       |
| 52 | CT Standard   |      | 38576.0 | 38551.0             | 4.53                 |                     |                       |
| 53 | CT Standard   |      | 38603.0 | 38578.0             | 4.53                 |                     |                       |
| 54 | CT Standard   |      | 39018.0 | 38993.0             | 4.53                 |                     |                       |
| 55 | CT Standard   |      | 45651.0 | 45626.0             | 45.30                |                     |                       |
| 56 | CT Standard   |      | 44595.0 | 44570.0             | 45.30                |                     |                       |
| 57 | CT Standard   |      | 45131.9 | 45106.9             | 45.30                |                     |                       |
| 58 | CT Standard   |      | 37202.0 | 37177.0             | 453.00               |                     |                       |
| 59 | CT Standard   |      | 36682.0 | 36657.0             | 453.00               |                     |                       |
| 60 | CT Standard   |      | 36798.0 | 36773.0             | 453.00               |                     |                       |
| 61 | Standard      |      | 34343.0 | 34318.0             | 0.05                 |                     |                       |
| 62 | Standard      |      | 34138.0 | 34113.0             | 0.05                 |                     |                       |
| 63 | Standard      |      | 34089.0 | 34064.0             | 0.05                 |                     |                       |
| 64 | Standard      |      | 38589.0 | 38564.0             | 0.45                 |                     |                       |
| 65 | Standard      |      | 38559.0 | 38534.0             | 0.45                 |                     |                       |
| 66 | Standard      |      | 38377.0 | 38352.0             | 0.45                 |                     |                       |
| 67 | Standard      |      | 39215.0 | 39190.0             | 4.53                 |                     |                       |
| 68 | Standard      |      | 39192.0 | 39167.0             | 4.53                 |                     |                       |
| 69 | Standard      |      | 38949.0 | 38924.0             | 4.53                 |                     |                       |
| 70 | Standard      |      | 46113.0 | 46088.0             | 45.30                |                     |                       |
| 71 | Standard      |      | 46415.0 | 46390.0             | 45.30                |                     |                       |
| 72 | Standard      |      | 46704.0 | 46679.0             | 45.30                |                     |                       |
| 73 | Standard      |      | 37011.0 | 36986.0             | 453.00               |                     |                       |
| 74 | Standard      |      | 37233.0 | 37208.0             | 453.00               |                     |                       |
| 75 | Standard      |      | 36837.0 | 36812.0             | 453.00               |                     |                       |

Buffer Experiment: B1  
 Experiment Dates 9/30/92 to 10/2/92

Objective: Determine the effect of pH on sorption.

Optical Density: 175 T#3: 0.69

| #  | Bact. | Buffer   | pH   |                      | CPM/mL  | CPM/mL -<br>Background | Initial<br>Conc.<br>(mg/L) | Sample<br>Conc.<br>(mg/L) | Sorbed<br>Amount<br>(mg/kg) |
|----|-------|----------|------|----------------------|---------|------------------------|----------------------------|---------------------------|-----------------------------|
|    |       |          | pH   | Ave. and<br>St. Dev. |         |                        |                            |                           |                             |
| 31 | No    | No       | 8.16 | 8.18                 | 215.0   | 181.9                  | 10.00                      | 0.13                      | 19.62                       |
| 32 | No    | No       | 8.12 | 0.08                 | 196.3   | 163.2                  | 10.00                      | 0.12                      | 19.65                       |
| 33 | No    | No       | 8.27 |                      | 228.7   | 195.6                  | 10.00                      | 0.14                      | 19.60                       |
| 34 | No    | Yes      | 7.93 | 7.89                 | 879.4   | 846.3                  | 10.00                      | 0.60                      | 18.69                       |
| 35 | No    | Yes      | 7.86 | 0.04                 | 836.4   | 803.3                  | 10.00                      | 0.57                      | 18.75                       |
| 36 | No    | Yes      | 7.88 |                      | 903.2   | 870.1                  | 10.00                      | 0.61                      | 18.65                       |
| 37 | Yes   | No       | 7.07 | 7.09                 | 2332.8  | 2299.7                 | 10.00                      | 1.62                      | 16.64                       |
| 38 | Yes   | No       | 7.14 | 0.04                 | 2092.1  | 2059.0                 | 10.00                      | 1.45                      | 16.98                       |
| 39 | Yes   | No       | 7.06 |                      | 2315.9  | 2282.8                 | 10.00                      | 1.61                      | 16.66                       |
| 40 | Yes   | Yes      | 7.82 | 7.79                 | 889.3   | 856.2                  | 10.00                      | 0.60                      | 18.67                       |
| 41 | Yes   | Yes      | 7.80 | 0.04                 | 796.2   | 763.1                  | 10.00                      | 0.54                      | 18.80                       |
| 42 | Yes   | Yes      | 7.75 |                      | 869.3   | 836.2                  | 10.00                      | 0.59                      | 18.70                       |
| 43 | CT    | Standard | 8.06 | 7.72                 | 28480.8 | 28447.7                | 20.00                      |                           |                             |
| 44 | CT    | Standard | 7.47 | 0.31                 | 27898.0 | 27864.9                | 20.00                      |                           |                             |
| 45 | CT    | Standard | 7.63 |                      | 28335.4 | 28302.3                | 20.00                      |                           |                             |

Ave. pH with buffer: 7.84

s of pH with buffer: 0.06

Note: Sample numbers started with 31 for this experiments.

## Appendix C

### Cd Batch Equilibrium Experiments

## APPENDIX C

### CADMIUM BATCH EQUILIBRIUM EXPERIMENTS

This section contains data from two experiments performed to determine the effect of microbes on  $\text{Cd}^{2+}$  sorption to crushed tuff (R2 and R3) and one experiment performed to determine when  $\text{Cd}^{2+}$  sorption to tuff reaches an equilibrium (Cd kinetic). In addition, there is a graph showing the results of the Cd kinetic experiment. Experiment R2 contains both the AA analyses from the New Mexico Bureau of Mines and Mineral Resources (NMBMMR) Chemistry Laboratory and the ICP analyses from the Soil, Plant, and Water (SWAT) laboratory of New Mexico State University. Samples from the NMIMT are replicates of SWAT samples having the same sample number. Figure 4 in Chapter 2 is from the SWAT data. Results from experiment R3 are displayed in Figure 5 of Chapter 2.

I did not use the lower  $\text{Cd}^{2+}$  concentrations data because the data appeared to be random. I concluded that the chemical analyses were not sensitive enough at low concentrations.

Batch Experiment: R2  
 Experiment Dates: 6/26/91 to 7/1/91

Objective: Find the effect of 50 T#7 and 175 T#1  
 on Cd sorption.

Optical Densities: 50 T#7: 0.95  
 175 T#1: 0.98

Analysis done at the SWAT Laboratory

| #  | Sample type | Initial Conc. x 2 (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|--------------------------|---------------------|-----------------------|
| 1  | 50 T#7      | 0.18                     | <.01                | -                     |
| 2  | 50 T#7      | 0.18                     | <.01                | -                     |
| 3  | 50 T#7      | 0.18                     | <.01                | -                     |
| 4  | 50 T#7      | 0.91                     | <.01                | -                     |
| 5  | 50 T#7      | 0.91                     | <.01                | -                     |
| 6  | 50 T#7      | 0.91                     | <.01                | -                     |
| 7  | 50 T#7      | 2.49                     | 0.03                | 2.43                  |
| 8  | 50 T#7      | 2.49                     | 0.03                | 2.43                  |
| 9  | 50 T#7      | 2.49                     | 0.02                | 2.45                  |
| 10 | 50 T#7      | 10.21                    | No analysis         | -                     |
| 11 | 50 T#7      | 10.21                    | 0.12                | 9.97                  |
| 12 | 50 T#7      | 10.21                    | 0.12                | 9.97                  |
| 13 | 50 T#7      | 25.46                    | 0.48                | 24.50                 |
| 14 | 50 T#7      | 25.46                    | 0.39                | 24.68                 |
| 15 | 50 T#7      | 25.46                    | 0.44                | 24.58                 |
| 16 | 50 T#7      | 103.58                   | 3.69                | 96.20                 |
| 17 | 50 T#7      | 103.58                   | 3.41                | 96.76                 |
| 18 | 50 T#7      | 103.58                   | 3.43                | 96.72                 |
| 19 | 50 T#7      | 253.08                   | 14.69               | 223.70                |
| 20 | 50 T#7      | 253.08                   | 15.91               | 221.26                |
| 21 | 50 T#7      | 253.08                   | 14.7                | 223.68                |
| 22 | 175 T#1     | 0.18                     | 0.02                | 0.14                  |
| 23 | 175 T#1     | 0.18                     | <.01                | -                     |
| 24 | 175 T#1     | 0.18                     | <.01                | -                     |
| 25 | 175 T#1     | 0.91                     | <.01                | -                     |
| 26 | 175 T#1     | 0.91                     | <.01                | -                     |
| 27 | 175 T#1     | 0.91                     | 0.05                | 0.81                  |
| 28 | 175 T#1     | 2.49                     | 0.05                | 2.39                  |
| 29 | 175 T#1     | 2.49                     | 0.2                 | Not used              |
| 30 | 175 T#1     | 2.49                     | 0.04                | 2.41                  |
| 31 | 175 T#1     | 10.21                    | 0.15                | 9.91                  |
| 32 | 175 T#1     | 10.21                    | 0.12                | 9.97                  |
| 33 | 175 T#1     | 10.21                    | 0.12                | 9.97                  |
| 34 | 175 T#1     | 25.46                    | 0.45                | 24.56                 |
| 35 | 175 T#1     | 25.46                    | 0.38                | 24.70                 |
| 36 | 175 T#1     | 25.46                    | 0.45                | 24.56                 |
| 37 | 175 T#1     | 103.58                   | 3.12                | 97.34                 |
| 38 | 175 T#1     | 103.58                   | 3.61                | 96.36                 |
| 39 | 175 T#1     | 103.58                   | 3.6                 | 96.38                 |

Batch Experiment: R2  
 Experiment Dates: 6/26/91 to 7/1/91

Objective: Find the effect of 50 T#7 and 175 T#1  
 on Cd sorption.

Optical Densities: 50 T#7: 0.95  
 175 T#1: 0.98

Analysis done at the SWAT Laboratory

| #  | Sample type | Initial Conc. x 2 (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|--------------------------|---------------------|-----------------------|
| 40 | 175 T#1     | 253.08                   | 14.02               | 225.04                |
| 41 | 175 T#1     | 253.08                   | 12.43               | 228.22                |
| 42 | 175 T#1     | 253.08                   | 13.1                | 226.88                |
| 43 | sterile     | 0.18                     | 0.01                | 0.16                  |
| 44 | sterile     | 0.18                     | <.01                | -                     |
| 45 | sterile     | 0.18                     | 0.02                | 0.14                  |
| 46 | sterile     | 0.91                     | <.01                | -                     |
| 47 | sterile     | 0.91                     | 0.02                | 0.87                  |
| 48 | sterile     | 0.91                     | 0.05                | 0.81                  |
| 49 | sterile     | 2.49                     | <.01                | -                     |
| 50 | sterile     | 2.49                     | 0.08                | 2.33                  |
| 51 | sterile     | 2.49                     | 0.11                | 2.27                  |
| 52 | sterile     | 10.21                    | 0.29                | 9.63                  |
| 53 | sterile     | 10.21                    | 0.11                | 9.99                  |
| 54 | sterile     | 10.21                    | 0.02                | 10.17                 |
| 55 | sterile     | 25.46                    | 0.05                | 25.36                 |
| 56 | sterile     | 25.46                    | 0.05                | 25.36                 |
| 57 | sterile     | 25.46                    | 0.04                | 25.38                 |
| 58 | sterile     | 103.58                   | 0.6                 | 102.38                |
| 59 | sterile     | 103.58                   | 0.57                | 102.44                |
| 60 | sterile     | 103.58                   | 0.58                | 102.42                |
| 61 | sterile     | 253.08                   | 5.38                | 242.32                |
| 62 | sterile     | 253.08                   | 5.71                | 241.66                |
| 63 | sterile     | 253.08                   | 5.48                | 242.12                |
| 64 | Standard    |                          | 0.18                |                       |
| 65 | Standard    |                          | 0.19                |                       |
| 66 | Standard    |                          | 0.18                |                       |
| 67 | Standard    |                          | 0.92                |                       |
| 68 | Standard    |                          | 0.87                |                       |
| 69 | Standard    |                          | 0.94                |                       |
| 70 | Standard    |                          | 2.48                |                       |
| 71 | Standard    |                          | 2.46                |                       |
| 72 | Standard    |                          | 2.52                |                       |
| 73 | Standard    |                          | 10.45               |                       |
| 74 | Standard    |                          | 10.11               |                       |
| 75 | Standard    |                          | 10.08               |                       |
| 76 | Standard    |                          | 25.65               |                       |
| 77 | Standard    |                          | 25.08               |                       |
| 78 | Standard    |                          | 25.64               |                       |



Batch Experiment: R2  
Experiment Dates: 6/26/91 to 7/1/91

Objective: Find the effect of 50 T#7 and 175 T#1  
on Cd sorption.

