

**Variation of P & S Wave
Velocities Before Earthquakes**

By

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ABSTRACT

In this study, predetermined P arrival times were used in conjunction with measured S-P intervals in an effort to detect any significant trends in Vp/Vs ratios preceding earthquakes of magnitude 0.3 or greater.

Records of 47 events, taken from a previous study by Sanford, Budding et al. (1972), were investigated. These events originated in the Rio Grande Rift Zone 20 kilometers north of Socorro, New Mexico at approximately $34^{\circ}13'N$, $106^{\circ}51'W$. They were recorded at four stations, centrally located around the events and at a maximum of 35 km. from the events.

Vp/Vs is plotted with time showing the changes in their ratios before the higher magnitude events. There is a definite increase of the Vp/Vs ratio preceding the higher order events and a decline in this ratio when they occur. These findings do not support the work of Aggarwal, Sykes et al. (1973).

INTRODUCTION

Changes in the ratio of seismic P and S wave velocities have received considerable attention as an effective method of the prediction of earthquakes, and according to Aggarwal, Sykes et al. (1973), have given highly successful results. These changes in P and S wave velocities are a result of dilatation as rock stresses increase. During dilatation, microfractures and cracks open up in the rock and slow down seismic waves since they need rigidity for propagation. These cracks begin to fill with water, thereby increasing the velocity of the waves. Nur and Simmons (1969) have found that Vs is not affected by the introduction of water into the cracks, and that Vp is affected if the pores are in the form of cracks and not in the form of round holes. This water flowing into the rock weakens the rock by increasing the effective stress and the rock eventually fails, causing an earthquake. The more stress applied to the rock, the larger the volume dilated, and the longer the time it takes to fill with water.

Semenov (1969) has found that the size of the earthquake is independent of the variation of Vp/Vs, but is dependent on the time that the lowered Vp/Vs ratio remains in effect. The longer the duration, the larger the event is likely to be.

By monitoring the Vp/Vs ratio through microearthquakes and the time span of these lowered ratios, it should be possible to predict earthquakes of higher magnitudes.

THEORY

The graph of P arrival time vs. the S-P interval indicates the following relations:

$$T = D/V \quad (T = \text{travel time})$$

$$S-P = D/V_s - D/V_p$$

$$S-P = D(1/V_s - 1/V_p)$$

$$S-P = D(V_p/V_s V_p - 1/V_p)$$

$$S-P = D/V_p (V_p/V_s - 1)$$

$$S-P = T_p (V_p/V_s - 1)$$

$$\frac{S-P}{T_p} = (V_p/V_s - 1)$$

$$\text{Slope} = (V_p/V_s - 1) \quad [\text{Formula 1}]$$

The theoretical velocity for P & S waves in an isotropic, homogeneous, linearly elastic substance is

$$V_p = \sqrt{\frac{E(1-\nu)}{\rho(1-2\nu)(1+\nu)}}$$

$$V_s = \sqrt{\frac{E}{2(1+\nu)}}$$

where E is Young's Modulus, ρ is density, and ν is poisson's ratio.

Solving for V_p/V_s ,

$$(V_p/V_s)^2 = \frac{\frac{E(1-\nu)}{\rho(1-2\nu)(1+\nu)}}{\frac{E}{2\rho(1+\nu)}}$$

$$(V_p/V_s)^2 = \frac{2(1-\nu)}{(1-2\nu)}$$

So when Poisson's ratio equals 0.25 which is commonly acceptable for most rocks,

$$V_p/V_s = \sqrt{\frac{2(1-0.25)}{[1-(2)(0.25)]}}$$

$$V_p/V_s = \sqrt{3}$$

When $V_p = 5.8$

$$5.8/V_s = \sqrt{3} \quad \text{and}$$

$$V_s = 5.8/\sqrt{3}$$

$$V_p'/V_s' = V_p/V_s$$

$$V_p'/V_s' = V_p/(5.8/\sqrt{3})$$

$$V_p'/V_s' = (V_p\sqrt{3})/5.8 \quad [\text{Formula 2}]$$

Substituting Formula 2 into Formula 1,

$$\text{Slope} = [(V_p\sqrt{3}/5.8) - 1]$$

$$V_p(\sqrt{3}/5.8) = \text{Slope} + 1$$

$$V_p = (\text{Slope} + 1)5.8/\sqrt{3} \quad [\text{Formula 3}]$$

$$V_p/V_s = \text{Slope} + 1$$

DATA

All earthquakes reviewed in this study originated at approximately $34^{\circ}13'N$, $106^{\circ}51'W$ and will be referred to as Class I events.

The location and elevation of all seismograph stations used in this study are listed in Table 1. SNM and SRM are both vertical instruments, SNM recording on paper and SRM on film. SBB and SCC are vertical and horizontal instruments recording on magnetic tape. The SRM events were developed on photographic paper, and SBB and SCC were played back on a visicorder for ease in handling and interpretation.

PROCEDURE

From the forty-seven records that were considered to be Class I events, nineteen were rejected because they were poor recordings or were recorded by only two stations. From the remaining records, the S-P interval was measured, and the P arrival time was accepted from previous work (Sanford, 1972.) The S-P interval was very difficult to measure accurately, since the S wave is often very ambiguous. To overcome this difficulty all of the records from each station were reviewed as a whole, making certain that the S waves were chosen consistently.

From this data P arrival time vs. S-P interval was plotted by the computer and a best fit was obtained by the least squares technique. The program used also gave the slope of the line, the correlation coefficient and the estimated error. The origin time is found at the X intercept (where S-P = 0.0). The P wave velocity is calculated from formula (3), and the travel time is found by taking the P arrival time minus the origin time. From the product of the travel time and the P wave velocity focal distances are calculated. With three or more stations, focal distances are plotted as circles with the station at the center. A correction of 0.66 seconds was applied to station SRM because of the thick section of low velocity rock beneath that station. The epicenters were found by the intersection of the

chords of the circles, and the epicentral distances were measured from the stations. The depth of focus is found by the following relation:

$$FD = \sqrt{R^2 - Del^2}$$

where R is the focal distance and Del is the epicentral distance.

After reviewing the results of P vs. S-P and the epicentral locations, it was determined that all of the SRM S-P intervals were high, causing the P wave velocities to be too low. It is assumed that this resulted from the thick alluvium cover in the vicinity of that station and is partially due to the vertical instrument at that station not fully responding to the S waves. All SRM S-P intervals were discarded, and P vs. S-P was replotted giving more reasonable results for the P wave velocity, although some were still very low. Epicentral locations were plotted again with the new velocities, still using the P arrival times from station SRM.

To further assure consistancy, a comparison was made of the differences in P arrival times for all stations. Events having approximately the same differences in P arrival times were assumed to have the same origin. The change in the Vp/Vs ratio as time increases is plotted, showing the magnitude for the larger events. This plot demonstrates the fluctuation in the Vp/Vs ratio.

PRESNTATION AND DISCUSSION OF DATA

The P arrival times and S-P intervals are listed in Table 2. The P arrival times were taken from previous work (Sanford, 1972) and the S-P intervals were measured from the records. the events that were discarded are denoted by an "X" in the right hand column. In the final plots, the S-P intervals from SRM records were not used, but the P arrival times were.

Focal depths and P wave velocities are listed in Table 3. Focal depths range from 8.35 km. to an anomalously high 36.11 km. The average focal depth is 16.4 km. P wave velocities range from 4.38 to 5.99 with an average of 5.2 km/sec. These P wave velocities seem to be consistantly low as the value of 5.8 is usually accepted for the Rio Grande Rift.

Table 4 lists the magnitudes of most of the events used in this study. These values have been accepted from previous work. The largest event is 2.1, but most of the events are 0.3 or less.

A computer print-out of information concerning each event is included in Table 5. This is taken from the main program and gives the calculated origin time, P wave velocity, focal depth and other values used in plotting the graphs.

The differences in P arrival times for all stations are given in Table 6. A deviation from the mean of 1 second for the differences in arrival time would indicate that it was not

a Class I event.

The changes in the ratio of Vp/Vs with time and magnitude of the events is shown in Figure 1. The spikes from the X axis are the magnitudes of the events and are numbered for events equal to or greater than 0.3. The largest (1.67) and the smallest (1.31) velocity ratios in Figure 1 differ by 22%.

It is shown here that before the higher order events the Vp/Vs ratio increased to a maximum, then decreased slightly over a two to three day period. After this hump the Vp/Vs ratio decreases to a minimum during the higher order event. This does not support the work of Aggarwal, Sykes et al (1973). They find that the Vp/Vs ratio decreased before the higher order events, then returned to a normal value during the event.

The time duration of the lowered Vp/Vs ratio for the 3.3 magnitude earthquake studied by Aggarwal is four days. The study which Whitcomb, Garmany et al. (1973) have made has indicated a relation between the magnitude of an event and its anomaly time of

$$\text{Log } t = 0.68M - 1.31$$

Using this relation to calculate the anomaly time for the 2.1 magnitude event used in this study yields an anomaly time of $2\frac{1}{2}$ days. We do not see any decrease for a $2\frac{1}{2}$ day period in the Vp/Vs ratio before this event, but find an increase for a two day period (March 17 and 18). It is assumed that we have different results for one of two reasons: That there is not enough data to

represent the actual situation or that the dilatancy model assumed for this study is not appropriate to this region.

P arrival time vs. S-P interval is plotted in Figure 2. SRM records are not used in the calculation of these plots, but this rejected data is shown for reference. Each station is represented by a different symbol given in the legend and the origin time is given when S-P equals zero. Some of the plots show a large amount of scatter due to the abundance of surficial sediments in the valley, while others indicate very little scattering of data. The Vp/Vs ratio is not shown but can be found easily by adding one to the slope.

The epicentral locations are plotted in Figure 3. The radii of the circles are given by the product of the P wave velocity and the travel time for each station. The intersection of the chords of the circles locates the epicenter. All of the epicenters are within a range of \pm 2.5 km. except four which are within a range of six km. of the cluster.

CONCLUSIONS

There is a definite change in the ratio of V_p/V_s as shown in Figure 1. Changes as large as 22% occurred in the two day period preceding the 2.1 magnitude event. This time is very short compared to geologic events, but large relative to seismic wave propagation. It seems that fluid flow, crack formation and creep would have appropriate time constants and fit the model of dilatation.

The events used in this study were of lower magnitudes, where the time anomaly is short (2 days for the largest event), and the time span between events is large. It would appear that more conclusive results could be reached in a study where such gaps did not exist.

TABLE 1

LOCATION OF SEISMOGRAPH STATIONS

| STATION | LOCATION | LAT N | LONG W | ELEVATION (METERS) |
|---------|--------------------------------|----------|-----------|--------------------|
| SFM | Socorro, N.M. | 34°04.2' | 106°56.6' | 1511 |
| SGM | West of La Joya New Mexico | 34°20.5' | 106°53.9' | 1522 |
| SGC | Magdalena Mts. New Mexico | 34°01.0' | 107°00.5' | 2200 |
| SFD | East of Bernardo New Mexico | 34°24.5' | 106°44.7' | 1525 |

| DATE | ETM | | ETM | | RBB | | S&P | | % |
|------------|------|------|------|------|------|------|------|------|----|
| | P | S-P | P | S-P | P | S-P | P | S-P | |
| 1/07 13:35 | 14.4 | 2.85 | 14.4 | 3.16 | | | | | 32 |
| 1/11 20:40 | 03.4 | 2.13 | | 2.56 | | | | | 33 |
| 2/12 05:17 | 18.6 | 3.10 | 16.9 | 1.78 | 20.5 | 2.34 | | | 33 |
| 2/13 06:36 | 38.6 | 2.50 | 39.1 | 2.30 | 40.4 | 3.56 | | | 33 |
| 3/02 11:35 | 04.2 | 2.25 | 04.7 | 2.00 | 06.0 | 3.53 | | | 33 |
| 3/17 06:40 | 56.7 | 2.32 | | 2.80 | 58.6 | 3.61 | 59.5 | 3.53 | |
| 3/17 06:39 | 13.1 | 2.25 | 12.7 | 2.01 | 15.0 | 3.36 | 15.9 | 3.54 | |
| 3/17 17:05 | 34.0 | 3.02 | 34.3 | 3.83 | 35.3 | 3.33 | 36.1 | 3.59 | |
| 3/18 07:29 | 26.9 | 2.25 | 27.1 | 2.09 | 28.4 | 3.84 | 29.3 | 3.55 | |
| 3/18 16:35 | 03.3 | 2.32 | 03.5 | 3.65 | 04.6 | 3.64 | 05.7 | 3.63 | |
| 3/20 04:34 | 56.9 | 2.41 | 57.3 | 2.00 | 58.6 | 3.43 | 59.4 | 3.59 | |
| 3/25 15:32 | 50.4 | 2.75 | | | 52.0 | 3.47 | 52.7 | 3.84 | |
| 3/26 09:02 | 50.0 | 2.20 | 49.6 | 2.82 | 53.5 | 2.20 | | | 33 |
| 3/30 02:51 | 47.7 | 3.25 | 48.0 | 1.96 | | 3.40 | | | 33 |
| 4/13 06:29 | 03.5 | 3.00 | 00.6 | 1.94 | | | | | 33 |
| 4/17 03:06 | 48.0 | 2.25 | 50.0 | 2.79 | | | 52.2 | 3.72 | |
| 4/18 03:44 | 33.3 | 2.50 | 33.2 | 2.81 | | | 35.5 | 3.76 | |
| 4/18 07:11 | 35.5 | 3.00 | 36.1 | 2.80 | | | 38.4 | 3.80 | |
| 4/18 07:34 | 50.6 | 2.50 | 59.0 | 2.74 | | | 62.1 | 3.66 | |
| 4/18 09:05 | 01.2 | 2.50 | 01.3 | 2.00 | | | 05.2 | 3.11 | |
| 4/18 09:12 | 36.9 | 2.50 | 37.0 | 2.00 | | | 39.2 | 4.04 | |
| 4/18 09:29 | 38.1 | 2.50 | 38.3 | 2.89 | | | 40.6 | 4.09 | |
| 4/18 19:18 | 19.7 | 2.50 | 19.9 | 2.81 | | | 22.2 | 3.59 | |
| 5/05 22:44 | 17.9 | 2.30 | 18.2 | 2.89 | 19.5 | 3.62 | 20.3 | 3.53 | |
| 5/05 22:46 | 53.0 | 2.50 | 54.1 | 2.12 | 55.3 | | 56.7 | 3.83 | |
| 5/05 23:03 | 18.0 | 2.18 | 18.2 | 3.10 | | 3.72 | 12.3 | 3.62 | |
| 5/11 08:07 | 51.6 | 3.13 | 51.9 | 2.85 | | | | | 33 |
| 5/13 02:31 | 02.1 | 2.45 | 02.6 | 2.92 | | | 04.6 | 3.66 | |
| 6/01 12:22 | 05.3 | 2.43 | 05.6 | 2.87 | | | | | 33 |
| 6/01 15:36 | 43.4 | 2.50 | 43.6 | 2.83 | | | 45.0 | 4.10 | |
| 6/01 22:17 | 53.8 | 2.68 | 54.0 | 2.67 | 55.4 | | 56.1 | 3.58 | |
| 6/02 00:22 | 43.5 | 2.45 | 43.6 | 2.67 | | | 45.0 | 3.56 | |
| 6/02 12:24 | 49.3 | 2.30 | 49.6 | 2.86 | | | | | 33 |
| 6/07 09:14 | 23.7 | 2.13 | 22.8 | 2.82 | | | | | 33 |
| 6/14 04:23 | 26.2 | 2.48 | 26.6 | 3.04 | | | 32.6 | 3.19 | |
| 6/14 04:31 | 12.9 | 2.20 | 13.1 | 2.86 | | | | | 33 |
| 6/14 04:36 | 31.8 | 2.38 | 32.1 | 2.80 | 32.4 | 3.36 | 34.3 | 3.65 | |
| 6/14 04:36 | 52.8 | 2.35 | 54.1 | 2.25 | 55.0 | 3.21 | 56.2 | 3.78 | |
| 6/14 07:04 | 32.9 | 2.32 | 33.0 | 2.11 | 34.6 | 6.15 | 35.2 | 6.12 | |
| 6/14 09:20 | 18.9 | 2.63 | 19.3 | 2.36 | 20.3 | 3.58 | 21.3 | | |
| 6/16 05:51 | 14.0 | 2.50 | 14.5 | | 15.0 | 3.70 | 16.0 | | 33 |
| 6/16 16:50 | 25.0 | 2.48 | 25.2 | 2.80 | 26.5 | | 27.5 | 3.52 | |
| 6/17 08:52 | 50.0 | 2.25 | 50.2 | 2.92 | | | | | 33 |
| 6/23 01:23 | 07.6 | 2.75 | | 2.30 | | | 13.4 | 4.29 | |
| 6/26 11:34 | 26.5 | 2.80 | 26.6 | 3.07 | 27.8 | 3.76 | 28.5 | 3.89 | |
| 7/07 02:51 | 26.3 | 2.38 | | | 26.8 | 3.69 | 27.4 | 3.71 | |
| 7/27 10:36 | 02.0 | 2.42 | | | 05.5 | 5.62 | 06.3 | 4.21 | |

TABLE II

P ARRIVAL TIMES AND S-P INTERVALS

TABLE 3
FOCAL DEPTH AND P WAVE VELOCITY

| DATE | TIME | FOCAL DEPTH Km. | P WAVE VELOCITY Km./sec. |
|------|-------|--------------------|-----------------------------|
| 3/13 | 08:36 | 15.99 | 5.32 |
| 3/02 | 11:35 | 8.53 | 5.73 |
| 3/17 | 06:40 | 20.51 | 4.92 |
| 3/17 | 06:39 | 16.69 | 5.01 |
| 3/17 | 17:05 | 15.42 | 5.11 |
| 3/18 | 07:20 | 13.06 | 5.40 |
| 3/19 | 16:35 | 17.13 | 5.14 |
| 3/20 | 06:34 | 10.62 | 5.00 |
| 3/25 | 15:32 | 24.93 | 4.00 |
| 4/17 | 03:06 | 10.55 | 5.40 |
| 4/18 | 03:04 | 14.30 | 5.27 |
| 4/18 | 07:34 | 22.25 | 4.30 |
| 4/18 | 09:12 | 11.33 | 5.50 |
| 4/18 | 09:29 | 32.27 | 5.49 |
| 4/18 | 19:18 | 21.81 | 4.81 |
| 5/05 | 22:44 | 15.10 | 5.20 |
| 5/05 | 23:03 | 9.17 | 5.45 |
| 5/13 | 02:31 | 19.76 | 4.94 |
| 6/01 | 15:36 | 11.92 | 5.50 |
| 6/01 | 22:17 | 36.11 | 4.38 |
| 6/02 | 00:29 | 10.05 | 4.96 |
| 6/14 | 04:36 | 16.22 | 5.13 |
| 6/14 | 04:36 | 13.49 | 5.26 |
| 6/14 | 07:04 | 8.25 | 5.99 |
| 6/14 | 09:20 | 36.21 | 5.40 |
| 6/16 | 16:50 | 10.50 | 4.85 |
| 6/20 | 11:34 | 21.11 | 5.12 |
| 9/27 | 10:36 | 21.40 | 5.71 |

TABLE 4
MAGNITUDE OF EVENTS

| DATE | TIME | MAGNITUDE |
|------|-------|-----------|
| 2/13 | 08:36 | 0.30 |
| 3/3 | 11:35 | -0.72 |
| 3/17 | 06:40 | 0.13 |
| 3/17 | 08:39 | -0.13 |
| 3/17 | 17:05 | 0.36 |
| 3/18 | 07:20 | 0.11 |
| 3/18 | 16:35 | 0.03 |
| 3/20 | 04:34 | 0.16 |
| 3/25 | 15:32 | 2.10 |
| 4/17 | 03:06 | 0.26 |
| 4/18 | 03:04 | 0.30 |
| 4/18 | 07:11 | -0.35 |
| 4/18 | 07:34 | -0.24 |
| 4/18 | 09:12 | 0.23 |
| 4/18 | 09:29 | -0.24 |
| 4/18 | 19:18 | 0.30 |
| 5/5 | 22:44 | 0.21 |
| 5/5 | 23:03 | -0.32 |
| 5/10 | 02:31 | 1.00 |
| 6/1 | 15:36 | 0.03 |
| 6/1 | 22:17 | 0.65 |
| 6/2 | 00:22 | -0.02 |
| 6/14 | 04:36 | 0.30 |
| 6/14 | 04:36 | 0.20 |
| 6/16 | 16:50 | 0.29 |
| 6/30 | 11:34 | 0.21 |

