

WELLBORE TEMPERATURE MEASUREMENTS IN AIR AND WATER  
USING CONTINUOUS AND EQUILIBRIUM LOGGING METHODS

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1977

## INTRODUCTION

The purpose of this paper is to summarize observations made in analyzing high precision wellbore temperature log data that were obtained in two distinct downhole environments using two logging methods. The two environments were either "water," a term which is here loosely applied to groundwater, various liquid hydrocarbons, or mixtures of both; or "air," which might be more accurately denoted as methane with respect to the wells considered in this paper. The two logging methods used were the equilibrium method and the continuous method, both of which are described later.

A comparison between the results obtained with the equilibrium method and those obtained with the continuous method is made in this paper. It is to be hoped that this comparison will (1) allow an evaluation to be made, with respect to accuracy and efficiency, of the two logging methods in a water column and in an air column, and (2) provide insight into appropriately interpreting data that is obtained in water and in air by either the continuous or the equilibrium logging method.

## PROCEDURE

Equipment. The major components of the data acquisition system used in obtaining the temperature logs to be presented here were a thermistor, an 8000-foot length of four-

conductor cable, an electronic digital ohmmeter, and an odometer which measured downhole cable length. The thermistor consisted of a device having a hydrodynamic profile and electrically conforming to a resistance of 100,000 ohms at 77° F. It was connected through the cable to the ohmmeter circuitry in a four-wire configuration. Thus, a constant current was supplied to the thermistor by the ohmmeter through two conductors while the resulting voltage drop across the thermistor was sensed via the remaining two conductors. This arrangement permitted measurement of the thermistor resistance while eliminating the effects of varying cable resistance. The current supplied to the thermistor was limited such that the  $I^2R$  loss occurring at the thermistor would be insignificant. The accuracy of the system was determined to be better than 0.05% for temperatures between 64.8° F. and 228.7° F.

Logging Methods. The equilibrium method of temperature logging consisted in lowering the probe into the well to a predetermined depth, then maintaining the probe at that depth for a period of time, usually fifteen to thirty minutes, while thermal equilibrium between the probe and its downhole environment was either attained or approached. During this stationary period the ohmmeter was actuated manually at regular intervals, usually thirty or sixty seconds. The probe resistance was automatically recorded via a thermal printer connected to the ohmmeter, thereby allowing the time response of the probe to be observed.

The preceding procedure was repeated at several successive depth intervals to obtain an "equilibrium log" of the well.

The continuous method of logging a well involved initially obtaining an equilibrium point near the upper part of the well as described above. Successive temperatures, however, were obtained by manually actuating the thermal printer as the probe passed certain predetermined depths as indicated by the cable odometer. The probe was generally lowered at the rate of sixty feet per minute and resistance was typically recorded at ten foot intervals. The resistance values recorded represented the average of the ten resistance measurements made in the most recent complete one-second averaging cycle of the ohmmeter.

Wells. Data from three wells are presented in this paper. The logging schedules of those wells are as follows:

Date: June 29, 1977      Well: Datil      Probe: #4

<u>Calibration Depths</u>	<u>Equilibrium Logging Interval</u>
60 - 150 ft	30 ft
150 - 250	50
250 - 450	100
450 - 600	150

	<u>Continuous Logging Interval</u>
600 ft	10 ft
1000	10
1200	10
1400	10
1600	10
1800	10
2000	10

Date: June 30, 1977 Well: Datil Probe: #4

Calibration Depths

Continuous Logging Interval

70 ft	10 ft
1000	10
2000	10
2200	10
2400	10
2600	10
2800	10
3000	10
3200	10
3400	10
3600	10
4600	10
4900	10

Date: July 11, 1977 Well: Red Wash Probe: #6

Calibration Depths

Equilib. Log Interval

Contin. Log Interval

500 - 1900 ft	100 ft	25 ft
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Continuous Logging Interval

1900 ft	10 ft
2500	10
3000	10
3500	10
4000	10
4500	10
4800	10

Date: July 12, 1977 Well: Red Wash Probe: #6

Calibration Depths

Continuous Logging Interval

500 ft	25 ft
600	25
1300	25
1900	10
2000	10
2100	10
2200	10
2300	10
3000	10
3100	10

Date: July 14, 1977

Well: Cache

Probe: #6

Calibration DepthsContinuous Logging Interval

400 ft	10 ft
900	10
1400	10
1600	10
1700	10
2000	10
3000	10
4000	10
5000	10
5500	10

## DATA

The depth and resistance data that were recorded on the thermal printer paper tape in the field were entered onto data cards for computer processing. The output of the program for interpretation of the resistance data included a listing of temperatures, depths, and temperature gradients and provided plots of depth vs. temperature. Listings and depth-temperature plots for the Datil, Red Wash, and Cache wells are found on the following pages. It should be noted that the temperatures appearing in the listings at each calibration point represent the <sup>final</sup> "touchdown" temperatures. The <sup>final</sup> TD temperature is the temperature recorded at the <sup>end of</sup> ~~time~~ ~~the probe reached a given depth and remained stationary~~ during the calibration interval.

DATIL 6/29/77, TOOL #4, SYSTRON DONNER, PC=190

DEPTH	METERS	DEG	GRAD	TEMPERATURE	DEG	RESISTANCE	DELTA
FEET		+	C/KM	DEG C	F	+	
60.0	18.3	-303.097		16.882	62.387	145330.00	
90.0	27.4	60.453		14.110	57.398	165789.94	
120.0	36.6	67.349		14.663	58.502	1561462.00	
150.0	45.7	98.386		15.778	59.502	156789.94	
200.0	61.0	56.650		16.741	62.755	146039.94	
250.0	76.2	51.799		17.641	63.755	140229.94	
300.0	91.4	56.656		19.246	66.596	130270.00	
350.0	106.7	66.556		20.949	69.702	120289.94	
400.0	122.0	68.314		23.989	75.180	104729.94	
450.0	137.3	99.903		24.197	75.554	103751.94	
500.0	152.6	108.944		24.501	76.103	102339.00	
550.0	167.9	65.491		24.833	76.700	100824.94	
600.0	183.2	51.839		25.033	77.060	99925.94	
650.0	198.5	35.043		25.191	77.344	99222.00	
700.0	213.8	30.798		25.298	77.705	98748.94	
750.0	229.1	30.841		25.322	77.735	98335.94	
800.0	244.4	21.862		25.455	77.820	98055.94	
850.0	259.7	23.098		25.522	77.939	97764.00	
900.0	275.0	33.066		25.593	78.066	97020.00	
950.0	290.3	43.879		25.627	78.248	96442.94	
1000.0	305.6	80.186		26.073	78.932	95389.00	
1050.0	320.9	80.168		26.348	78.927	94229.94	
1100.0	336.2	73.706		26.592	79.466	93212.00	
1150.0	351.5	70.166		26.817	79.871	92287.94	
1200.0	366.8	49.761		27.031	80.656	91417.94	
1250.0	382.1	39.744		27.183	80.929	90805.94	
1300.0	397.4	57.961		27.304	81.147	90320.00	
1350.0	412.7	70.301		27.465	81.619	89619.00	
1400.0	428.0	49.526		27.695	81.851	88774.94	
1450.0	443.3	41.716		27.943	82.122	88186.00	
1500.0	458.6	50.332		27.973	82.351	87694.00	
1550.0	473.9	41.809		28.126	82.627	87104.00	
1600.0	489.2	40.103		28.254	82.857	86617.00	
1650.0	504.5	39.582		28.376	83.077	86152.94	
1700.0	519.8	36.764		28.498	83.294	85699.00	
1750.0	535.1	39.881		28.608	83.495	85279.94	
1800.0	550.4	49.022		28.720	83.697	84861.94	
1850.0	565.7	49.746		28.842	83.915	84410.94	
1900.0	581.0	55.518		28.924	84.123	83976.94	
1950.0	596.3	52.003		29.194	84.727	83376.94	
2000.0	611.6	36.509		29.453	85.017	82759.94	
2050.0	626.9	22.508		29.563	85.182	82182.00	
2100.0	642.2	23.208		29.703	85.338	81791.00	
2150.0	657.5	33.898		29.806	85.465	81546.94	
2200.0	672.8	37.493		29.896	85.651	81296.00	
2250.0	688.1	37.079		29.896	85.802	80930.94	
2300.0	703.4	37.079		29.896	85.802	80636.00	





110	0	2	460	49	125	108	100	5689
115	0	3	463	49	126	109	101	5651
115	0	4	466	49	127	109	101	5615
115	0	5	472	49	128	109	101	5580
115	0	6	475	49	129	109	101	5546
115	0	7	478	49	130	109	101	5494
115	0	8	481	49	131	109	101	5457
116	0	9	487	49	132	109	101	5410
116	0	0	490	49	133	109	101	5373
116	0	1	493	49	134	109	101	5336
116	0	2	496	49	135	109	101	5299
116	0	3	499	49	136	109	101	5262
116	0	4	502	49	137	109	101	5225
116	0	5	506	49	138	109	101	5188
116	0	6	509	49	139	109	101	5151
116	0	7	512	49	140	109	101	5114
116	0	8	515	49	141	109	101	5077
116	0	9	518	49	142	109	101	5040
117	0	0	521	49	143	109	101	5003
117	0	1	524	49	144	109	101	4966
117	0	2	527	49	145	109	101	4929
117	0	3	530	49	146	109	101	4892
117	0	4	533	49	147	109	101	4855
117	0	5	536	49	148	109	101	4818
117	0	6	539	49	149	109	101	4781
117	0	7	542	49	150	109	101	4744
117	0	8	545	49	151	109	101	4707
118	0	9	548	49	152	109	101	4670
118	0	0	551	49	153	109	101	4633
118	0	1	554	49	154	109	101	4596
118	0	2	557	49	155	109	101	4559
118	0	3	560	49	156	109	101	4522
118	0	4	563	49	157	109	101	4485
118	0	5	566	49	158	109	101	4448
118	0	6	570	49	159	109	101	4411
118	0	7	573	49	160	109	101	4374
118	0	8	576	49	161	109	101	4337
118	0	9	579	49	162	109	101	4300
119	0	0	582	49	163	109	101	4263
119	0	1	585	49	164	109	101	4226
119	0	2	588	49	165	109	101	4189
119	0	3	591	49	166	109	101	4152
119	0	4	594	49	167	109	101	4115
119	0	5	597	49	168	109	101	4078
119	0	6	600	49	169	109	101	4041
119	0	7	603	49	170	109	101	4004
119	0	8	606	49	171	109	101	3967
120	0	9	609	49	172	109	101	3930
120	0	0	610	49	173	109	101	3893
120	0	1	610	49	174	109	101	3856
120	0	2	610	49	175	109	101	3819
120	0	3	610	49	176	109	101	3782
120	0	4	610	49	177	109	101	3745
120	0	5	610	49	178	109	101	3708
120	0	6	610	49	179	109	101	3671
120	0	7	610	49	180	109	101	3634
120	0	8	610	49	181	109	101	3597
120	0	9	610	49	182	109	101	3560
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120	0	2	610	49	185	109	101	3449
120	0	3	610	49	186	109	101	3412
120	0	4	610	49	187	109	101	3375
120	0	5	610	49	188	109	101	3338
120	0	6	610	49	189	109	101	3301
120	0	7	610	49	190	109	101	3264
120	0	8	610	49	191	109	101	3227
120	0	9	610	49	192	109	101	3190
120	0	0	610	49	193	109	101	3153
120	0	1	610	49	194	109	101	3116
120	0	2	610	49	195	109	101	3079
120	0	3	610	49	196	109	101	3042
120	0	4	610	49	197	109	101	3005
120	0	5	610	49	198	109	101	2968
120	0	6	610	49	199	109	101	2931
120	0	7	610	49	200	109	101	2894
120	0	8	610	49	201	109	101	2857
120	0	9	610	49	202	109	101	2820
120	0	0	610	49	203	109	101	2783
120	0	1	610	49	204	109	101	2746
120	0	2	610	49	205	109	101	2709
120	0	3	610	49	206	109	101	2672
120	0	4	610	49	207	109	101	2635
120	0	5	610	49	208	109	101	2598
120	0	6	610	49	209	109	101	2561
120	0	7	610	49	210	109	101	2524
120	0	8	610	49	211	109	101	2487
120	0	9	610	49	212	109	101	2450
120	0	0	610	49	213	109	101	2413
120	0	1	610	49	214	109	101	2376
120	0	2	610	49	215	109	101	2339
120	0	3	610	49	216	109	101	2302
120	0	4	610	49	217	109	101	2265
120	0	5	610	49	218	109	101	2228
120	0	6	610	49	219	109	101	2191
120	0	7	610	49	220	109	101	2154
120	0	8	610	49	221	109	101	2117
120	0	9	610	49	222	109	101	2080
120	0	0	610	49	223	109	101	2043
120	0	1	610	49	224	109	101	2006
120	0	2	610	49	225	109	101	1969
120	0	3	610	49	226	109	101	1932
120	0	4	610	49	227	109	101	1895
120	0	5	610	49	228	109	101	1858
120	0	6	610	49	229	109	101	1821
120	0	7	610	49	230	109	101	1784
120	0	8	610	49	231	109	101	1747
120	0	9	610	49	232	109	101	1710
120	0	0	610	49	233	109	101	1673
120	0	1	610	49	234	109	101	1636
120	0	2	610	49	235	109	101	1599
120	0	3	610	49	236	109	101	1562
120	0	4	610	49	237	109	101	1525
120	0	5	610	49	238	109	101	1488
120	0	6	610	49	239	109	101	1451
120	0	7	610	49	240	109	101	1414
120	0	8	610	49	241	109	101	1377
120	0	9	610	49	242	109	101	1340
120	0	0	610	49	243	109	101	1303
120	0	1	610	49	244	109	101	1266
120	0	2	610	49	245	109	101	1229
120	0	3	610	49	246	109	101	1192
120	0	4	610	49	247	109	101	1155
120	0	5	610	49	248	109	101	1118
120	0	6	610	49	249	109	101	1081
120	0	7	610	49	250	109	101	1044
120	0	8	610	49	251	109	101	1007
120	0	9	610	49	252	109	101	970
120	0	0	610	49	253	109	101	933
120	0	1	610	49	254	109	101	896
120	0	2	610	49	255	109	101	859
120	0	3	610	49	256	109	101	822
120	0	4	610	49	257	109	101	785
120	0	5	610	49	258	109	101	748
120	0	6	610	49	259	109	101	711
120	0	7	610	49	260	109	101	674
120	0	8	610	49	261	109	101	637
120	0	9	610	49	262	109	101	600
120	0	0	610	49	263	109	101	563
120	0	1	610	49	264	109	101	526
120	0	2	610	49	265	109	101	489
120	0	3	610	49	266	109	101	452
120	0	4	610	49	267	109	101	415
120	0	5	610	49	268	109	101	378
120	0	6	610	49	269	109	101	341
120	0	7	610	49	270	109	101	304
120	0	8	610	49	271	109	101	267
120	0	9	610	49	272	109	101	230
120	0	0	610	49	273	109	101	193
120	0	1	610	49	274	109	101	156
120	0	2	610	49	275	109	101	119
120	0	3	610	49	276	109	101	82
120	0	4	610	49	277	109	101	45
120	0	5	610	49	278	109	101	8
120	0	6	610	49	279	109	101	-29
120	0	7	610	49	280	109	101	-66
120	0	8	610	49	281	109	101	-133
120	0	9	610	49	282	109	101	-200
120	0	0	610	49	283	109	101	-267
120	0	1	610	49	284	109	101	-334
120	0	2	610	49	285	109	101	-401
120	0	3	610	49	286	109	101	-468
120	0	4	610	49	287	109	101	-535
120	0	5	610	49	288	109	101	-602
120	0	6	610	49	289	109	101	-669
120	0	7	610	49	290	109	101	-736
120	0	8	610	49	291	109	101	-803
120	0	9	610	49	292	109	101	-870
120	0	0	610	49	293	109	101	-937
120	0	1	610	49	294	109	101	