Optical Densities: 50 T#7: 0.95  
175 T#1: 0.98

Analysis done at the SWAT Laboratory

| #  | Sample type | Initial Conc. x 2 (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|--------------------------|---------------------|-----------------------|
| 79 | Standard    |                          | 107.12              |                       |
| 80 | Standard    |                          | 101.34              |                       |
| 81 | Standard    |                          | 102.29              |                       |
| 82 | Standard    |                          | 259.77              |                       |
| 83 | Standard    |                          | 250.49              |                       |
| 84 | Standard    |                          | 248.99              |                       |

Batch Experiment: R2  
 Experiment Dates: 6/26/91 to 7/1/91

Objective: Find the effect of 50 T#7 and 175 T#1  
 on Cd sorption.

Data from the NMBMMR Chemistry Laboratory:

| #   | Sample type | Initial Conc. x 2 (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|-----|-------------|--------------------------|---------------------|-----------------------|
| 3A  | 50 T#7      | 0.1                      | <.05                | -                     |
| 6A  | 50 T#7      | 0.8                      | <.05                | -                     |
| 8A  | 50 T#7      | 2.2                      | <.05                | -                     |
| 10  | 50 T#7      | 9.2                      | 0.1                 | 9                     |
| 13A | 50 T#7      | 23                       | 0.4                 | 22.2                  |
| 16A | 50 T#7      | 90                       | 3                   | 84                    |
| 20A | 50 T#7      | 220                      | 12.2                | 195.6                 |
| 23A | 175 T#1     | 0.1                      | <.05                | -                     |
| 26A | 175 T#1     | 0.8                      | <.05                | -                     |
| 30A | 175 T#1     | 2.2                      | <.05                | -                     |
| 32A | 175 T#1     | 9.2                      | 0.09                | 9.02                  |
| 34A | 175 T#1     | 23                       | 0.3                 | 22.4                  |
| 39A | 175 T#1     | 90                       | 2.6                 | 84.8                  |
| 42A | 175 T#1     | 220                      | 10.3                | 199.4                 |
| 45A | sterile     | 0.1                      | <.05                | -                     |
| 48A | sterile     | 0.8                      | <.05                | -                     |
| 50A | sterile     | 2.2                      | <.05                | -                     |
| 54A | sterile     | 9.2                      | <.05                | -                     |
| 56A | sterile     | 23                       | <.05                | -                     |
| 58A | sterile     | 90                       | 0.4                 | 89.2                  |
| 63A | sterile     | 220                      | 5.2                 | 209.6                 |
| 64A | Standard    |                          | 0.1                 |                       |
| 67A | Standard    |                          | 0.8                 |                       |
| 70A | Standard    |                          | 2.2                 |                       |
| 73A | Standard    |                          | 9.2                 |                       |
| 76A | Standard    |                          | 23                  |                       |
| 79A | Standard    |                          | 90                  |                       |
| 82A | Standard    |                          | 220                 |                       |

Batch Experiment: R3  
 Experiment Dates: 8/5/91 to 8/7/91

Objective: Find the effect of 50 T#12 and 175 T#3 on Cd sorption to tuff.

Optical Densities: 50 T#12: 1.80  
 175 T#3: 0.85

Analysis done at the SWAT Laboratory

| #  | Sample type | Initial Conc. x 2 (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|--------------------------|---------------------|-----------------------|
| 1  | 50 T#12     | 0.16                     | 0.01                | 0.14                  |
| 2  | 50 T#12     | 0.16                     | <.01                | -                     |
| 3  | 50 T#12     | 0.16                     | <.01                | -                     |
| 4  | 50 T#12     | 1.87                     | 0.02                | 1.83                  |
| 5  | 50 T#12     | 1.87                     | 0.02                | 1.83                  |
| 6  | 50 T#12     | 1.87                     | 0.02                | 1.83                  |
| 7  | 50 T#12     | 9.88                     | 0.16                | 9.56                  |
| 8  | 50 T#12     | 9.88                     | 0.15                | 9.58                  |
| 9  | 50 T#12     | 9.88                     | 0.16                | 9.56                  |
| 10 | 50 T#12     | 25.97                    | 0.59                | 24.79                 |
| 11 | 50 T#12     | 25.97                    | 0.61                | 24.75                 |
| 12 | 50 T#12     | 25.97                    | 0.66                | 24.65                 |
| 13 | 50 T#12     | 248.76                   | 19.88               | 209.00                |
| 14 | 50 T#12     | 248.76                   | 19.26               | 210.24                |
| 15 | 50 T#12     | 248.76                   | 17.60               | 213.56                |
| 16 | 175 T#3     | 0.16                     | <.01                | -                     |
| 17 | 175 T#3     | 0.16                     | 0.01                | 0.14                  |
| 18 | 175 T#3     | 0.16                     | 0.01                | 0.14                  |
| 19 | 175 T#3     | 1.87                     | 0.03                | 1.81                  |
| 20 | 175 T#3     | 1.87                     | 0.03                | 1.81                  |
| 21 | 175 T#3     | 1.87                     | 0.03                | 1.81                  |
| 22 | 175 T#3     | 9.88                     | 0.18                | 9.52                  |
| 23 | 175 T#3     | 9.88                     | 0.22                | 9.44                  |
| 24 | 175 T#3     | 9.88                     | 0.20                | 9.48                  |
| 25 | 175 T#3     | 25.97                    | 0.66                | 24.65                 |
| 26 | 175 T#3     | 25.97                    | 0.63                | 24.71                 |
| 27 | 175 T#3     | 25.97                    | 0.63                | 24.71                 |
| 28 | 175 T#3     | 248.76                   | 19.64               | 209.48                |
| 29 | 175 T#3     | 248.76                   | 19.83               | 209.10                |
| 30 | 175 T#3     | 248.76                   | 19.45               | 209.86                |
| 31 | sterile     | 0.16                     | 0.02                | 0.12                  |
| 32 | sterile     | 0.16                     | <.01                | -                     |
| 33 | sterile     | 0.16                     | <.01                | -                     |
| 34 | sterile     | 1.87                     | <.01                | -                     |
| 35 | sterile     | 1.87                     | <.01                | -                     |
| 36 | sterile     | 1.87                     | <.01                | -                     |
| 37 | sterile     | 9.88                     | 0.02                | 9.84                  |
| 38 | sterile     | 9.88                     | 0.02                | 9.84                  |
| 39 | sterile     | 9.88                     | 0.03                | 9.82                  |

Batch Experiment: R3  
Experiment Dates: 8/5/91 to 8/7/91

Objective: Find the effect of 50 T#12 and 175 T#3 on Cd sorption to tuff.

Optical Densities: 50 T#12: 1.80  
175 T#3: 0.85

Analysis done at the SWAT Laboratory

| #  | Sample type | Initial Conc. x 2 (mg/L) | Sample Conc. (mg/L) | Sorbed Amount (mg/kg) |
|----|-------------|--------------------------|---------------------|-----------------------|
| 40 | sterile     | 25.97                    | 0.05                | 25.87                 |
| 41 | sterile     | 25.97                    | 0.05                | 25.87                 |
| 42 | sterile     | 25.97                    | 0.05                | 25.87                 |
| 43 | sterile     | 248.76                   | 6.93                | 234.90                |
| 44 | sterile     | 248.76                   | 6.56                | 235.64                |
| 45 | sterile     | 248.76                   | 7.04                | 234.68                |
| 46 | Standard    |                          | 0.19                |                       |
| 47 | Standard    |                          | 0.15                |                       |
| 48 | Standard    |                          | 0.14                |                       |
| 49 | Standard    |                          | 1.83                |                       |
| 50 | Standard    |                          | 1.90                |                       |
| 51 | Standard    |                          | 1.87                |                       |
| 52 | Standard    |                          | 9.62                |                       |
| 53 | Standard    |                          | 10.02               |                       |
| 54 | Standard    |                          | 9.99                |                       |
| 55 | Standard    |                          | 25.71               |                       |
| 56 | Standard    |                          | 25.70               |                       |
| 57 | Standard    |                          | 26.51               |                       |
| 58 | Standard    |                          | 243.83              |                       |
| 59 | Standard    |                          | 252.19              |                       |
| 60 | Standard    |                          | 250.27              |                       |

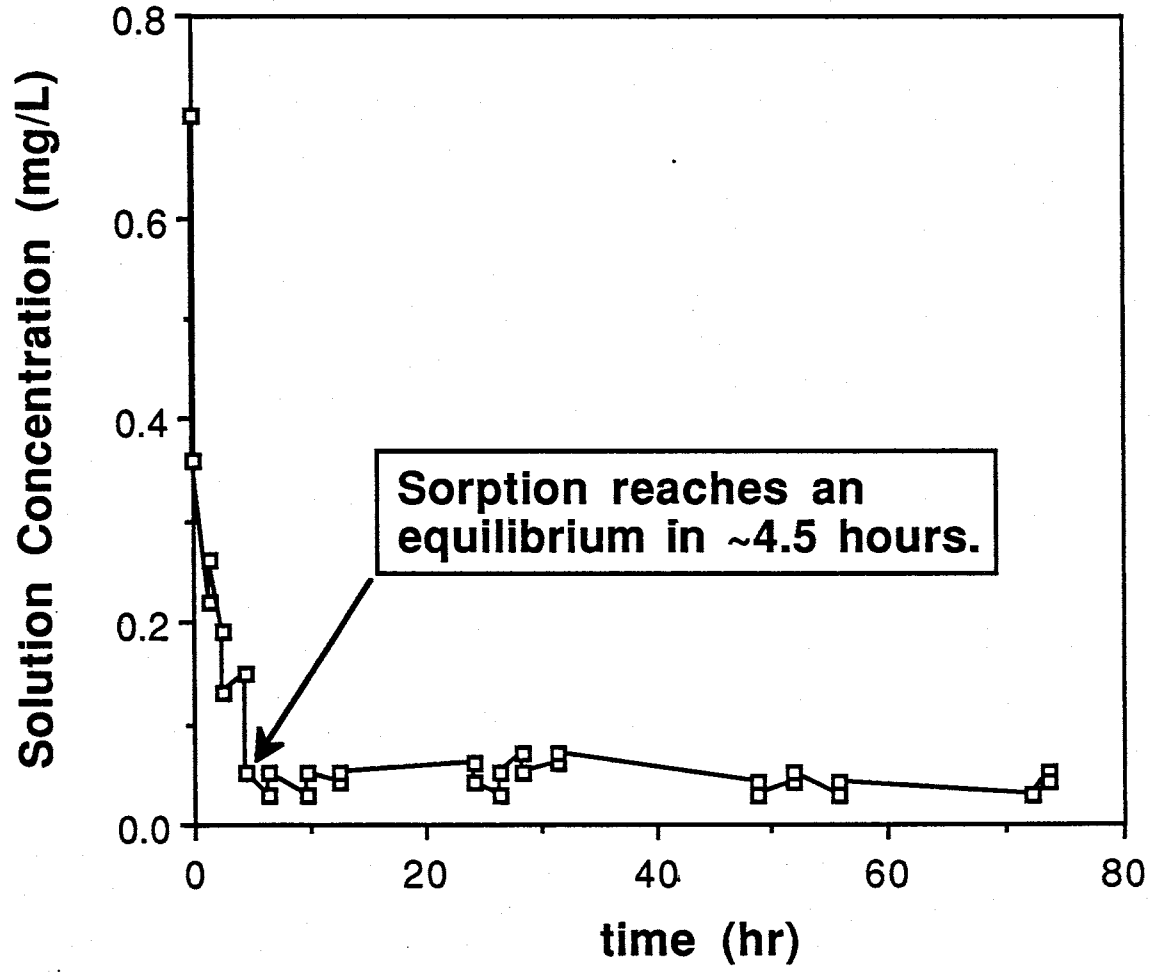
Experiment: Cd kinetic

Experiment Dates: 7/9/92 to 7/12/91

Objective: Determine how fast Cd in solution reaches an equilibrium with Cd sorbed to crushed tuff.

| #  | Time (hr) | Sample Conc. C (mg/L) | Amount Sorbed S (mg/kg) |
|----|-----------|-----------------------|-------------------------|
| 1  | 0.1       | 0.7                   | 48.40                   |
| 2  | 0.1       | 0.36                  | 49.08                   |
| 3  | 1.3       | 0.22                  | 49.36                   |
| 4  | 1.3       | 0.26                  | 49.28                   |
| 5  | 2.5       | 0.19                  | 49.42                   |
| 6  | 2.5       | 0.13                  | 49.54                   |
| 7  | 4.5       | 0.15                  | 49.50                   |
| 8  | 4.5       | 0.05                  | 49.70                   |
| 9  | 6.5       | 0.03                  | 49.74                   |
| 10 | 6.5       | 0.05                  | 49.70                   |
| 11 | 9.8       | 0.03                  | 49.74                   |
| 12 | 9.8       | 0.05                  | 49.70                   |
| 13 | 12.5      | 0.04                  | 49.72                   |
| 14 | 12.5      | 0.05                  | 49.70                   |
| 15 | 24.3      | 0.06                  | 49.68                   |
| 16 | 24.3      | 0.04                  | 49.72                   |
| 17 | 26.5      | 0.03                  | 49.74                   |
| 18 | 26.5      | 0.05                  | 49.70                   |
| 19 | 28.5      | 0.07                  | 49.66                   |
| 20 | 28.5      | 0.05                  | 49.70                   |
| 21 | 31.5      | 0.06                  | 49.68                   |
| 22 | 31.5      | 0.07                  | 49.66                   |
| 23 | 48.8      | 0.04                  | 49.72                   |
| 24 | 48.8      | 0.03                  | 49.74                   |
| 25 | 51.8      | 0.04                  | 49.72                   |
| 26 | 51.8      | 0.05                  | 49.70                   |
| 27 | 55.7      | 0.03                  | 49.74                   |
| 28 | 55.7      | 0.04                  | 49.72                   |
| 29 | 72.3      | 0.03                  | 49.74                   |
| 30 | 72.3      | 0.03                  | 49.74                   |
| 31 | 73.5      | 0.05                  | 49.70                   |
| 32 | 73.5      | 0.04                  | 49.72                   |
| 33 | Standard  | 24.74                 |                         |
| 34 | Standard  | 25.06                 |                         |

### Experiment: Cd kinetic



## Appendix D

# Transport Experiment

## APPENDIX D

### TRANSPORT EXPERIMENT

This appendix contains the results of a transport experiment designated as 'C2' in my laboratory notebook and results of a saturated conductivity test (D1) carried out on columns packed separately from the columns packed for 'C2'. Information from 'C2' include the effluent flux (D2), dead volume in the apparatus (D3), pore volumes determination (D4), liquid scintillation counts from influent solutions (D5), atomic adsorption analyses of Ni influent solutions (D6), Br<sup>-</sup> effluent concentrations (D7), Ni<sup>2+</sup> effluent concentrations (D8), and the column effluent pH measurements (D9). I have not presented any parameters determined by fitting the BTCs to the CXTFIT two-region model because the optimization of the Br<sup>-</sup> BTCs did not converge and there were too many variables (with the addition of R) for the optimization of Ni<sup>2+</sup> BTCs to converge to reasonable parameter values.