TABLE 5

STANDARD INFORMATION FROM EACH EVENT

DATE * 2/13/1970 ORIGIN TIME * 08/26/34.55
 P TT R S-P
 SNM * 39.60 4.25 22.62 2.50 * FD 15.40
 SRM * 39.10 4.09 21.77 2.62 * VP 5.32
 SBB * 40.37 6.02 32.63 3.54 * CC 1.00

DATE * 3/02/1970 ORIGIN TIME * 11/35/ 1.64
 P TT R S-P
 SNM * 4.20 3.16 18.12 1.25 * FD 6.53
 SRM * 4.70 3.00 17.21 2.80 * VP 5.73
 SBB * 6.00 4.96 20.44 3.59 * CC 1.00

DATE * 3/17/1970 ORIGIN TIME * 08/40/51.50
 P TT R S-P
 SNM * 56.70 6.17 35.41 2.53 * FD 20.51
 SRM * 6.0 0.0 0.0 0.0 * VP 4.52
 SBB * 58.60 7.37 34.76 3.61 * CC 0.93
 SCC * 59.50 7.97 30.13 3.65 * FE 0.25

DATE * 3/17/1970 ORIGIN TIME * 08/39/ 8.50
 P TT R S-P
 SNM * 13.10 4.60 33.07 2.25 * FD 16.63
 SRM * 13.70 4.54 22.77 1.81 * VP 4.01
 SBB * 15.00 6.50 32.60 3.26 * CC 0.99
 SCC * 15.80 7.30 36.61 3.54 * FE 0.31

DATE * 3/17/1970 ORIGIN TIME * 11/05/29.15
 P TT R S-P
 SNM * 33.50 4.85 22.22 2.26 * FD 15.42
 SRM * 34.00 4.19 21.40 2.82 * VP 5.11
 SBB * 35.25 6.10 31.17 1.33 * CC 0.99
 SCC * 36.12 6.97 35.62 3.89 * FE 0.31

DATE * 3/18/1970 ORIGIN TIME * 07/20/22.03
 P TT R S-P
 SNM * 26.90 3.97 21.44 2.625 * FD 16.06
 SPM * 27.10 3.51 18.95 2.749 * VP 5.40
 SBB * 28.40 3.47 29.53 3.604 * CC 0.86
 SCC * 29.25 3.32 34.32 2.559 * LF 0.43

DATE * 3/18/1970 ORIGIN TIME * 16/35/-1.40
 P TT R S-P
 SNM * 3.80 4.76 24.69 2.639 * FD 17.13
 SPM * 3.60 4.30 22.12 2.635 * VP 5.14
 SBB * 4.60 6.06 31.13 2.259 * CC 0.89
 SCC * 5.70 7.16 36.94 3.645 * LF 0.26

DATE * 3/20/1970 ORIGIN TIME * 04/24/51.82
 P TT R S-P
 SNM * 56.00 4.98 24.88 2.641 * FD 16.62
 SPM * 57.30 4.70 22.53 2.690 * VP 5.00
 SBB * 58.04 6.72 33.57 2.647 * CC 0.94
 SCC * 59.40 7.49 37.37 3.660 * LF 0.12

DATE * 3/25/1970 ORIGIN TIME * 16/32/44.41
 P TT R S-P
 SNM * 50.36 5.95 29.00 2.715 * FD 24.92
 SPM * 50.0 0.0 0.0 0.0 * VP 0.82
 SBB * 52.00 7.59 37.32 3.647 * CC 1.20
 SCC * 52.70 8.29 40.54 3.634 * LF 0.02

DATE * 4/17/1970 ORIGIN TIME * 02/06/46.13
 P TT R S-P
 SNM * 49.80 3.67 19.84 2.625 * FD 16.55
 SPM * 50.00 3.21 17.35 2.779 * VP 5.40
 SBB * 52.20 6.07 32.70 3.677 * LF 0.0

DATE * 4/18/1970 ORIGIN TIME * 03/14/20.89
 P TT R S-P
 SNM * 53.80 4.37 21.93 2.559 * FD 16.36
 SPM * 53.20 3.61 18.93 2.811 * VP 5.27
 SBB * 55.50 6.57 34.57 3.766 * CC 0.0

DATE * 4/18/1970 ORIGIN TIME * 07/34/53.07
 P TT R S-P
 SNM * 59.60 5.93 26.49 2.58 * FD 23.75
 SRM * 59.80 5.67 26.38 2.74 * VP 4.80
 SCC * 62.10 6.43 40.50 3.66 * FE 0.0

DATE * 4/18/1970 ORIGIN TIME * 09/12/33.17
 P TT R S-P
 SNM * 36.90 3.73 20.87 2.50 * FD 11.86
 SRM * 37.00 3.17 17.74 2.80 * VP 5.56
 SCC * 39.20 5.03 33.75 4.04 * FE 0.0

DATE * 4/18/1970 ORIGIN TIME * 09/29/34.17
 P TT R S-P
 SNM * 36.10 3.93 21.53 2.50 * FD 12.27
 SRM * 36.25 3.42 15.74 2.80 * VP 5.81
 SCC * 40.50 6.43 35.23 4.04 * FE 0.0

DATE * 4/18/1970 ORIGIN TIME * 10/18/13.47
 P TT R S-P
 SNM * 10.70 5.73 27.57 2.50 * FD 21.31
 SRM * 19.90 5.27 25.35 2.81 * VP 4.81
 SCC * 22.20 8.23 39.50 3.59 * FE 0.0

DATE * 5/05/1970 ORIGIN TIME * 22/04/13.53
 P TT R S-P
 SNM * 17.90 4.37 22.74 2.30 * FD 15.10
 SRM * 18.20 4.01 20.27 2.30 * VP 5.20
 SBD * 19.46 5.92 30.81 3.52 * CC 0.01
 SCC * 20.30 6.77 35.23 3.59 * FE 0.30

DATE * 5/05/1970 ORIGIN TIME * 23/03/ 6.54
 P TT R S-P
 SNM * 10.00 3.46 18.03 2.03 * FD 0.17
 SRM * 10.20 3.00 16.37 2.10 * VP 4.46
 SCC * 12.30 5.76 31.42 3.62 * FE 0.0

DATE * 5/13/1970 ORIGIN TIME * 02/31/-3.04
 P TT R S-P
 SNM * 2.10 5.14 25.43 2.45 * FD 19.76
 SRM * 2.30 5.18 25.62 2.92 * VP 4.94
 SCC * 4.64 7.68 37.88 3.00 * FE 0.0

DATE * 6/01/1970 ORIGIN TIME * 13/30/59.85
 P TT R S-P
 SNM * 43.40 3.75 20.93 2.80 * FD 11.92
 SRM * 43.60 3.29 12.36 2.62 * VP 5.50
 SCC * 45.80 6.15 34.32 4.10 * FE 0.0

DATE * 6/01/1970 ORIGIN TIME * 22/17/46.42
 P TT R S-P
 SNM * 53.80 9.38 41.04 2.83 * FD 34.11
 SRM * 54.00 8.92 39.02 2.67 * VP 4.38
 SCC * 56.10 11.62 51.10 2.58 * FE 0.0

DATE * 6/02/1970 ORIGIN TIME * 03/22/38.42
 P TT R S-P
 SNM * 43.50 5.08 25.80 2.45 * FD 19.05
 SRM * 43.80 4.72 23.42 2.67 * VP 4.96
 SCC * 45.80 7.38 36.62 3.36 * FE 0.0

DATE * 6/14/1970 ORIGIN TIME * 04/26/27.28
 P TT R S-P
 SNM * 31.80 4.52 25.23 2.68 * FD 16.22
 SRM * 32.10 4.16 23.56 2.80 * VP 5.72
 SBB * 33.40 6.12 31.47 3.30 * UC 0.40
 SCC * 34.25 6.97 35.74 3.65 * FE 0.0

DATE * 6/14/1970 ORIGIN TIME * 04/26/40.77
 P TT R S-P
 SNM * 53.80 4.03 21.51 2.35 * FD 13.43
 SRM * 54.10 3.67 19.59 2.83 * VP 5.34
 SBB * 55.00 5.23 27.92 3.21 * UC 0.99
 SCC * 56.20 6.43 34.34 3.78 * FE 0.08

DATE * 6/14/1970 ORIGIN TIME * 07/04/29,04
 P TT R S-P
 SNM * 32.80 3.16 18.94 2.48 * FD 0.06
 SRM * 33.00 2.70 16.13 3.11 * VP 5.99
 SBB * 34.44 4.80 26.76 4.16 * CC 0.99
 SCC * 35.20 5.56 33.30 4.18 * LE 0.33

DATE * 6/14/1970 ORIGIN TIME * 09/20/14,02
 P TT R S-P
 SNM * 18.00 4.26 22.13 2.52 * FD 16.21
 SRM * 19.27 3.99 21.57 3.26 * VP 5.40
 SBB * 20.46 5.42 21.30 3.51 * CC 1.00

DATE * 6/16/1970 ORIGIN TIME * 26/50/19,00
 P TT R S-P
 SNM * 25.00 5.40 26.20 2.48 * FD 19.50
 SRM * 25.20 4.94 23.97 2.99 * VP 4.89
 SBB * 27.46 7.36 39.14 3.53 * CC 0.0
 SCC * 27.46 7.36 39.14 3.53 * LE 0.0

DATE * 6/30/1970 ORIGIN TIME * 11/34/31,09
 P TT R S-P
 SNM * 26.50 6.41 27.74 2.80 * FD 21.11
 SRM * 26.62 4.87 24.98 3.07 * VP 5.12
 SBB * 27.80 6.72 34.40 3.76 * CC 0.55
 SCC * 28.50 7.41 37.90 3.90 * LE 0.10

DATE * 9/27/1970 ORIGIN TIME * 10/30/ 0,45
 P TT R S-P
 SNM * 3.90 3.45 19.60 2.48 * FD 11.49
 SRM * 0.0 0.0 0.0 0.0 * VP 5.71
 SBB * 5.50 5.95 21.82 2.62 * CC 0.99
 SCC * 6.30 5.85 23.39 4.23 * LE 0.17

TABLE 6

| | SNC | SRM | SBD | SCC |
|------------|------|------|------|------|
| 1/17-13.38 | 34.4 | 14.8 | 0.0 | 0.0 |
| 1/17-14.60 | 3.4 | 0.0 | 0.0 | 0.0 |
| 2/12-05.17 | 38.6 | 16.9 | 20.5 | 0.0 |
| 2/13-07.36 | 38.0 | 35.1 | 40.4 | 0.0 |
| 3/02-11.25 | 4.2 | 4.7 | 6.0 | 0.0 |
| 3/17-06.40 | 25.7 | 0.0 | 58.6 | 59.5 |
| 3/17-08.39 | 23.1 | 31.7 | 15.0 | 15.8 |
| 3/27-17.95 | 35.5 | 34.0 | 35.2 | 36.1 |
| 3/29-07.26 | 16.9 | 27.1 | 20.4 | 22.3 |
| 3/30-16.55 | 2.3 | 3.5 | 4.6 | 5.7 |
| 5/20-04.24 | 50.7 | 57.3 | 58.4 | 59.4 |
| 3/26-15.52 | 30.4 | 0.0 | 52.0 | 52.7 |
| 2/16-00.32 | 50.0 | 49.6 | 55.5 | 0.0 |
| 3/30-02.51 | 47.7 | 48.0 | 0.0 | 0.0 |
| 4/17-05.26 | 35.0 | 50.0 | 0.0 | 52.2 |
| 4/19-03.64 | 30.3 | 35.2 | 0.0 | 35.5 |
| 4/19-07.17 | 15.5 | 36.1 | 0.0 | 38.4 |
| 4/18-07.34 | 54.6 | 59.3 | 0.0 | 62.3 |
| 4/18-07.37 | 1.2 | 1.3 | 0.0 | 5.2 |
| 4/18-09.37 | 36.9 | 37.0 | 0.0 | 39.2 |
| 4/18-10.27 | 20.1 | 28.2 | 0.0 | 40.6 |
| 4/19-13.70 | 19.7 | 16.0 | 0.0 | 22.2 |
| 5/05-17.46 | 17.9 | 18.2 | 19.5 | 20.3 |
| 5/05-22.40 | 50.7 | 54.1 | 55.2 | 56.7 |
| 5/15-03.05 | 10.0 | 19.2 | 0.0 | 12.3 |
| 6/01-10.07 | 51.6 | 51.9 | 0.0 | 0.0 |
| 5/13-02.81 | 2.3 | 2.5 | 0.0 | 4.6 |
| 6/01-10.23 | 5.3 | 5.6 | 0.0 | 0.0 |
| 6/01-15.85 | 4.0 | 43.6 | 0.0 | 45.9 |
| 6/02-12.17 | 53.8 | 54.0 | 55.4 | 56.1 |
| 6/02-30.71 | 43.5 | 43.6 | 0.0 | 45.0 |
| 6/02-17.84 | 4.0 | 4.6 | 0.0 | 0.0 |
| 6/07-20.14 | 53.7 | 53.8 | 0.0 | 0.0 |
| 6/14-04.22 | 26.2 | 26.6 | 0.0 | 32.6 |
| 6/14-04.31 | 12.9 | 13.1 | 0.0 | 0.0 |
| 6/14-14.31 | 31.9 | 32.1 | 23.4 | 34.3 |
| 6/14-04.36 | 5.8 | 54.1 | 55.0 | 56.2 |
| 6/14-07.34 | 32.8 | 33.0 | 34.4 | 35.2 |
| 6/14-10.20 | 10.9 | 19.3 | 20.5 | 21.3 |
| 6/16-05.47 | 24.0 | 14.5 | 15.9 | 16.5 |
| 6/16-11.60 | 25.0 | 25.2 | 26.5 | 27.5 |
| 6/17-12.73 | 56.0 | 50.2 | 0.0 | 0.0 |
| 6/18-01.33 | 7.6 | 0.0 | 0.0 | 10.4 |
| 6/19-11.32 | 26.5 | 26.6 | 27.0 | 28.5 |
| 7/07-04.51 | 26.3 | 0.0 | 26.8 | 27.4 |
| 9/27-10.36 | 3.9 | 0.0 | 5.5 | 6.3 |

* 100% completion rate for all 2000 cases

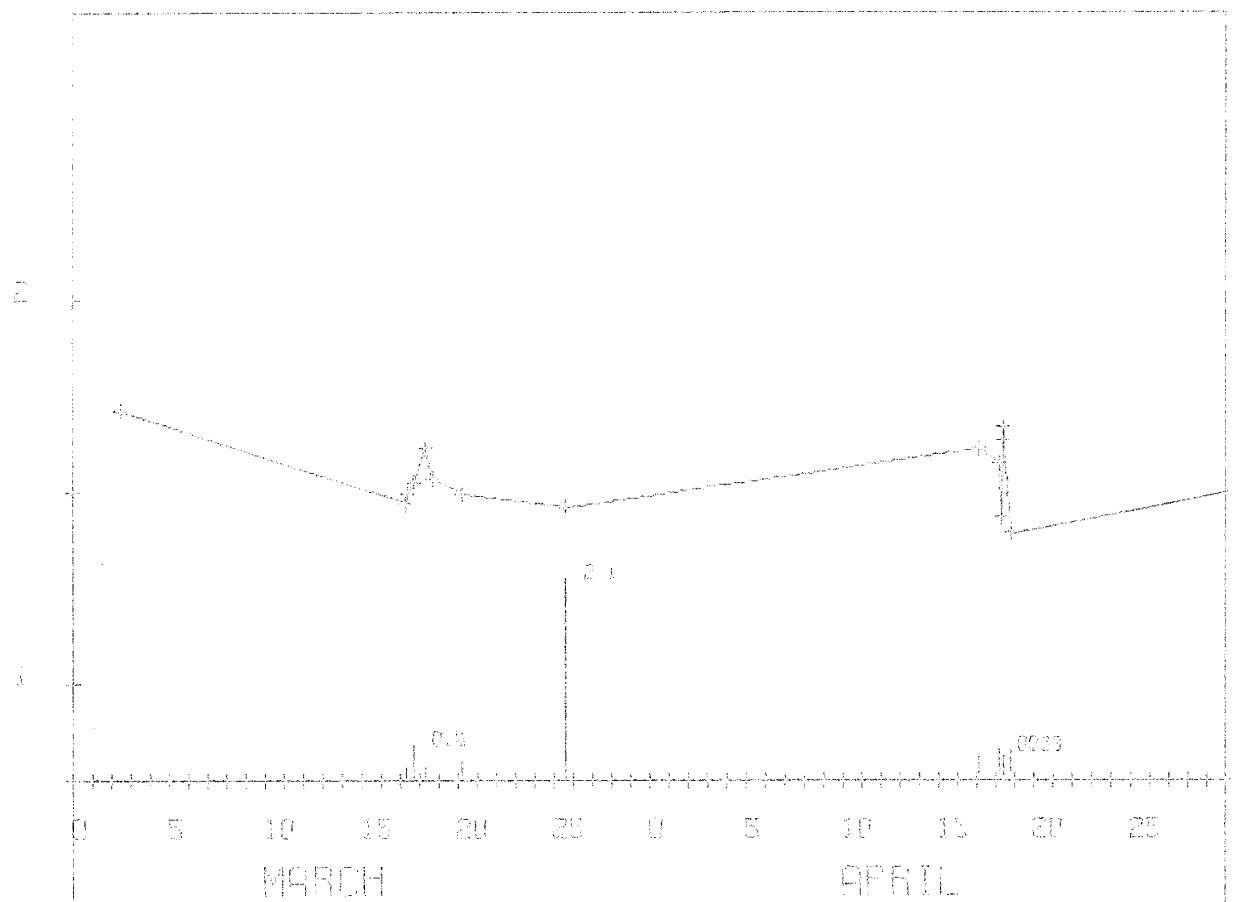
| DATE | S3-3 | S3-4 | S3-5 | S3-6 | S3-7 | S3-8 | S3-9 | S3-10 | S3-11 |
|--------------|-------|------|------|------|------|------|------|-------|-------|
| 1/07-14.56 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 1/11-20.40 | 0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2/12-05.77 | -1.07 | 3.04 | 4.02 | 3.06 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 2/13-04.36 | 0.25 | 1.00 | 0.00 | 1.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/02-13.75 | 0.08 | 1.00 | 0.00 | 1.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/17-03.40 | 0.03 | 1.04 | 2.08 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/17-04.30 | 0.05 | 1.09 | 2.07 | 1.03 | 2.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/17-17.05 | 0.05 | 1.07 | 2.06 | 1.02 | 2.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/18-07.40 | 0.02 | 1.08 | 2.04 | 1.03 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/19-16.75 | 0.02 | 1.03 | 2.04 | 1.01 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/20-04.36 | 0.04 | 1.05 | 2.05 | 1.01 | 2.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/22-15.32 | 0.00 | 1.06 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/25-09.02 | -1.04 | 5.03 | 0.00 | 5.09 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 3/30-02.51 | 0.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/17-03.06 | 0.02 | 0.06 | 2.04 | 0.00 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/18-03.74 | -0.01 | 0.00 | 2.02 | 0.00 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/18-07.12 | 0.01 | 0.06 | 2.09 | 0.00 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/19-07.52 | 0.02 | 0.06 | 2.05 | 0.00 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/19-09.05 | 0.02 | 0.03 | 4.00 | 0.00 | 3.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/20-03.62 | 0.01 | 0.00 | 2.03 | 0.00 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/20-04.77 | 0.02 | 0.06 | 2.03 | 0.00 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/21-19.16 | 0.02 | 0.00 | 2.05 | 0.00 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/22-02.46 | 0.02 | 0.00 | 2.04 | 0.00 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/23-02.46 | 0.02 | 0.00 | 2.04 | 0.00 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 |
| 4/24-03.07 | 0.03 | 0.00 | 2.03 | 0.00 | 2.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 5/12-02.31 | 0.07 | 0.00 | 2.05 | 0.00 | 1.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/01-3.20.23 | 0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/01-17.31 | 0.02 | 0.00 | 2.04 | 0.00 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/01-22.17 | 0.02 | 1.00 | 2.03 | 1.04 | 2.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/02-00.22 | 0.03 | 0.00 | 2.03 | 0.00 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/02-12.27 | 0.03 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/07-09.14 | 0.01 | 0.00 | 2.00 | 0.00 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/14-04.33 | 0.04 | 0.00 | 0.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/14-04.31 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/14-04.33 | 0.03 | 1.00 | 2.02 | 1.03 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/14-04.33 | 0.03 | 1.00 | 2.02 | 0.09 | 2.01 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/14-07.04 | 0.02 | 1.00 | 2.04 | 1.04 | 2.02 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/14-07.70 | 0.02 | 1.00 | 2.04 | 1.02 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/16-05.53 | 0.03 | 1.00 | 2.05 | 1.04 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/16-13.50 | 0.02 | 1.05 | 2.05 | 1.03 | 2.03 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/17-12.52 | 0.02 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/23-03.33 | 0.00 | 0.00 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 6/23-11.32 | 0.01 | 1.00 | 2.00 | 1.02 | 2.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 7/07-02.01 | 0.01 | 0.00 | 1.01 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 9/27-10.76 | 0.00 | 1.06 | 2.04 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