DATIL 6/30/77, TOOL #4, SYSTRON DONNER, RC=190

FEET	DEPTH METERS	* * DEG	GRAD C/KM	* * DEG C	TEMPERATURE	DEG F	* * RESISTANCE	* * DELTA
70.0	21.3	17.288	19.805	14.013	57.224	166559.94	+	
80.0	24.4	19.331	27.455	14.066	57.319	166139.94		
90.0	27.5	27.354	30.819	14.126	57.427	165660.00		
100.0	30.6	28.470	33.555	14.210	57.744	165000.00		
110.0	33.7	33.574	39.091	14.302	57.902	164270.00		
120.0	36.8	35.574	42.777	14.495	58.091	162759.94		
130.0	39.9	37.877	45.889	14.403	58.286	161919.94		
140.0	43.0	40.336	49.917	14.724	58.503	160990.00		
150.0	46.1	42.649	51.923	14.956	58.712	160100.00		
160.0	49.2	45.048	55.725	14.979	58.920	159220.00		
170.0	52.3	47.561	59.739	15.193	59.147	158289.94		
180.0	55.4	50.048	62.725	16.051	60.893	157429.94		
190.0	58.5	52.632	65.749	16.851	62.332	155139.94		
200.0	61.6	55.232	68.749	17.083	62.749	153960.00		
210.0	64.7	57.848	71.749	17.285	63.104	142630.00		
220.0	67.8	60.475	74.739	17.643	63.420	141460.00		
230.0	70.9	63.125	77.739	17.865	63.757	140220.00		
240.0	74.0	65.805	80.734	18.097	64.156	138770.00		
250.0	77.1	68.515	83.742	18.341	64.575	137270.00		
260.0	80.2	71.245	86.749	18.573	65.015	135710.00		
270.0	83.3	74.005	89.749	18.805	65.428	134250.00		
280.0	86.4	76.795	92.734	18.805	65.849	132809.94		
290.0	89.5	79.615	95.734	18.956	66.121	131880.00		
300.0	92.6	82.465	98.734	19.088	66.121	131070.00		
310.0	95.7	85.338	101.734	19.232	66.359	130199.94		
320.0	98.8	88.238	104.734	19.376	66.617	129330.00		
330.0	101.9	91.165	107.734	19.576	66.823	128139.94		
340.0	105.0	94.115	110.734	19.769	67.236	127000.00		
350.0	108.1	97.085	113.734	19.969	67.583	125830.00		
360.0	111.2	100.075	116.734	20.157	67.943	124740.00		
370.0	114.3	103.085	119.734	20.317	68.271	123820.00		
380.0	117.4	106.115	122.734	20.442	68.596	123110.00		
390.0	120.5	109.165	125.734	20.589	69.060	122279.94		
400.0	123.6	112.235	128.734	20.793	69.771	121139.94		
410.0	126.7	115.325	131.734	20.984	70.060	120080.00		
420.0	129.8	118.435	134.734	21.204	70.546	118869.94		
430.0	132.9	121.565	137.734	21.415	71.168	117729.94		
440.0	136.0	124.715	140.734	21.644	71.646	116541.00		
450.0	139.1	127.885	143.734	21.850	72.046	115410.00		
460.0	142.2	131.075	146.734	22.075	72.329	114229.94		
470.0	145.3	134.285	149.734	22.242	72.746	113339.94		
480.0	148.4	137.515	152.734	22.423	73.165	111410.00		
490.0	151.5	140.765	155.734	22.623	73.528	110169.94		
500.0	154.6	144.035	158.734	22.870	73.873	109169.94		
510.0	157.7	147.325	161.734	23.071	74.200	108169.94		
520.0	160.8	150.635	164.734	23.276	74.511	107169.94		
530.0	163.9	153.965	167.734	23.485	74.806	106169.94		
540.0	167.0	157.315	170.734	23.697	75.086	105169.94		
550.0	170.1	160.685	173.734	23.912	75.351	104169.94		
560.0	173.2	164.075	176.734	24.129	75.600	103169.94		
570.0	176.3	167.485	179.734	24.349	75.834	102169.94		
580.0	179.4	170.915	182.734	24.571	76.053	101169.94		
590.0	182.5	174.365	185.734	24.795	76.257	100169.94		
600.0	185.6	177.835	188.734	25.021	76.446	99169.94		
610.0	188.7	181.325	191.734	25.249	76.620	98169.94		
620.0	191.8	184.835	194.734	25.479	76.779	97169.94		
630.0	194.9	188.365	197.734	25.711	76.924	96169.94		
640.0	198.0	191.915	200.734	25.945	77.055	95169.94		
650.0	201.1	195.485	203.734	26.181	77.173	94169.94		
660.0	204.2	199.075	206.734	26.419	77.278	93169.94		
670.0	207.3	202.685	209.734	26.659	77.370	92169.94		
680.0	210.4	206.315	212.734	26.901	77.449	91169.94		
690.0	213.5	210.965	215.734	27.145	77.515	90169.94		
700.0	216.6	215.635	218.734	27.391	77.568	89169.94		
710.0	219.7	220.325	221.734	27.639	77.609	88169.94		
720.0	222.8	225.035	224.734	27.889	77.637	87169.94		
730.0	225.9	229.765	227.734	28.141	77.652	86169.94		
740.0	229.0	234.515	230.734	28.395	77.654	85169.94		
750.0	232.1	239.285	233.734	28.651	77.643	84169.94		
760.0	235.2	244.075	236.734	28.909	77.619	83169.94		
770.0	238.3	248.885	239.734	29.169	77.582	82169.94		
780.0	241.4	253.715	242.734	29.431	77.532	81169.94		
790.0	244.5	258.565	245.734	29.695	77.469	80169.94		
800.0	247.6	263.435	248.734	29.961	77.393	79169.94		
810.0	250.7	268.325	251.734	30.229	77.304	78169.94		
820.0	253.8	273.235	254.734	30.499	77.202	77169.94		
830.0	256.9	278.165	257.734	30.771	77.087	76169.94		
840.0	260.0	283.115	260.734	31.045	76.959	75169.94		
850.0	263.1	288.085	263.734	31.321	76.818	74169.94		
860.0	266.2	293.075	266.734	31.599	76.664	73169.94		
870.0	269.3	298.085	269.734	31.879	76.497	72169.94		
880.0	272.4	303.115	272.734	32.161	76.317	71169.94		
890.0	275.5	308.165	275.734	32.445	76.124	70169.94		
900.0	278.6	313.235	278.734	32.731	75.918	69169.94		
910.0	281.7	318.325	281.734	33.019	75.700	68169.94		
920.0	284.8	323.435	284.734	33.309	75.469	67169.94		
930.0	287.9	328.565	287.734	33.601	75.226	66169.94		
940.0	291.0	333.715	290.734	33.895	74.971	65169.94		
950.0	294.1	338.885	293.734	34.191	74.704	64169.94		
960.0	297.2	344.075	296.734	34.489	74.425	63169.94		
970.0	300.3	349.285	299.734	34.789	74.134	62169.94		
980.0	303.4	354.515	302.734	35.091	73.831	61169.94		
990.0	306.5	359.765	305.734	35.395	73.516	60169.94		
1000.0	309.6	365.035	308.734	35.701	73.189	59169.94		
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1080.0	334.4	407.915	332.734	38.221	70.141	51169.94		
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1100.0	340.6	418.835	338.734	38.871	69.259	49169.94		
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1140.0	353.0	440.915	350.734	40.195	67.351	45169.94		
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1310.0	405.7	538.325	401.734	46.179	57.102	28169.94		
1320.0	408.8	544.235	404.734	46.549	56.393	27169.94		
1330.0	411.9	550.165	407.734	46.921	55.674	26169.94		
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3240.00	984.6	59.076	62.632	144.737	144.737	221825.00
3250.00	987.6	49.139	62.812	145.062	145.062	221707.99
3260.00	990.6	46.471	63.062	145.381	145.381	221595.00
3270.00	993.7	55.515	63.107	145.586	145.586	221476.00
3280.00	996.7	55.552	63.427	145.863	145.863	221345.00
3290.00	999.7	44.879	63.563	146.168	146.168	221240.00
3300.00	1002.8	53.679	63.567	146.414	146.414	221145.00
3310.00	1005.9	32.086	62.725	146.705	146.705	221194.00
3320.00	1008.9	43.048	62.048	147.286	147.286	220871.99
3330.00	1011.0	45.095	64.185	147.534	147.534	220769.00
3340.00	1015.0	54.727	64.359	147.830	147.830	220646.00
3350.00	1018.1	52.248	64.458	148.098	148.098	220535.99
3360.00	1021.1	52.112	64.657	148.384	148.384	220419.00
3370.00	1024.2	48.328	64.817	148.670	148.670	220302.99
3380.00	1030.3	52.358	64.964	148.923	148.923	220196.00
3390.00	1033.3	58.350	65.120	149.223	149.223	220080.99
3400.00	1036.4	51.646	65.302	149.544	149.544	19953.00
3410.00	1039.4	47.322	65.460	149.828	149.828	19841.00
3420.00	1042.5	54.135	65.604	150.087	150.087	19739.00
3430.00	1045.5	46.310	65.769	150.385	150.385	19623.99
3440.00	1048.6	54.543	65.915	150.635	150.635	19524.99
3450.00	1051.6	56.509	66.075	150.935	150.935	19410.00
3460.00	1054.7	53.509	66.223	151.212	151.212	19308.00
3470.00	1057.7	48.021	66.359	151.505	151.505	19190.99
3480.00	1060.8	46.896	66.559	151.809	151.809	19078.99
3490.00	1063.8	48.377	66.705	152.069	152.069	18979.99
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3520.00	1072.9	55.521	67.277	152.858	152.858	18687.00
3530.00	1075.9	46.776	67.446	153.098	153.098	18599.00
3540.00	1082.0	51.066	67.589	153.403	153.403	18488.00
3550.00	1085.1	42.274	67.744	153.659	153.659	18394.00
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3580.00	1109.1	46.771	68.023	154.444	154.444	18114.00

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3600.00 1097.33 45.611 68.327 154.988 17922.00  
3620.00 1100.04 46.174 68.482 155.265 17825.00  
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4090.00	1246.67	46.583	75.668	168.201	3906.00
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4110.00	1255.88	49.275	75.947	168.963	3775.00
4120.00	1258.99	45.663	76.091	169.242	3708.00
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4150.00	1271.00	46.174	76.675	169.015	3518.00
4160.00	1277.11	46.716	76.828	170.290	3440.00
4170.00	1277.47	44.739	76.970	170.546	3371.00
4180.00	1277.00	49.051	77.106	170.791	3307.00
4200.00	1283.23	35.663	77.286	171.115	3246.00
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4220.00	1289.24	51.051	77.570	171.622	3118.00
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4270.00	1304.76	45.875	78.314	172.964	2780.00
4280.00	1307.66	42.937	78.455	173.219	2660.00
4290.00	1310.37	47.861	78.595	173.471	2601.00
4300.00	1313.19	42.863	78.722	173.706	2546.00
4310.00	1316.98	42.920	78.872	173.969	2485.00
4320.00	1319.78	42.740	79.031	174.255	2419.00
4330.00	1322.55	44.628	79.161	174.491	2365.00
4340.00	1325.89	40.149	79.342	174.815	2291.00
4350.00	1328.20	50.405	79.467	175.035	2241.00
4360.00	1333.55	46.561	79.617	175.311	2179.00
4370.00	1338.11	55.907	79.771	175.584	2117.00
4380.00	1341.22	57.119	79.913	175.849	2060.00
4400.00	1344.77	51.106	80.057	176.143	1992.00
4410.00	1347.23	43.687	80.214	176.463	1923.00
4420.00	1350.33	55.652	80.417	176.784	1861.00
4430.00	1353.44	55.269	80.571	177.090	1809.00
4440.00	1355.96	55.421	80.716	177.297	1749.00
4450.00	1359.44	57.676	80.882	177.587	1679.00
4460.00	1362.55	49.919	81.051	177.891	1614.00
4470.00	1366.25	55.952	81.202	178.170	1555.00
4480.00	1368.68	55.744	81.382	178.487	1488.00
4490.00	1371.77	53.481	81.533	178.759	1431.00
4500.00	1374.77	50.377	81.707	179.066	1367.00
4510.00	1377.77	65.445	81.862	179.361	1306.00
4520.00	1383.21	55.673	82.211	179.680	1249.00
4530.00	1388.21	58.753	82.381	179.985	1179.00
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4560.00	1408.11	45.360	83.714	182.685	1013.20
4600.00	1411.11	48.903	83.851	182.932	1059.70
4630.00	1414.11	43.903	84.029	183.252	10534.60

4640.0	1414.3	84.163	183.493	10488.90
4650.0	1417.4	84.348	184.088	10376.90
4660.0	1420.4	84.493	184.389	10320.80
4670.0	1423.5	84.661	184.625	10277.10
4680.0	1426.5	84.792	184.924	10221.90
4690.0	1429.6	84.958	185.101	10174.60
4700.0	1432.6	85.148	185.452	10125.50
4710.0	1435.7	85.315	185.714	10078.00
4720.0	1438.7	85.498	185.898	10045.90
4730.0	1441.8	85.610	186.322	10008.90
4740.0	1444.8	85.734	186.961	9968.40
4750.0	1447.8	85.890	187.259	9855.40
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4770.0	1453.9	86.216	187.840	9752.00
4780.0	1456.0	86.478	188.116	9654.50
4790.0	1460.0	86.731	188.405	9604.80
4800.0	1463.0	86.892	188.687	9556.80
4810.0	1466.1	87.049	188.959	9510.80
4820.0	1469.1	87.199	189.248	9462.10
4830.0	1472.2	87.360	189.518	9416.80
4840.0	1475.3	87.510	189.794	9370.80
4850.0	1478.3	87.663	190.073	9324.50
4860.0	1481.4	87.818	190.332	9281.90
4870.0	1484.4	87.962	190.642	9231.10
4880.0	1487.4	88.134	190.914	9186.80
4890.0	1490.5	88.285		
4900.0	1493.0			
5	STOP			

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RED WASH #137, 7/11/77, TOOL #6, SYSTRON DONNER, RC = 190

DEPTH	METERS	FEET	DEG C/KM	GRAD	TEMPERATURE	DEG F	F	RESISTANCE	DELTA
1500.0	152.4	0	15.497	15.497	59.894	894	155169.94		
525.0	160.0	0	15.222	15.222	59.400	400	1572210.00		
575.0	167.6	0	15.245	15.245	59.388	388	1572259.94		
600.0	175.3	0	15.309	15.309	59.441	441	1570339.94		
625.0	182.5	0	15.418	15.418	59.557	557	1565750.00		
675.0	198.1	0	15.539	15.539	59.753	753	1555369.94		
700.0	205.7	0	15.674	15.674	59.846	846	1548660.00		
725.0	213.0	0	15.871	15.871	60.184	184	153990.00		
750.0	221.0	0	15.953	15.953	60.573	573	152419.94		
775.0	236.6	0	16.042	16.042	60.715	715	151850.00		
800.0	243.5	0	16.454	16.454	61.092	092	151199.94		
825.0	251.1	0	16.546	16.546	61.617	617	150350.00		
850.0	259.7	0	16.642	16.642	61.963	963	148289.94		
875.0	267.4	0	16.769	16.769	61.782	782	147649.94		
900.0	274.9	0	16.877	16.877	62.172	172	146149.94		
925.0	281.6	0	17.053	17.053	62.696	696	144150.00		
950.0	289.2	0	17.188	17.188	62.938	938	1432460.00		
975.0	297.4	0	17.305	17.305	63.150	150	142460.00		
1000.0	304.4	0	17.430	17.430	63.374	374	141630.00		
1025.0	312.0	0	17.769	17.769	63.985	985	139389.94		
1050.0	320.7	0	17.877	17.877	64.179	179	138690.00		
1075.0	327.3	0	17.994	17.994	64.390	390	137929.94		
1100.0	335.3	0	18.128	18.128	64.631	631	137070.00		
1125.0	343.0	0	18.454	18.454	65.217	217	135000.00		
1150.0	350.5	0	18.567	18.567	65.421	421	134289.94		
1175.0	358.1	0	18.703	18.703	65.666	666	133440.00		
1200.0	365.4	0	18.826	18.826	65.887	887	132679.94		
1225.0	373.0	0	19.214	19.214	66.585	585	130309.94		
1250.0	381.6	0	19.336	19.336	66.805	805	129570.00		
1275.0	389.2	0	19.461	19.461	67.030	030	128820.00		
1300.0	396.9	0	19.576	19.576	67.236	236	128139.94		
1325.0	403.5	0	19.895	19.895	67.811	811	126259.94		
1350.0	411.1	0	20.056	20.056	68.102	102	125320.00		
1375.0	419.7	0	20.114	20.114	68.204	204	124990.00		
1400.0	426.3	0	20.275	20.275	68.446	446	124220.00		
1425.0	434.0	0	20.575	20.575	69.034	034	122360.00		
1450.0	442.0	0	20.689	20.689	69.240	240	121720.00		
1475.0	449.2	0	20.807	20.807	69.452	452	121059.94		
1500.0	457.8	0	20.933	20.933	69.680	680	120360.00		
1525.0	464.4	0	21.270	21.270	70.287	287	118511.00		
1550.0	472.4	0	21.383	21.383	70.489	489	117901.00		
1575.0	480.1	0	21.496	21.496	70.692	692	117294.00		
1600.0	487.3	0	21.616	21.616	70.910	910	116645.94		
1625.0	495.5	0	21.892	21.892	71.406	406	115186.94		
1650.0	502.5	0	22.034	22.034	71.662	662	114440.94		
1675.0	510.5	0	22.160	22.160	71.888	888	113787.00		