Results from the saturated conductivity tests (D1) are reported in the Transport Experiment methods section of Chapter 2.

The section on effluent flux (D2) also contains both the date and days from the beginning of the experiment at which the columns had a certain flux. Fluxes were calculated by measuring the column effluent volume accumulated over time.

Section D3 contains information on the volume of water within the apparatus (dead volume). The dead volume includes volume in connecting tubing, porous endplates, and the endspace existing in the top and bottom of the columns. An illustration in section D3 shows the location and dimensions of these parts of the apparatus.



Section D4 contains information on the volume of water (one pore volume) contained in each column at the end of the experiment and on the dry bulk density of the packed columns. The volume of water was found by subtracting the dried column apparatus mass and the oven-dried tuff mass from the mass of the wet packed column. I used the average volume from all four columns to calculate the number of pore volumes passing through each individual column. Reasons for this include (1) I believe that the volume of water may have changed during the experiment due to trapped air, since I did not use deaired water and did not saturate the columns with CO<sub>2</sub> prior to starting the experiment and (2) the columns were all packed in the same manner. Upon reviewing my results, I now believe that a better method to calculate pore volumes is to use the measured volume in each column. This would result in different CXTFIT optimized parameters. However, the trends for the fitted parameters would be the same as those using the average pore volumes; therefore the discussion found in chapter 2 would not change.

Section D5 contains information on liquid scintillation count of the influent solution. I used 20 bottles of influent solution for columns 1 and 2 (sterile) and 12 bottles for columns 3 and 4 (inoculated). I measured the LSC of the solution within the bottles before attaching them to the columns (notated 'before' in the appendix) and the solution left over in the bottom of the bottle after removing the solution from the columns (notated 'after' in the appendix).

To make the influent solution, I first made up a stock solution containing approximately 1000 mg L<sup>-1</sup> Ni<sup>2+</sup> labeled with <sup>63</sup>Ni. This solution was autoclaved and kept in sealed containers. I marked the 6 L line on the influent bottles, so that after autoclaving solutions containing CaCl<sub>2</sub>, I could add 60 mL

of the stock solution, then fill the bottles up to the 6 L line with NANOpure water. To prepare the solutions for the sterile columns, I autoclaved concentrated solutions of  $\text{NaN}_3$  and added them to the influent bottles prior to filling with NANOpure water because when  $\text{Ni}^{2+}$  and  $\text{NaN}_3$  are heated together, a precipitate forms. I used disconnects between tubing to prevent microbial contamination when I changed the solutions.

Section D6 shows the results of atomic adsorption analyses of  $\text{Ni}^{2+}$  influent solution concentrations. This data is not extensive, so my conclusion that the average influent solution concentration is 9.3 mg/L is probably not correct; however, the actual concentration of the influent solution does not affect the conclusions, since I used relative concentrations ( $C/C_0$ ) for parameter fitting of the  $\text{Ni}^{2+}$  BTCs.

Bromide effluent concentrations are given in section D7 of this appendix along with the high performance liquid chromatography (HPLC) peak heights used to calculate these concentrations. The  $\text{Br}^-$  concentration of the effluent prior to adding  $\text{Br}^-$  to the columns and for the influent solutions to each column is also given. The actual volume of each sample was not measured, but I did measure the flux before adding the slug, after taking samples for the upward limb, and after the slug finished. Therefore, to calculate PV's, I used the flux measured before the columns were attached for the upward limb of the BTCs and the flux measured after  $\text{Br}^-$  slug finished for the downward limb of the BTCs. Note that to optimize the velocity, I needed to use time instead of PVs. Since the flux changed during the time I added  $\text{Br}^-$ , I recalculated time at a constant flux.

The flux I used for this was the same as the measured flux during the middle part of the breakthrough curve. After determining the PV's for each column, I subtracted 0.3 PV to account for dead volume.

Nickel effluent concentrations are given in section D8. The dead volume was subtracted from the number of pore volumes even though the amount was negligible.  $C/C_0$  was calculated by dividing the sample CPM by the average standard CPM after background counts were subtracted from each value.

The pH values of the column influent and effluent solutions are given in section D9.

**SECTION D1**  
**SATURATED CONDUCTIVITY TESTS**

The following tests were performed on unautoclaved tuff.  
 The item being tested was saturated with CO<sub>2</sub> before the test begun  
 and the water was deaired.  
 The water in the falling head permeameter test was run from the top  
 to the bottom of the columns.

| Date     | Hydraulic<br>Conductivity<br>(m/sec) | Comment                                     |
|----------|--------------------------------------|---|
| 12/22/91 | 4.80E-07                             | Conductivity of the frit                    |
| 12/22/91 | 3.10E-06                             | Conductivity of column packed without frits |
| 12/23/91 | 2.80E-06                             | Conductivity of 1st column packed with frit |
| 12/27/91 | 1.80E-06                             | Conductivity of 2nd column packed with frit |

The following tests were performed on a column packed with autoclaved tuff.  
 The column was saturated with CO<sub>2</sub> before the test begun and the water  
 was deaired.

| Date    | Hydraulic<br>Conductivity<br>(m/sec) | Comment  |
|---------|--------------------------------------|--|
| 3/21/92 | 7.70E-06                             | With frit, Made sure air was bled from<br>the top using a syringe.                   |
| 3/22/92 | 4.10E-06                             | Same column, Lower K with time:  |
| 3/24/92 | 2.50E-06                             | Due to compaction? Note large pores or<br>bubbles appear near the top of the column. |

**SECTION D2  
EFFLUENT FLUX**

Dates: 7/7/92 to 9/11/93

I used the following to calculate the number of PV's passing through the columns:

Day 0 to day 3: Used the average flux of 0.42 mL/min for all columns.  
 Day 3 to day 15: Used the average flux of 0.42 mL/min for all columns.  
     except day 5, when, from 5.17 to 5.96 days, only 105.5 mL passed through  
     column 3 and 73.8 mL passed through column 4.  
 Day 15 to day 34: Used the average flux of 0.42 mL/min for all columns.  
 Day 34 to end: Due to variability in pumping, used the fluxes listed.

| Date         | Days from<br>start | Column fluxes in mL/min |             |             |             |
|--------------|--------------------|-------------------------|-------------|-------------|-------------|
|              |                    | Column<br>1             | Column<br>2 | Column<br>3 | Column<br>4 |
| 7/6/92       | -1                 | 0.42                    | 0.42        | 0.43        | 0.43        |
| 7/6/92       | -1                 | 0.41                    | 0.42        | 0.42        | 0.43        |
| 7/10/92      | 3                  | 0.41                    | 0.40        | 0.41        | 0.40        |
| 7/11 to 7/12 | 3.25 to 4.75       | 0.21                    | 0.21        | 0.21        | 0.20        |
| 7/12 to 7/14 | 5.2 to 7.5         | 0.21                    | 0.21        | 0.21        | 0.21        |
| 7/16 to 7/21 | 9.1 to 14.5        | 0.20                    | 0.21        | 0.21        | 0.20        |
| 7/22 to 7/23 | 15 to 16           | 0.40                    | 0.41        | 0.41        | 0.40        |
| 7/23 to 7/24 | 16 to 17           | 0.42                    | 0.42        | 0.42        | 0.42        |
| 7/26 to 7/27 | 19 to 20           | 0.41                    | 0.42        | 0.43        | 0.41        |
| 7/27 to 7.28 | 20 to 21           | 0.42                    | 0.42        | 0.41        | 0.40        |
| 7/29 to 7/30 | 21 to 22           | 0.41                    | 0.42        | 0.41        | 0.40        |
| 7/31 to 8/1  | 23 to 24           | 0.43                    | 0.41        | 0.41        | 0.41        |
| 8/1 to 8/2   | 24 to 25           | 0.42                    | 0.41        | 0.41        | 0.42        |
| 8/4 to 8/5   | 28 to 29           | 0.40                    | 0.40        | 0.41        | 0.40        |
| 8/9 to 8/10  | 33 to 34           | 0.41                    | 0.40        | 0.41        | 0.40        |
| 8/12 to 8/13 | 36 to 37           | 0.40                    | 0.39        | 0.40        | 0.41        |
| 8/17 to 8/18 | 41 to 42           | 0.40                    | 0.37        | 0.40        | 0.40        |
| 8/20 to 8/21 | 44 to 45           | 0.39                    | 0.39        |             |             |
| 8/22 to 8/23 | 46 to 47           | 0.35                    | 0.34        |             |             |
| 8/23 to 8/24 | 47 to 48           | 0.34                    | 0.38        |             |             |
| 8/24 to 8/25 | 48 to 49           | 0.38                    | 0.39        |             |             |
| 8/25 to 8/26 | 49 to 50           | 0.38                    | 0.40        |             |             |
| 8/26 to 8/27 | 50 to -51          | 0.38                    | 0.38        |             |             |
| 8/28 to 8/29 | 52 to 53           | 0.38                    | 0.39        |             |             |
| 8/29 to 8/30 | 53 to 54           | 0.38                    | 0.38        |             |             |
| 8/30 to 8/31 | 54 to 55           | 0.38                    | 0.38        |             |             |
| 8/31 to 9/1  | 55 to 56           | 0.36                    | 0.36        |             |             |
| 9/1 to 9/2   | 56 to 57           | 0.38                    | 0.37        |             |             |
| 9/2 to 9/3   | 57 to 58           | 0.39                    | 0.39        |             |             |
| 9/3 to 9/4   | 58 to 59           | 0.33                    | 0.37        |             |             |
| 9/4 to 9/5   | 59 to 60           | 0.34                    | 0.36        |             |             |
| 9/5 to 9/6   | 60 to 61           | 0.33                    | 0.36        |             |             |
| 9/6 to 9/7   | 61 to 62           | 0.32                    | 0.34        |             |             |
| 9/7 to 9/8   | 62 to 63           | 0.34                    | 0.37        |             |             |
| 9/8 to 9/9   | 63 to 64           | 0.35                    | 0.38        |             |             |
| 9/9 to 9/10  | 64 to 65           | 0.34                    | 0.38        |             |             |
| 9/10 to 9/11 | 65 to 66           | 0.35                    | 0.38        |             |             |

**SECTION D3  
COLUMN APPARATUS VOLUME**

Date: 10/2/92

Method: To determine the maximum dead volume in the apparatus, I put the column together without any crushed tuff, then pumped CO<sub>2</sub> through the column.

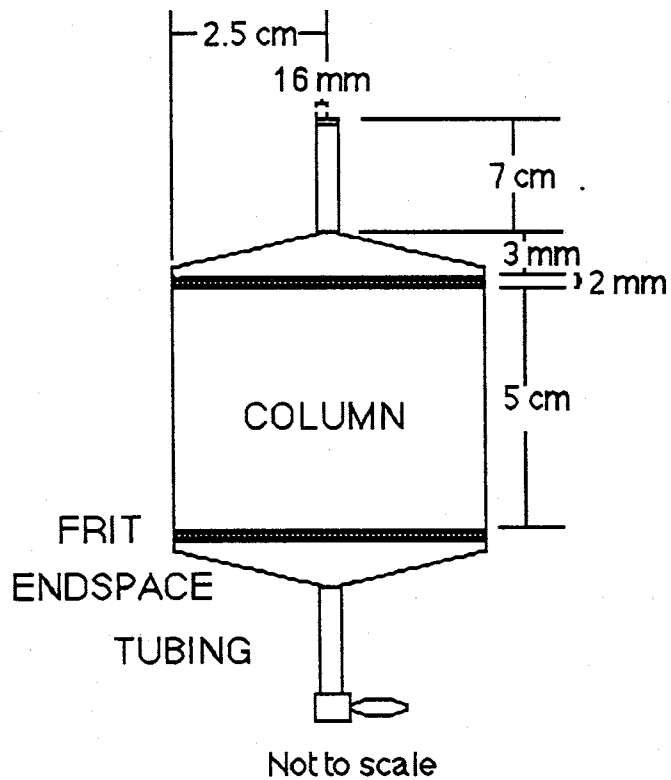
I deaired a water by attaching the solution to a vacuum, then slowly pumped the water through the column. The wet mass of the column was subtracted from the dry mass to determine the volume of water in the column and in the apparatus, then I subtracted the volume of water in the column from the total volume:

|                                   |          |
|-----------------------------------|----------|
| Mass of dry column:               | 429.9 g  |
| Mass of column and water:         | 539.0 g  |
| Volume of water:                  | 110.0 mL |
| Mass of water in column           |          |
| $(\pi \times 2.5^2 \times 5)$ mL: | 98.2 mL  |
| Mass of water in apparatus:       | 11.8 mL  |

Based on the following calculations, a dead space of 11.8 mL is reasonable (note that various parts of the apparatus including the tubing, frit, and endspace are shown in the figure on the next page:

|   |           |
|---|-----------|
| Volume of water in tubing = $2 \times \pi r^2$                      | = 1.1 mL  |
| Volume of water in endplates = $2 \times (\pi r^2 h + \pi r^2 h/3)$ | = 6.5 mL  |
| Volume of water in frits = $2 \times n \times \pi r^2$              | = 3.2 mL  |
| (n = frit porosity)   |           |
| Total   | = 10.8 mL |

**SECTION D3**  
**COLUMN APPARATUS VOLUME**



Column apparatus showing the deadspace.