1.00 = 100% survival
 0.00 = 0% survival
 0.00 = 0% survival
 0.00 = 0% survival

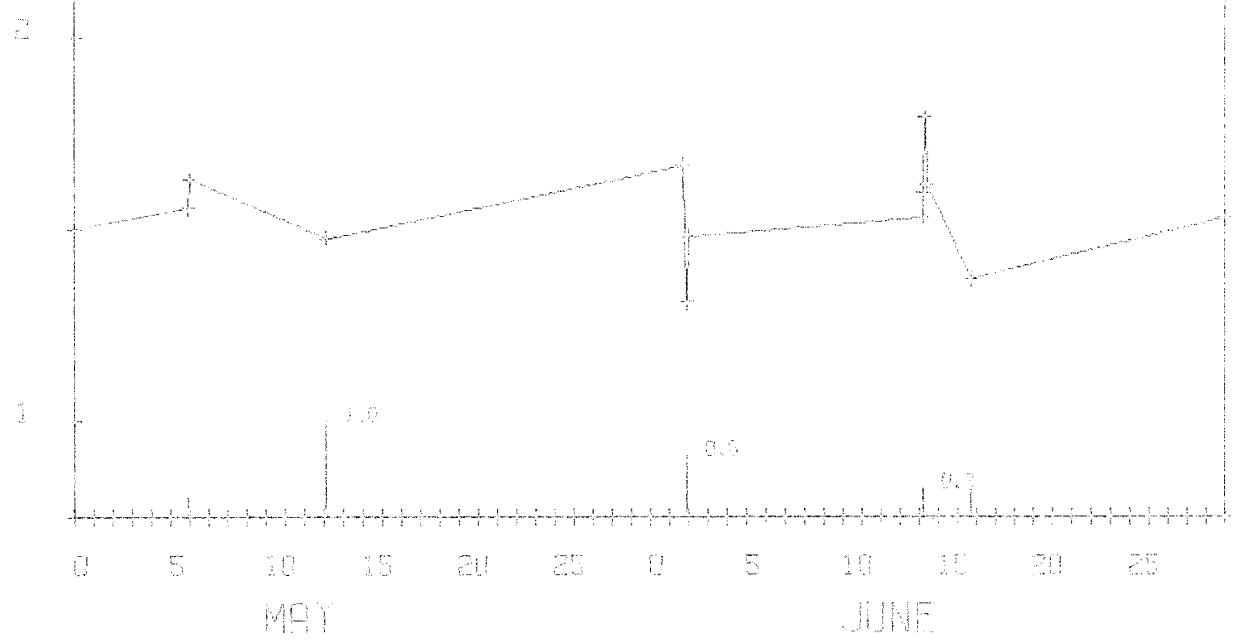
7 7 9 11 12 13

YOGA RATIO YR. TIME. Magnitude for larger events are shown

\dot{M}_p/\dot{M}_s



\dot{M}_p/\dot{M}_s

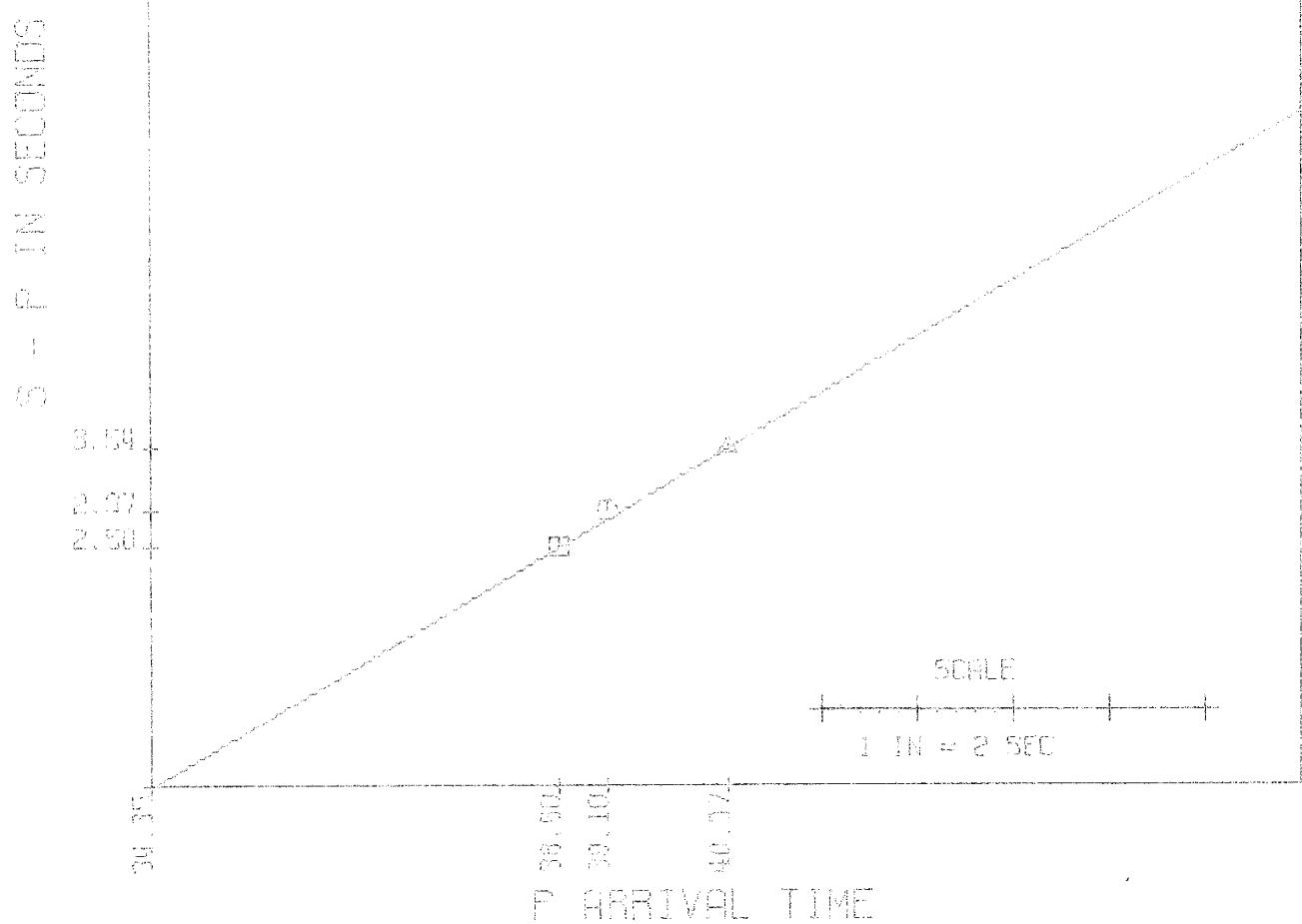


3 3 3 3 3 3

3 APPENDIX THREE U.S. C-13 TRANSMISSION

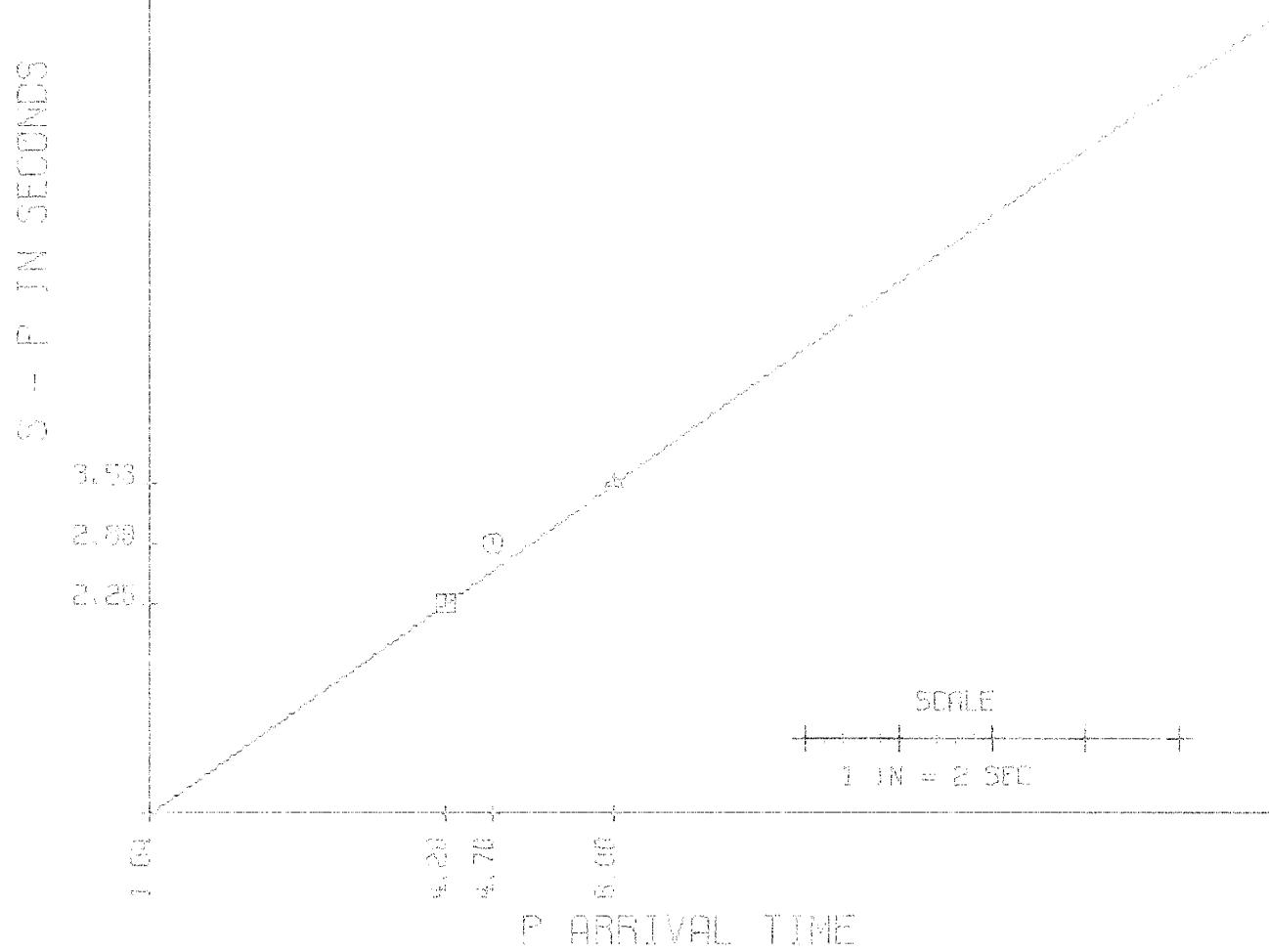
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SLOPE 0.58757
VP 0.316

SNN C
SPM G
SES A
SOC P



B RATE 8/62 7/670
ORIGIN 11.35.1.04
SLOPE 0.71101
VP 5.730

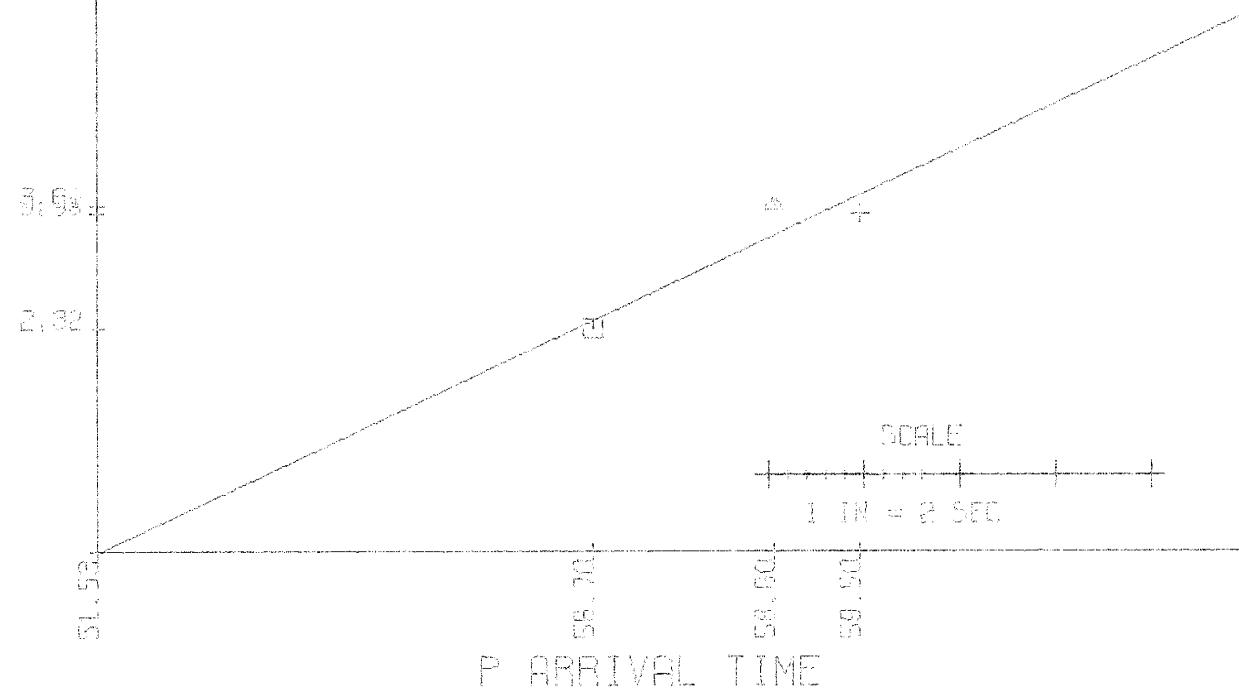
SIM 01
SEM 00
SSD 00
SOC 04



DATE 5/17/1970
ORIGIN 05.40.51.53
SLOPE 0.45347
VP 4.917

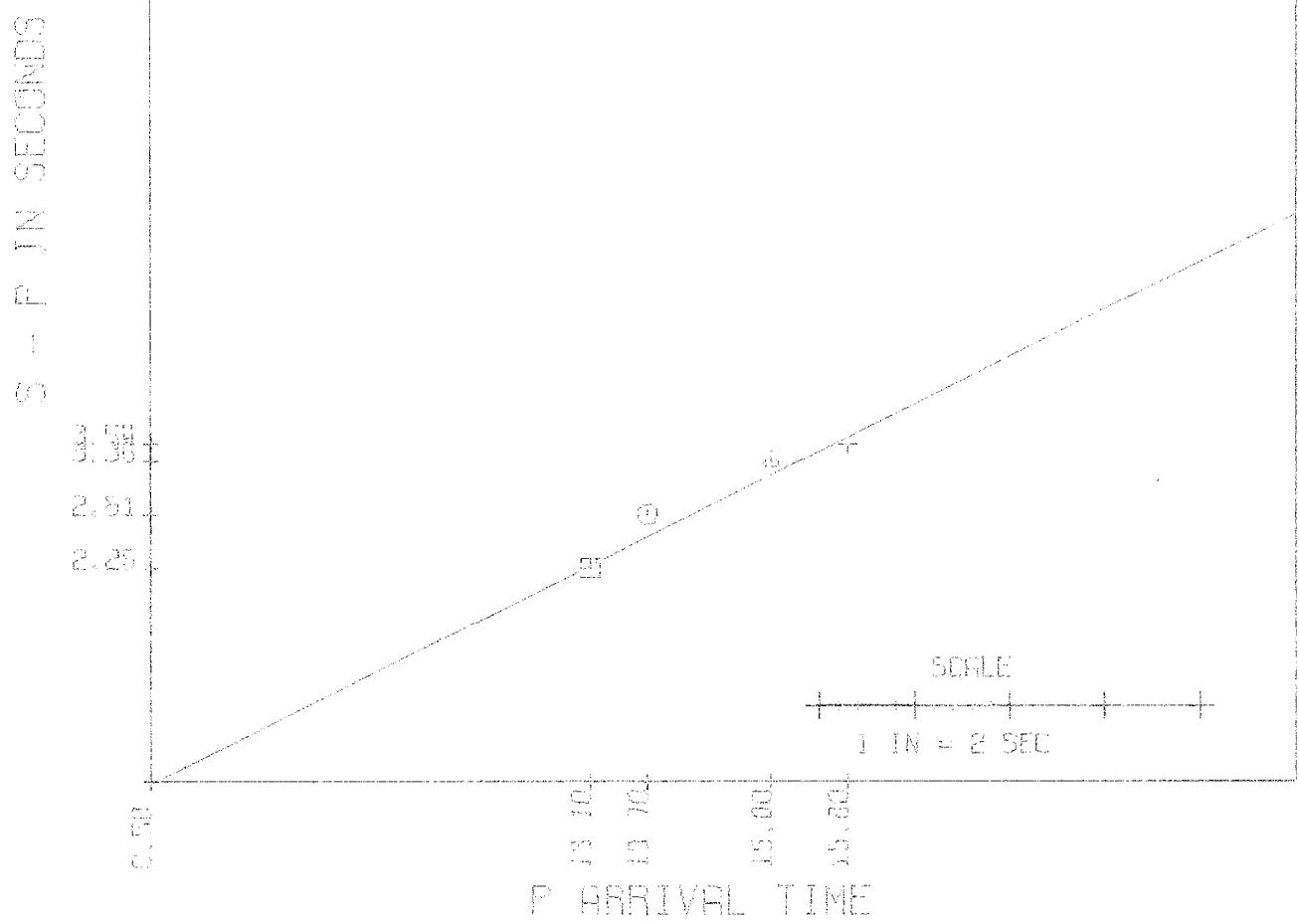
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SRM 60
SEC 3
SEC 4