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RED WASH #137, 7/12/77, TOOL #6, SYSTRON DONNER, RC=190

DEPTH	METERS	FEET	GRAD	DEG C/KM	TEMPERATURE	DEG F	RESISTANCE	DELTA
500.0	152.0	497	23.897	14.779	58.602	160570.00		
525.0	160.0	524	1.724	14.961	58.930	159179.94		
550.0	167.6	550	7.975	14.974	58.953	159080.00		
600.0	182.3	600	6.786	15.035	59.063	158619.94		
625.0	190.5	625	3.14	15.087	59.156	158229.94		
650.0	198.1	650	7.055	15.318	59.572	156500.00		
670.0	203.7	670	3.712	15.371	59.668	156100.00		
705.0	213.4	705	5.909	15.400	59.719	155889.94		
725.0	221.6	725	2.244	15.555	60.002	154009.94		
775.0	236.8	775	11.941	15.648	60.347	153330.00		
800.0	243.5	800	7.456	15.739	60.341	152669.94		
825.0	251.1	825	5.45	15.872	60.750	151710.00		
850.0	259.1	850	6.15	16.143	61.057	150490.00		
900.0	274.3	900	14.247	16.261	61.270	149649.94		
925.0	281.9	925	1.094	16.403	61.720	148649.94		
950.0	289.6	950	1.933	16.511	61.929	1477080.00		
975.0	297.8	975	4.769	16.788	62.561	144669.94		
1000.0	304.4	1000	1.699	17.167	62.900	1443389.94		
1050.0	320.7	1050	18.925	17.332	63.198	142279.94		
1100.0	335.9	1100	21.642	17.476	63.455	141320.00		
1110.0	342.5	1110	19.407	17.641	63.755	140229.94		
1120.0	350.5	1120	1.832	17.956	64.320	139259.94		
1130.0	358.5	1130	8.222	18.130	64.634	138179.94		
1140.0	365.4	1140	0.554	18.305	64.949	137059.94		
1150.0	373.0	1150	6.82	18.513	65.326	135940.00		
1160.0	381.0	1160	2.718	18.713	65.683	134619.94		
1170.0	389.6	1170	2.053	18.866	65.994	133380.00		
1180.0	401.9	1180	7.17	19.059	66.506	132309.94		
1190.0	411.5	1190	1.228	19.189	66.743	130460.00		
1200.0	426.3	1200	10.627	19.843	67.527	126479.94		
1210.0	434.0	1210	5.228	20.024	67.897	125979.94		
1220.0	444.9	1220	0.950	20.288	68.051	125509.94		
1230.0	454.6	1230	8.795	20.444	68.185	124839.94		
1240.0	462.4	1240	15.601	20.515	68.306	123990.00		
1250.0	470.1	1250	7.475	20.635	68.518	122200.00		
1260.0	487.3	1260	1.295	20.769	68.943	122020.00		
1270.0	495.9	1270	6.488	21.042	69.385	121270.00		
1280.0	502.5	1280	17.388	21.191	69.675	120529.94		
1290.0	510.0	1290	19.841	21.493	70.145	119759.94		
1300.0	517.5	1300	22.841	21.644	70.387	118940.00		
1310.0	525.0	1310	19.038	21.849	70.695	118220.00		
1320.0	532.5	1320	21.038	22.064	71.021	117309.94		

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CACHE #19, TOOL #5, SYSTRON DONNER, RC = 190

DEPTH FEET	DEPTH METERS	* * DEG GRAD C/KM	* * TEMPERATURE DEG C	* * DEG F	* * RESISTANCE +	* * RESISTANCE -	DELTA
400.0	121.9	82.416	17.310	63.158	142429.94		
410.0	125.0	82.488	17.561	63.610	140759.94		
420.0	128.0	82.469	17.553	63.596	140809.94		
430.0	131.1	82.487	17.547	63.577	140880.00		
440.0	134.2	82.470	17.547	63.585	140850.00		
450.0	137.2	82.479	17.561	63.610	140759.94		
460.0	140.3	82.472	17.579	63.643	140639.94		
470.0	143.3	82.472	17.590	63.662	140570.00		
480.0	146.4	82.477	17.606	63.692	140460.00		
490.0	149.4	82.484	17.625	63.724	140339.94		
500.0	152.4	82.490	17.641	63.755	140229.94		
510.0	155.5	82.493	17.662	63.793	139989.94		
520.0	158.5	82.499	17.682	63.828	139960.00		
530.0	161.6	82.505	17.707	63.872	139800.00		
540.0	164.6	82.516	17.733	63.919	139630.00		
550.0	167.7	82.527	17.760	63.968	139449.94		
560.0	170.7	82.537	17.791	64.023	139250.00		
570.0	173.8	82.546	17.820	64.076	139059.94		
580.0	176.8	82.554	17.848	64.126	138880.00		
590.0	179.9	82.561	17.883	64.190	138649.94		
600.0	182.9	82.568	17.914	64.245	138449.94		
610.0	185.9	82.574	17.945	64.301	138250.00		
620.0	188.9	82.579	17.977	64.359	138039.94		
630.0	191.9	82.583	18.007	64.410	137860.00		
640.0	194.9	82.586	18.037	64.465	137589.94		
650.0	197.9	82.588	18.068	64.528	137330.00		
660.0	200.9	82.590	18.098	64.595	137020.00		
670.0	203.9	82.591	18.127	64.665	1366289.94		
680.0	206.9	82.592	18.157	64.740	135990.00		
690.0	209.9	82.593	18.187	64.820	1355679.94		
700.0	212.9	82.594	18.217	64.905	1351330.00		
710.0	215.9	82.595	18.247	64.995	134690.00		
720.0	218.9	82.596	18.277	65.090	134220.00		
730.0	221.9	82.597	18.307	65.190	133730.00		
740.0	224.9	82.598	18.337	65.295	133220.00		
750.0	227.9	82.599	18.367	65.405	132690.00		
760.0	230.9	82.600	18.397	65.520	132140.00		
770.0	233.9	82.601	18.427	65.640	131570.00		
780.0	236.9	82.602	18.457	65.765	131000.00		
790.0	239.9	82.603	18.487	65.895	130430.00		
800.0	242.9	82.604	18.517	66.030	129860.00		
810.0	245.9	82.605	18.547	66.170	129290.00		
820.0	248.9	82.606	18.577	66.315	128720.00		
830.0	251.9	82.607	18.607	66.465	128150.00		
840.0	254.9	82.608	18.637	66.620	127580.00		
850.0	257.9	82.609	18.667	66.780	127010.00		
860.0	260.9	82.610	18.697	66.945	126440.00		
870.0	263.9	82.611	18.727	67.115	125870.00		
880.0	266.9	82.612	18.757	67.290	125300.00		