**SECTION D4**  
**COLUMN PORE VOLUMES, BULK DENSITY**

Dates: 7/7/92 to 9/11/92

|   | Column<br>1 | Column<br>2 | Column<br>3 | Column<br>4 | average | standard<br>deviation |
|---|-------------|-------------|-------------|-------------|---------|-----------------------|
| 1 Mass of tuff (g):                               | 137.7       | 136.3       | 136.9       | 134.95      | 136.5   | 1.2                   |
| 2 Mass of water in the column<br>+ apparatus (g): | 51.5        | 54.4        | 52.9        | 48.2        | 51.8    | 2.6                   |
| 3 Pore Volumes (mL)<br>(subtract 11.8 from row 2) | 39.7        | 42.6        | 41.1        | 36.4        | 40.0    | 2.6                   |

Ave. porosity = average PV/column volume: 0.41

Ave. bulk density = ave. tuff mass/column mass 1.39 g/mL



**SECTION D5  
NI INFLUENT SOLUTION LIQUID SCINTILLATION COUNTS**

Dates: 7/7/92 to 7/25/92

Summary statistics

Universol Cocktale:

Average influent solution CPM/mL: 13053.2  
 Standard deviation of influent solution CPM/mL: 704  
 Average background CPM/mL: 37.7  
 Standard deviation of background CPM/mL: 4.2

Scintiverse Cocktale:

Average influent solution CPM/mL: 13133.9  
 Standard deviation of influent solution CPM/mL: 610

Using Universol Cocktale:

|                   | first   | second  | third   | fourth  | fifth    | sixth      |
|-------------------|---------|---------|---------|---------|----------|------------|
| Date of influent  |         |         |         |         |          | 7/27-Co1&2 |
| soln. connection: | 7/7/92  | 7/12/92 | 7/15/92 | 7/23/92 | 7/25/92  | 7/29-Co3&4 |
| Col 1 (before)    | 13682.2 | 10840.0 | 13427.5 | 13337.8 |          | 12504.6    |
| Col 1 (after)     | Too low | 13471.8 | 13054.3 |         |          |            |
| Col 2 (before)    | 12036.1 | 12939.0 | 13242.8 | 12730.5 |          | 14918.9    |
| Col 2 (after)     | 13314.8 | 13726.9 | 13321.7 |         |          |            |
| Col 3 (before)    | 13187.7 | 13089.3 | 13688.4 | 13174.9 |          | 13568.8    |
| Col 3 (after)     | 11364.5 | 12947.0 | 11856.1 |         | 13549.00 |            |
| Col 4 (before)    | 12510.7 | 13093.5 | 13300.7 | 13260.2 |          | 14313.8    |
| Col 4 (after)     | 12610.7 | 13138.7 | 13210.5 |         | 13586.40 |            |

**SECTION D5  
NI INFLUENT SOLUTION LIQUID SCINTILLATION COUNTS**

Dates: 7/7/92 to 7/25/92

Using Scintiverse Cocktale:

|                  | 4th     | 5th*    | 6th         | 7th     | 8th      |
|------------------|---------|---------|-------------|---------|----------|
| Date of infl     |         |         | 7/27-Co1&2  |         |          |
| soln connection: | 7/23/92 | 7/25/92 | 7/29-Co 3&4 | 7/31/92 | 8/2/92   |
| Col 1 (before)   |         | 11627.9 |             | 14490.9 | too high |
| Col 1 (after)    | 13013.0 | 12716.5 | 13037.7     | 13704.0 | 14524.30 |
| Col 2 (before)   |         | 11292.9 |             | 13530.0 | too high |
| Col 2 (after)    | 13139.8 | 12471.9 | 13439.7     | 13240.3 |          |
| Col 3 (before)   |         | 12520.6 |             | 13683.9 | too high |
| Col 3 (after)    | 13055.7 | 13400.5 | 14086.6     | 13542.6 | 14745.80 |
| Col 4 (before)   |         | 12765.0 |             | 13498.5 | too high |
| Col 4 (after)    | 12875.0 | 13231.6 | 14176.8     | 12895.5 |          |

|                  | 9th     | 10th    | 11th    | 12th    | 13th     | 14th       |
|------------------|---------|---------|---------|---------|----------|------------|
| Date of infl     |         |         |         |         |          |            |
| soln connection: | 8/6/92  | 8/8/92  | 8/12/92 | 8/14/92 | 8/19/92? | 8/24/1992? |
| Col 1&2 (before) | 13381.2 | 13582.8 | 13224.6 | 13157.0 | 14788.1  | 13678.4    |
| Col 1&2 (after)  | 10039.4 | 13366.7 | 13331.2 | 13566.3 | 13044.1  | 12934.2    |
| Col 3&4 (before) | 13598.2 | 13183.8 | 13415.3 | 13756.4 |          |            |
| Col 3&4 (after)  | 12170.9 | 13590.7 | 13308.0 | 13614.4 |          |            |

|                  | 15th    | 16th    | 17th    | 18th    | 19th    | 20th    |
|------------------|---------|---------|---------|---------|---------|---------|
| Date of infl     |         |         |         |         |         |         |
| soln connection: | 8/28/92 | 9/2/92  | 9/7/92  | 9/12/92 | 9/17/92 | 9/22/92 |
| Col 1&2 (before) | 13120.1 | 13938.3 | 13045.1 | 11924.1 | 13069.1 | 13485.9 |
| Col 1&2 (after)  | 12866.4 | 13391.1 | 12894.4 | 12675.6 | 14093.3 |         |

\* The 5th influent soln contained colloids or suspended particals:  
When mixed, the samples showed a higher count, possibly due to the particals in suspensior  
which could either be molecules containing Nickel or molecules with sorbed Ni.  
This solution was warm when the Ni was mixed in.

**SECTION D6**  
**ATOMIC ADSORPTION ANALYSES ON COLUMN INFLUENT SOLUTIONS**

| Stock | Solution Concentration | ave. | ave. of last 3 (No LSC done) |
|-------|------------------------|------|------------------------------|
| #1    | 9.76                   | 9.42 | 9.31                         |
| #2    | 9.20                   |      |                              |
| #3    | 9.36                   |      |                              |
| #4    | 9.37                   |      |                              |

The following table compares results of LSC analysis verses AA  
if C is calculated from LSC using C = 9.31 when CPM/mL is 13100 CF

| Sample          | CPM     | C (mg/L)<br>(from CPM) | C (mg/L)<br>AA | difference |
|-----------------|---------|------------------------|----------------|------------|
| 1st, 7/7 Col1   | 13682.2 | 9.72                   | 11.05          | -1.3262    |
| 1st, 7/12 Col1  | 8321.5  | 5.91                   | 5.41           | 0.5040     |
| 3rd 7/23 Col 1  | 13054.3 | 9.28                   | 8.04           | 1.2375     |
| 4th 7/23 Col4   | 13260.2 | 9.42                   | 8.66           | 0.7639     |
| 6th 7/31 Col3   | 14086.6 | 10.01                  | 9.12           | 0.8912     |
| 8th 8/2 Col 1   | 20986.0 | 14.91                  | 14.57          | 0.3445     |
| 8th 8/6 Col 1&2 | 14524.3 | 10.32                  | 9.45           | 0.8722     |
| 6th,7/27,col1   | 12504.6 | 8.89                   | 8.72           | 0.1669     |
| 6th,7/29,Col3   | 13568.8 | 9.64                   | 10.68          | -1.0368    |

**SECTION D7  
BROMIDE EFFLUENT CONCENTRATIONS**

Experiment Dates: 7/31/92 to 8/2/92

BR DATA, Analyzed using the HPLC  
HPLC Br standard concentration = 20 mg/L

| Solution Type                | HPLC<br>sample<br>reading | HPLC<br>standard<br>reading | Sample<br>Conc.<br>(mg/L) |
|------------------------------|---------------------------|-----------------------------|---------------------------|
| Column 1 effluent before Br  | 0                         | 129072                      | 0.00                      |
| Column 3 effluent before Br  | 325                       | 144692                      | 0.04                      |
| Column 1&2 influent solutior | 77976                     | 184104                      | 8.47                      |
| Column 1&2 influent solutior | 78472                     | 184104                      | 8.52                      |
| Column 3&4 influent solutior | 54091                     | 144692                      | 7.48                      |
| Column 3&4 influent solutior | 53715                     | 144692                      | 7.42                      |

Column 1

| time<br>(hr) | HPLC<br>sample<br>reading | HPLC<br>standard<br>reading | Sample<br>Conc.<br>(mg/L) | Relative<br>Conc.<br>C/Co | Pore<br>Volumes | Pore Vol. -<br>Dead Volume | Calc.<br>time<br>(d) |
|--------------|---------------------------|-----------------------------|---------------------------|---------------------------|-----------------|----------------------------|----------------------|
| 0.4          | 0                         | 184104                      | 0.00                      | 0.00                      | 0.25            | -0.04                      | 0.00                 |
| 0.6          | 0                         | 184104                      | 0.00                      | 0.00                      | 0.38            | 0.08                       | 0.01                 |
| 0.8          | 10392                     | 184104                      | 1.13                      | 0.13                      | 0.50            | 0.21                       | 0.01                 |
| 1.0          | 13653                     | 184104                      | 1.48                      | 0.17                      | 0.63            | 0.34                       | 0.02                 |
| 1.2          | 17109                     | 184104                      | 1.86                      | 0.22                      | 0.76            | 0.46                       | 0.03                 |
| 1.4          | 21555                     | 184104                      | 2.34                      | 0.28                      | 0.88            | 0.59                       | 0.04                 |
| 1.8          | 31709                     | 183384                      | 3.46                      | 0.41                      | 1.14            | 0.84                       | 0.05                 |
| 2.2          | 43933                     | 183384                      | 4.79                      | 0.56                      | 1.39            | 1.09                       | 0.07                 |
| 2.6          | 55421                     | 183384                      | 6.04                      | 0.71                      | 1.64            | 1.34                       | 0.09                 |
| 3.0          | 66661                     | 183384                      | 7.27                      | 0.86                      | 1.89            | 1.60                       | 0.10                 |
| 48.0         | 79421                     | 183384                      | 8.66                      | 1.02                      | 30.95           | 30.66                      | 2.00                 |
| 48.4         | 79333                     | 183384                      | 8.65                      | 1.02                      | 31.21           | 30.91                      | 2.01                 |
| 48.8         | 74768                     | 183384                      | 8.15                      | 0.96                      | 31.46           | 31.17                      | 2.03                 |
| 49.2         | 69224                     | 183384                      | 7.55                      | 0.89                      | 31.72           | 31.42                      | 2.05                 |
| 49.6         | 60632                     | 183384                      | 6.61                      | 0.78                      | 31.97           | 31.68                      | 2.06                 |
| 50.0         | 49027                     | 183384                      | 5.35                      | 0.63                      | 32.23           | 31.93                      | 2.08                 |
| 50.4         | 35299                     | 184323                      | 3.83                      | 0.45                      | 32.49           | 32.19                      | 2.10                 |
| 50.8         | 20456                     | 184323                      | 2.22                      | 0.26                      | 32.74           | 32.45                      | 2.11                 |
| 51.2         | 4304                      | 184323                      | 0.47                      | 0.05                      | 33.00           | 32.70                      | 2.13                 |
| 51.6         | 1595                      | 144692                      | 0.22                      | 0.03                      | 33.25           | 32.96                      | 2.15                 |
| 52.0         | 0                         | 144692                      | 0.00                      | 0.00                      | 33.51           | 33.21                      | 2.16                 |
| 52.4         | 789                       | 144692                      | 0.11                      | 0.01                      | 33.76           | 33.47                      | 2.18                 |
| 52.8         | 931                       | 144692                      | 0.13                      | 0.02                      | 34.02           | 33.72                      | 2.20                 |