S = P IN SECONDS



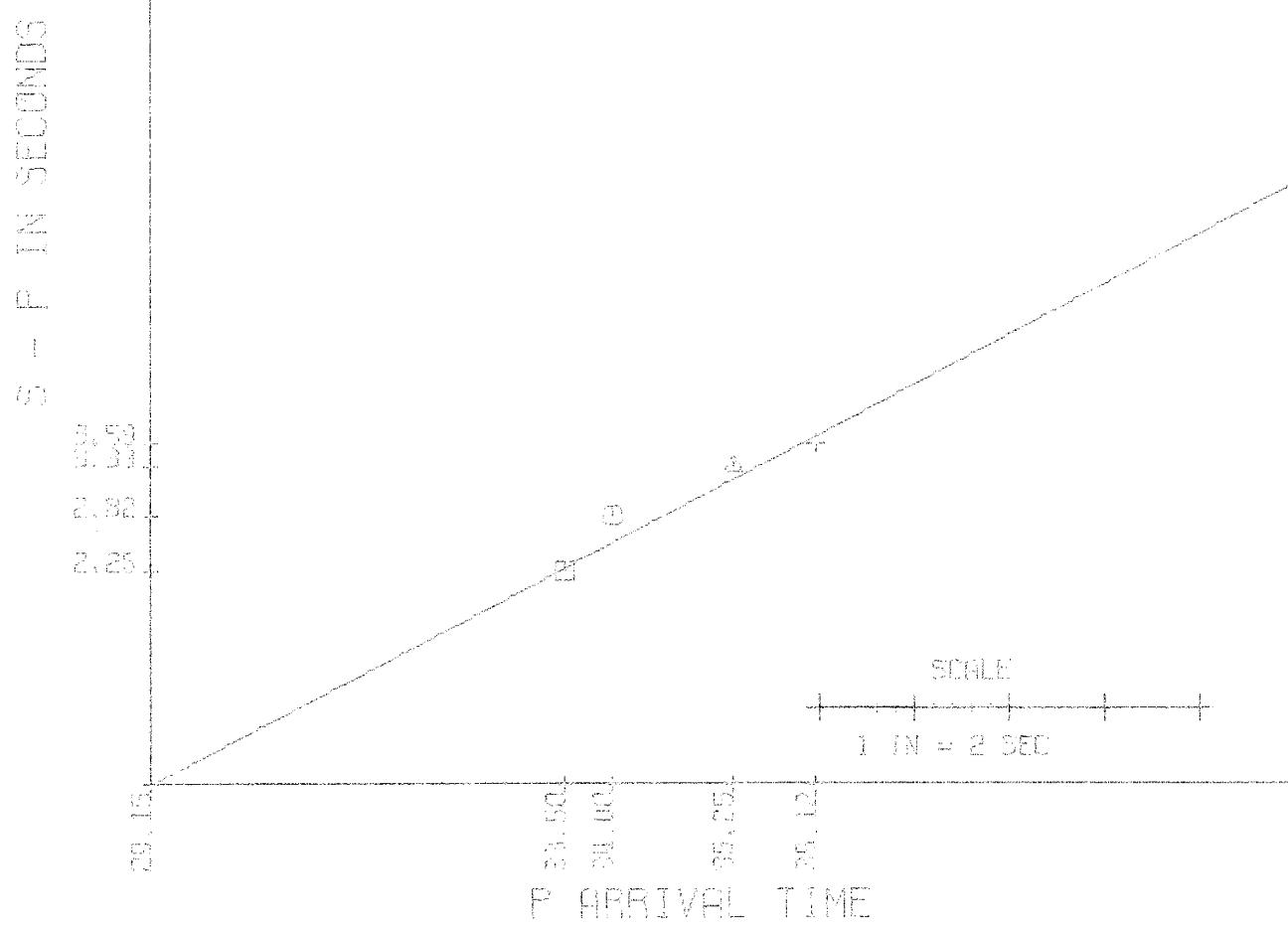
DATE 6/17/1970
ORIGIN 06.30.0.00
SLOPE 0.49705
VR 5.013

SN4 0
SEN 0
SER A
SEC +



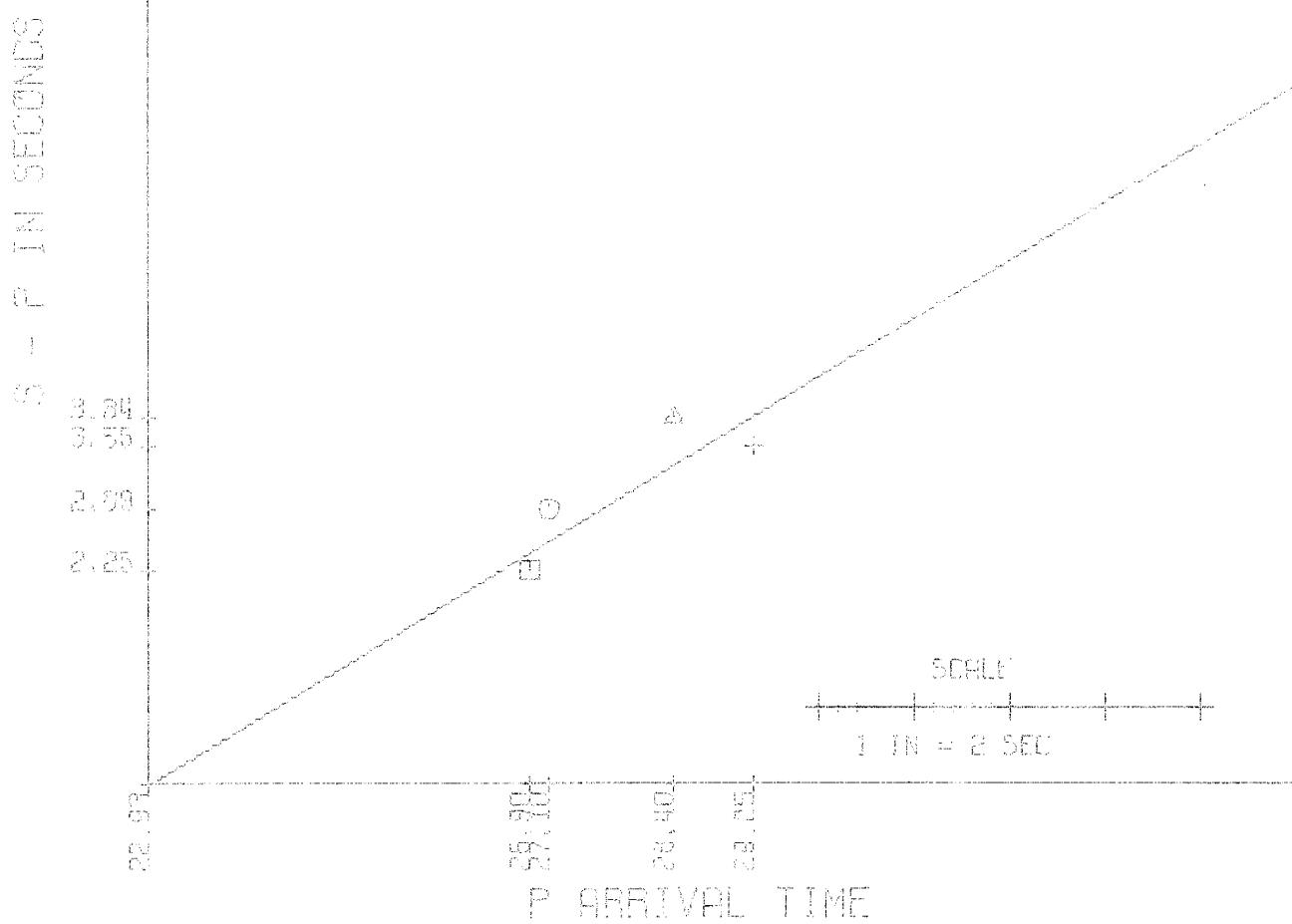
DATE 3/17/1970
CREDIT 17,05,29,15
SLR# 01-52693
VP 5,113

5000
5000
5000
5000



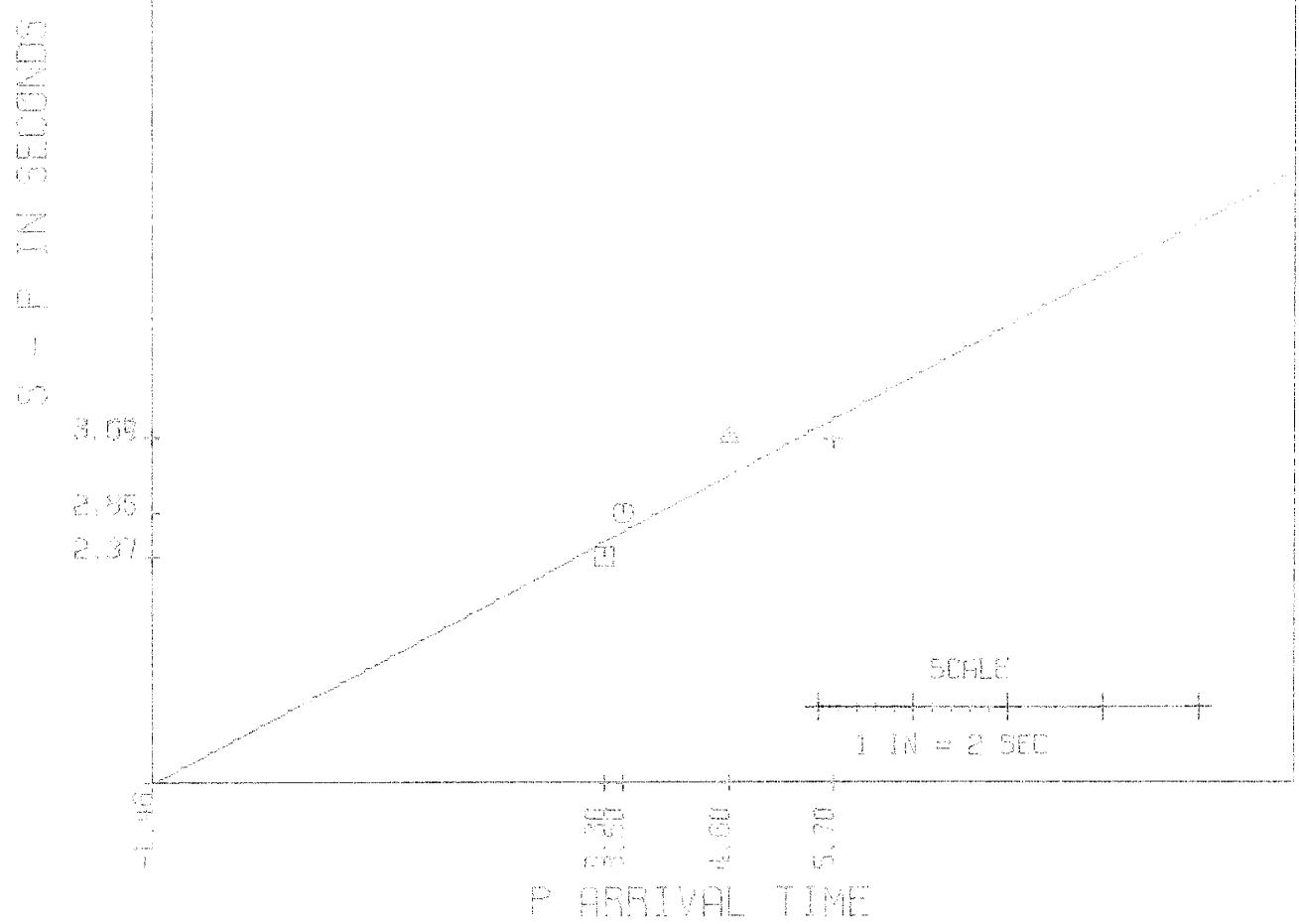
DATE 3/18/1970
ORIGIN 07.20.22.93
SLOPE 0.61136
NP 5,386

SNR m
SEM @
SSE s
SEC +



DATE 3/18/1970
ORIGIN 16.35 -1.45
SLOPE 0.50543
VP 5.145

SIM P
SIM O
SBB A
SCC A

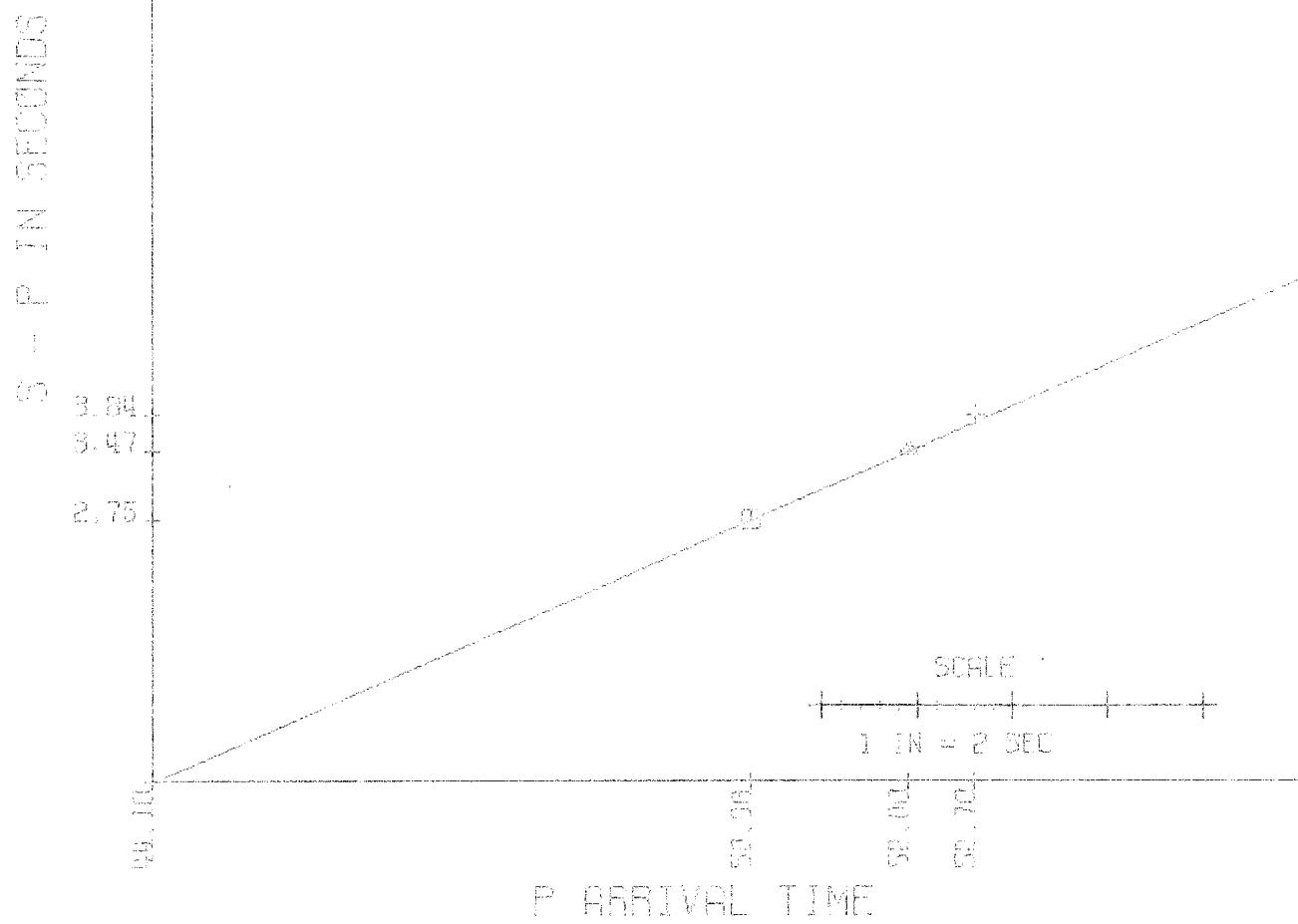


DATE 3/20/1970
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 SLOPE 0.49212
 V.P. 4.897

SHM
SHM
SEC
SEC

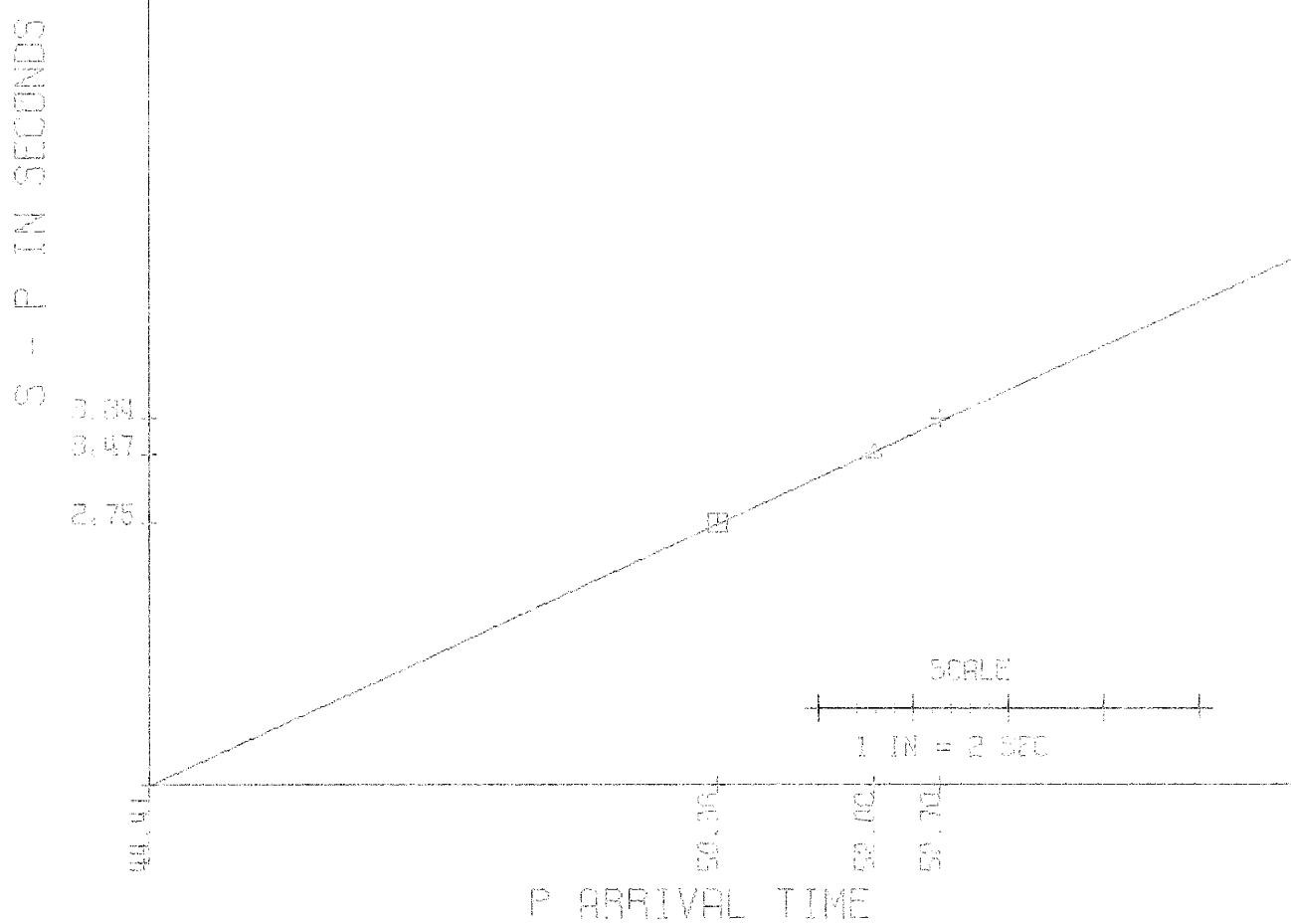
DATE 3/25/1970
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VP 0.812

SNA 0
584 0
585 A
586 +



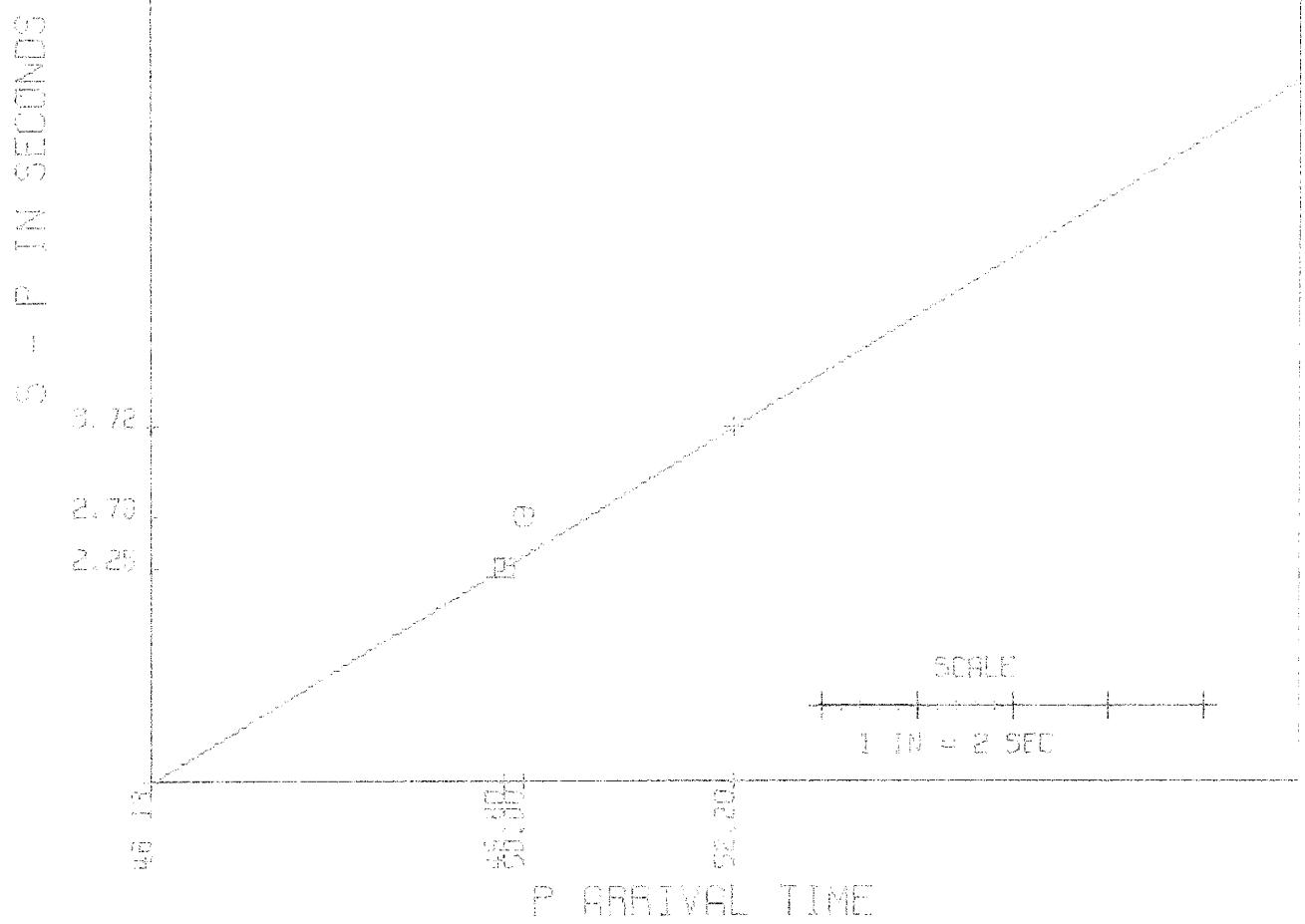
DATE 3/25/1978
CITY/IN 15.32.44.41
SLPFF 0.46104
VP 4.392