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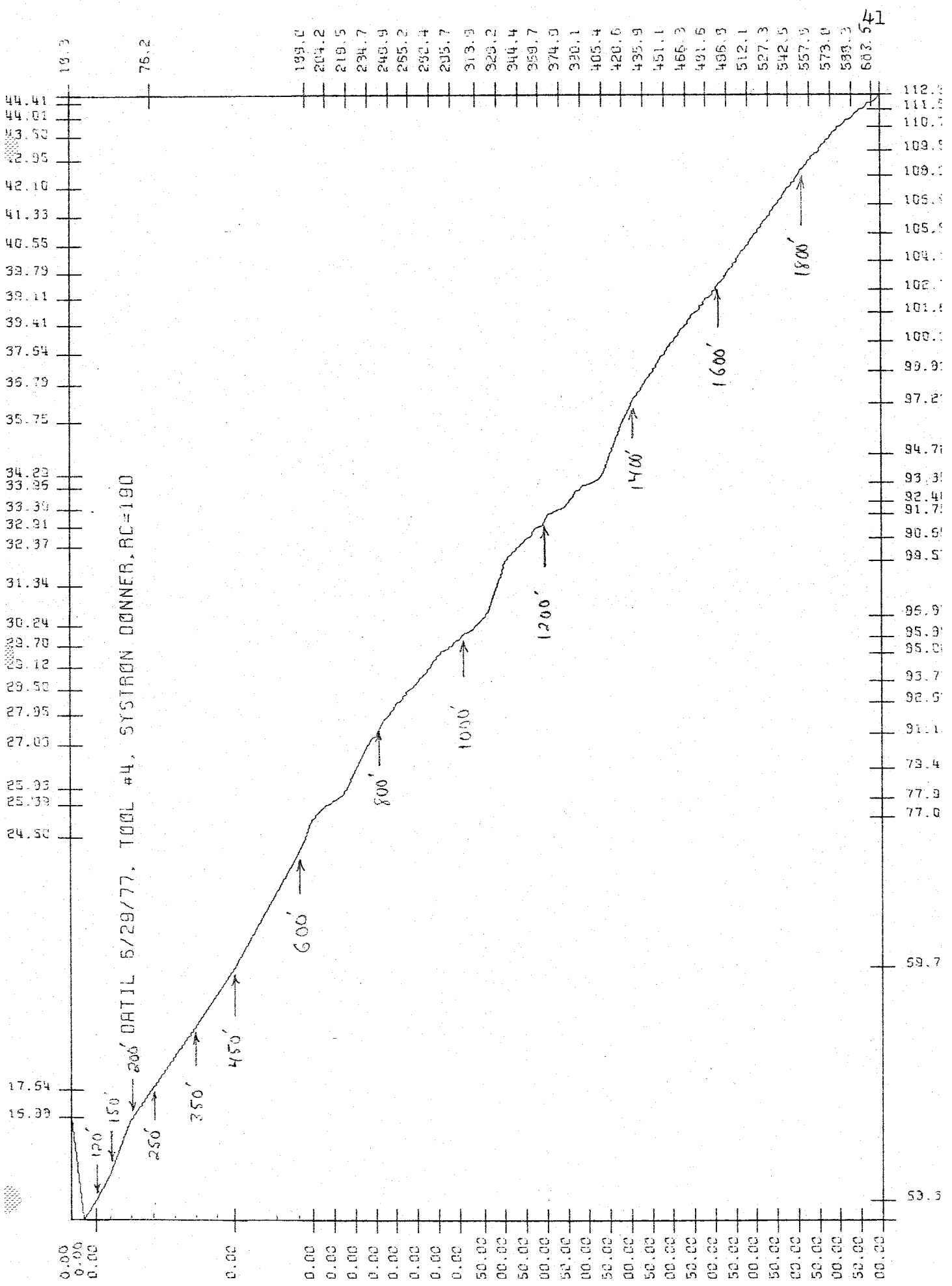
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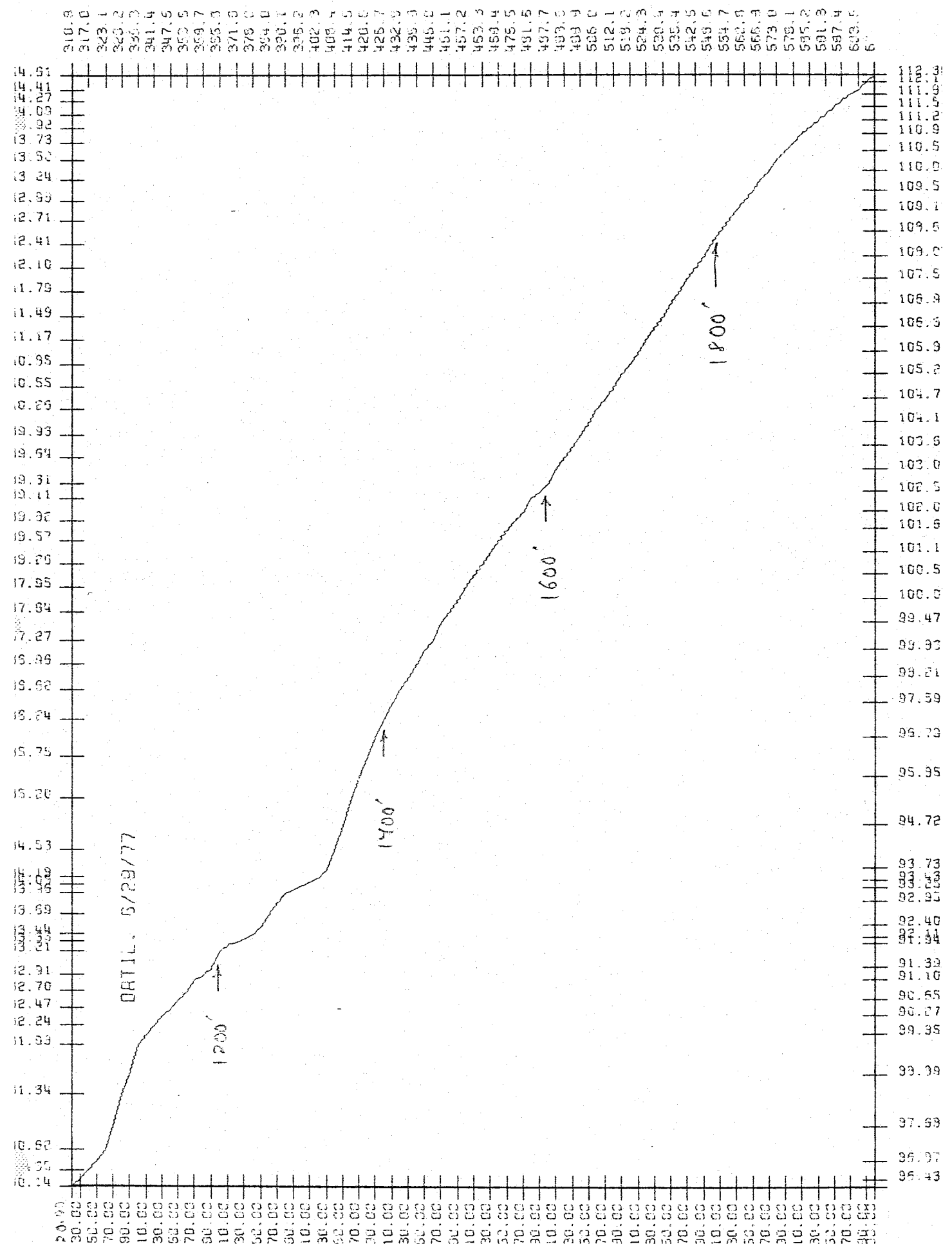
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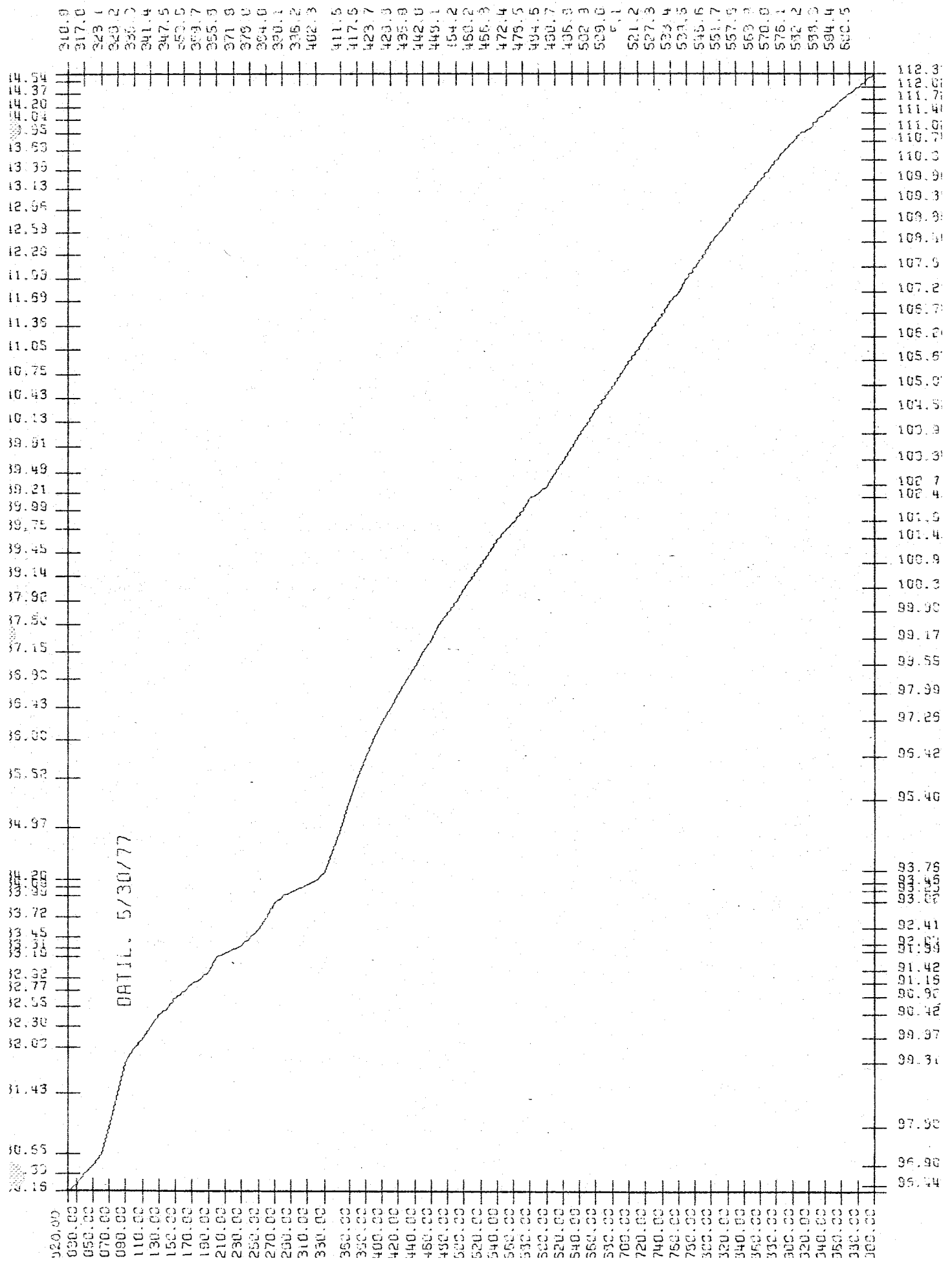
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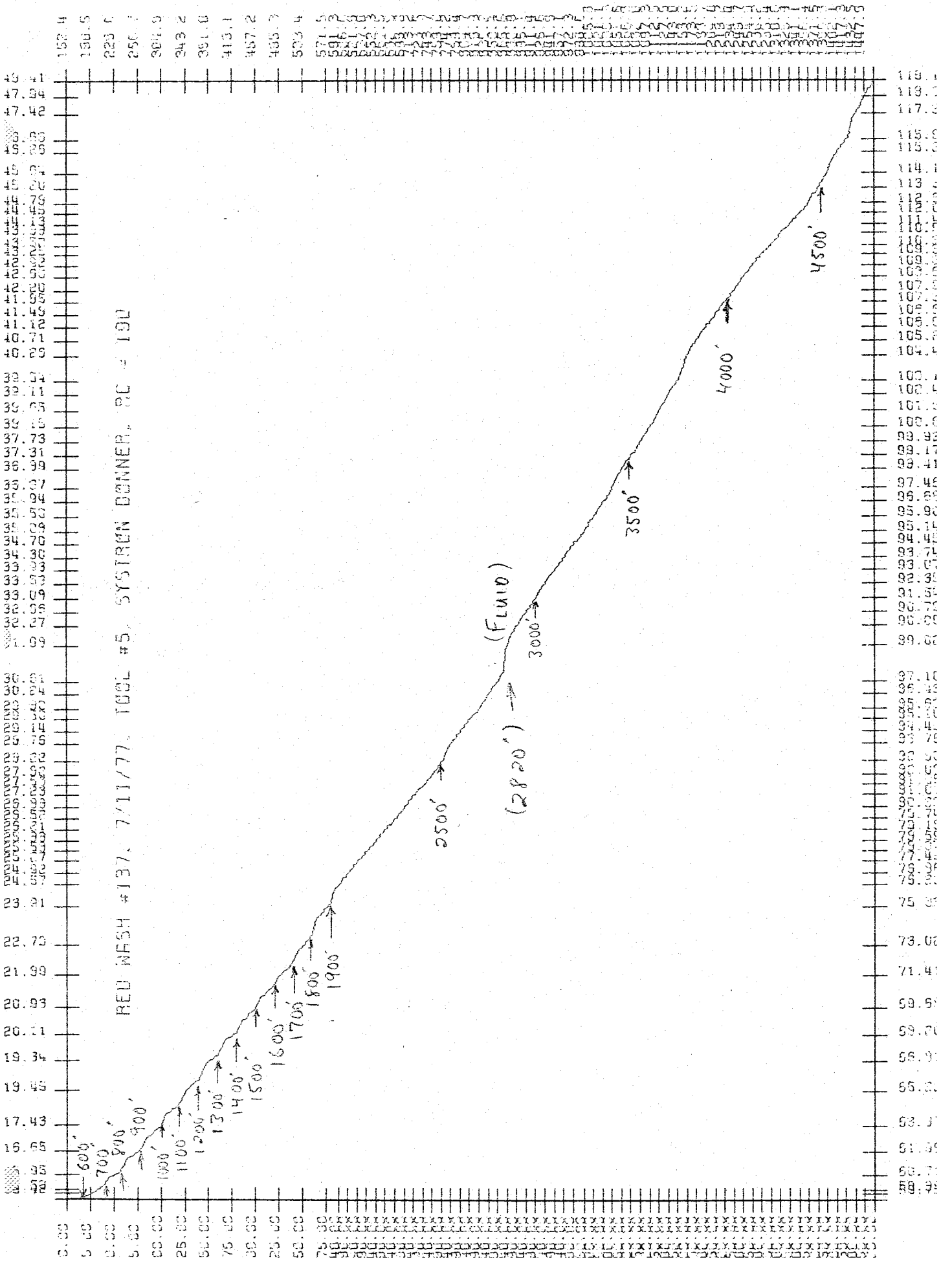
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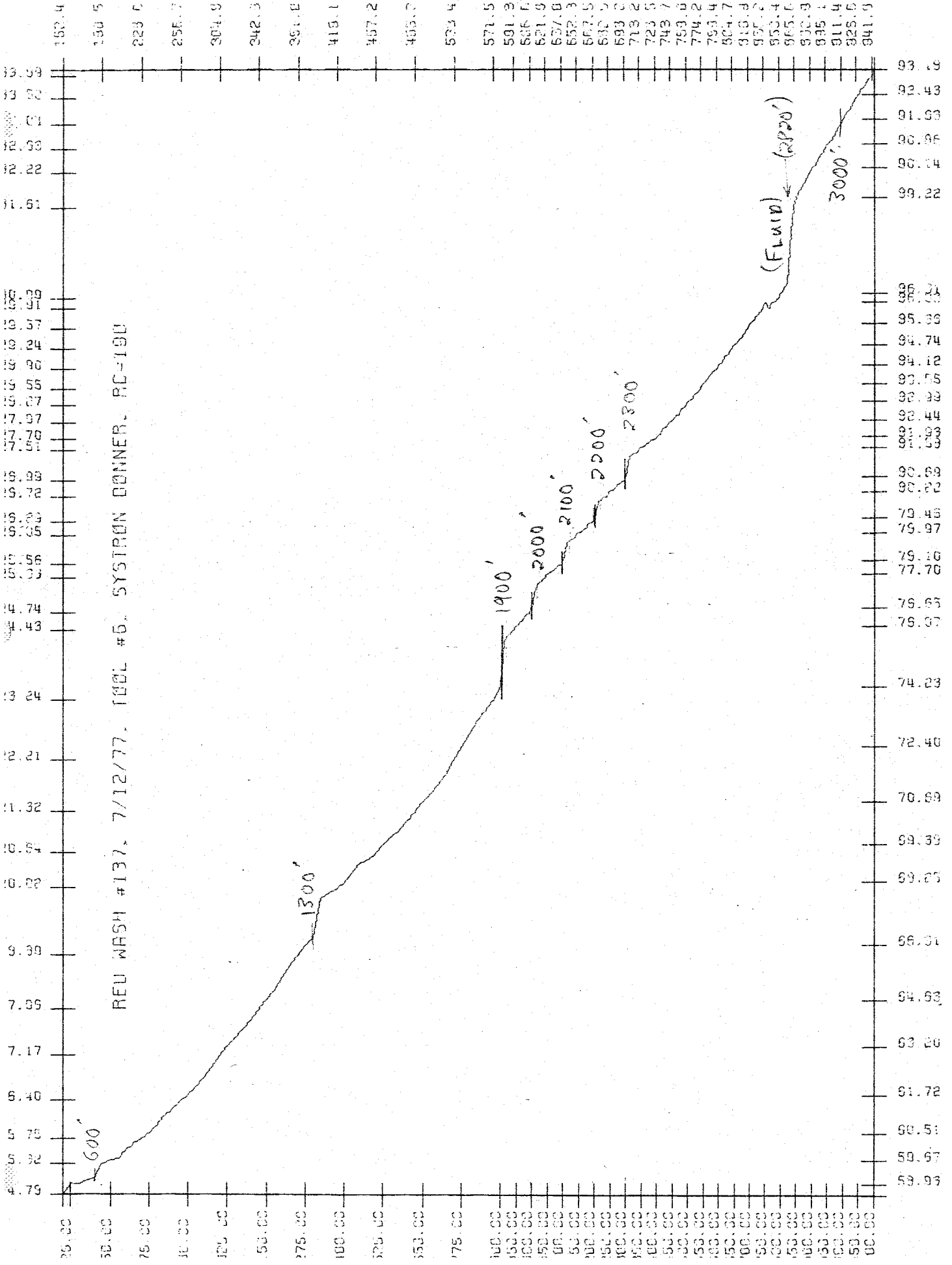
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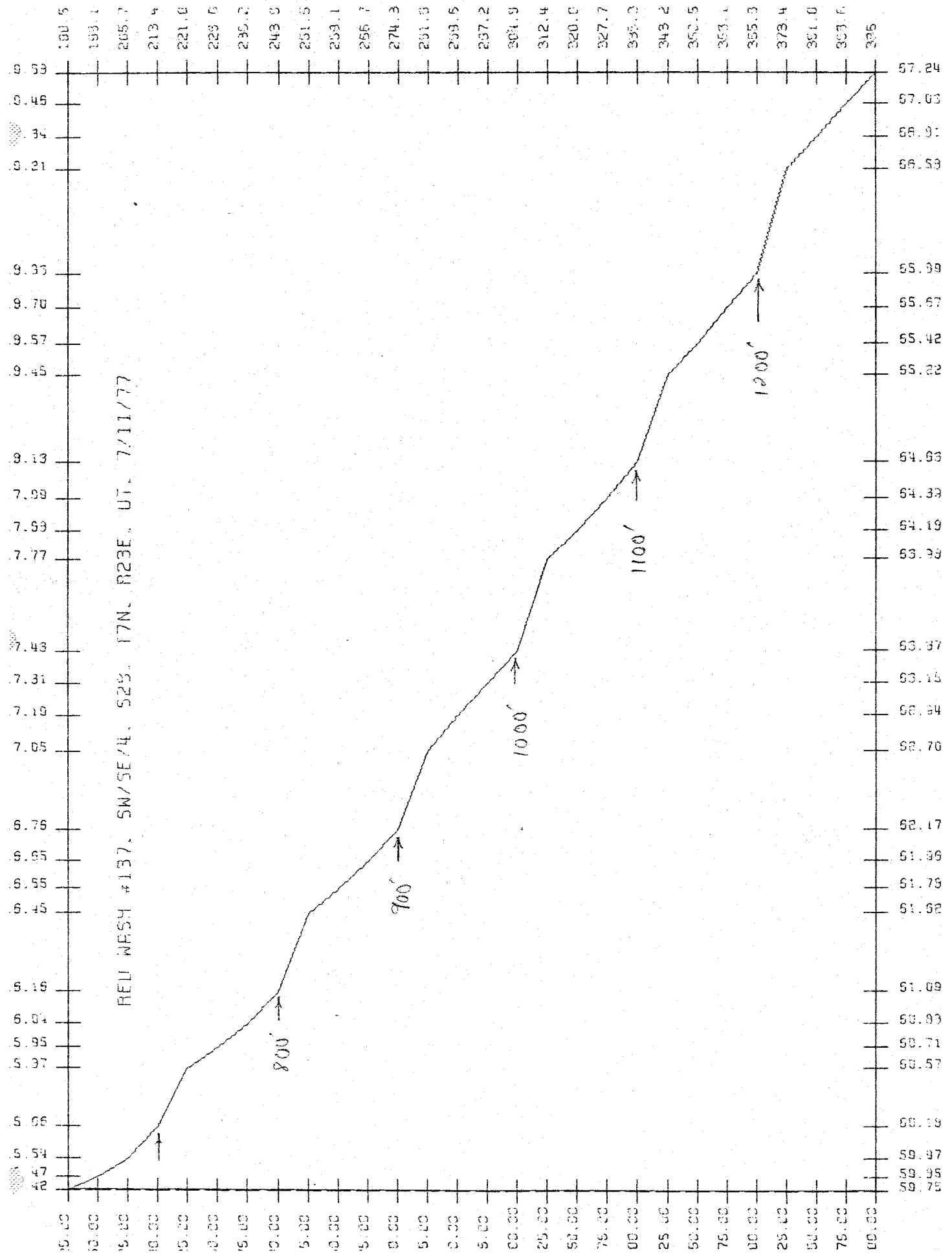
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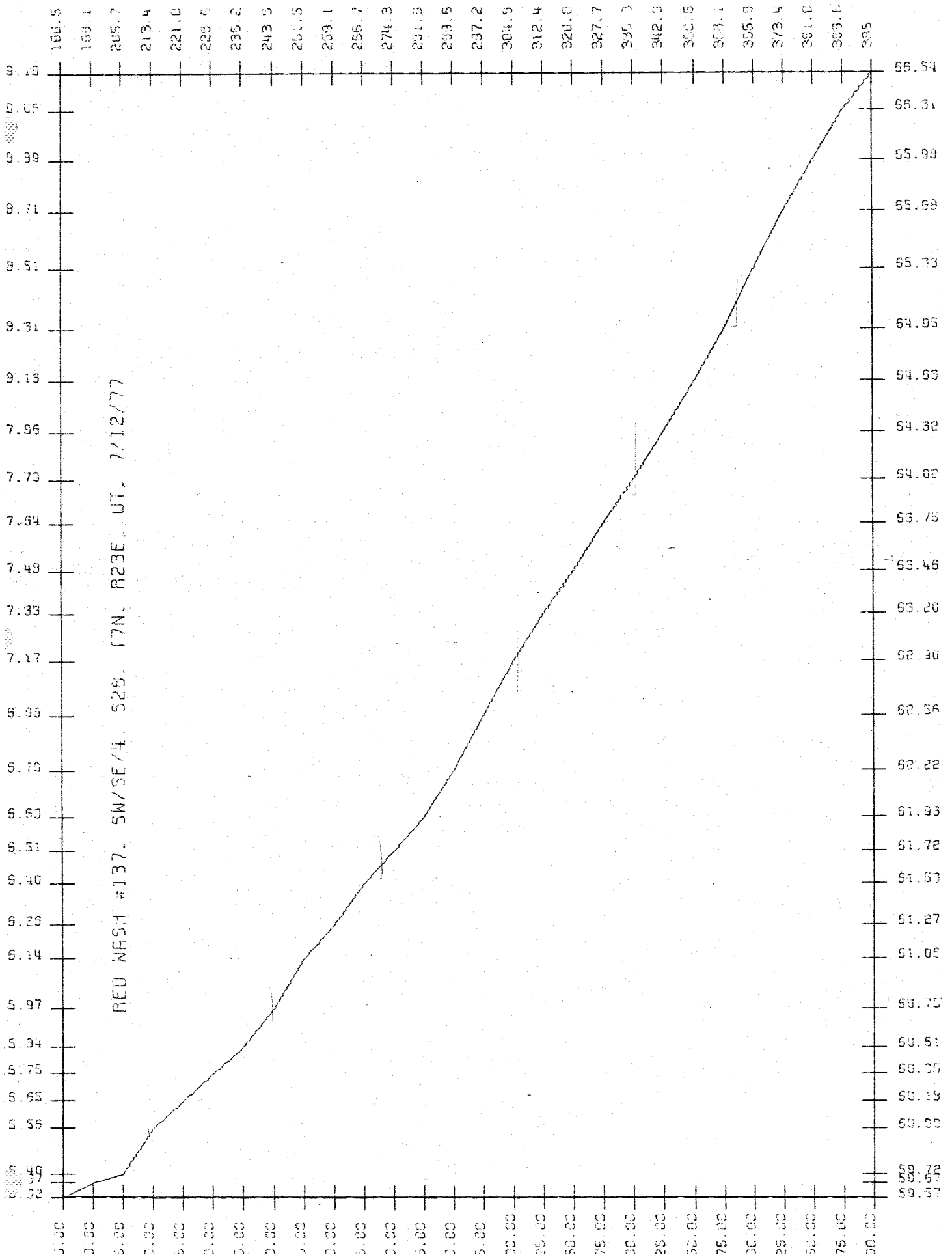
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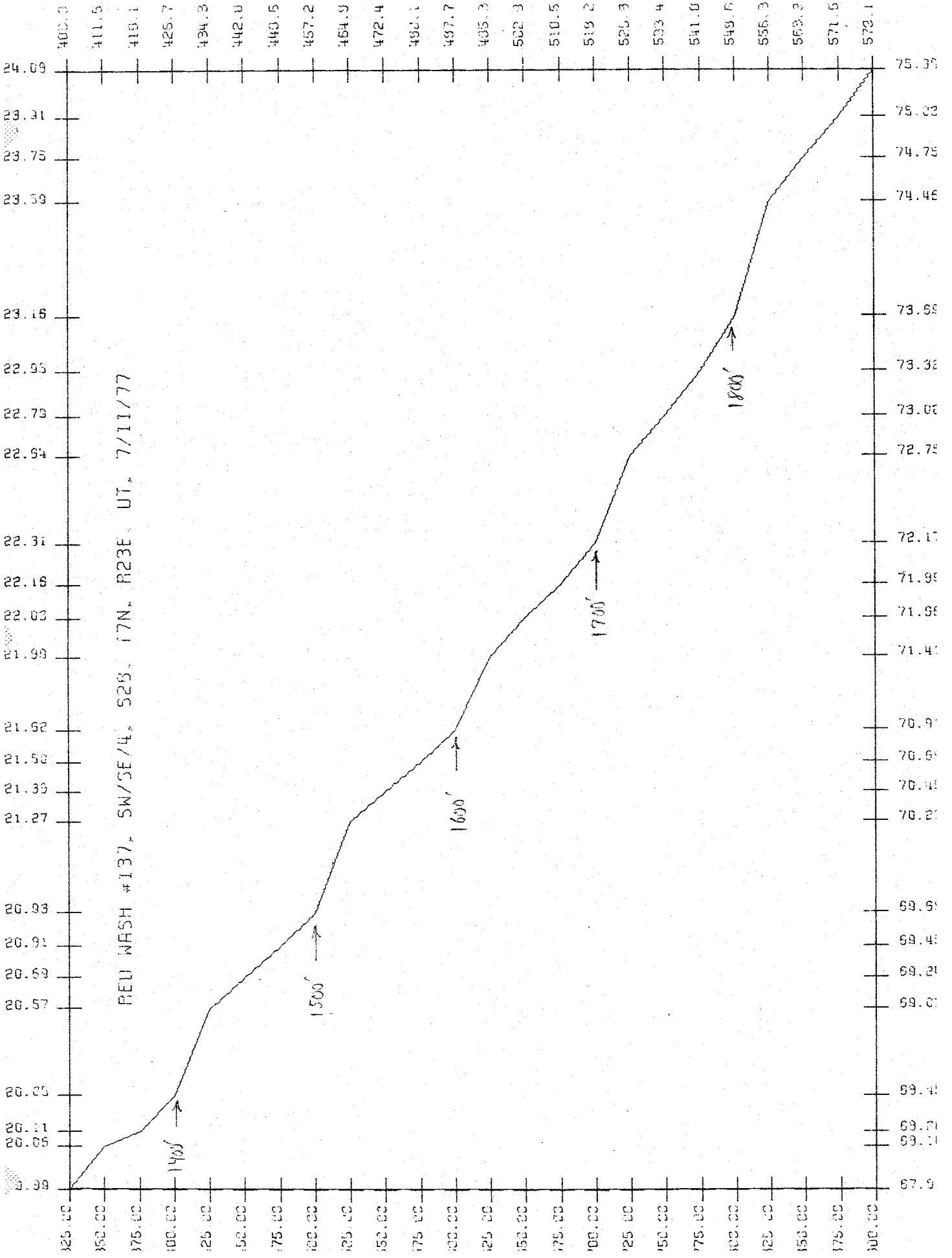