**SECTION D7  
BROMIDE EFFLUENT CONCENTRATIONS**

Experiment Dates: 7/31/92 to 8/2/92

BR DATA, Analyzed using the HPLC  
HPLC Br standard concentration = 20 mg/L

Column 2

| HPLC<br>time<br>(hr) | HPLC<br>sample<br>reading | HPLC<br>standard<br>reading | Sample<br>Conc.<br>(mg/L) | Relative<br>Conc.<br>C/Co | Pore<br>Volumes | Pore Vol. -<br>Dead Volume | Calc.<br>time<br>(d) |
|----------------------|---------------------------|-----------------------------|---------------------------|---------------------------|-----------------|----------------------------|----------------------|
| 0.2                  | 0                         | 125003                      | 0.00                      | 0.00                      | 0.12            | -0.17                      | -0.01                |
| 0.6                  | 2616                      | 125003                      | 0.42                      | 0.05                      | 0.37            | 0.08                       | 0.01                 |
| 1.0                  | 10525                     | 125003                      | 1.68                      | 0.20                      | 0.62            | 0.33                       | 0.02                 |
| 1.4                  | 17544                     | 125003                      | 2.81                      | 0.33                      | 0.87            | 0.58                       | 0.04                 |
| 1.8                  | 23051                     | 125003                      | 3.69                      | 0.43                      | 1.12            | 0.83                       | 0.06                 |
| 2.2                  | 28709                     | 125003                      | 4.59                      | 0.54                      | 1.37            | 1.08                       | 0.07                 |
| 2.6                  | 33691                     | 125003                      | 5.39                      | 0.63                      | 1.62            | 1.33                       | 0.09                 |
| 3.0                  | 38360                     | 125003                      | 6.14                      | 0.72                      | 1.87            | 1.57                       | 0.11                 |
| 48.2                 | 50472                     | 125003                      | 8.08                      | 0.95                      | 29.70           | 29.41                      | 1.98                 |
| 48.6                 | 50056                     | 125003                      | 8.01                      | 0.94                      | 29.95           | 29.65                      | 1.99                 |
| 49.0                 | 42152                     | 123808                      | 6.81                      | 0.80                      | 30.20           | 29.90                      | 2.01                 |
| 49.4                 | 35315                     | 123808                      | 5.70                      | 0.67                      | 30.44           | 30.15                      | 2.03                 |
| 49.8                 | 29221                     | 123808                      | 4.72                      | 0.56                      | 30.69           | 30.39                      | 2.04                 |
| 50.2                 | 23528                     | 123808                      | 3.80                      | 0.45                      | 30.93           | 30.64                      | 2.06                 |
| 50.6                 | 18401                     | 123808                      | 2.97                      | 0.35                      | 31.18           | 30.89                      | 2.08                 |
| 51.0                 | 13571                     | 123808                      | 2.19                      | 0.26                      | 31.43           | 31.13                      | 2.09                 |
| 51.4                 | 9672                      | 123808                      | 1.56                      | 0.18                      | 31.67           | 31.38                      | 2.11                 |
| 51.8                 | 6896                      | 123808                      | 1.11                      | 0.13                      | 31.92           | 31.62                      | 2.13                 |
| 52.2                 | 4728                      | 123808                      | 0.76                      | 0.09                      | 32.17           | 31.87                      | 2.14                 |
| 52.6                 | 2592                      | 123808                      | 0.42                      | 0.05                      | 32.41           | 32.12                      | 2.16                 |
| 53.0                 | 2241                      | 123787                      | 0.36                      | 0.04                      | 32.66           | 32.36                      | 2.17                 |

**SECTION D7  
BROMIDE EFFLUENT CONCENTRATIONS**

Experiment Dates: 7/31/92 to 8/2/92

BR DATA, Analyzed using the HPLC  
HPLC Br standard concentration = 20 mg/L

Column 3

| time<br>(hr) | HPLC<br>sample<br>reading | HPLC<br>standard<br>reading | Sample<br>Conc.<br>(mg/L) | Relative<br>Conc.<br>C/Co | Pore<br>Volumes | Pore Vol. -<br>Dead Volume | Calc.<br>time<br>(d) |
|--------------|---------------------------|-----------------------------|---------------------------|---------------------------|-----------------|----------------------------|----------------------|
| 0.0          | 0                         | 184323                      | 0.00                      | 0.00                      | 0.00            | -0.30                      | -0.02                |
| 0.2          | 0                         | 185759                      | 0.00                      | 0.00                      | 0.12            | -0.17                      | -0.01                |
| 0.4          | 0                         | 185759                      | 0.00                      | 0.00                      | 0.25            | -0.05                      | 0.00                 |
| 0.6          | 0                         | 185759                      | 0.00                      | 0.00                      | 0.37            | 0.07                       | 0.01                 |
| 0.8          | 0                         | 185759                      | 0.00                      | 0.00                      | 0.49            | 0.20                       | 0.01                 |
| 1.0          | 0                         | 144692                      | 0.00                      | 0.00                      | 0.62            | 0.32                       | 0.02                 |
| 1.4          | 1333                      | 144692                      | 0.18                      | 0.02                      | 0.86            | 0.57                       | 0.04                 |
| 1.8          | 24363                     | 185759                      | 2.62                      | 0.35                      | 1.11            | 0.81                       | 0.05                 |
| 2.0          | 37440                     | 185759                      | 4.03                      | 0.54                      | 1.23            | 0.94                       | 0.06                 |
| 2.2          | 34245                     | 144692                      | 4.73                      | 0.64                      | 1.35            | 1.06                       | 0.07                 |
| 2.4          | 36121                     | 125184                      | 5.77                      | 0.77                      | 1.48            | 1.18                       | 0.08                 |
| 2.6          | 39643                     | 125184                      | 6.33                      | 0.85                      | 1.60            | 1.31                       | 0.09                 |
| 2.8          | 41909                     | 125184                      | 6.70                      | 0.90                      | 1.72            | 1.43                       | 0.10                 |
| 3.0          | 43752                     | 125184                      | 6.99                      | 0.94                      | 1.85            | 1.55                       | 0.10                 |
| 49.2         | 47605                     | 125184                      | 7.61                      | 1.02                      | 30.30           | 30.00                      | 2.03                 |
| 49.4         | 47393                     | 125184                      | 7.57                      | 1.02                      | 30.42           | 30.12                      | 2.03                 |
| 49.8         | 42805                     | 125184                      | 6.84                      | 0.92                      | 30.67           | 30.37                      | 2.05                 |
| 50.0         | 34593                     | 125184                      | 5.53                      | 0.74                      | 30.79           | 30.49                      | 2.06                 |
| 50.2         | 25485                     | 125184                      | 4.07                      | 0.55                      | 30.91           | 30.62                      | 2.07                 |
| 50.6         | 12688                     | 125184                      | 2.03                      | 0.27                      | 31.16           | 30.86                      | 2.08                 |
| 51.0         | 6373                      | 125184                      | 1.02                      | 0.14                      | 31.40           | 31.11                      | 2.10                 |
| 51.4         | 2645                      | 125184                      | 0.42                      | 0.06                      | 31.65           | 31.36                      | 2.12                 |
| 51.8         | 1395                      | 125184                      | 0.22                      | 0.03                      | 31.90           | 31.60                      | 2.13                 |
| 52.0         | 1141                      | 125184                      | 0.18                      | 0.02                      | 32.02           | 31.72                      | 2.14                 |
| 52.2         | 1128                      | 125184                      | 0.18                      | 0.02                      | 32.14           | 31.85                      | 2.15                 |
| 52.4         | 16                        | 125184                      | 0.00                      | 0.00                      | 32.27           | 31.97                      | 2.16                 |
| 52.6         | 0                         | 125184                      | 0.00                      | 0.00                      | 32.39           | 32.09                      | 2.17                 |
| 52.8         | 0                         | 125184                      | 0.00                      | 0.00                      | 32.51           | 32.22                      | 2.17                 |

**SECTION D7  
BROMIDE EFFLUENT CONCENTRATIONS**

Experiment Dates: 7/31/92 to 8/2/92

BR DATA, Analyzed using the HPLC  
HPLC Br standard concentration = 20 mg/L

Column 4

| HPLC<br>time<br>(hr) | HPLC<br>sample<br>reading | HPLC<br>standard<br>reading | Sample<br>Conc.<br>(mg/L) | Relative<br>Conc.<br>C/Co | Pore<br>Volumes | Pore Vol. -<br>Dead Volume | Calc.<br>time<br>(d) |
|----------------------|---------------------------|-----------------------------|---------------------------|---------------------------|-----------------|----------------------------|----------------------|
| 1.0                  | 0                         | 123787                      | 0.00                      | 0.00                      | 0.61            | 0.31                       | 0.02                 |
| 1.4                  | 867                       | 123787                      | 0.14                      | 0.02                      | 0.85            | 0.56                       | 0.04                 |
| 1.8                  | 17245                     | 123787                      | 2.79                      | 0.37                      | 1.09            | 0.80                       | 0.05                 |
| 2.0                  | 29185                     | 123787                      | 4.72                      | 0.63                      | 1.22            | 0.92                       | 0.06                 |
| 2.2                  | 35707                     | 123787                      | 5.77                      | 0.77                      | 1.34            | 1.04                       | 0.07                 |
| 2.4                  | 39768                     | 123787                      | 6.43                      | 0.86                      | 1.46            | 1.16                       | 0.08                 |
| 2.6                  | 41645                     | 123787                      | 6.73                      | 0.90                      | 1.58            | 1.29                       | 0.09                 |
| 2.8                  | 43443                     | 123787                      | 7.02                      | 0.94                      | 1.70            | 1.41                       | 0.09                 |
| 3.0                  | 44333                     | 123787                      | 7.16                      | 0.96                      | 1.82            | 1.53                       | 0.10                 |
| 48.8                 | 48736                     | 128037                      | 7.61                      | 1.02                      | 30.03           | 29.74                      | 1.99                 |
| 49.0                 | 49168                     | 128037                      | 7.68                      | 1.03                      | 30.16           | 29.86                      | 2.00                 |
| 49.2                 | 49647                     | 128037                      | 7.76                      | 1.04                      | 30.28           | 29.99                      | 2.01                 |
| 49.8                 | 46088                     | 128037                      | 7.20                      | 0.97                      | 30.66           | 30.36                      | 2.03                 |
| 50.0                 | 37584                     | 128037                      | 5.87                      | 0.79                      | 30.78           | 30.49                      | 2.04                 |
| 50.2                 | 25267                     | 128037                      | 3.95                      | 0.53                      | 30.91           | 30.61                      | 2.05                 |
| 50.4                 | 49403                     | 128037                      | 7.72                      | 1.04                      | 31.03           | 30.73                      |                      |
| 50.6                 | 8315                      | 128037                      | 1.30                      | 0.17                      | 31.15           | 30.86                      | 2.06                 |
| 51.0                 | 3451                      | 128037                      | 0.54                      | 0.07                      | 31.40           | 31.11                      | 2.08                 |
| 51.4                 | 1837                      | 128037                      | 0.29                      | 0.04                      | 31.65           | 31.36                      | 2.10                 |
| 51.8                 | 656                       | 128445                      | 0.10                      | 0.01                      | 31.90           | 31.61                      | 2.11                 |
| 52.0                 | 536                       | 128445                      | 0.08                      | 0.01                      | 32.03           | 31.73                      | 2.12                 |
| 52.2                 | 0                         | 128445                      | 0.00                      | 0.00                      | 32.15           | 31.86                      | 2.13                 |