SNM B
SMM C
SAR E
SOC F



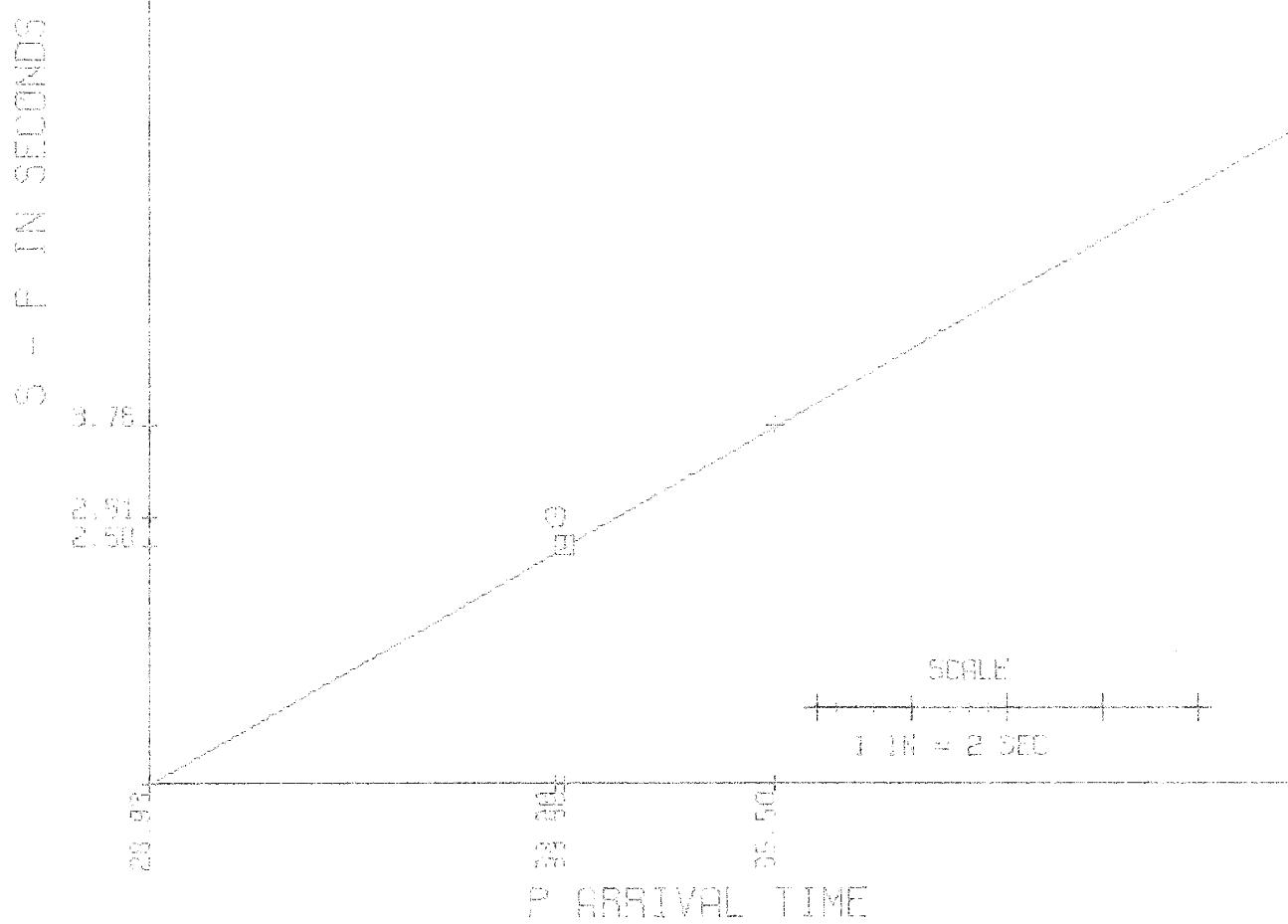
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VF 5.400

5M4 □
5M1 ○
5B2 △
5C2 ▲



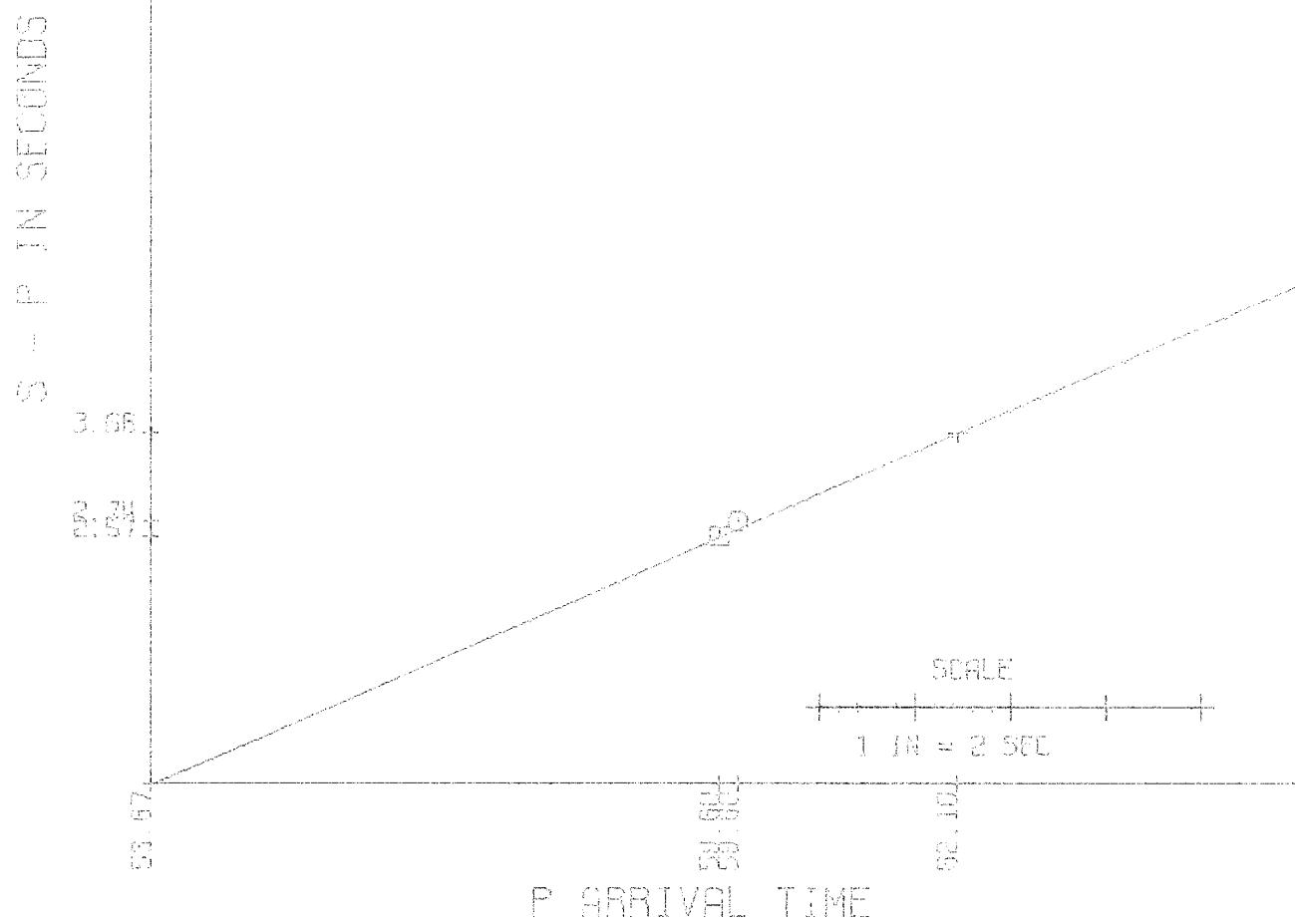
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SLOPE 11.57273
VP 5.286

SNM m
SRM o
SBS a
SOC +



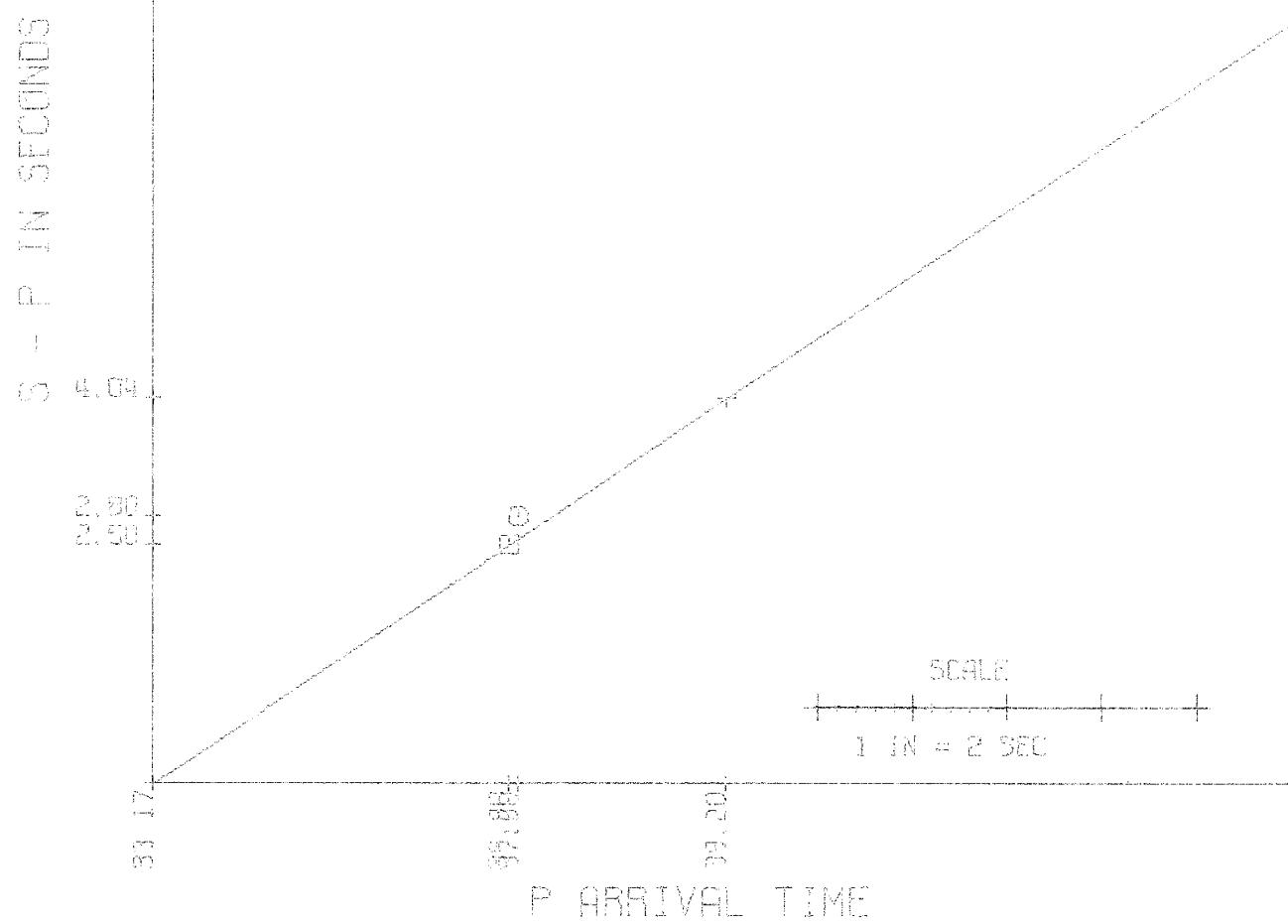
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SLOPE 0.43402
VF 4.862

SMA 25
SPM 25
SSP 4
SOC 4



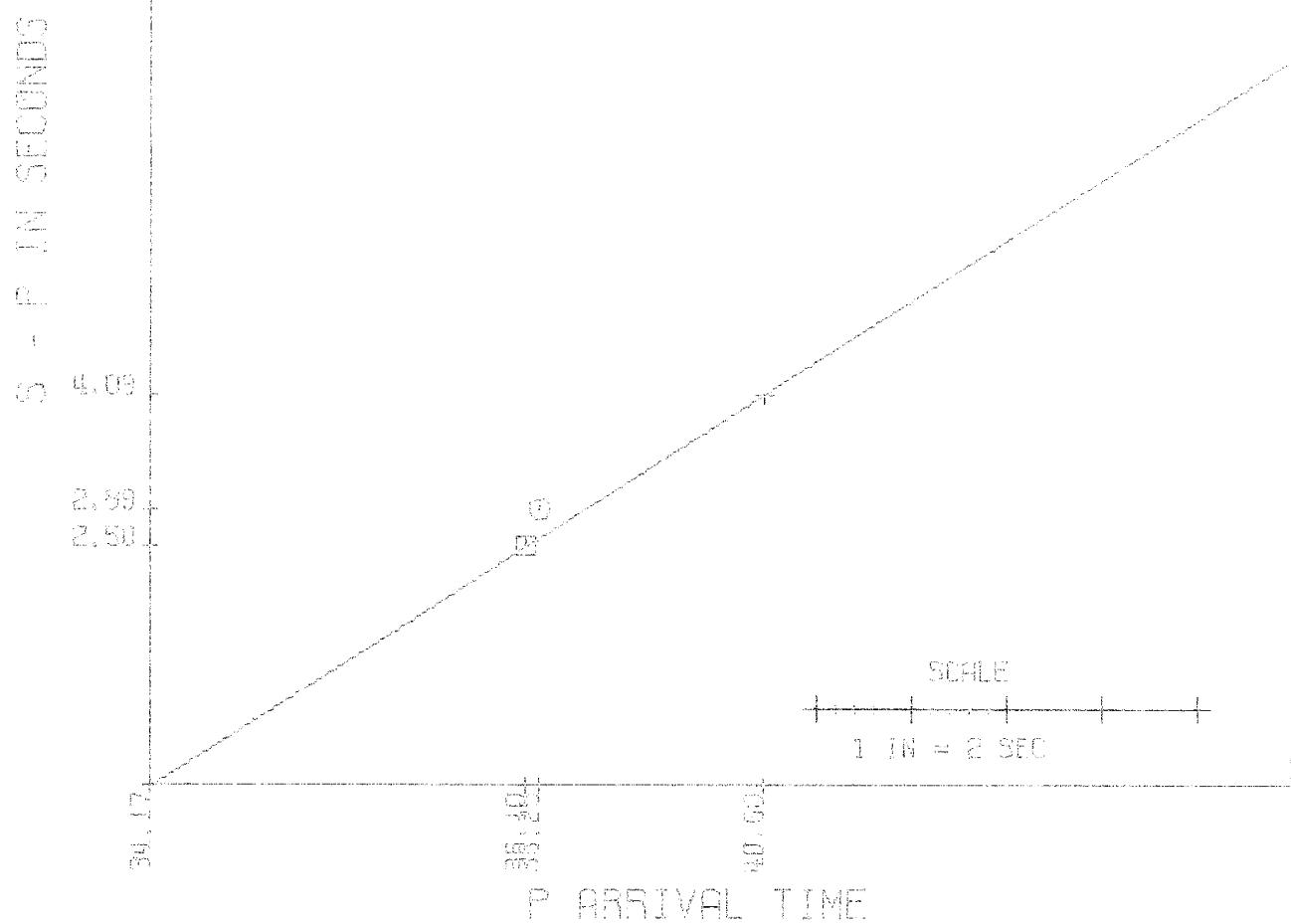
DATE 4/18 /1970
ORIGIN 03.12.33.17
SLOPE 0.66957
VP 5.591