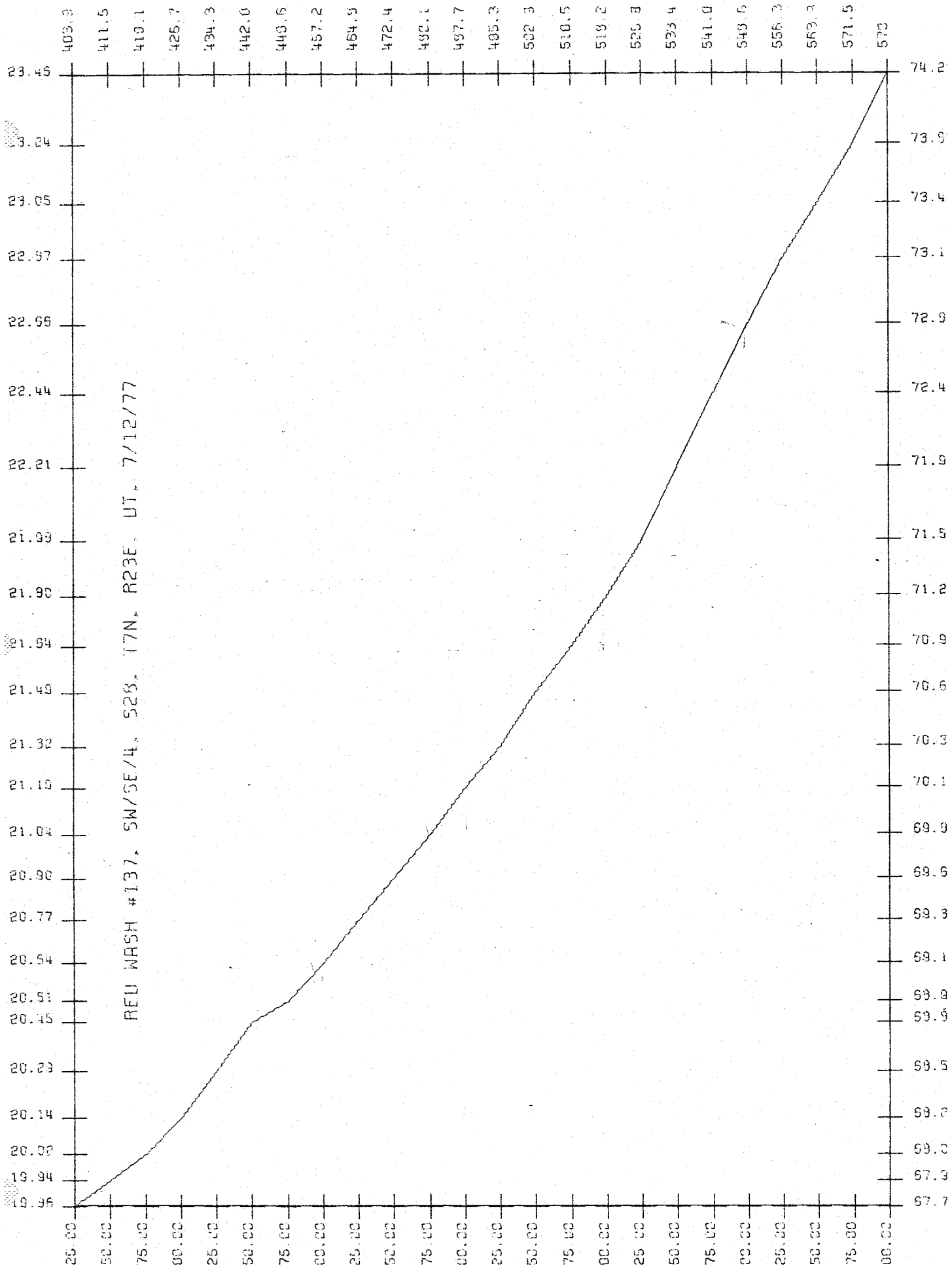
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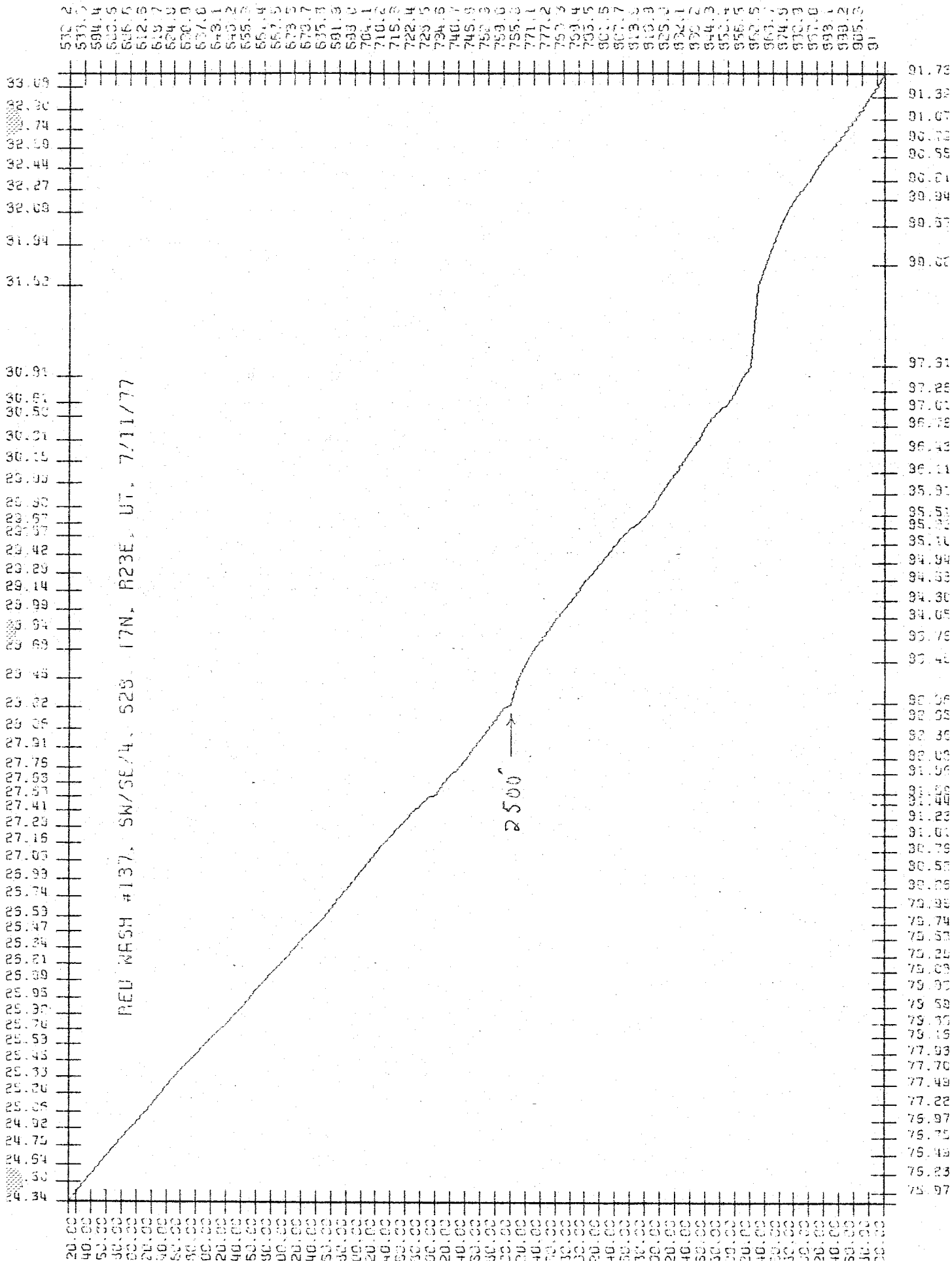




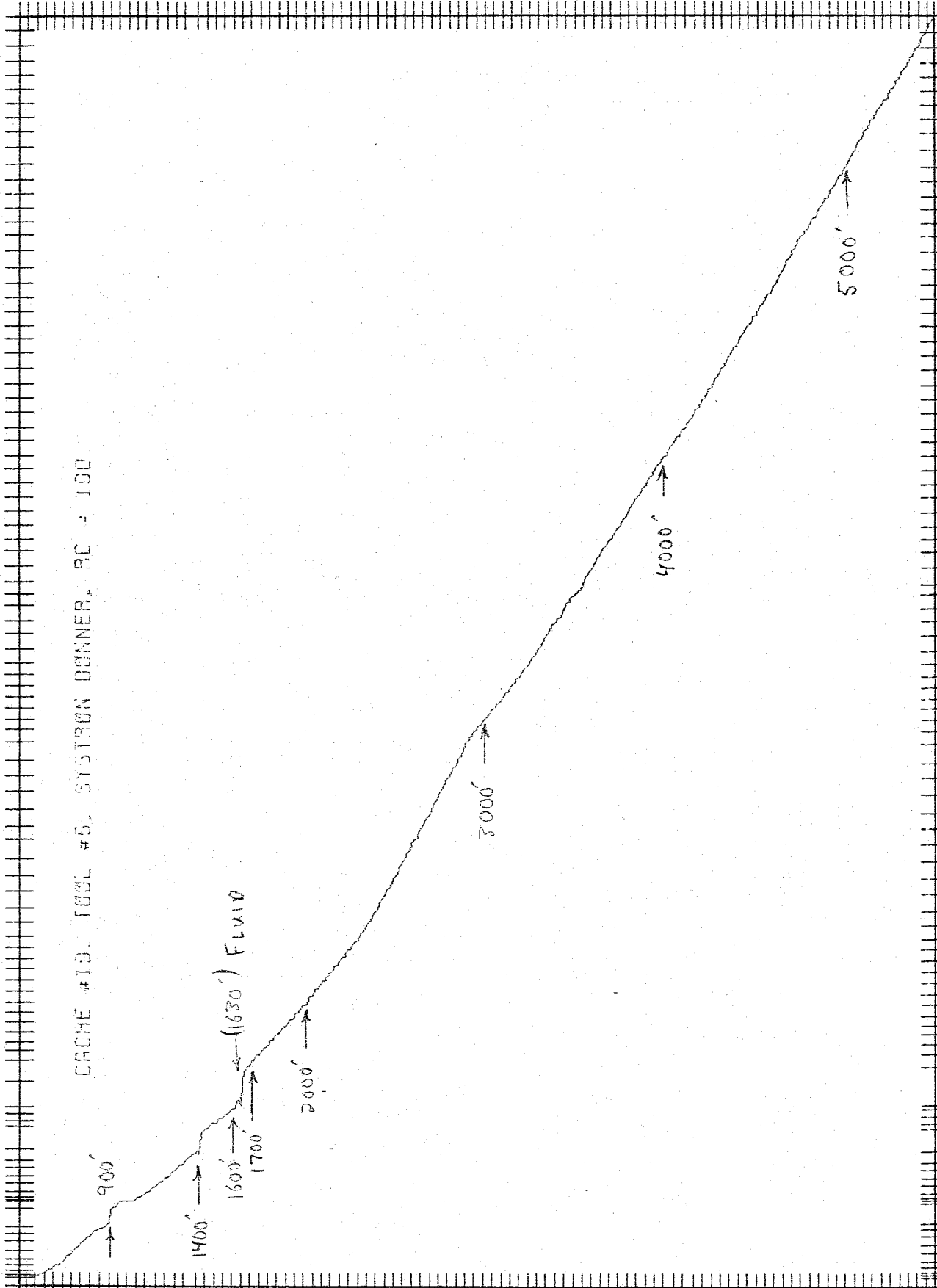








CACHE #10. TOOL #5. SYSTEM DINNER. RC = 100



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Table 1. Comparison of TD temperature to average temperature and final temperature in water.