**SECTION D8  
NICKEL EFFLUENT CONCENTRATIONS**

Dates: 7/7/92 to 9/25/92

Column 1

| Time<br>(d) | Sample<br>LSC<br>(CPM/mL) | Sample -<br>Background<br>(CPM/mL) | Pore<br>Volumes | Pore Vol. -<br>Dead Vol. | Conc. | Relative<br>Conc. |
|-------------|---------------------------|------------------------------------|-----------------|--------------------------|-------|-------------------|
| 0.00        | 35.8                      | -1.9                               | 0.06            | -0.23                    | 0.00  | 0.00              |
| 1.00        | 36.5                      | -1.2                               | 15.14           | 14.84                    | 0.00  | 0.00              |
| 2.00        | 43.4                      | 5.7                                | 30.28           | 29.98                    | 0.00  | 0.00              |
| 3.00        | 33.4                      | -4.3                               | 45.42           | 45.12                    | 0.00  | 0.00              |
| 4.00        | 47.6                      | 9.9                                | 54.88           | 54.58                    | 0.01  | 0.00              |
| 4.50        | 182.4                     | 144.7                              | 58.66           | 58.37                    | 0.10  | 0.01              |
| 5.00        | 1206.7                    | 1169.0                             | 62.45           | 62.15                    | 0.83  | 0.09              |
| 5.50        | 775.3                     | 737.6                              | 66.23           | 65.94                    | 0.53  | 0.06              |
| 6.00        | 1212.0                    | 1174.3                             | 70.02           | 69.72                    | 0.84  | 0.09              |
| 7.00        | 1523.9                    | 1486.2                             | 77.59           | 77.29                    | 1.06  | 0.11              |
| 7.93        | 1913.5                    | 1875.8                             | 84.65           | 84.36                    | 1.34  | 0.14              |
| 8.93        | 3556.0                    | 3518.3                             | 92.22           | 91.93                    | 2.51  | 0.27              |
| 9.93        | 2924.2                    | 2886.5                             | 99.79           | 99.50                    | 2.06  | 0.22              |
| 10.93       | 3790.6                    | 3752.9                             | 107.36          | 107.06                   | 2.68  | 0.29              |
| 11.93       | 3288.4                    | 3250.7                             | 114.93          | 114.63                   | 2.32  | 0.25              |
| 12.93       | 3130.8                    | 3093.1                             | 122.50          | 122.20                   | 2.21  | 0.24              |
| 13.93       | 3576.2                    | 3538.5                             | 130.07          | 129.77                   | 2.52  | 0.27              |
| 14.93       | 3342.6                    | 3304.9                             | 137.64          | 137.34                   | 2.36  | 0.25              |
| 15.96       | 5385.0                    | 5347.3                             | 151.61          | 151.31                   | 3.81  | 0.41              |
| 16.20       | 5201.6                    | 5163.9                             | 155.16          | 154.86                   | 3.68  | 0.40              |
| 17.00       | 4963.0                    | 4925.3                             | 166.98          | 166.68                   | 3.51  | 0.38              |
| 17.26       | 4821.4                    | 4783.7                             | 170.82          | 170.53                   | 3.41  | 0.37              |
| 18.10       | 4846.8                    | 4809.1                             | 183.24          | 182.94                   | 3.43  | 0.37              |
| 19.30       | 4097.2                    | 4059.5                             | 200.97          | 200.67                   | 2.90  | 0.31              |
| 19.96       | 5415.6                    | 5377.9                             | 210.72          | 210.43                   | 3.84  | 0.41              |
| 20.96       | 9070.2                    | 9032.5                             | 225.50          | 225.21                   | 6.44  | 0.69              |
| 21.96       | 7328.0                    | 7290.3                             | 240.28          | 239.98                   | 5.20  | 0.56              |
| 22.96       | 7896.3                    | 7858.6                             | 255.06          | 254.76                   | 5.57  | 0.60              |
| 23.98       | 8044.0                    | 8006.3                             | 270.13          | 269.84                   | 5.68  | 0.61              |
| 24.96       | 8267.8                    | 8230.1                             | 284.62          | 284.32                   | 5.83  | 0.63              |
| 25.96       | 8646.6                    | 8608.9                             | 299.39          | 299.10                   | 6.10  | 0.66              |
| 27.96       | 9137.3                    | 9099.6                             | 328.95          | 328.66                   | 6.45  | 0.69              |
| 28.94       | 9002.8                    | 8965.1                             | 343.43          | 343.14                   | 6.35  | 0.68              |
| 29.96       | 10210.0                   | 10172.3                            | 358.51          | 358.21                   | 7.21  | 0.77              |
| 30.96       | 10266.2                   | 10228.5                            | 373.29          | 372.99                   | 7.25  | 0.78              |
| 31.92       | 10196.8                   | 10159.1                            | 387.47          | 387.18                   | 7.20  | 0.77              |
| 33.09       | 8931.5                    | 8893.8                             | 404.76          | 404.47                   | 6.30  | 0.68              |
| 33.94       | 8978.4                    | 8940.7                             | 417.33          | 417.03                   | 6.34  | 0.68              |
| 34.93       | 9903.6                    | 9865.9                             | 431.96          | 431.66                   | 6.99  | 0.75              |
| 35.96       | 9756.7                    | 9719.0                             | 446.81          | 446.51                   | 6.89  | 0.74              |
| 36.96       | 10572.7                   | 10535.0                            | 461.23          | 460.93                   | 7.47  | 0.80              |
| 37.96       | 10311.2                   | 10273.5                            | 475.64          | 475.35                   | 7.28  | 0.78              |
| 39.06       | 10205.6                   | 10167.9                            | 491.50          | 491.21                   | 7.21  | 0.77              |



**SECTION D8  
NICKEL EFFLUENT CONCENTRATIONS**

Dates: 7/7/92 to 9/25/92

Column 1

| Time<br>(d) | Sample<br>LSC<br>(CPM/mL) | Sample -<br>Background<br>(CPM/mL) | Pore<br>Volumes | Pore Vol. -<br>Dead Vol. | Conc. | Relative<br>Conc. |
|-------------|---------------------------|------------------------------------|-----------------|--------------------------|-------|-------------------|
| 39.97       | 11079.7                   | 11042.0                            | 504.62          | 504.33                   | 7.83  | 0.84              |
| 40.95       | 11492.3                   | 11454.6                            | 518.75          | 518.46                   | 8.12  | 0.87              |
| 41.96       | 11379.2                   | 11341.5                            | 533.32          | 533.02                   | 8.04  | 0.86              |
| 42.96       | 11634.0                   | 11596.3                            | 547.73          | 547.44                   | 8.22  | 0.88              |
| 44.02       | 12143.2                   | 12105.5                            | 562.63          | 562.34                   | 8.58  | 0.92              |
| 44.94       | 12240.0                   | 12202.3                            | 575.57          | 575.27                   | 8.65  | 0.93              |
| 45.96       | 12590.2                   | 12552.5                            | 589.24          | 588.95                   | 8.90  | 0.96              |
| 47.00       | 12176.2                   | 12138.5                            | 602.36          | 602.07                   | 8.60  | 0.92              |
| 47.93       | 12024.6                   | 11986.9                            | 613.76          | 613.47                   | 8.50  | 0.91              |
| 48.96       | 12226.2                   | 12188.5                            | 627.87          | 627.57                   | 8.64  | 0.93              |
| 49.95       | 11622.5                   | 11584.8                            | 641.43          | 641.13                   | 8.21  | 0.88              |
| 50.96       | 11358.3                   | 11320.6                            | 655.26          | 654.97                   | 8.02  | 0.86              |
| 51.96       | 11597.3                   | 11559.6                            | 668.96          | 668.66                   | 8.19  | 0.88              |
| 52.92       | 11124.2                   | 11086.5                            | 682.11          | 681.81                   | 7.86  | 0.84              |
| 54.08       | 10772.1                   | 10734.4                            | 698.00          | 697.70                   | 7.61  | 0.82              |
| 54.96       | 11374.9                   | 11337.2                            | 710.05          | 709.76                   | 8.04  | 0.86              |
| 55.97       | 11311.3                   | 11273.6                            | 723.16          | 722.86                   | 7.99  | 0.86              |
| 56.93       | 11518.5                   | 11480.8                            | 736.31          | 736.01                   | 8.14  | 0.87              |
| 57.97       | 11678.3                   | 11640.6                            | 750.93          | 750.63                   | 8.25  | 0.89              |
| 58.94       | 11962.7                   | 11925.0                            | 762.46          | 762.17                   | 8.45  | 0.91              |
| 59.95       | 11337.6                   | 11299.9                            | 774.84          | 774.55                   | 8.01  | 0.86              |
| 60.95       | 11327.0                   | 11289.3                            | 786.74          | 786.44                   | 8.00  | 0.86              |
| 61.97       | 11120.4                   | 11082.7                            | 798.50          | 798.21                   | 7.86  | 0.84              |
| 62.96       | 9750.0                    | 9712.3                             | 810.64          | 810.34                   | 6.88  | 0.74              |
| 63.95       | 11056.8                   | 11019.1                            | 823.12          | 822.83                   | 7.81  | 0.84              |
| 64.96       | 11068.0                   | 11030.3                            | 835.50          | 835.21                   | 7.82  | 0.84              |
| 65.95       | 11214.9                   | 11177.2                            | 847.99          | 847.70                   | 7.92  | 0.85              |
| 66.95       | 11333.1                   | 11295.4                            |                 |                          | 8.01  | 0.86              |
| 68.00       | 11430.7                   | 11393.0                            |                 |                          | 8.08  | 0.87              |
| 69.00       | 11279.0                   | 11241.3                            |                 |                          | 7.97  | 0.86              |
| 70.00       | 11232.8                   | 11195.1                            |                 |                          | 7.94  | 0.85              |
| 72.00       | 11315.2                   | 11277.5                            |                 |                          | 7.99  | 0.86              |
| 72.90       | 11911.8                   | 11874.1                            |                 |                          | 8.42  | 0.90              |
| 74.00       | 12230.3                   | 12192.6                            |                 |                          | 8.64  | 0.93              |
| 75.00       | 12528.4                   | 12490.7                            |                 |                          | 8.85  | 0.95              |
| 75.90       | 12793.3                   | 12755.6                            |                 |                          | 9.04  | 0.97              |
| 76.90       | 12341.6                   | 12303.9                            |                 |                          | 8.72  | 0.94              |

**SECTION D8  
NICKEL EFFLUENT CONCENTRATIONS**

Dates: 7/7/92 to 9/25/92

Column 2

| Time<br>(d) | Sample<br>LSC<br>(CPM/mL) | Sample -<br>Background<br>(CPM/mL) | Pore<br>Volumes | Pore Vol. -<br>Dead Vol. | Conc. | Relative<br>Conc. |
|-------------|---------------------------|------------------------------------|-----------------|--------------------------|-------|-------------------|
| 0.00        | 32.4                      | -5.3                               | 0.06            | -0.23                    | 0.00  | 0.00              |
| 1.00        | 35.1                      | -2.6                               | 15.14           | 14.84                    | 0.00  | 0.00              |
| 2.00        | 43.4                      | 5.7                                | 30.28           | 29.98                    | 0.00  | 0.00              |
| 3.00        | 57.8                      | 20.1                               | 45.42           | 45.12                    | 0.01  | 0.00              |
| 4.00        | 212.3                     | 174.6                              | 54.88           | 54.58                    | 0.12  | 0.01              |
| 4.50        | 348.7                     | 311.0                              | 58.66           | 58.37                    | 0.22  | 0.02              |
| 5.00        | 753.4                     | 715.7                              | 62.45           | 62.15                    | 0.51  | 0.05              |
| 5.50        | 484.3                     | 446.6                              | 66.23           | 65.94                    | 0.32  | 0.03              |
| 6.00        | 735.2                     | 697.5                              | 70.02           | 69.72                    | 0.50  | 0.05              |
| 7.00        | 1191.8                    | 1154.1                             | 77.59           | 77.29                    | 0.82  | 0.09              |
| 7.93        | 1414.4                    | 1376.7                             | 84.65           | 84.36                    | 0.98  | 0.11              |
| 8.93        | 3386.8                    | 3349.1                             | 92.22           | 91.93                    | 2.39  | 0.26              |
| 9.93        | 2245.7                    | 2208.0                             | 99.79           | 99.50                    | 1.57  | 0.17              |
| 10.93       | 3103.4                    | 3065.7                             | 107.36          | 107.06                   | 2.19  | 0.23              |
| 11.93       | 2577.5                    | 2539.8                             | 114.93          | 114.63                   | 1.81  | 0.19              |
| 12.93       | 2512.5                    | 2474.8                             | 122.50          | 122.20                   | 1.77  | 0.19              |
| 13.93       | 3131.1                    | 3093.4                             | 130.07          | 129.77                   | 2.21  | 0.24              |
| 14.93       | 3039.2                    | 3001.5                             | 137.64          | 137.34                   | 2.14  | 0.23              |
| 15.96       | 5482.0                    | 5444.3                             | 145.41          | 145.11                   | 3.88  | 0.42              |
| 16.20       | 5731.4                    | 5693.7                             | 155.16          | 154.86                   | 4.06  | 0.44              |
| 17.00       | 5732.2                    | 5694.5                             | 166.98          | 166.68                   | 4.06  | 0.44              |
| 17.26       | 5599.8                    | 5562.1                             | 170.82          | 170.53                   | 3.97  | 0.43              |
| 18.10       | 5269.1                    | 5231.4                             | 183.24          | 182.94                   | 3.73  | 0.40              |
| 19.30       | 4777.5                    | 4739.8                             | 200.97          | 200.67                   | 3.38  | 0.36              |
| 19.96       | 5577.1                    | 5539.4                             | 210.72          | 210.43                   | 3.95  | 0.42              |
| 20.96       | 8060.3                    | 8022.6                             | 225.50          | 225.21                   | 5.72  | 0.61              |
| 21.96       | 6868.2                    | 6830.5                             | 240.28          | 239.98                   | 4.87  | 0.52              |
| 22.96       | 7529.5                    | 7491.8                             | 255.06          | 254.76                   | 5.31  | 0.57              |
| 23.98       | 7728.8                    | 7691.1                             | 270.13          | 269.84                   | 5.45  | 0.59              |
| 24.96       | 8051.6                    | 8013.9                             | 284.62          | 284.32                   | 5.68  | 0.61              |
| 25.96       | 8312.7                    | 8275.0                             | 299.39          | 299.10                   | 5.87  | 0.63              |
| 27.96       | 8870.7                    | 8833.0                             | 328.95          | 328.66                   | 6.26  | 0.67              |
| 28.94       | 8869.4                    | 8831.7                             | 343.43          | 343.14                   | 6.26  | 0.67              |
| 29.96       | 9888.4                    | 9850.7                             | 358.51          | 358.21                   | 6.98  | 0.75              |
| 30.96       | 10140.6                   | 10102.9                            | 373.29          | 372.99                   | 7.16  | 0.77              |
| 31.92       | 10317.3                   | 10279.6                            | 387.47          | 387.18                   | 7.29  | 0.78              |
| 33.09       | 9071.7                    | 9034.0                             | 404.76          | 404.47                   | 6.40  | 0.69              |
| 33.94       | 9037.6                    | 8999.9                             | 417.33          | 417.03                   | 6.38  | 0.69              |
| 34.93       | 9954.1                    | 9916.4                             | 431.96          | 431.66                   | 7.03  | 0.76              |
| 35.96       | 9813.5                    | 9775.8                             | 446.44          | 446.14                   | 6.93  | 0.74              |
| 36.96       | 10793.9                   | 10756.2                            | 460.49          | 460.20                   | 7.62  | 0.82              |
| 37.96       | 10714.0                   | 10676.3                            | 474.55          | 474.26                   | 7.57  | 0.81              |