SMA 00
SMR 00
SEB 00
SEC 00



DATE 4/18/1970
ORIGIN 68.2S, 34.17
SLOPE 0.63600
VP 5.478

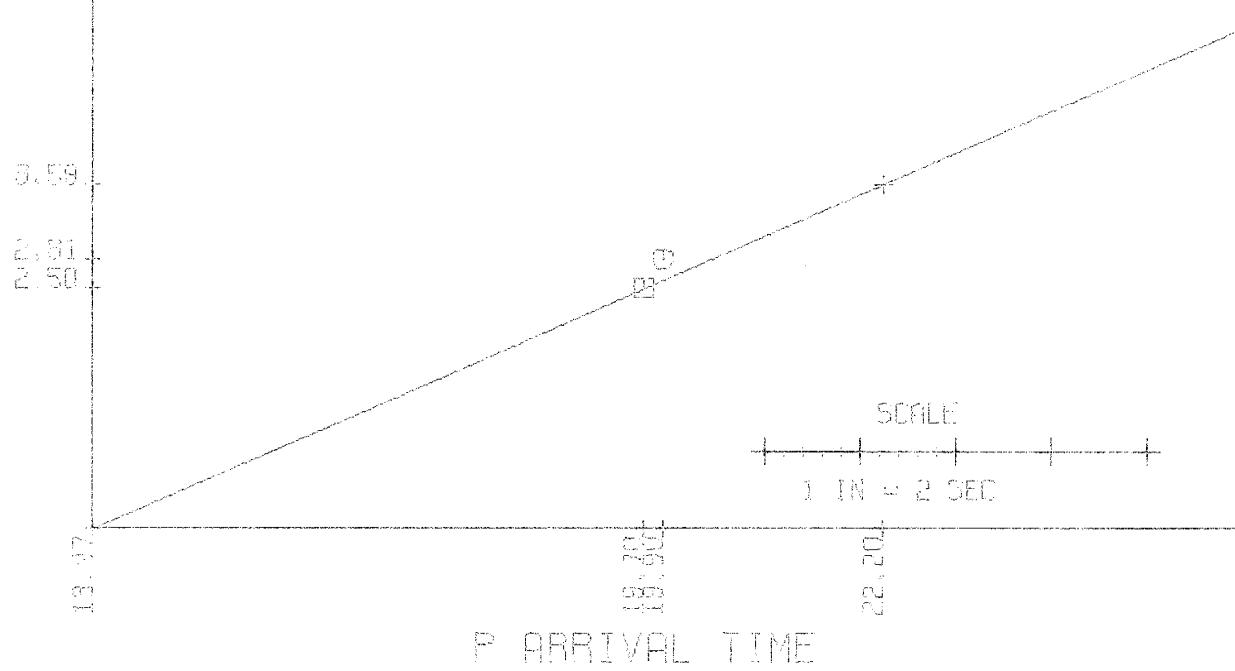
SIM 25
SMI 0
SBR 4
SCU 4



DATE 4/13/1970
ORIGIN 18.18.12.87
SLOPE 0.43600
VP 4.809

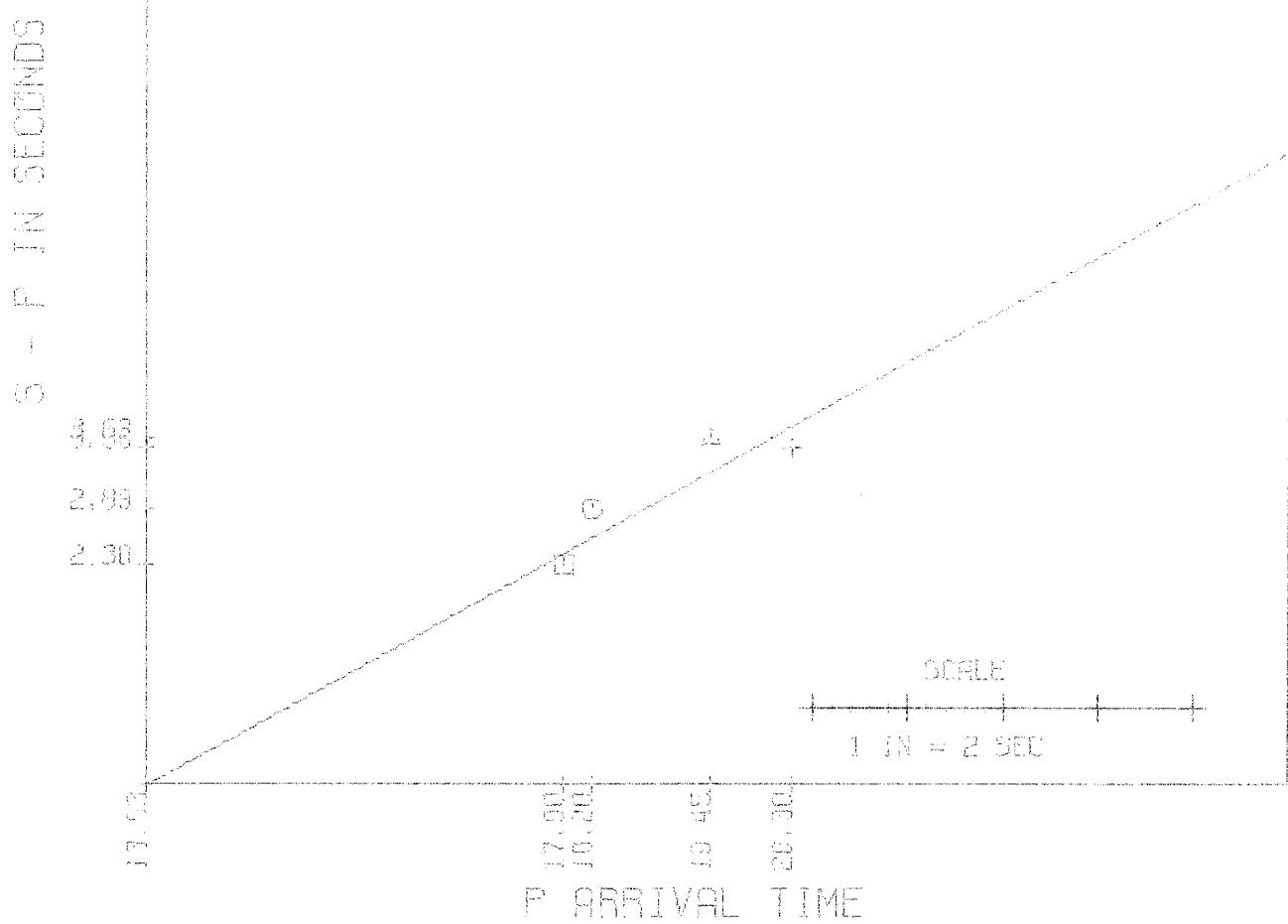
SNR B
SDM D
SBS A
SOC C

CHANGES IN P-VELOCITY



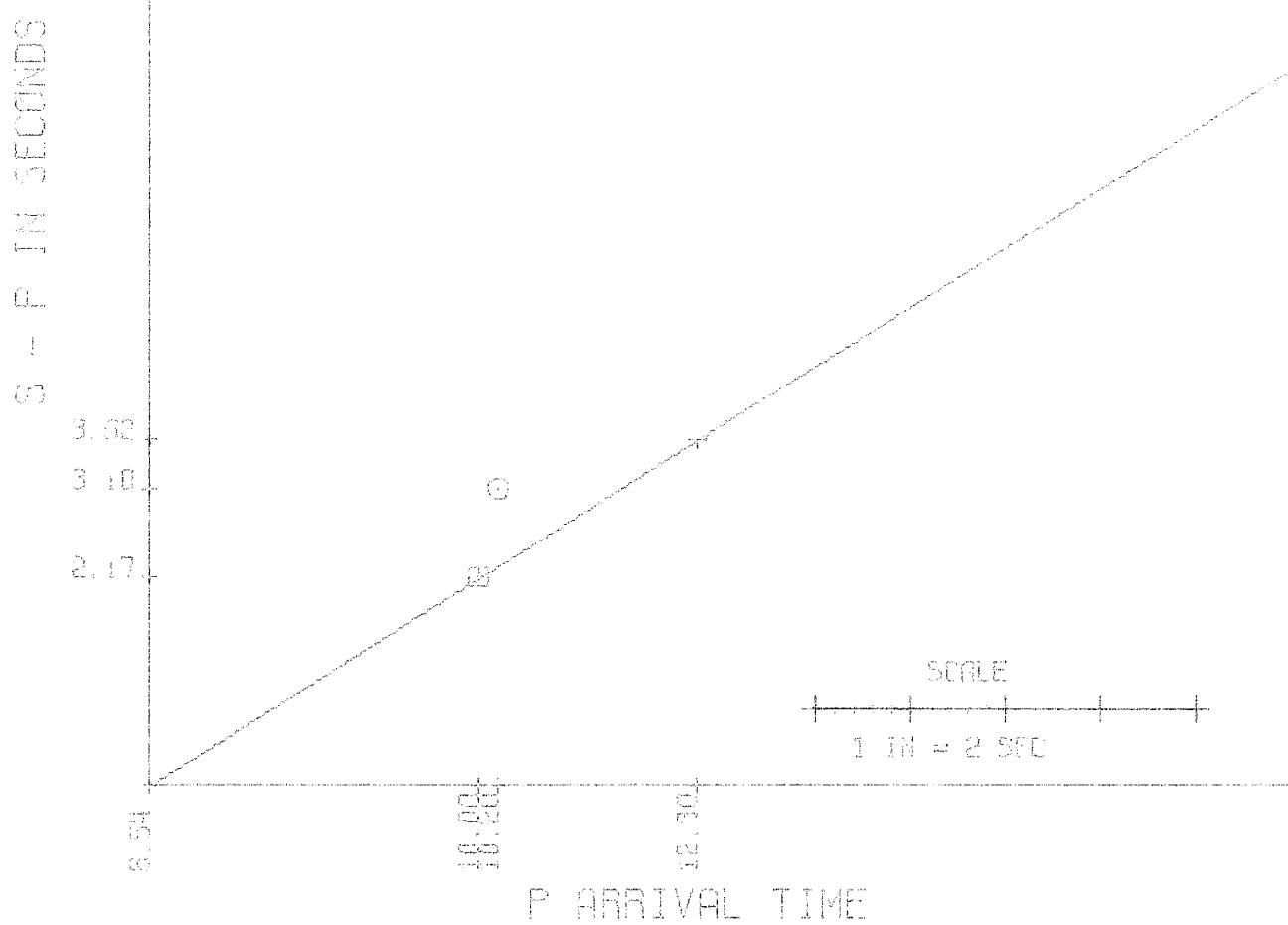
DATE 6/05/1970
ORIGIN 22.44.13.75
DEPTH 0.55341
VP 5.203

SNM E
SEM O
SAB A
SOC P



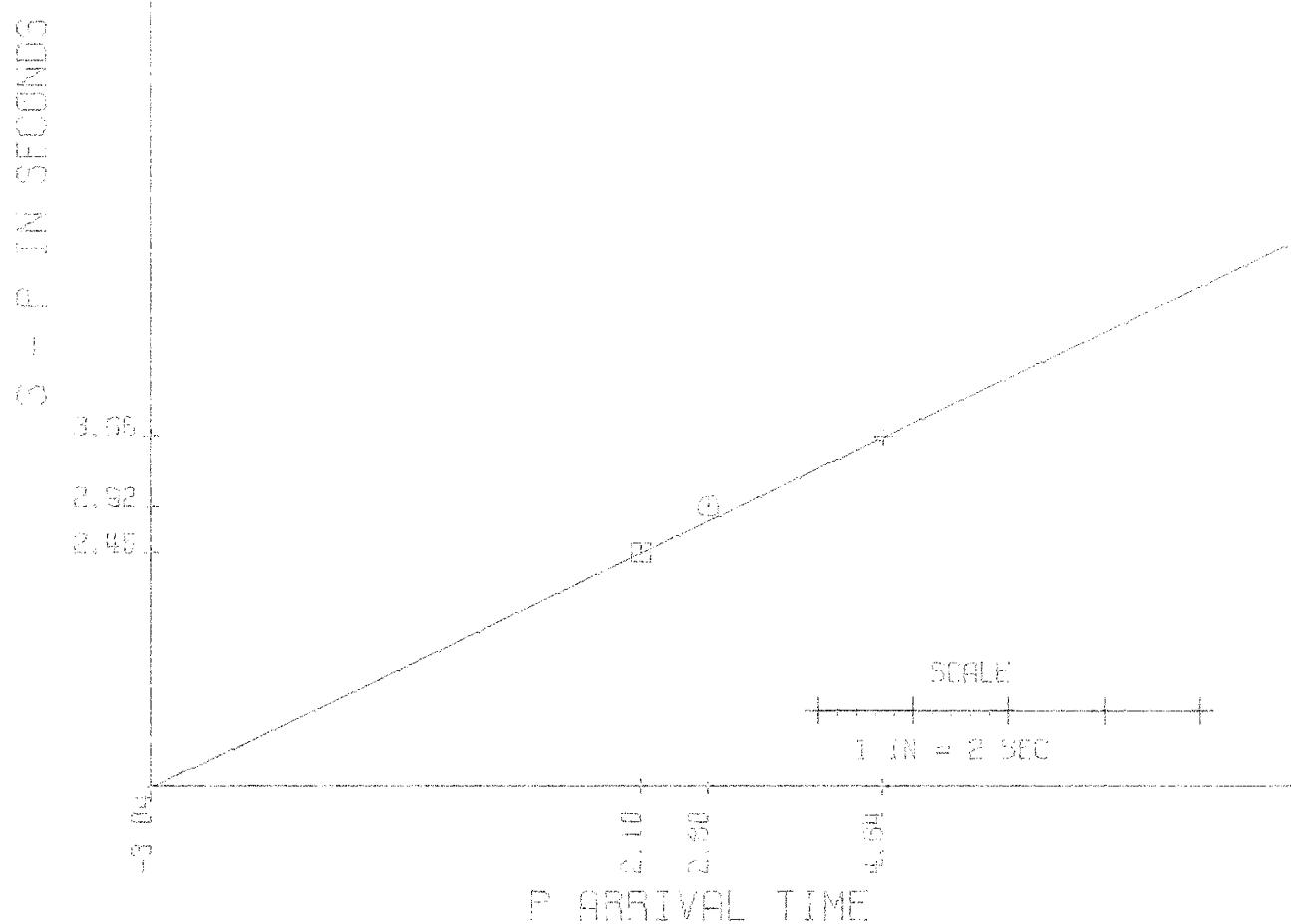
DATE 5/05/1970
ORIGIN 23.03.6.64
SLOPE 0.62326
VP 5.452

SNM 12
SPM 20
SSB 24
SSC 4



DATE 5/13/1970
ORIGIN 02.31.-3.64
SLOPE 0.47533
VF 0.344

SMI 01
SPM 00
SSB 00
SOC 00

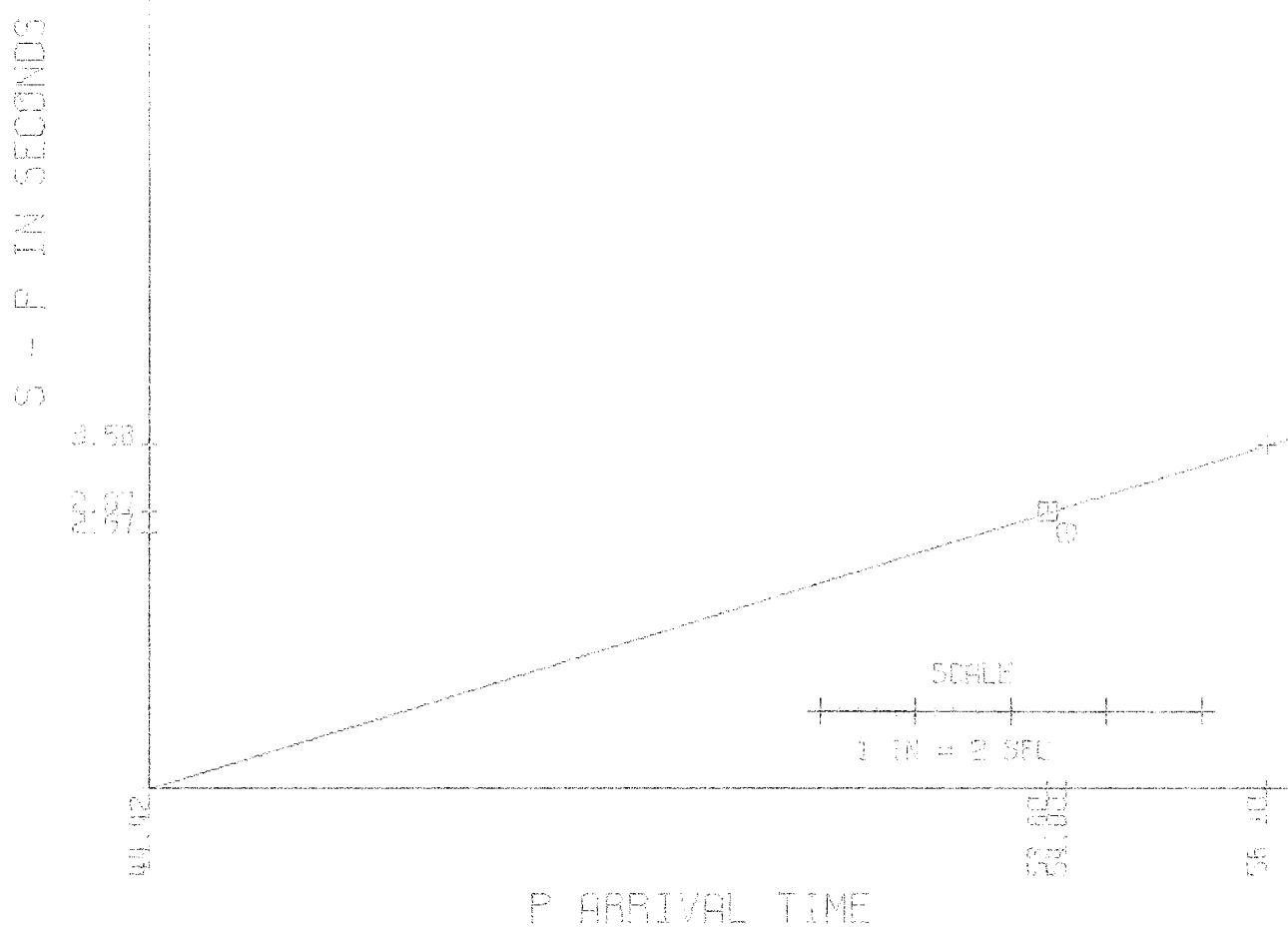


| | |
|--------|-------------|
| DATE | 5/01/1878 |
| ORIGIN | 15,36,38,75 |
| SLR# | 0,66667 |
| VP | 5,561 |

SNM
SEM
SER
SOC

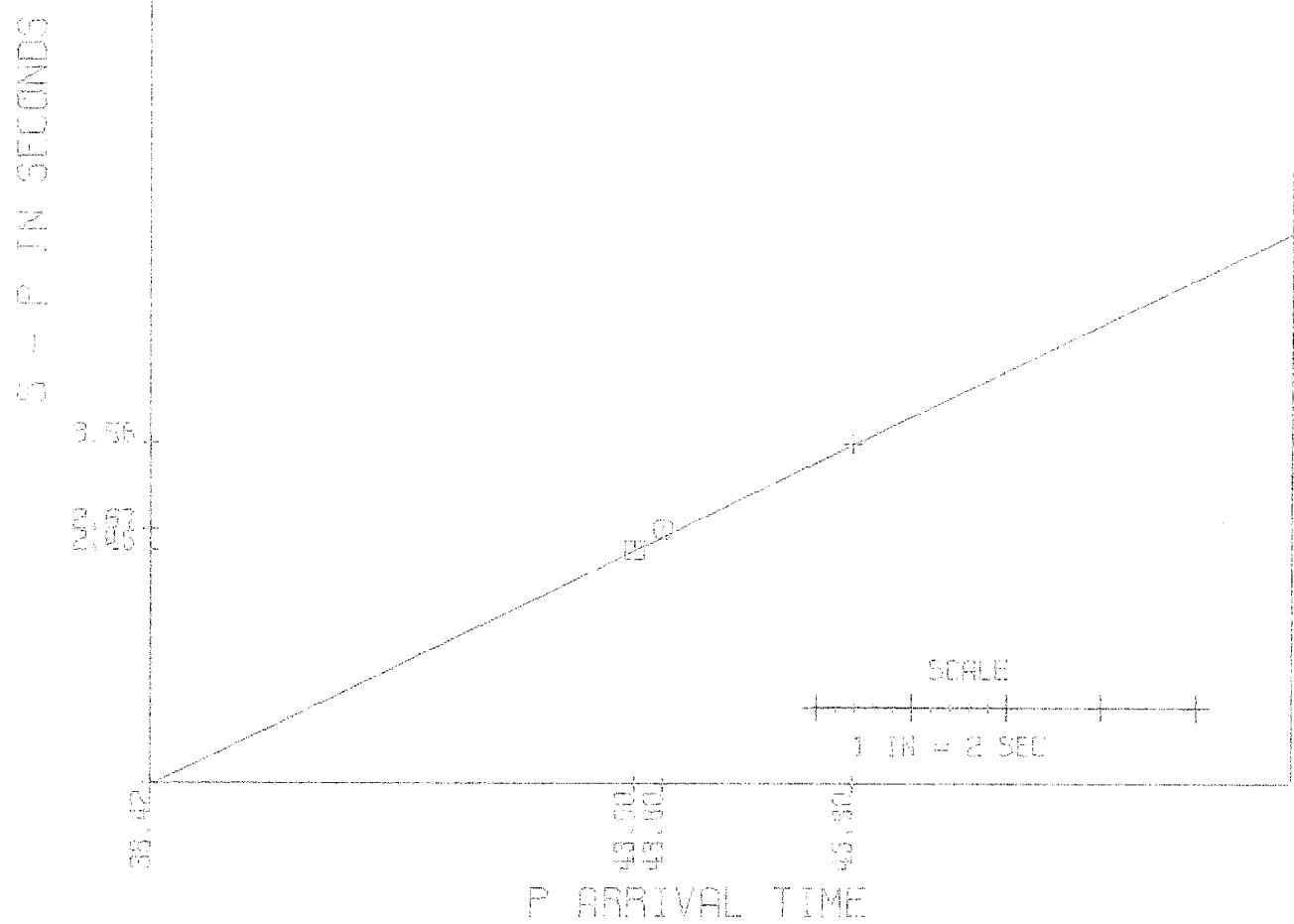
DATE 5/31/1970
BRICKIN 22.17.41.42
SLOPE 0.30852
qP 0.375