	Cal Depth (ft)	TD Temp (°F)	Ave Temp (°F)	Final Temp (°F)	Time (min)	TD vs Ave (%)	TD vs Final (%)
Datil 6/29/77	250	63.77	63.86	63.89	6	-0.14	-0.19
	350	66.60	66.56	66.58	5	+0.06	+0.03
	450	69.68	69.61	69.64	5.5	+0.10	+0.06
	600	75.18	75.06	75.17	5	+0.16	+0.01
	800	81.46	81.55	81.61	4.5	-0.11	-0.18
	1000	86.03	85.96	85.97	6.5	+0.08	+0.07
	1200	91.81	91.79	91.78	9	+0.02	+0.03
	1400	97.07	97.29	97.36	11	-0.23	-0.30
	1600	102.77	102.77	102.76	5	0.00	+0.01
	1800	108.33	108.28	108.33	5	+0.05	0.00
	2000	112.29	112.23	112.34	4.5	+0.05	-0.04
Datil 6/30/77	2000	112.32	112.17	112.24	5	+0.13	+0.07
	2200	114.77	114.71	114.75	5	+0.05	+0.02
	2400	119.93	119.77	119.84	5	+0.13	+0.08
	2600	126.87	126.69	126.73	5	+0.14	+0.11
	2800	132.83	132.74	132.79	6	+0.07	+0.03
	3000	138.31	138.24	138.28	5	+0.05	+0.02
	3200	143.88	143.76	143.81	5	+0.08	+0.05
	3400	149.49	149.33	149.39	5	+0.11	+0.07
	3600	155.00	154.90	155.00	5	+0.06	0.00
	4600	182.38	182.29	182.35	5.5	+0.05	+0.02
Red Wash 7/11/77	3000	91.75	91.75	91.66	10	0.00	+0.10
	3500	99.16	99.05	99.11	7.5	+0.11	+0.05
	4000	107.33	107.22	107.13	5	+0.10	+0.19
	4500	113.37	113.34	113.40	5	+0.03	-0.03
	4800	119.12	118.96	118.96	5	+0.13	+0.13
Cache 7/14/77	1700	75.08	74.82	74.91	9	+0.35	+0.23
	2000	78.09	78.03	78.12	12	+0.08	-0.04
	3000	93.06	92.87	92.97	10	+0.20	+0.10
	4000	106.91	106.85	106.91	11	+0.06	0.00
	5000	121.86	121.76	121.89	10.5	+0.08	-0.02
	5500	129.85	129.91	129.99	16	<u>-0.05</u>	<u>-0.11</u>
Average Values:						+0.06	+0.02

Table 2. Estimating temperature at calibration points by linear regression of continuous data. Datil 6/29/77 and Datil 6/30/77 data in water.

Cal Depth (ft)	TD Temp (°F)	Contin Temp (°F)	Est Temp (°F)	Contin vs TD Temp (%)	Est vs TD Temp (%)	Est vs Contin Temp (%)
250	63.755	63.757	63.814	+0.003	+0.093	+0.089
350	66.596	66.617	66.648	+0.032	+0.078	+0.047
450	69.702	69.771	69.800	+0.099	+0.141	+0.042
600	75.180	75.217	75.283	+0.049	+0.137	+0.088
800	81.465	81.529	81.560	+0.079	+0.117	+0.038
1200	91.786	91.745	91.630	-0.045	-0.170	-0.125
1400	97.233	97.257	97.171	+0.025	-0.064	-0.088
1600	102.761	102.758	102.857	-0.003	+0.093	+0.096
1800	108.337	108.398	108.370	+0.056	+0.030	-0.026
		Average Values:		+0.033	+0.051	+0.018

Table 3. Time response of #4 probe at 1200 foot calibration point in water. Datil well. 6/29/77.

Time (min)	Temp (°F)
0	91.81
1	91.77
2	91.82
3	91.82
4	91.76
5	91.78
6	91.80
7	91.75
8	91.76
9	91.78

Table 4. Time response of #6 probe at 3000 foot calibration point in water. Red Wash well. 7/11/77.

Time (min)	Temp (°F)
0	91.75
1	91.64
2	91.57
3	91.70
4	91.72
5	91.72
6	91.62
7	91.70
8	91.69
9	91.68
10	91.66



Table 5. Time response of #6 probe at 3000 foot calibration point in water. Cache well. 7/14/77.

<u>Time (min)</u>	<u>Temp (°F)</u>
0.0	93.06
0.5	92.90
1.0	92.93
1.5	92.88
2.0	92.77
2.5	92.65
3.0	92.75
3.5	92.71
4.0	92.77
4.5	92.85
5.0	92.82
5.5	92.90
6.0	92.88
6.5	92.88
7.0	92.89
7.5	92.86
8.0	92.94
8.5	92.93
9.0	92.98
9.5	93.01
10.0	92.97

Table 6. Comparison of TD temperature to average temperature and final temperature in air.

	<u>Cal Depth (ft)</u>	<u>TD Temp (°F)</u>	<u>Ave Temp (°F)</u>	<u>Final Temp (°F)</u>	<u>Time (min)</u>	<u>TD vs Ave (%)</u>	<u>TD vs Final (%)</u>
Red Wash	500	58.59	58.99	59.04	15	-0.68	-0.76
7/11/77	600	59.53	59.70	59.72	15	-0.28	-0.32
7/12/77	700	60.15	60.30	60.43	15	-0.25	-0.46
	800	61.07	61.21	61.39	15	-0.23	-0.52
	900	62.17	62.27	62.43	15	-0.16	-0.42
	1000	63.38	63.54	63.71	15	-0.25	-0.52
	1100	64.65	64.77	64.94	15	-0.19	-0.45
	1200	65.89	66.08	66.26	15	-0.29	-0.56
	1300	67.23	67.38	67.53	15	-0.22	-0.44
	1400	68.43	68.58	68.75	15	-0.22	-0.47
	1500	69.66	69.82	69.99	15	-0.23	-0.47
	1600	70.88	70.96	71.12	15	-0.11	-0.34
	1700	72.18	72.24	72.39	15	-0.08	-0.29
	1800	73.71	73.83	74.07	15	-0.16	-0.49
	1900	75.35	75.34	75.54	14	-0.01	-0.25
	2000	76.63	76.84	77.10	15	-0.27	-0.61
	2100	78.10	78.27	78.50	15	-0.22	-0.51
	2200	79.43	79.49	79.75	15	-0.08	-0.40
	2300	80.67	80.81	81.10	15	-0.17	-0.53
Cache	400	63.16	63.64	63.68	15	-0.76	-0.82
7/14/77	900	66.51	66.57	66.93	15	-0.09	-0.63
	1400	70.13	70.37	70.80	15	-0.34	-0.96
						<u>-0.22</u>	<u>-0.46</u>

Red Wash Average Values:

Figure 14. Time response of #4 probe at 1200 foot calibration point in water. Datil well. 6/29/77.

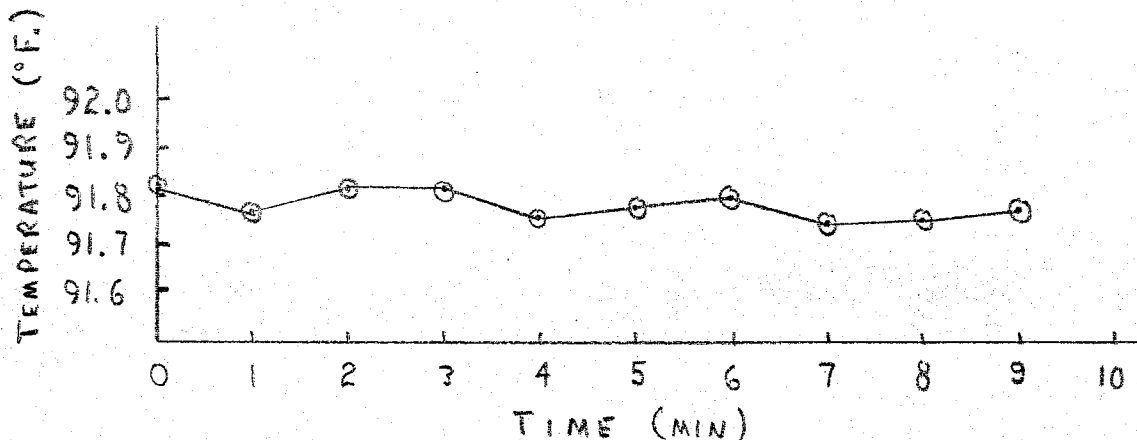


Figure 15. Time response of #6 probe at 3000 foot calibration point in water. Red Wash well. 7/11/77.

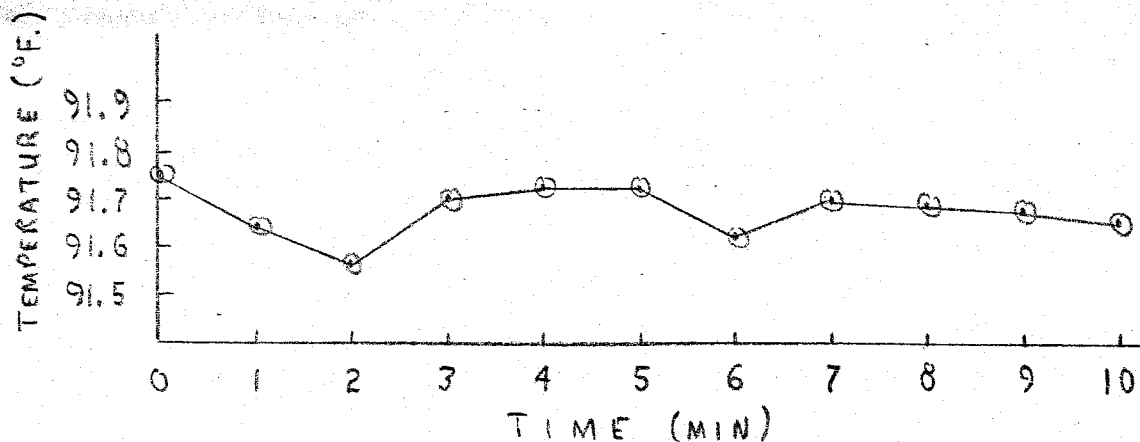


Figure 16. Time response of #6 probe at 3000 foot calibration point in water. Cache well. 7/14/77.

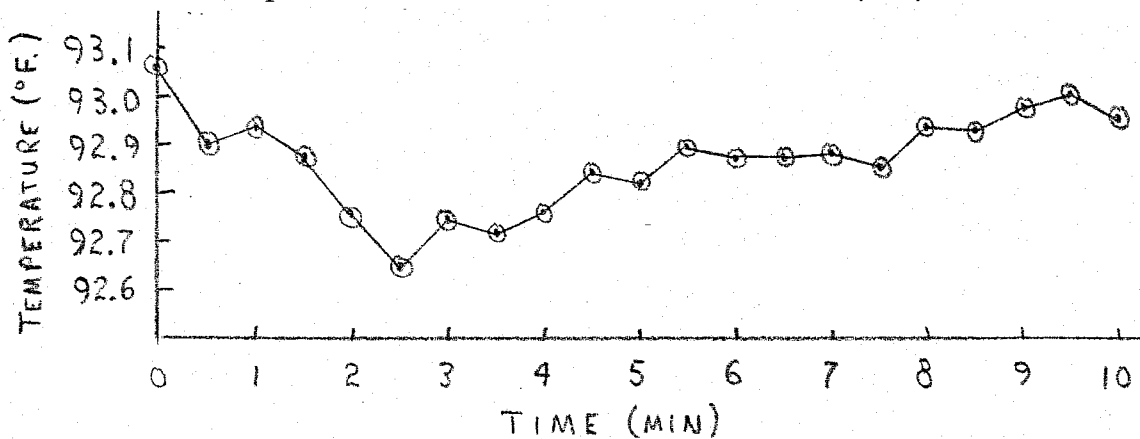


Table 7. Estimating temperature at calibration points by linear regression of continuous data. Red Wash 7/11/77 and Red Wash 7/12/77 data in air.

Cal Depth (ft)	TD Temp (°F)	Final Temp (°F)	Contin Temp (°F)	Est Temp (°F)
700	60.184	60.43	60.002	-
800	61.092	61.39	60.750	-
900	62.172	62.43	61.720	-
1000	63.374	63.71	62.900	-
1100	64.631	64.94	64.021	-
1200	65.887	66.30	65.326	-
1400	68.446	68.75	68.251	-
1500	69.680	69.99	69.143	-
1600	70.910	71.12	70.145	-
1700	72.167	72.39	71.247	-
1800	73.690	74.07	72.797	-
2000	76.650	77.10	76.970	76.983
2100	78.101	78.50	78.155	78.144
2200	79.446	79.75	79.291	79.300
2300	80.692	81.10	80.519	80.517

Table 7 (continued):

Cal Depth (ft)	Contin vs TD (%)	Contin vs Final (%)	Est vs TD (%)	Est vs Final (%)	Est vs Contin (%)
700	-0.302	-0.71	-	-	-
800	-0.560	-1.04	-	-	-
900	-0.727	-1.14	-	-	-
1000	-0.748	-1.27	-	-	-
1100	-0.944	-1.42	-	-	-
1200	-0.851	-1.47	-	-	-
1400	-0.285	-0.73	-	-	-
1500	-0.771	-1.21	-	-	-
1600	-1.079	-1.37	-	-	-
1700	-1.275	-1.58	-	-	-
1800	-1.212	-1.72	-	-	-
2000	+0.417	-0.17	+0.434	-0.15	+0.017
2100	+0.069	-0.44	+0.055	-0.45	-0.014
2200	-0.195	-0.58	-0.184	-0.56	+0.011
2300	-0.214	-0.72	-0.217	-0.72	-0.002
Ave:	-0.533	-0.95	+0.022	-0.47	+0.003

Table 8. Time response of #4 probe at 120 foot calibration point in air. Datil well. 6/29/77.

<u>Time</u> <u>(min)</u>	<u>Temperature</u> <u>(°F)</u>
0	58.35
1	58.45
2	58.50
3	58.56
4	58.64
5	58.69
6	58.71
7	58.72
8	58.73
9	58.76
10	58.76
11	58.79
12	58.84
13	58.88
14	58.91
15	58.95

Table 9. Time response of #6 probe at 1100 foot calibration point in air. Red Wash well. 7/11/77.

<u>Time</u> <u>(min)</u>	<u>Temperature</u> <u>(°F)</u>
0	64.65
3	64.60
6	64.73
9	64.81
12	64.88
15	64.94

Table 10. Time response of #6 probe at 900 foot calibration point in air. Cache well. 7/14/77.

<u>Time</u> <u>(min)</u>	<u>Temperature</u> <u>(°F)</u>
0	66.51
1	66.40
2	66.34
3	66.37
4	66.41
5	66.48
6	66.51
7	66.56
8	66.60
9	66.66
11	66.76
12	66.80
13	66.84
14	66.88

Figure 17. Time response of #4 probe at 120 foot calibration point in air. Datil well. 6/29/77.

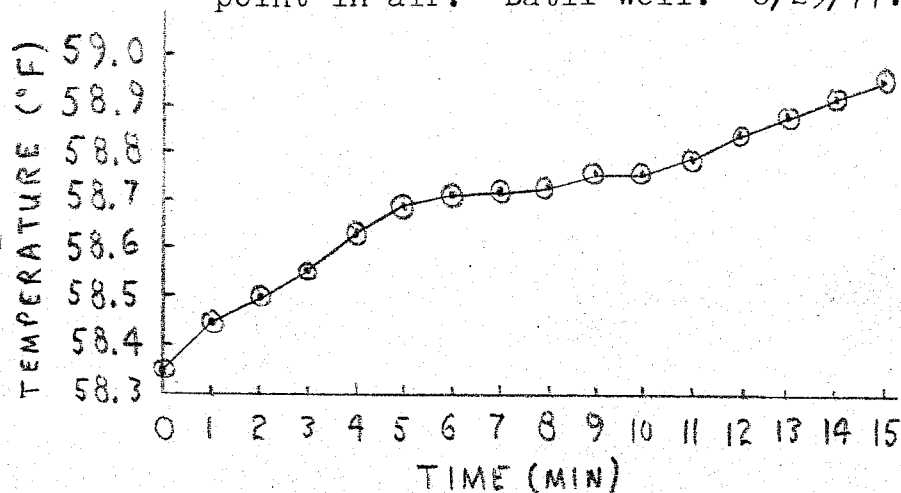


Figure 18. Time response of #6 probe at 1100 foot calibration point in air. Red Wash well. 7/11/77.