**SECTION D8  
NICKEL EFFLUENT CONCENTRATIONS**

Dates: 7/7/92 to 9/25/92

Column 2

| Time<br>(d) | Sample<br>LSC<br>(CPM/mL) | Sample -<br>Background<br>(CPM/mL) | Pore<br>Volumes | Pore Vol. -<br>Dead Vol. | Conc. | Relative<br>Conc. |
|-------------|---------------------------|------------------------------------|-----------------|--------------------------|-------|-------------------|
| 39.06       | 10351.8                   | 10314.1                            | 490.01          | 489.72                   | 7.31  | 0.79              |
| 39.97       | 11405.0                   | 11367.3                            | 502.15          | 501.86                   | 8.06  | 0.87              |
| 40.95       | 11550.8                   | 11513.1                            | 515.22          | 514.93                   | 8.16  | 0.88              |
| 41.96       | 11559.5                   | 11521.8                            | 528.69          | 528.40                   | 8.17  | 0.88              |
| 42.96       | 11605.3                   | 11567.6                            | 542.03          | 541.73                   | 8.20  | 0.88              |
| 44.02       | 12311.9                   | 12274.2                            | 556.93          | 556.63                   | 8.70  | 0.93              |
| 44.94       | 12275.3                   | 12237.6                            | 569.86          | 569.57                   | 8.67  | 0.93              |
| 45.96       | 12776.8                   | 12739.1                            | 583.37          | 583.08                   | 9.03  | 0.97              |
| 47.00       | 12243.0                   | 12205.3                            | 596.12          | 595.82                   | 8.65  | 0.93              |
| 47.93       | 12358.1                   | 12320.4                            | 608.86          | 608.56                   | 8.73  | 0.94              |
| 48.96       | 12199.9                   | 12162.2                            | 623.33          | 623.04                   | 8.62  | 0.93              |
| 49.95       | 11581.1                   | 11543.4                            | 637.61          | 637.31                   | 8.18  | 0.88              |
| 50.96       | 11485.5                   | 11447.8                            | 651.44          | 651.15                   | 8.11  | 0.87              |
| 51.96       | 11660.5                   | 11622.8                            | 665.31          | 665.01                   | 8.24  | 0.88              |
| 52.92       | 11261.6                   | 11223.9                            | 678.80          | 678.51                   | 7.96  | 0.85              |
| 54.08       | 10918.4                   | 10880.7                            | 694.69          | 694.39                   | 7.71  | 0.83              |
| 54.96       | 11433.4                   | 11395.7                            | 706.74          | 706.45                   | 8.08  | 0.87              |
| 55.97       | 11585.6                   | 11547.9                            | 719.85          | 719.55                   | 8.19  | 0.88              |
| 56.93       | 11523.5                   | 11485.8                            | 732.65          | 732.36                   | 8.14  | 0.87              |
| 57.97       | 11784.9                   | 11747.2                            | 747.27          | 746.98                   | 8.33  | 0.89              |
| 58.94       | 12027.2                   | 11989.5                            | 760.21          | 759.91                   | 8.50  | 0.91              |
| 59.95       | 11631.9                   | 11594.2                            | 773.31          | 773.02                   | 8.22  | 0.88              |
| 60.95       | 11565.2                   | 11527.5                            | 786.29          | 786.00                   | 8.17  | 0.88              |
| 61.97       | 11430.0                   | 11392.3                            | 798.79          | 798.50                   | 8.08  | 0.87              |
| 62.96       | 10154.2                   | 10116.5                            | 811.99          | 811.70                   | 7.17  | 0.77              |
| 63.95       | 11329.8                   | 11292.1                            | 825.55          | 825.26                   | 8.00  | 0.86              |
| 64.96       | 11390.3                   | 11352.6                            | 839.39          | 839.09                   | 8.05  | 0.86              |
| 65.95       | 11461.6                   | 11423.9                            | 852.95          | 852.65                   | 8.10  | 0.87              |
| 66.95       | 11442.6                   | 11404.9                            |                 |                          | 8.08  | 0.87              |
| 68.00       | 11452.2                   | 11414.5                            |                 |                          | 8.09  | 0.87              |
| 69.00       | 11511.8                   | 11474.1                            |                 |                          | 8.13  | 0.87              |
| 70.00       | 11437.5                   | 11399.8                            |                 |                          | 8.08  | 0.87              |
| 72.00       | 11500.3                   | 11462.6                            |                 |                          | 8.13  | 0.87              |
| 72.90       | 12414.3                   | 12376.6                            |                 |                          | 8.77  | 0.94              |
| 74.00       | 12135.3                   | 12097.6                            |                 |                          | 8.58  | 0.92              |
| 75.00       | 12609.3                   | 12571.6                            |                 |                          | 8.91  | 0.96              |
| 75.90       | 12704.0                   | 12666.3                            |                 |                          | 8.98  | 0.96              |
| 76.90       | 11241.9                   | 11204.2                            |                 |                          | 7.94  | 0.85              |

**SECTION D8  
NICKEL EFFLUENT CONCENTRATIONS**

Dates: 7/7/92 to 9/25/92

Column 3

| Time<br>(d) | Sample<br>LSC<br>(CPM/mL) | Sample -<br>Background<br>(CPM/mL) | Pore<br>Volumes | Pore Vol. -<br>Dead Vol. | Conc. | Relative<br>Conc. |
|-------------|---------------------------|------------------------------------|-----------------|--------------------------|-------|-------------------|
| 0.00        | 49.0                      | 11.3                               | 0.06            | -0.23                    | 0.01  | 0.00              |
| 1.00        | 42.8                      | 5.1                                | 15.14           | 14.84                    | 0.00  | 0.00              |
| 2.00        | 34.9                      | -2.8                               | 30.28           | 29.98                    | 0.00  | 0.00              |
| 3.00        | 39.9                      | 2.2                                | 45.42           | 45.12                    | 0.00  | 0.00              |
| 4.00        | 43.2                      | 5.5                                | 54.88           | 54.58                    | 0.00  | 0.00              |
| 5.00        | 35.4                      | -2.3                               | 62.45           | 62.15                    | 0.00  | 0.00              |
| 6.00        | 42.1                      | 4.4                                | 66.63           | 66.33                    | 0.00  | 0.00              |
| 7.00        | 35.4                      | -2.3                               | 74.21           | 73.91                    | 0.00  | 0.00              |
| 7.93        | 37.6                      | -0.1                               | 81.27           | 80.98                    | 0.00  | 0.00              |
| 8.93        | 40.7                      | 3.0                                | 88.84           | 88.55                    | 0.00  | 0.00              |
| 9.93        | 43.3                      | 5.6                                | 96.41           | 96.12                    | 0.00  | 0.00              |
| 10.93       | 66.2                      | 28.5                               | 103.98          | 103.68                   | 0.02  | 0.00              |
| 11.93       | 95.9                      | 58.2                               | 111.55          | 111.25                   | 0.04  | 0.00              |
| 12.93       | 110.6                     | 72.9                               | 119.12          | 118.82                   | 0.05  | 0.01              |
| 13.93       | 278.7                     | 241.0                              | 126.69          | 126.39                   | 0.17  | 0.02              |
| 14.93       | 417.8                     | 380.1                              | 134.26          | 133.96                   | 0.27  | 0.03              |
| 15.96       | 2259.1                    | 2221.4                             | 149.43          | 149.14                   | 1.58  | 0.17              |
| 16.20       | 3238.4                    | 3200.7                             | 152.98          | 152.68                   | 2.28  | 0.25              |
| 17.00       | 4381.5                    | 4343.8                             | 164.80          | 164.50                   | 3.10  | 0.33              |
| 17.26       | 4244.1                    | 4206.4                             | 168.64          | 168.35                   | 3.00  | 0.32              |
| 18.10       | 4902.1                    | 4864.4                             | 181.06          | 180.76                   | 3.47  | 0.37              |
| 19.30       | 5351.1                    | 5313.4                             | 198.79          | 198.50                   | 3.79  | 0.41              |
| 19.96       | 7965.1                    | 7927.4                             | 208.54          | 208.25                   | 5.65  | 0.61              |
| 20.96       | 9309.9                    | 9272.2                             | 223.32          | 223.03                   | 6.61  | 0.71              |
| 21.96       | 9898.1                    | 9860.4                             | 238.10          | 237.81                   | 7.03  | 0.76              |
| 22.96       | 10963.5                   | 10925.8                            | 252.88          | 252.58                   | 7.74  | 0.83              |
| 23.98       | 11359.4                   | 11321.7                            | 267.95          | 267.66                   | 8.03  | 0.86              |
| 24.96       | 11122.5                   | 11084.8                            | 282.44          | 282.14                   | 7.86  | 0.84              |
| 25.96       | 11390.7                   | 11353.0                            | 297.22          | 296.92                   | 8.05  | 0.86              |
| 27.96       | 12331.2                   | 12293.5                            | 326.77          | 326.48                   | 8.71  | 0.94              |
| 28.94       | 12307.5                   | 12269.8                            | 341.26          | 340.96                   | 8.70  | 0.93              |
| 29.96       | 13056.0                   | 13018.3                            | 356.33          | 356.03                   | 9.23  | 0.99              |
| 30.96       | 12346.3                   | 12308.6                            | 371.11          | 370.81                   | 8.72  | 0.94              |
| 31.92       | 12503.2                   | 12465.5                            | 385.30          | 385.00                   | 8.84  | 0.95              |
| 33.09       | 11892.8                   | 11855.1                            | 402.59          | 402.29                   | 8.40  | 0.90              |
| 33.94       | 11864.2                   | 11826.5                            | 415.15          | 414.85                   | 8.38  | 0.90              |
| 34.93       | 12040.2                   | 12002.5                            | 429.78          | 429.48                   | 8.51  | 0.91              |
| 35.96       | 12464.1                   | 12426.4                            | 444.63          | 444.33                   | 8.81  | 0.95              |
| 36.96       | 12323.8                   | 12286.1                            | 459.05          | 458.75                   | 8.71  | 0.94              |
| 37.96       | 12438.0                   | 12400.3                            | 473.46          | 473.17                   | 8.79  | 0.94              |
| 39.06       | 12694.3                   | 12656.6                            | 489.32          | 489.03                   | 8.97  | 0.96              |
| 39.97       | 13196.1                   | 13158.4                            | 502.45          | 502.15                   | 9.33  | 1.00              |
| 40.95       | 13208.2                   | 13170.5                            | 516.57          | 516.28                   | 9.34  | 1.00              |
| 41.96       | 13126.6                   | 13088.9                            | 531.14          | 530.84                   | 9.28  | 1.00              |

**SECTION D8  
NICKEL EFFLUENT CONCENTRATIONS**

Dates: 7/7/92 to 9/25/92

Column 4

| Time<br>(d) | Sample<br>LSC<br>(CPM/mL) | Sample -<br>Background<br>(CPM/mL) | Pore<br>Volumes | Pore Vol. -<br>Dead Vol. | Conc. | Relative<br>Conc. |
|-------------|---------------------------|------------------------------------|-----------------|--------------------------|-------|-------------------|
| 0.00        | 36.0                      | -1.7                               | 0.06            | -0.23                    | 0.00  | 0.00              |
| 1.00        | 35.9                      | -1.8                               | 15.14           | 14.84                    | 0.00  | 0.00              |
| 2.00        | 43.1                      | 5.4                                | 30.28           | 29.98                    | 0.00  | 0.00              |
| 3.00        | 38.5                      | 0.8                                | 45.42           | 45.12                    | 0.00  | 0.00              |
| 4.00        | 34.8                      | -2.9                               | 54.88           | 54.58                    | 0.00  | 0.00              |
| 5.00        | 36.4                      | -1.3                               | 62.45           | 62.15                    | 0.00  | 0.00              |
| 6.00        | 32.3                      | -5.4                               | 65.84           | 65.54                    | 0.00  | 0.00              |
| 7.00        | 32.6                      | -5.1                               | 73.41           | 73.11                    | 0.00  | 0.00              |
| 7.93        | 36.9                      | -0.8                               | 80.47           | 80.18                    | 0.00  | 0.00              |
| 8.93        | 40.3                      | 2.6                                | 88.04           | 87.75                    | 0.00  | 0.00              |
| 9.93        | 43.9                      | 6.2                                | 95.61           | 95.32                    | 0.00  | 0.00              |
| 10.93       | 55.9                      | 18.2                               | 103.18          | 102.88                   | 0.01  | 0.00              |
| 11.93       | 67.8                      | 30.1                               | 110.75          | 110.45                   | 0.02  | 0.00              |
| 12.93       | 82.8                      | 45.1                               | 118.32          | 118.02                   | 0.03  | 0.00              |
| 13.93       | 172.1                     | 134.4                              | 125.89          | 125.59                   | 0.10  | 0.01              |
| 14.93       | 298.1                     | 260.4                              | 133.46          | 133.16                   | 0.19  | 0.02              |
| 15.96       | 2290.6                    | 2252.9                             | 148.63          | 148.34                   | 1.61  | 0.17              |
| 16.20       | 2873.3                    | 2835.6                             | 152.18          | 151.88                   | 2.02  | 0.22              |
| 17.00       | 5279.6                    | 5241.9                             | 164.00          | 163.70                   | 3.74  | 0.40              |
| 17.26       | 5003.9                    | 4966.2                             | 167.84          | 167.55                   | 3.54  | 0.38              |
| 18.10       | 5849.2                    | 5811.5                             | 180.26          | 179.96                   | 4.14  | 0.45              |
| 19.30       | 6384.2                    | 6346.5                             | 197.99          | 197.70                   | 4.53  | 0.49              |
| 19.96       | 8966.9                    | 8929.2                             | 207.74          | 207.45                   | 6.37  | 0.68              |
| 20.96       | 10016.3                   | 9978.6                             | 222.52          | 222.23                   | 7.12  | 0.76              |
| 21.96       | 10205.9                   | 10168.2                            | 237.30          | 237.01                   | 7.25  | 0.78              |
| 22.96       | 11301.2                   | 11263.5                            | 252.08          | 251.78                   | 7.98  | 0.86              |
| 23.98       | 11630.2                   | 11592.5                            | 267.15          | 266.86                   | 8.22  | 0.88              |
| 24.96       | 11383.1                   | 11345.4                            | 281.64          | 281.34                   | 8.04  | 0.86              |
| 25.96       | 11441.1                   | 11403.4                            | 296.42          | 296.12                   | 8.08  | 0.87              |
| 27.96       | 12479.4                   | 12441.7                            | 325.97          | 325.68                   | 8.82  | 0.95              |
| 28.94       | 12307.5                   | 12269.8                            | 340.46          | 340.16                   | 8.70  | 0.93              |
| 29.96       | 13142.1                   | 13104.4                            | 355.53          | 355.23                   | 9.29  | 1.00              |
| 30.96       | 12310.7                   | 12273.0                            | 370.31          | 370.01                   | 8.70  | 0.93              |
| 31.92       | 12472.7                   | 12435.0                            | 384.50          | 384.20                   | 8.81  | 0.95              |
| 33.09       | 12107.5                   | 12069.8                            | 401.79          | 401.49                   | 8.56  | 0.92              |
| 33.94       | 13205.8                   | 13168.1                            | 414.35          | 414.05                   | 9.33  | 1.00              |
| 34.93       | 12679.0                   | 12641.3                            | 428.98          | 428.68                   | 8.96  | 0.96              |
| 35.96       | 12509.7                   | 12472.0                            | 444.20          | 443.90                   | 8.84  | 0.95              |
| 36.96       | 12398.5                   | 12360.8                            | 458.98          | 458.68                   | 8.76  | 0.94              |
| 37.96       | 12490.6                   | 12452.9                            | 473.76          | 473.46                   | 8.83  | 0.95              |
| 39.06       | 12863.9                   | 12826.2                            | 490.01          | 489.72                   | 9.09  | 0.98              |