SIM C
SEM O
SSC A
SPC P



DATE 6/02 /1970
ORIGIN 00.22.38.42
SLOPE 0.43261
VP 4.985

SNM ②
SNM ③
SEC 5
SEC +

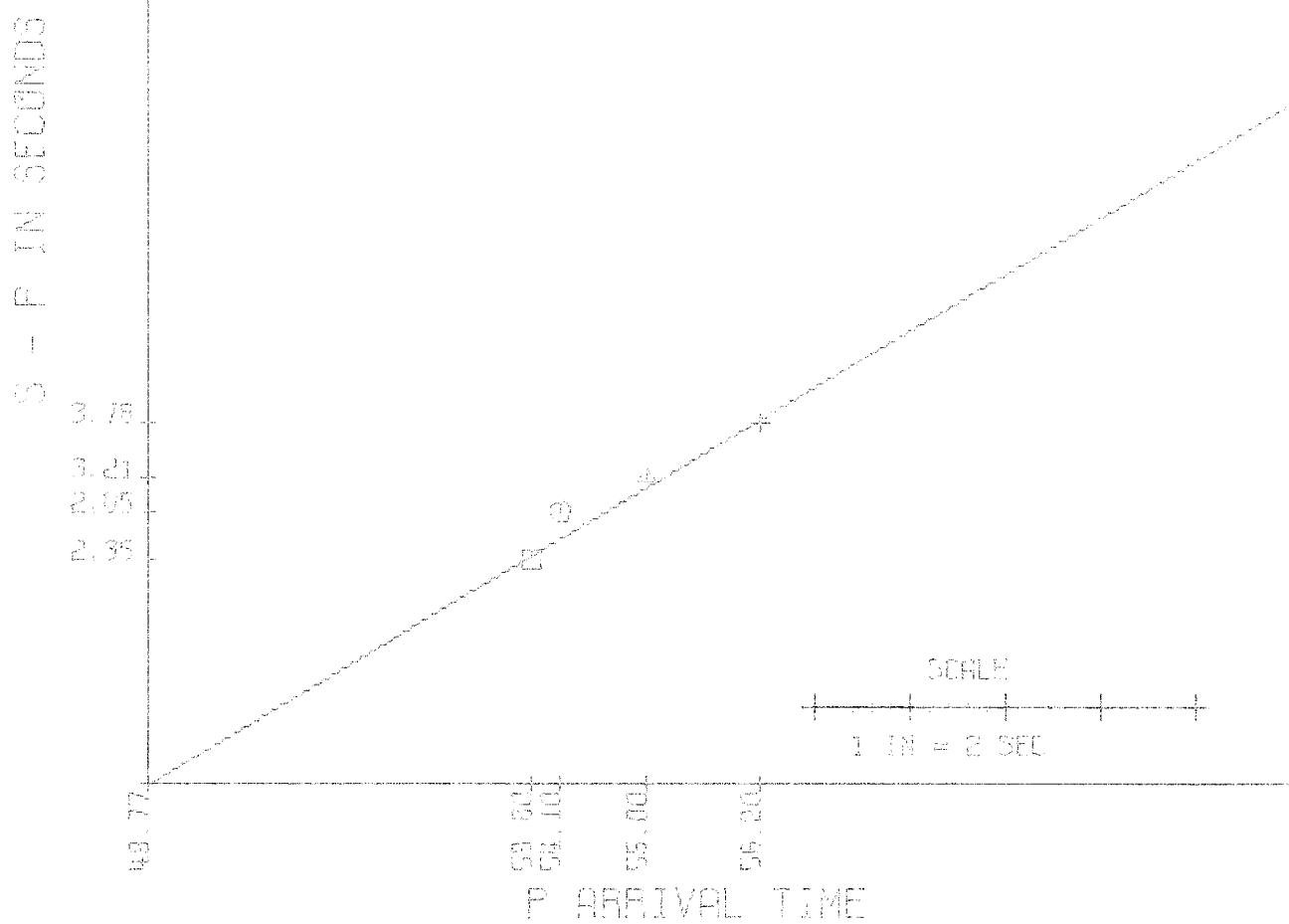


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|--------|-------------|
| DATE | 6/14/1978 |
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| REF ID | C. 53271 |
| VP | 5.102 |

SHE
SEN
SBR
SPC

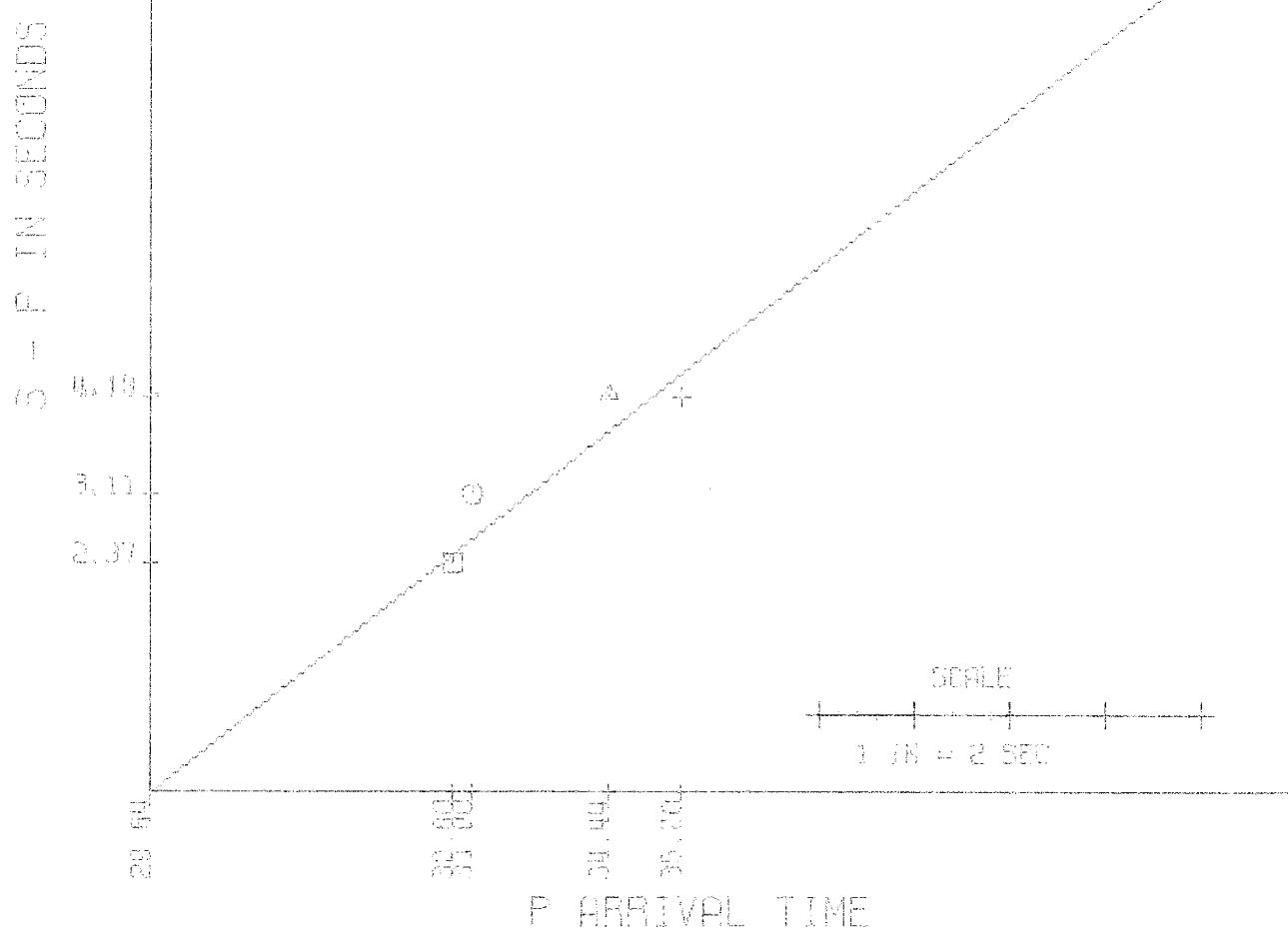
| | |
|--------|-------------------|
| DATE | 5/14 /1970 |
| ORIGIN | CA , BC , AB , YT |
| SLOPE | 0.59502 |
| WP | R , CBU |

卷之三



| | |
|---------|-------------|
| DATE | 6/14/1970 |
| ORIGIN | 07.04.28.64 |
| SLEEPER | U. 78729 |
| VP | 5.935 |

SNM
SEM
SRE
SGE



| | |
|--------|-------------|
| DATE | 5/14/1870 |
| ORIGIN | 09.00.14.62 |
| SLOPE | 0.61200 |
| VP | 0.001 |

SNM
SRM
SBB
SOC

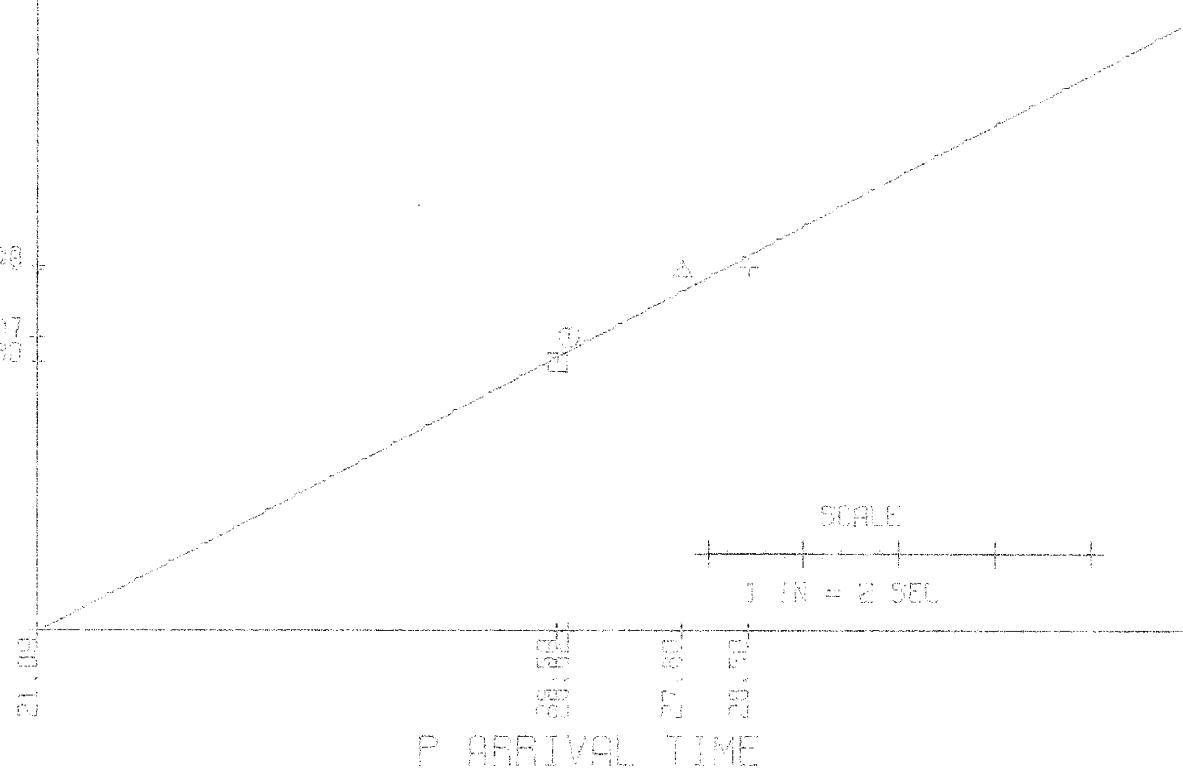
DATE 6/16/1976
 ORIGIN 16.53, 16.50
 SLOPE 0.44619
 VP 14.855

SHM
SPM
SOM
SOC

3 - P ARRIVAL TIMES

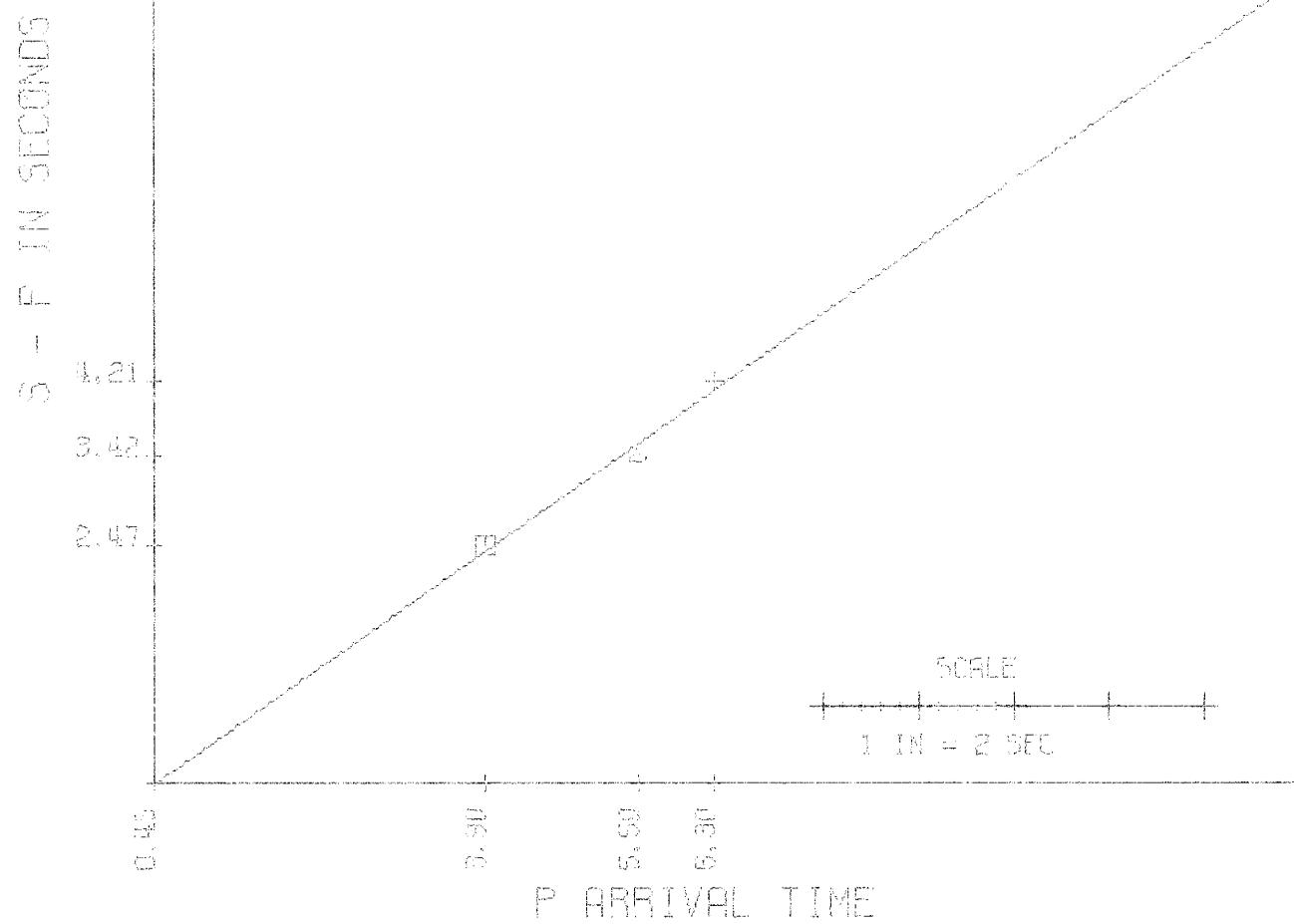
DATE 6/30/1978
TIME 11:30:20 08
SLC# 0.58010
VP 5.124

SIM
SIM
SBC
SOC
P
P
P
P
P
P

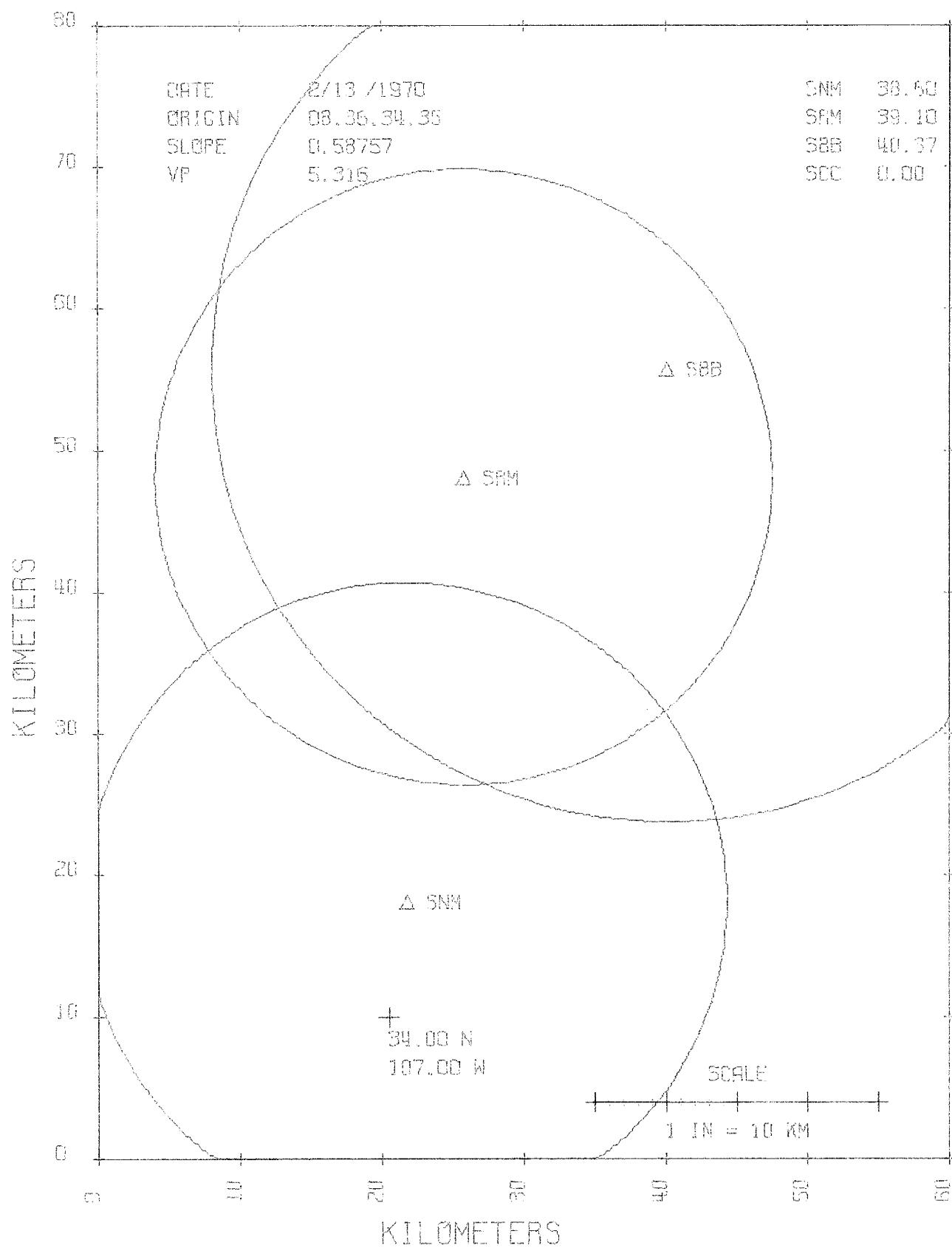


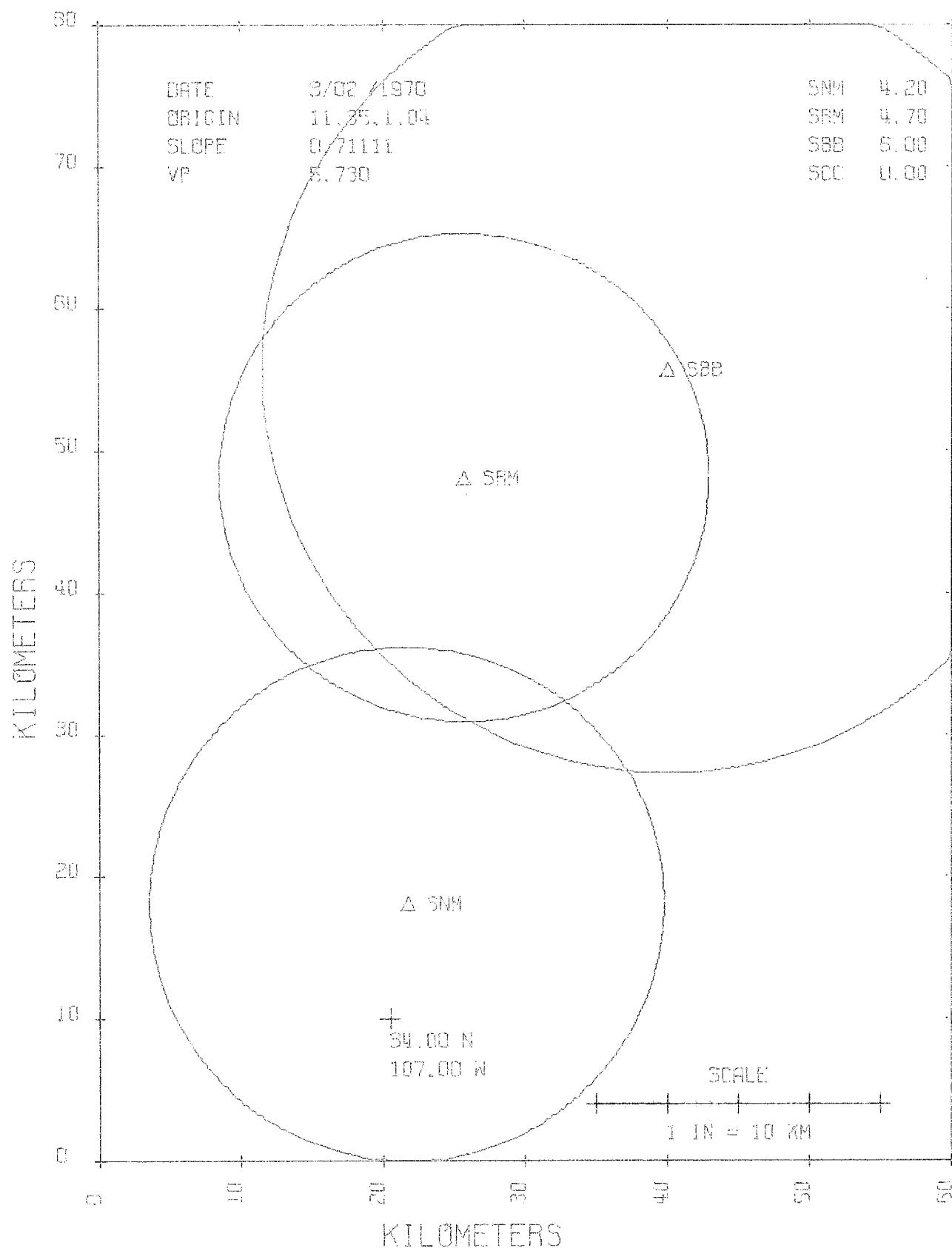
DATE 3/27/1970
ORIGIN 10.36, 0.45
SLOPE 0.70402
VP 5.700