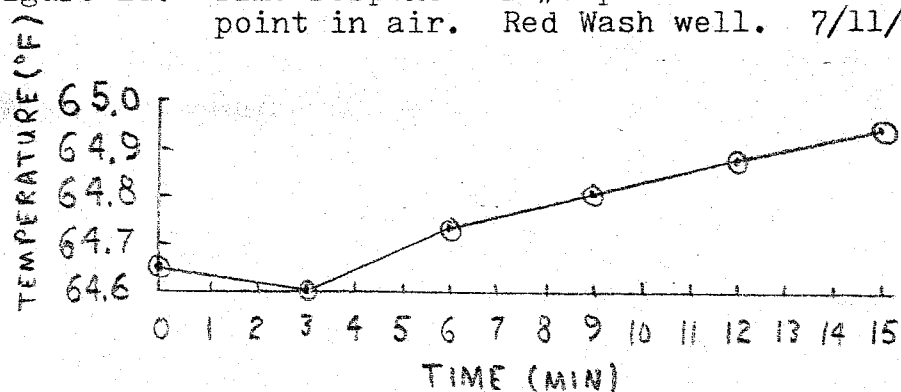


Figure 19. Time response of #6 probe at 900 foot calibration point in air. Cache well. 7/14/77.

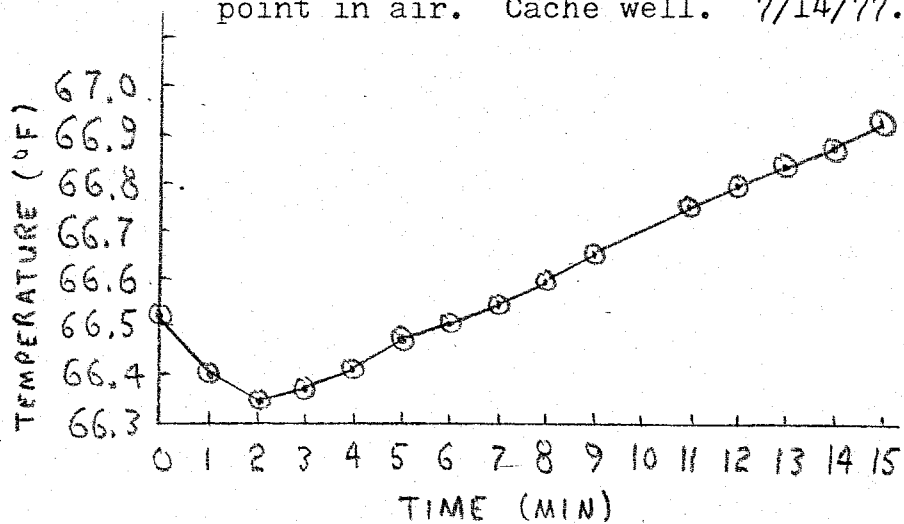


Figure 20. Equilibrium final temperature minus continuous temperature vs depth. Red Wash well. 7/11/77 and 7/12/77.

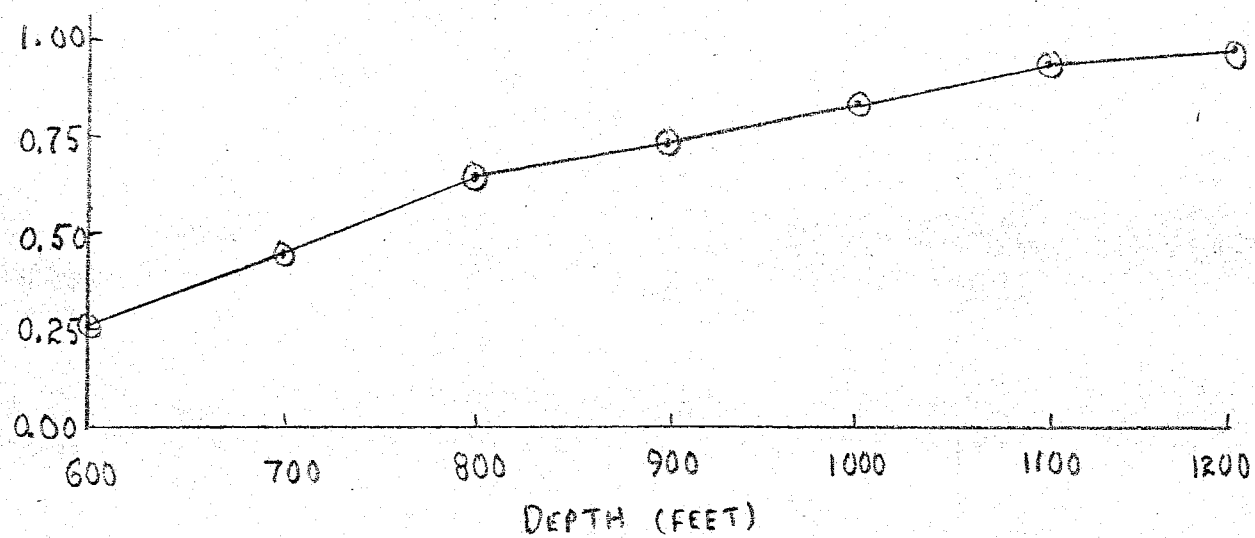
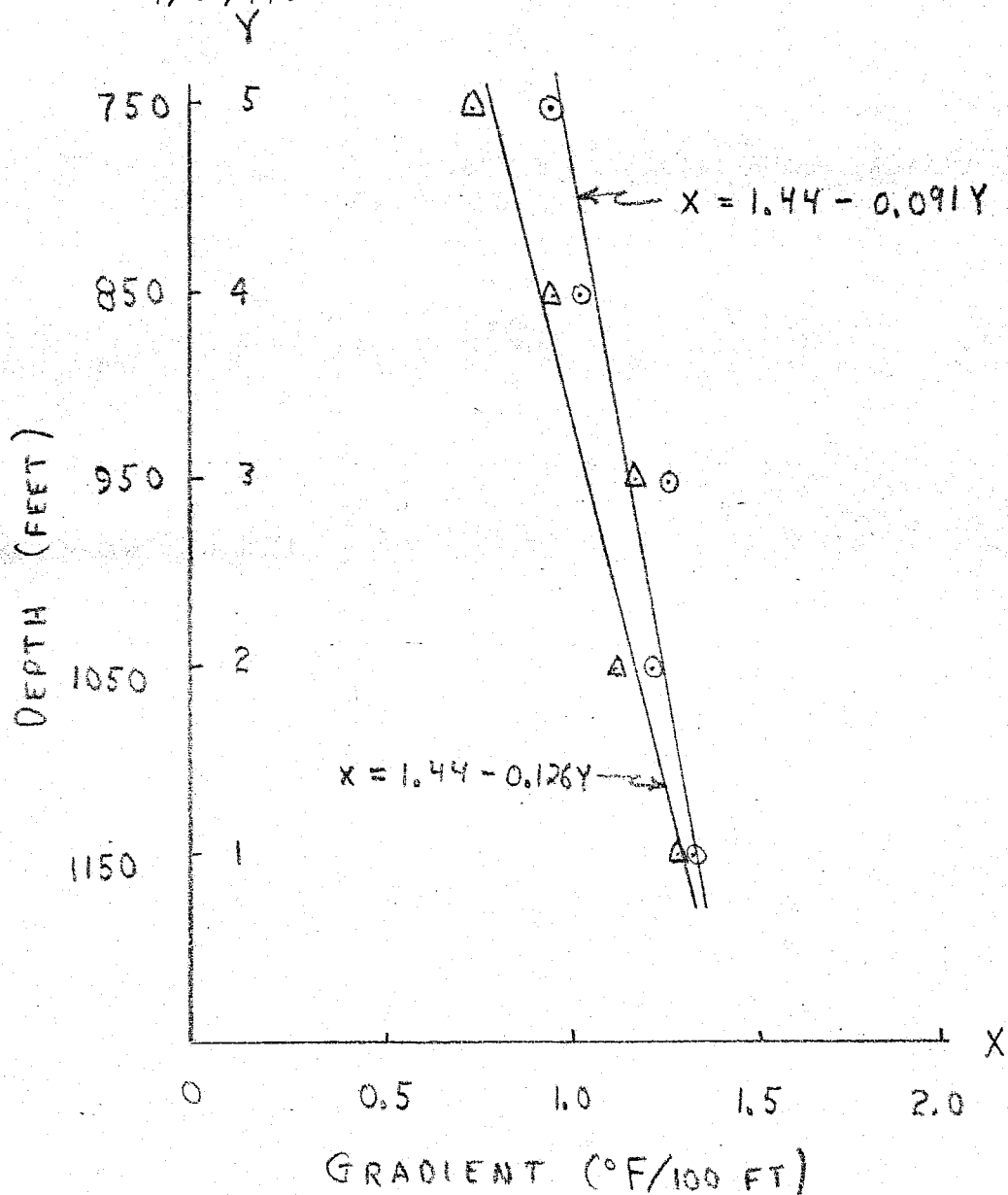


Table 11. Comparison of equilibrium gradient and continuous gradient in air. Red Wash well. 7/11/77 and 7/12/77.

<u>Depth (ft)</u>	<u>Continuous Temp Grad (°F/100 ft)</u>	<u>Equilib Final Temp Grad (°F/100 ft)</u>
700	0.7480	0.960
800	0.9700	1.040
900	1.180	1.280
1000	1.121	1.230
1100	1.305	1.320
1200		
Ave:	1.065	1.166
1400	0.892	1.24
1500	1.002	1.13
1600	1.102	1.27
1700	1.550	1.68
1800		
Ave:	1.136	1.33
2000	1.185	1.40
2100	1.136	1.25
2200	1.228	1.35
2300		
Ave:	1.183	1.33

Figure 21. Comparison of equilibrium gradient and continuous gradient in air. Red Wash well. 7/11/77 and 7/12/77.

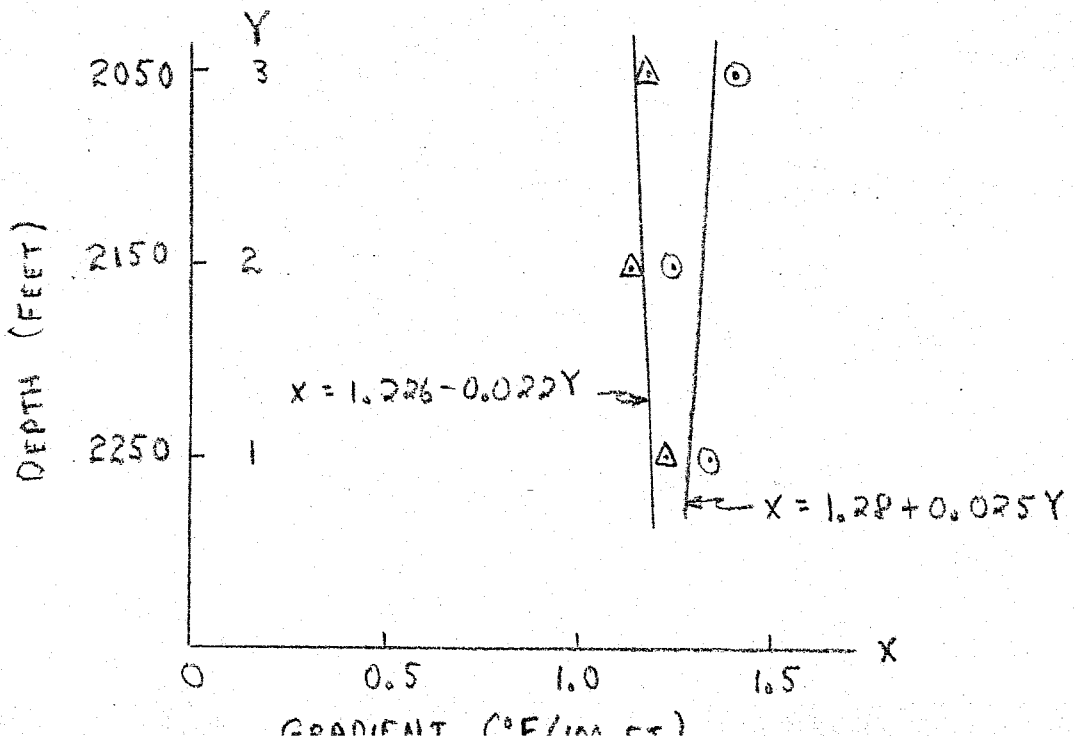
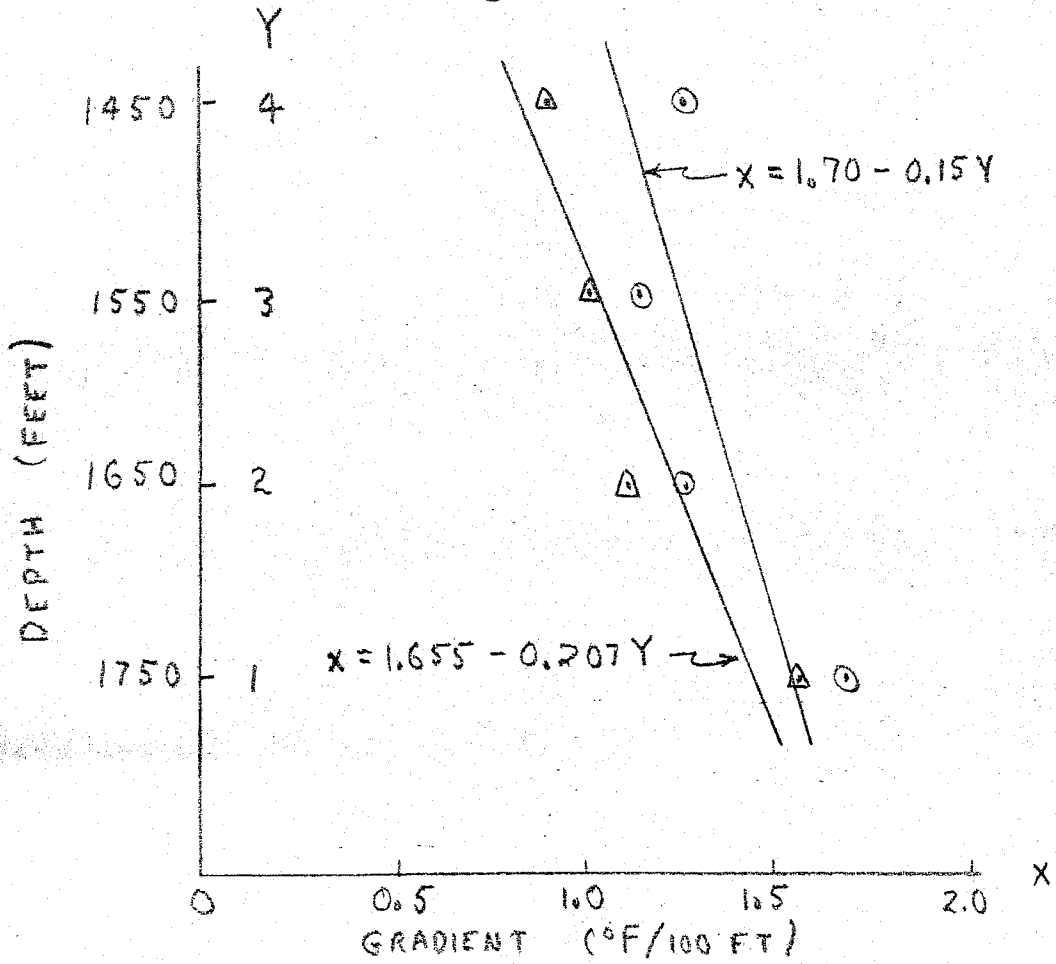


⊙ EQUILIBRIUM DATA

△ CONTINUOUS DATA



Figures 22 & 23. Comparison of equilibrium gradient and continuous gradient in air. Red Wash.