**SECTION D8  
NICKEL EFFLUENT CONCENTRATIONS**

Dates: 7/7/92 to 9/25/92

Column 4

| Time<br>(d) | Sample<br>LSC<br>(CPM/mL) | Sample -<br>Background<br>(CPM/mL) | Pore<br>Volumes | Pore Vol. -<br>Dead Vol. | Conc. | Relative<br>Conc. |
|-------------|---------------------------|------------------------------------|-----------------|--------------------------|-------|-------------------|
| 39.97       | 13207.2                   | 13169.5                            | 503.13          | 502.84                   | 9.34  | 1.00              |
| 40.95       | 13266.6                   | 13228.9                            | 517.26          | 516.97                   | 9.38  | 1.01              |
| 41.96       | 13157.2                   | 13119.5                            | 531.83          | 531.53                   | 9.30  | 1.00              |

**SECTION D9**  
**pH VALUES**

**INFLUENT SOLUTION:**

Measured: 2/10/93

| pH   | Solution   |
|------|--|
| 7.31 | 10 mg/L Ni, 0.005 M CaCl <sub>2</sub>                              |
| 7.22 | 10 mg/L Ni, 0.100 g/L NaN <sub>3</sub> , 0.005 M CaCl <sub>2</sub> |

**EFFLUENT SOLUTION:**

| Day      | Sterile Columns |          | Inoculated Columns |          | daily   | daily    |
|----------|-----------------|----------|--------------------|----------|---------|----------|
|          | column1         | column 2 | column 3           | column 4 | average | st. dev. |
| 3        | 8.18            | 7.85     | 7.97               | 7.9      | 7.98    | 0.15     |
| 10       | 7.88            | 7.96     | 7.92               | 7.9      | 7.92    | 0.03     |
| 17       | 7.22            | 7.26     | 7.7                | 7.71     | 7.47    | 0.27     |
| 24       | 7.78            | 7.76     | 7.58               | 7.51     | 7.66    | 0.13     |
| 49       | 7.27            | 7.29     | -                  | -        | 7.28    | 0.01     |
| 54       | 7.36            | 8.03     | -                  | -        | 7.70    | 0.47     |
| average  | 7.62            | 7.69     | 7.79               | 7.76     |         |          |
| st. dev. | 0.39            | 0.34     | 0.18               | 0.19     |         |          |

|                          | Column 1 and 2 | Column 3 and 4 |
|--------------------------|----------------|----------------|
| Average by column group: | 7.65           | 7.77           |
| Standard deviation:      | 0.35           | 0.17           |

overall average: 7.70  
overall st. dev.: 0.29

**Appendix E**  
**Microbial Numbers**



## APPENDIX E

### MICROBIAL NUMBERS

This appendix gives results of standard plate counts and direct microscopic counts. Results of plate counts from experiments 'V1' and 'L2' are summarized in Table 3 of Chapter 2. These plate counts were performed to determine the effect of  $\text{Ni}^{2+}$  in batch samples on culturable cell numbers for both freshly washed microbes (V1) and freeze-dried microbes (L2). Results of plate counts performed at the end of the columns experiment (C2) are given and are summarized in the 'Microbial Numbers' section of the Results and Discussion section of Chapter 2. This appendix also contains information from four direct counts which relate the optical density of various microbial suspensions to the number of cells. The direct count performed on the suspension used in experiment 'L2' was used to relate numbers of culturable cells to total cells.

PLATE COUNT RESULTS

**Experiment: V1**

**NICKEL EFFECT ON THE VIABILITY OF FRESHLY WASHED MICROBES**

| FIRST COUNT:  |                         |                         |                         |
|---|-------------------------|-------------------------|-------------------------|
|   | SPC A                   | SPC B                   | SPC C                   |
|   | Plated: 2/29/92         | Plated: 3/1/92          | Plated: 3/2/92          |
|   | <u>Counted: 3/4/92</u>  | <u>Counted: 3/5/92</u>  | <u>Counted: 3/6/92</u>  |
| Average (CFU/g tuff):   | 4.70E+07                | 1.07E+07                | 7.86E+06                |
| St. Dev. (CFU/g tuff):  | 3.4E+06                 | 1.6E+06                 | 1.7E+06                 |
| n:  | 6                       | 3                       | 6                       |
|   | SPC D                   | SPC E                   | SPC F                   |
|   | Plated 3/2/92           | Plated 3/2/92           | Plated 3/2/92           |
|   | <u>Counted: 3/6/92</u>  | <u>Counted: 3/6/92</u>  | <u>Counted: 3/6/92</u>  |
| Average (CFU/g tuff):   | 9.24E+06                | 1.03E+07                | 1.42E+07                |
| St. Dev. (CFU/g tuff):  | 1.5E+06                 | 3.8E+06                 | 1.2E+07                 |
| n:  | 6                       | 6                       | 6                       |
| SECOND COUNT:   |                         |                         |                         |
|   | Plated: 2/29/92         | Plated: 3/1/92          | Plated: 3/2/92          |
|   | <u>Counted: 3/11/92</u> | <u>Counted: 3/12/92</u> | <u>Counted: 3/13/92</u> |
| Average (CFU/g tuff):   | 4.66E+07                | 1.08E+07                | 7.91E+06                |
| St. Dev. (CFU/g tuff):  | 3.0E+06                 | 1.5E+06                 | 1.7E+06                 |
| n:  | 6                       | 3                       | 6                       |
|   | Plated 3/2/92           | Plated 3/2/92           | Plated 3/2/92           |
|   | <u>Counted: 3/13/92</u> | <u>Counted: 3/13/92</u> | <u>Counted: 3/13/92</u> |
| Average (CFU/g tuff):   | 9.27E+06                | 8.02E+07                | 1.33E+07                |
| St. Dev. (CFU/g tuff):  | 2.4E+06                 | 9.3E+07                 | 1.2E+07                 |
| n:  | 3                       | 6                       | 6                       |
| <p>SPC A = Sample take on the first day, prior to shaking.<br/>                     SPC B = Sample take on the second day, after 24 hr shaking, prior to adding Ni.<br/>                     SPC C = Sample taken on third day, no Ni solution added.<br/>                     SPC D = Sample taken on third day, after shaking with .01 mg/L Ni for 24 hr.<br/>                     SPC E = Sample taken on third day, after shaking with 1 mg/L Ni for 24 hr.<br/>                     SPC F = Sample taken on third day, after shaking with 100 mg/L Ni for 24 hr.</p> |                         |                         |                         |

PLATE COUNT RESULTS

**Experiment: L2**  
**NICKEL EFFECT ON FREEZE-DRIED MICROBE VIABILITY**

|                       |                         |                         |                         |
|-----------------------|-------------------------|-------------------------|-------------------------|
|                       | Plated: 9/16/92         | Plated: 9/17/92         | Plated: 9/18/92         |
|                       | <u>Counted: 9/23/92</u> | <u>Counted: 9/23/92</u> | <u>Counted: 9/23/92</u> |
| Average (CFU/g tuff): | 2.91E+07                | 1.15E+07                | 1.19E+07                |
| St. Dev.:             | 6.3E+06                 | 1.4E+06                 | 3.1E+06                 |
| n:                    | 3                       | 3                       | 3                       |
|                       | Plated: 9/16/92         | Plated: 9/17/92         | Plated: 9/18/92         |
|                       | <u>Counted: 10/8/92</u> | <u>Counted: 10/8/92</u> | <u>Counted: 10/8/92</u> |
| Average (CFU/g tuff): | 2.90E+07                | 1.13E+07                | 1.42E+07                |
| St. Dev.:             | 6.1E+06                 | 1.4E+06                 | 2.3E+06                 |
| n:                    | 3                       | 3                       | 3                       |

**Experiment: C2**  
**CULTURABLE MICROBES IN COLUMNS AT THE END OF THE**  
**TRANSPORT EXPERIMENT**

|                       |  |                 |
|-----------------------|--|-----------------|
| Column 1 and 2:       | Plated: 9/25/92  |                 |
|                       | Counted: 10/8/92   |                 |
|                       | All counts were <= 4 CFU/g; thus the number was statistically insignificant. |                 |
|                       | Counted colonies could have been from contamination of plates.               |                 |
| Column 3 and 4:       | Plated: 8/18/92  |                 |
|                       | Counted: 8/25/92   |                 |
|                       | <u>Column 3</u>  | <u>Column 4</u> |
| average (CFU/g tuff): | 1.44E+05   | 1.73E+05        |
| st dev (CFU/g tuff):  | 1.2E+04  | 1.3E+04         |
| n:                    | 3  | 3               |

## DIRECT COUNTS

Experiment: no number

Date: 3/18/92

objective: Find the approximate number of 175 T#3 cells at an optical density of 0.8.

Average(cells/mL): 2.45E+08

Experiment: no number

Date: ?

objective: Find the approximate number of 175 T#3 cells at an optical density of 0.75.

Average(cells/mL): 3.76E+08

Experiment: L1

Date: 6/29/92

objective: Find the approximate number of 175 T3 cells at an optical density of 0.75.

Average(cells/mL): 5.14E+07

Experiment: L2

Date: 9/25/92

objective: Find the approximate number of 175 T3 cells at an optical density of 0.75.

Average(cells/mL): 5.22E+08

st dev: 1.42E+08

Note: The cells were difficult to count because they clumped together.

For this reason, we doubled the original count to get these numbers.

## Appendix F

### Moisture Content Increase Resulting from Autoclaving

## APPENDIX F

### MOISTURE CONTENT ADDED BY AUTOCLAVING

This appendix gives information on the mass of water added to tuff by autoclaving. The mass of water present in the samples is given relative to the mass measured after the tuff was air dried for several days and before the first day of autoclaving. Note that water added by autoclaving evaporated, thus the mass of water in the samples decreased from one day after autoclaving (A) to the next day before autoclaving (B).

The results show the mass of water added to the crushed tuff by the autoclave is negligible ( $<0.06$  g) compared to the amount of solution added to samples for the batch sorption experiments (20 mL).

Experiment Date: Feb. 1992

#### Method

The experiment was done with triplicate samples. Sample averages are given in the results table.

1. ~10 g of crushed tuff was measured into polyallomer centrifuge tubes.
2. The tubes containing the tuff were weighed .
3. The tubes were autoclaved, then reweighed.
4. On days 2 and 3 the tubes were weighed again before and after autoclaving.

#### Results

| <u>Day</u> | <u>before/after<br/>autoclaving</u> | <u>ave. mass<br/>of water<br/>added (g)</u> | <u>st. dev.<br/>mass<br/>added</u> |
|------------|-------------------------------------|---|------------------------------------|
| 1          | B                                   | 0   | n/a                                |
| 1          | A                                   | 0.039                                       | 0.0034                             |
| 2          | B                                   | 0.008                                       | 0.0018                             |
| 2          | A                                   | 0.057                                       | 0.0034                             |
| 3          | B                                   | 0.011                                       | 0.0020                             |
| 3          | A                                   | 0.030                                       | 0.0072                             |

This thesis is accepted on behalf of the faculty of the Institute  
by the following committee:

Robert A. Bowman      1 July 1993  
Advisor                                  Date

Thomas L. Klett      7/1/93  
Date

Hendricks      7/1/93  
Date