## RESULTS AND CONCLUSIONS

Water Level Determination

Continuous Mode. The water level is indicated for the Datil, Red Wash, and Cache wells on Figures 2, 5, and 13, respectively. The water level is apparent on a depth vs. temperature plot as a region of very gentle negative slope. This region represents a relatively large increase in probe temperature over a relatively small depth interval, which is interpreted by the computer program as a large temperature gradient. Thus, the water level may also be determined from the tabulations of temperature gradient. The water levels in the Datil, Red Wash, and Cache wells appear to be at 190 feet, 2820 feet, and 1630 feet, respectively. The temperature gradients for the Datil, Red Wash, and Cache wells at those depths are 281 °C/km, 291°C/km, and 213°C/km, respectively. The water level at the Red Wash well was verified by "shooting" the well.

It might be concluded from these data that the water level will be associated with an apparent temperature gradient of about 200°C/km to 300°C/km. This sudden gradient increase represents, of course, an artifact of the probe response rather than the actual temperature gradient in the well. If the probe temperature is considered to lag the well temperature when moving downhole at sixty ft/min in air but to quickly attain thermal equilibrium with the well in water, then a sudden transition in downhole environment from air to water would explain the observed gradient at the transition level.

Equilibrium Mode. The water level was observed at depths traversed in a continuous logging mode. A large temperature gradient also appears, however, at the calibration points that occur in air in the equilibrium mode, as seen in Figures 5 and 13. Similar gradient anomalies are not observed at the calibration points that occur in water, as may be noted in Figures 2, 5, and 13. These observations may indicate, on the one hand, that the probe is in thermal equilibrium with the well when traveling downhole at sixty ft/min in water. The probe absorbs very little additional heat from the well during the stationary calibration interval, thereby resuming its downhole travel after calibration without introducing a temperature increment that is due to its response time. On the other hand, the probe does not appear to be in thermal equilibrium with the well when traveling downhole at sixty ft/min in air. During the stationary calibration interval, the probe apparently continues to absorb heat from the well, thereby introducing a temperature increment in the first continuous reading following calibration. The large temperature gradient observed in air at a calibration point in the equilibrium mode, then, is due to the time constant of the probe rather than an actual gradient increase and does not indicate water level.

#### Water Data

TD Temperature vs. Final Temperature. Table 1 represents data compiled in an effort to evaluate the equilibrium method of logging in water. By comparing the equilibrium

data below the water level in the three wells, the following results were obtained: (1) The TD temperature was found to be 0.06% greater than the average temperature of the calibration period. (2) The TD temperature was found to be 0.02% greater than the final temperature of the calibration period. It may be concluded from these data that, in water, (a) the probe tends to cool slightly during the calibration period, and (b) the TD temperature may be used as a close approximation to the equilibrium temperature.

TD Temperature vs. Continuous Temperature. Table 2 represents a comparison between the equilibrium and the continuous methods of temperature logging. An "estimated temperature" was calculated at a given calibration depth in water for the Datil well by applying linear regression to the two adjacent depths both above and below the calibration depth. Averaging the results of the comparisons, it was found that (1) the temperature at the calibration depth in the continuous mode was 0.033% higher than the TD temperature at that depth, also (2) the estimated temperature at the calibration depth was 0.051% higher than the TD temperature at that depth, and finally (3) the estimated temperature at the calibration depth was 0.018% higher than the temperature observed at that depth in the continuous mode. These results seem to support the following conclusions: (a) A continuous temperature log in water may be expected to yield results that are about 0.03% higher than the TD temperatures of an equilibrium log, which, in turn, are 0.02% higher than the equilibrium temperatures. (b) The TD temperatures of

an equilibrium log may be predicted approximately from a continuous log.

Plot Comparison: Continuous vs. Equilibrium Logs.

Figure 3 represents an equilibrium log of the Datil well from 1020 feet to 2000 feet with an interval of 200 feet. It may be noted that readings were also taken within this interval every ten feet in a continuous logging mode.

Figure 4 represents a continuous log of the same section of the well taken about twenty-four hours later. By superimposing the two plots, it may be seen that the curves very nearly coincide. Thus, a graphical verification of the conclusion suggested by Table 2 has been obtained. That is, a continuous temperature log in water very closely approximates an equilibrium temperature log that is based on TD temperatures in water.

Probe Response. The above conclusion may be considered in terms of probe response by examining Tables 3, 4, and 5 and associated Figures 14, 15, and 16, respectively. These three sets of data show the time response of the probe at a stationary calibration point below the water level at around 92°F. in the three wells. Each plot displays a TD temperature that is slightly higher than the final temperature. This initial and final temperature difference was seen in the data of Table 1. Each plot displays a non-monotonic curve which is initially downward-going. That is, the curve represents an oscillation in temperature over a time interval. The above-mentioned two features were observed in nearly all plots of probe response in water for

the three wells. It may be concluded that an initially downward-going oscillating response and a final temperature that approaches but does not attain the TD temperature in a ten-minute time interval are very likely to be associated with a downhole water environment. Further, this characteristic response of the probe in water would seem to strongly indicate that the probe is very nearly in thermal equilibrium with the downhole environment at touchdown. This would imply that the probe is in thermal equilibrium as it is traveling downhole, assuming the rate of travel to be no greater than the sixty ft/min rate as used in acquiring the data presented in this paper.

The data that has been considered up to this point has been taken from below the water level and subjected to examination in terms of (a) TD temperature vs. final temperature, (b) TD temperature vs. continuous temperature, and (c) probe response. These same considerations will next be applied to the data that were obtained above the water level, that is, in the air column.

#### Air Data

TD Temperature vs. Final Temperature. Table 6 represents a means of evaluating the equilibrium temperature logging method in air. It was found that the average TD temperatures for the Red Wash well were 0.46% lower than the final temperature and 0.22% lower than the average temperatures. It was also determined that the average TD temperatures for the Cache well, for which there were only

three useable calibration points in air, were 0.80% lower than the final temperatures and 0.40% lower than the average temperatures. These data might be explained by the concept of a probe which continues to absorb heat from the well during the calibration interval. It may therefore be concluded that the probe was not in thermal equilibrium with the well in an air column at touchdown. The average temperature appears to be about midway between the TD temperature and the final temperature for both wells. This may indicate that the probe was experiencing a linear increase in temperature during the fifteen-minute calibration interval. It may also be concluded that the probe had not attained thermal equilibrium at the end of the fifteen-minute calibration interval.

TD Temperature vs. Continuous Temperature. Table 7 represents a comparison between the equilibrium and continuous methods of temperature logging in air. An "estimated temperature" was calculated only for those calibration depths that corresponded to depths at which the continuous logging interval was ten feet. Since data above 2000 feet was taken at twenty-five foot intervals, which would seem to reduce the meaning of predicted temperatures based on linear regression to such widely spaced points, predicted (or estimated) temperatures occur in the table only below 1800 feet. It was found that the continuous temperature was about 0.5% lower than the TD temperature and about 1.0% lower than the final temperature. It would not seem to be appropriate to draw conclusions based on these particular

observations, however, because the equilibrium temperatures obtained at the calibration depths of the two successive logging days do not coincide. For example, at 600 feet on the first day at Red Wash, a final temperature of  $59.72^{\circ}\text{F}$  was recorded while at the same depth on the second day, a final temperature of  $59.45^{\circ}\text{F}$  was attained. In contrast to this situation, the data recorded below the water level at Red Wash show a temperature of  $91.70^{\circ}\text{F}$  after seven minutes at 3000 feet on the first day and a temperature of  $91.69^{\circ}\text{F}$  after seven minutes at 3000 feet on the second day. Therefore, a comparison between the continuous data of the second day and equilibrium data of the first day in terms of absolute temperatures was found to be possible only in water.

Plot Comparison: Continuous vs. Equilibrium Logs. The same problem in comparing the continuous data with the equilibrium data in air may be observed graphically by considering the Red Wash data plots through three sections of the air column. Figure 7 is an equilibrium log from 625 feet to 1300 feet. Figure 8 is a continuous log through the same section. Comparison of these two plots by superposition is not meaningful because the horizontal scales represent different total temperature intervals while the vertical scales represent equal depth intervals. That is, the initial reading on the first day was  $59.75^{\circ}\text{F}$ . The final reading was  $67.24^{\circ}\text{F}$ , resulting in a total temperature interval of  $7.49^{\circ}\text{F}$ . The initial reading on the second day was  $59.57^{\circ}\text{F}$ . The final reading was  $66.54^{\circ}\text{F}$ , resulting in a total temperature interval for the second day of  $6.97^{\circ}\text{F}$ .



The vertical scales on both plots, however, represent total depth intervals of 675 feet. It is therefore not meaningful to superimpose the two plots in an attempt to compare the continuous data with the equilibrium data. Figures 9 and 10 are equilibrium and continuous logs, respectively, from 1325 feet to 1900 feet. Comparison between the two plots of the continuous and equilibrium data is not appropriate for the reasons mentioned above. Figures 11 and 12 are equilibrium and continuous logs, respectively, from 1910 feet to 3000 feet. Again, plot comparisons are not meaningful in this case for reasons indicated above. It may be concluded that it is not possible to evaluate the continuous method of temperature logging relative to the equilibrium method in air based on the TD temperature data vs. continuous temperature data as presented in Table 7 and in Figures 7 through 12.

Probe Response. It may be possible to relate the time response of the probe in air to the above-mentioned difficulty of obtaining compatible data on separate logging days. Tables 8, 9, and 10 and associated Figures 17, 18, and 19 represent the time response of the probe in air in the three wells. These three particular response curves were selected as being characteristic of the response curves of each of the three wells. Figure 17 shows a monotonic increase in temperature from the TD temperature at a generally decreasing rate. The difference between final and TD temperature over a fifteen-minute interval was  $0.60^{\circ}\text{F}$ . Figure 18 shows an initial three-minute cooling trend followed by a monotonic increase in temperature at a generally decreasing rate.

The initial cooling trend in air was generally observed only at calibration depths below 700 feet in the Red Wash well. The difference between final and TD temperature over a fifteen-minute interval was  $0.29^{\circ}\text{F}$ . Figure 19 shows an initial two-minute cooling trend followed by a nearly linear increase in temperature. The initial cooling trend in air was observed only at calibration depths below 400 feet in the Cache well. The difference between final and TD temperature over a fifteen-minute interval was  $0.42^{\circ}\text{F}$ . Thus, the monotonically increasing response curve seems to be characteristic of the probe response in air. The initial cooling trend appears to be depth-dependent. It may also be concluded from these data that the probe is not in thermal equilibrium with the well in air at touchdown. Furthermore, it is not in thermal equilibrium with the well after fifteen minutes at a calibration depth. The problem of obtaining compatible data in air on successive logging days in the same well, then, seems to be related to the problem of achieving thermal equilibrium at a given calibration depth.

#### Offset between Continuous and Equilibrium Temperatures.

The problem of comparing the continuous logging method to the equilibrium logging method in air may be approached in terms of temperature differences instead of absolute temperatures. Figure 20 is a plot of the difference between the equilibrium final temperature and the continuous temperature vs. depth for the upper part of the air column of the Red Wash well. The difference between the two temperatures

is observed to increase with depth at a decreasing rate. While the plot does not appear to provide conclusive evidence, it does suggest perhaps the possibility that a constant difference is eventually attained between the continuous and equilibrium temperatures.

Temperature Gradients. The above possibility may be pursued in terms of the temperature gradients observed with the two logging methods. If the gradient obtained using the continuous method approaches and becomes equal to the gradient observed using the equilibrium method, then a constant temperature offset results. Table 11 represents gradients calculated for the two methods through three air sections of the Red Wash well. Figures 21, 22, and 23 are plots of these data showing the regression lines of X on Y and their slopes. It may be observed from these data that (1) the gradient of the continuous log is generally less than the gradient of the equilibrium log, (2) the gradients generally tend to increase with depth within each section and across sections, (3) the gradient obtained in the continuous mode increases with depth at a higher rate than the equilibrium gradient, and (4) the gradients obtained by the two methods approach a common gradient value. Observation #1 might be explained by considering that, between two given calibration depths, the probe in the equilibrium mode undergoes a component of temperature increase which the probe in continuous mode does not experience. That is, in equilibrium mode a temperature increment occurs between the touchdown temperature and the final temperature which is nonexistent in

the continuous mode. Observation #2 may provide evidence for a geothermal gradient at Red Wash that increases moderately from 700 feet to 1200 feet, continues to increase but at a higher rate from 1400 feet to 1800 feet, then remains at a nearly constant value from 2000 feet to 2300 feet. Observation #3 is equivalent to noting that the change between successive temperature increments for the continuous mode is greater than it is for the equilibrium mode. This might be explained in terms of an equilibrium time response which is superimposed upon the dynamic response of the probe as it is traveling downhole. The data under consideration here, however, do not provide sufficient evidence to support such a mechanism. Observation #4 is a direct result of observation #3. Extrapolation of the converging curves to a common gradient raises the question of whether the curves subsequently diverge or proceed with a common slope. It may be concluded from the preceding four observations that the gradient data presented here is insufficient for purposes of evaluating continuous temperature data with respect to equilibrium temperature data in air.

#### DISCUSSION

Water Level. A second method of determining water level may be briefly mentioned here. As a means of verifying the water level obtained in a downhole mode, the uphole temperature data may be examined for a temperature reversal. This refers to a short heating trend that occurs within the overall cooling trend of the uphole data and may be considered

to be a direct result of the change in the thermal properties of the media surrounding the probe. Thus, as the probe leaves the water, its thermal inertia causes it to heat slightly as its rate of cooling suddenly acquires a reduced value in air.

Downhole temperature reversals were noted in the Red Wash (Figure 6) and Cache wells (Figure 13) immediately above the water level. The reversal was not obtained, however, on successive days in the Red Wash well (Figures 11 and 12). The relation, if any, of the reversal to the water level therefore remains questionable although it may merit further investigation over a broader data base.

Water Data. The data obtained in water appears to be fairly conclusive with respect to an evaluation of the continuous logging mode vs. the equilibrium logging mode. The continuous logging method may be considered to provide results that are no greater than 0.03% of the TD temperatures obtained in the equilibrium mode in water. Considering that the continuous method is a more efficient logging technique in terms of logging time, it is to be preferred over the equilibrium method.

The primary source of error that is unique to the continuous mode lies in the operator error associated with activating the temperature recording device at the proper depth interval. If this error is  $\pm 1$  foot, then an error of  $\pm 0.01$  °F is possible. This source of error may be practically eliminated, however, by automating the triggering process.

Air Data. The data obtained in air does not provide conclusive evidence for interpreting and evaluating the continuous logging mode. One difficulty with this lies in the incompatibility of data for successive days of logging. The reason for the non-coincidence of temperatures at calibration depths between days may be related to the ease with which an air column may be disturbed by the logging process. Further study of this aspect of the problem, perhaps in terms of convection cells in air, would seem to be quite complex and theoretical.

A possibly promising approach to interpreting temperature data in air may lie in further study of the time response of the probe. Data was obtained in the present study for the Red Wash well which indicated that the temperature continued to increase, after an initial thirty-second cooling period, as long as thirty-nine minutes after touchdown at 1300 feet. It may be useful to extend the time interval at the calibration depths sufficiently to observe the complete response of the probe. Alternatively, a time constant for the probe might be experimentally determined by observing the time response of the probe to a step function of temperature in the laboratory. A knowledge of the probe response may provide a means of interpreting a continuous temperature log in air by using a deconvolution process of extracting the actual downhole temperature data from the observed data.

Subtle difficulties may be involved in determining the response characteristic of the probe in air. It is conceivable that the temperature vs. time curve may not

approach an asymptotic value but continue to absorb heat from nearby sources such as the lead weights that are mounted above the probe on the cable. Another such difficulty may be indicated by existing probe response data in air for the wells mentioned in this paper and for other wells. That is, the probe response in air may be dependent upon well geometry factors, including the effects of casing, tubing, and well-bore diameter. Further consideration must be given to these factors if the interpretation of either continuous or equilibrium temperature logging data in air for a given well is to be possible.

The most promising approach to interpreting temperature data in air would seem to be that involving temperature gradients rather than absolute temperatures. If the continuous gradient approaches the value of the equilibrium gradient in air, as evidence presented in this paper seems to indicate, then the equilibrium log may be related to the continuous log and the true gradient may be determined from either one. The longest section through which the two logs may be compared using the present data is 500 feet. The section is too short to provide sufficient evidence for equal gradients, indicating the need for further data in air through a longer depth interval.