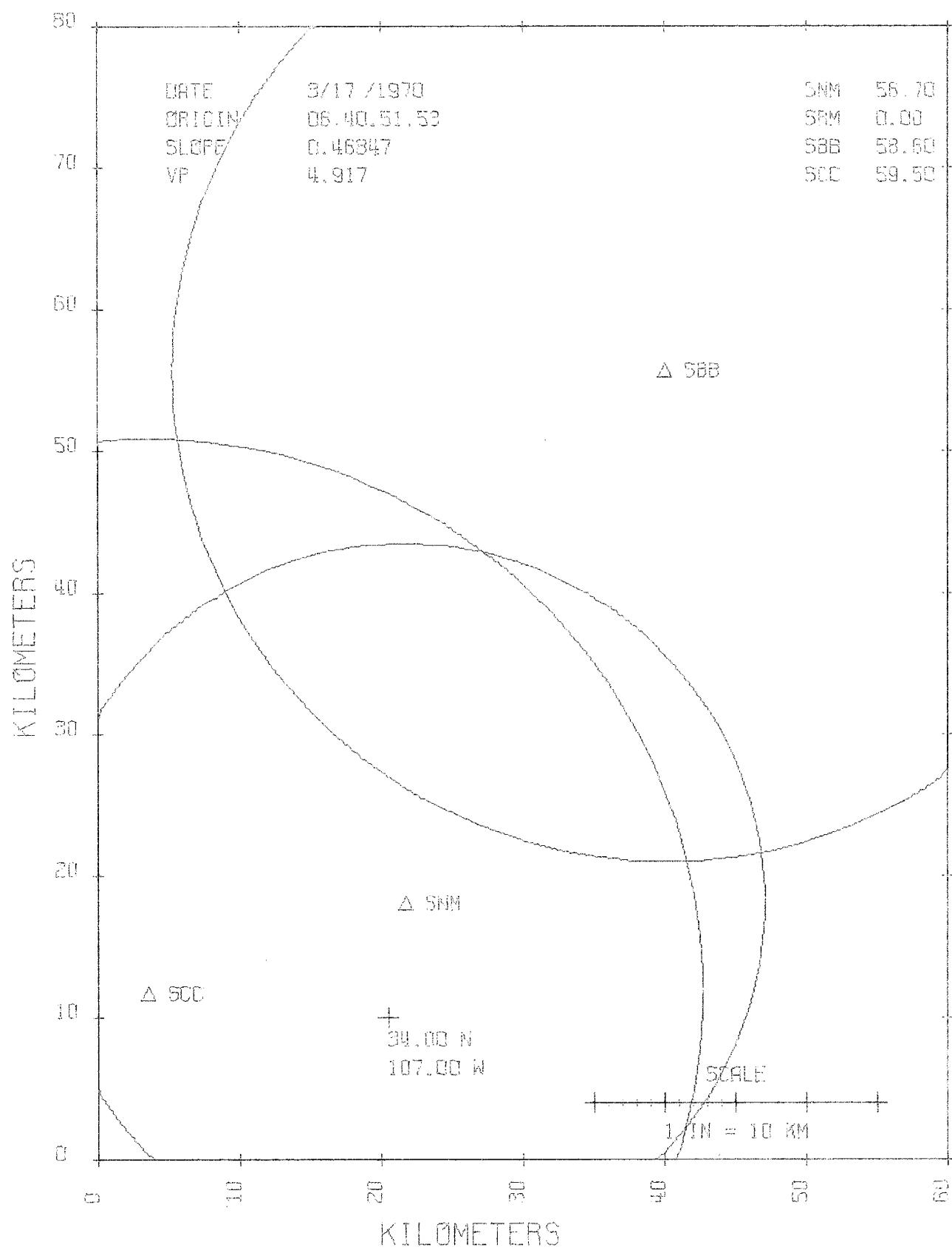
CNM
Stab
S88
500
P
A
E
F
H

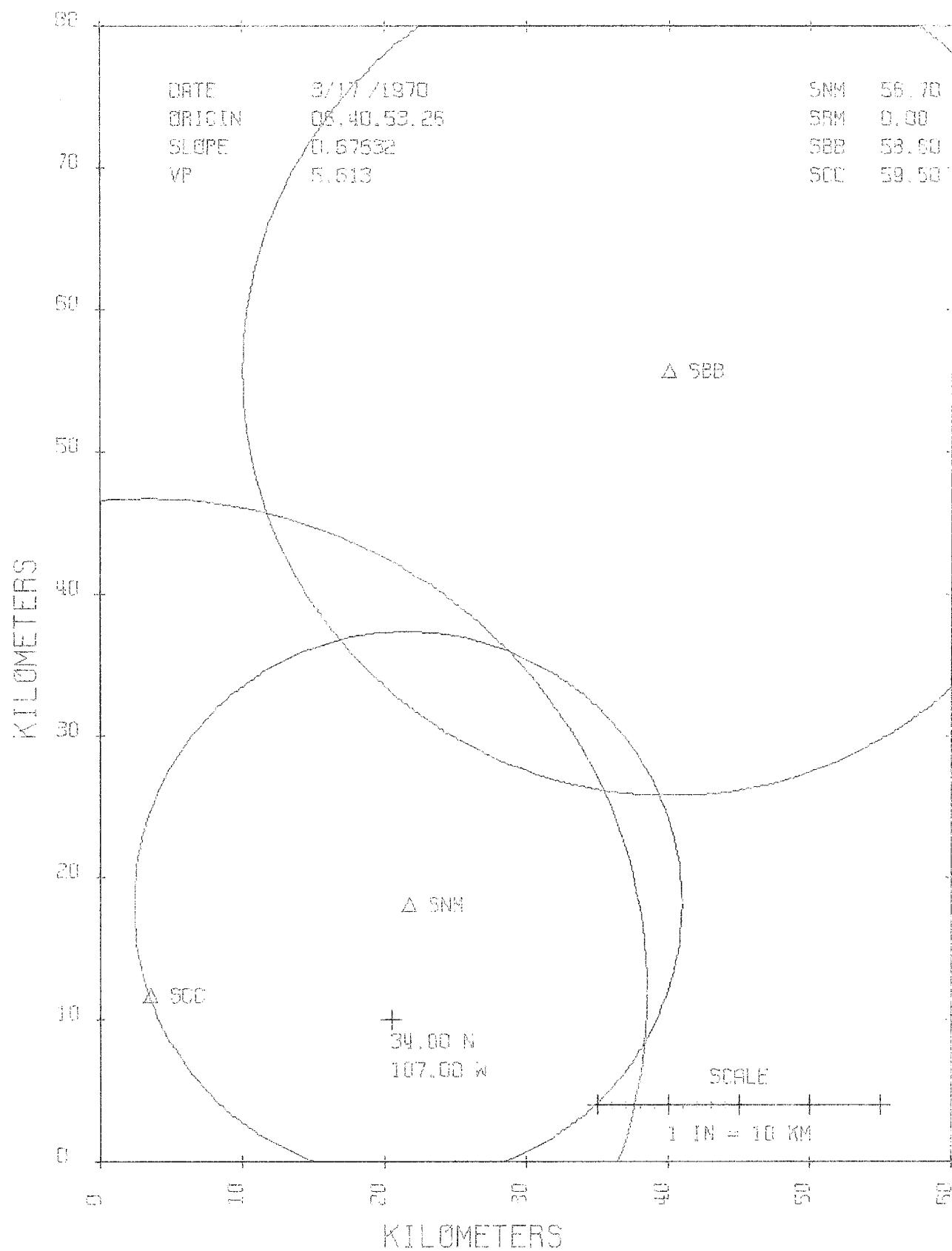


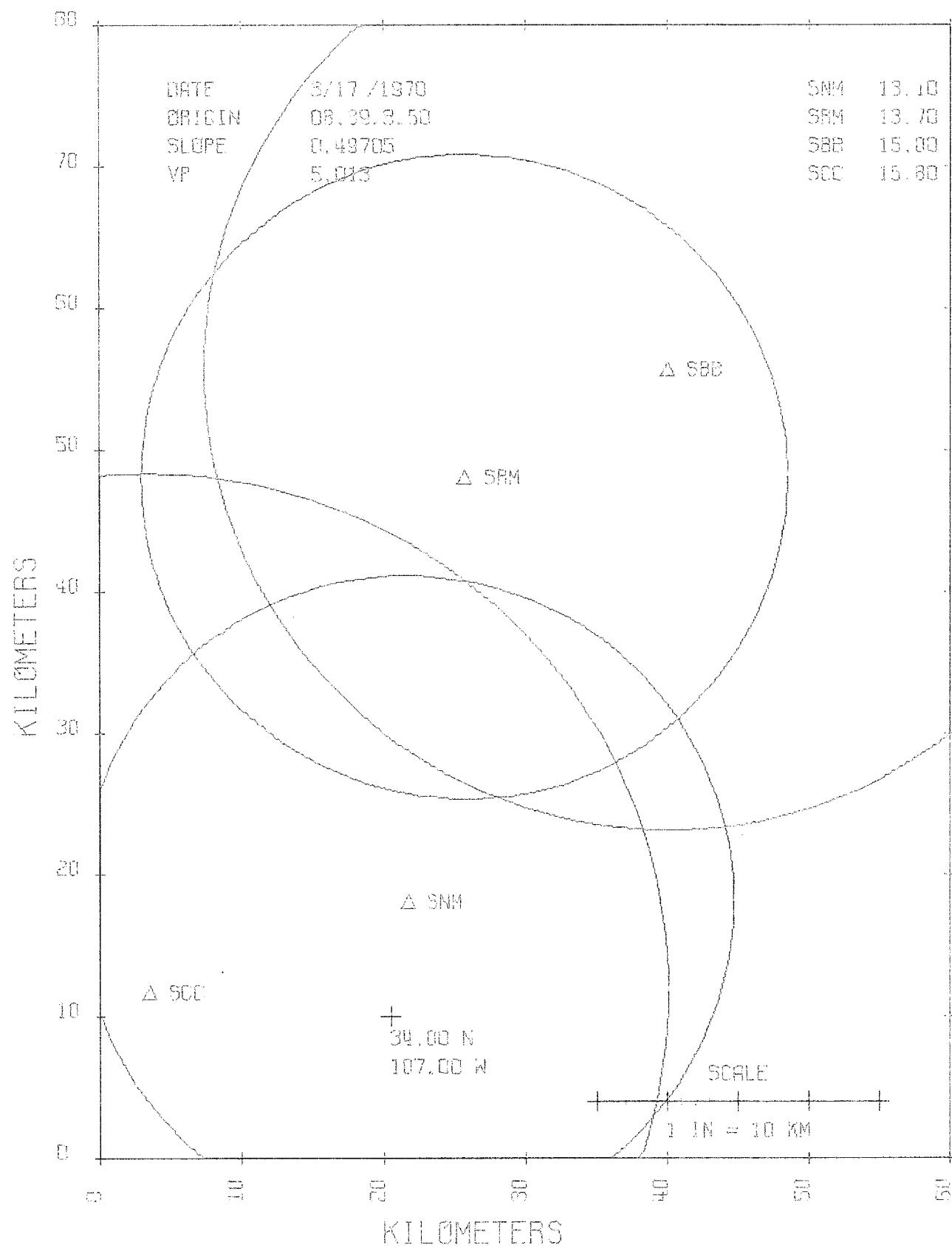
W. E. GUNNARSON
EPIDEMIOLOGIC, TOXICOLOGIC

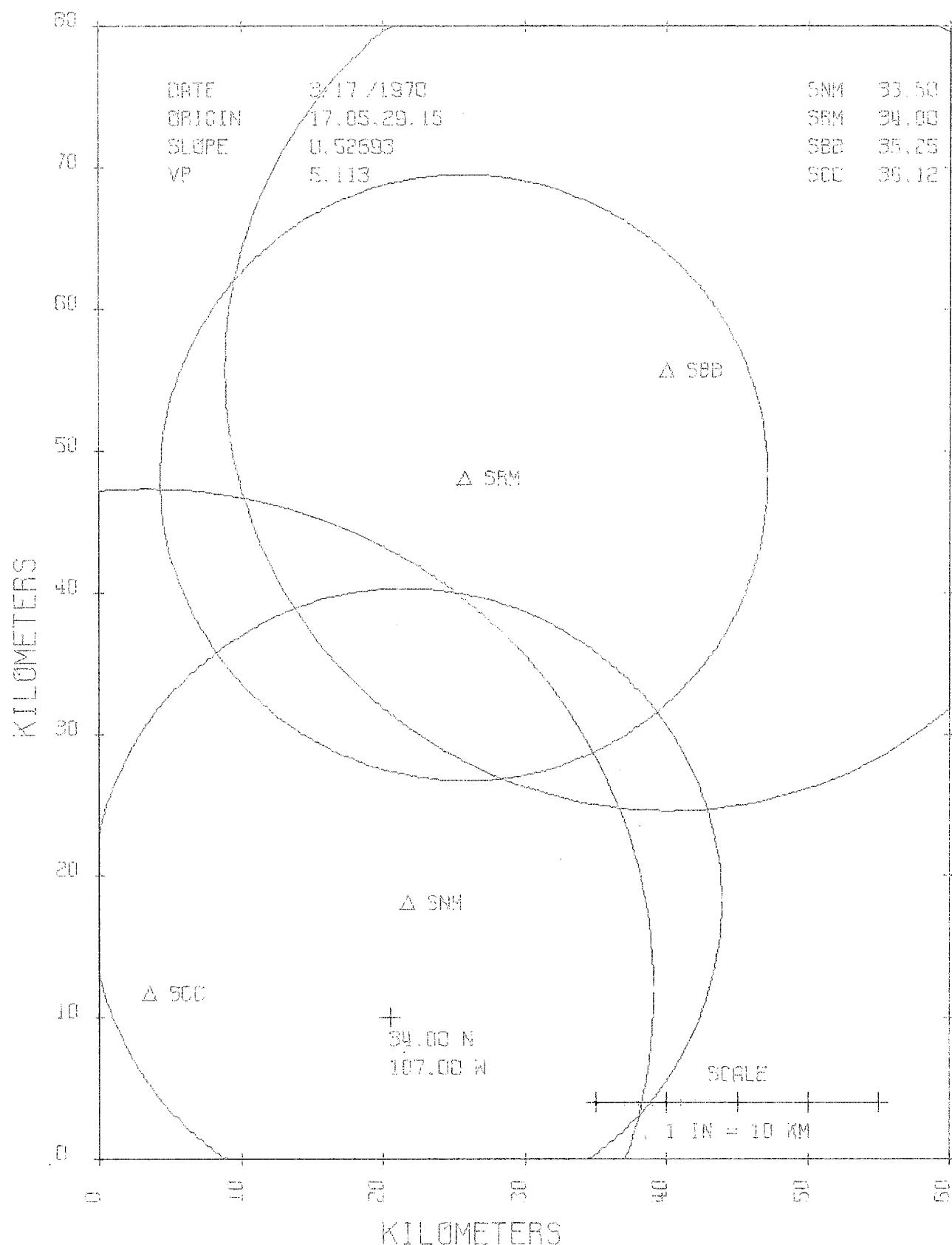


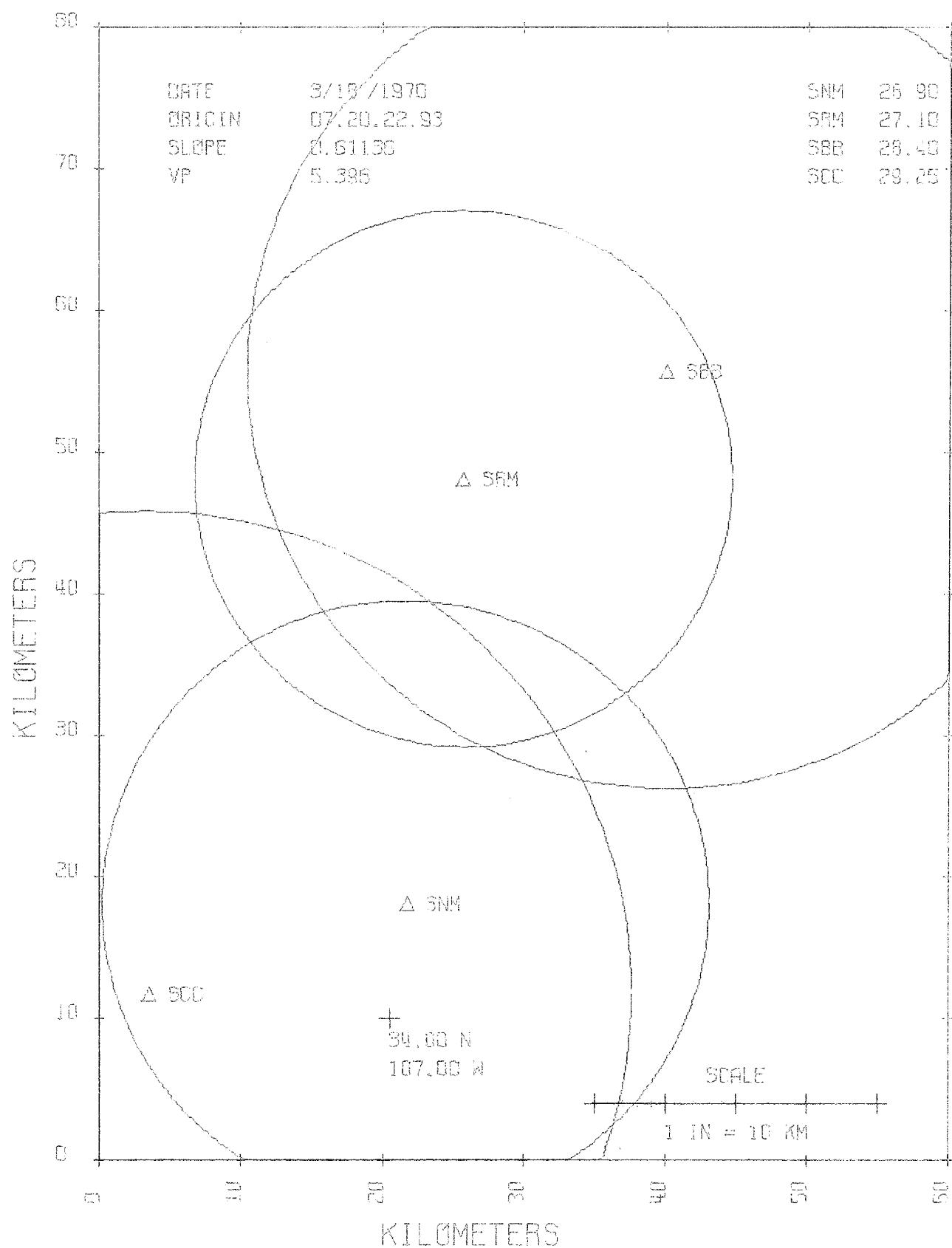


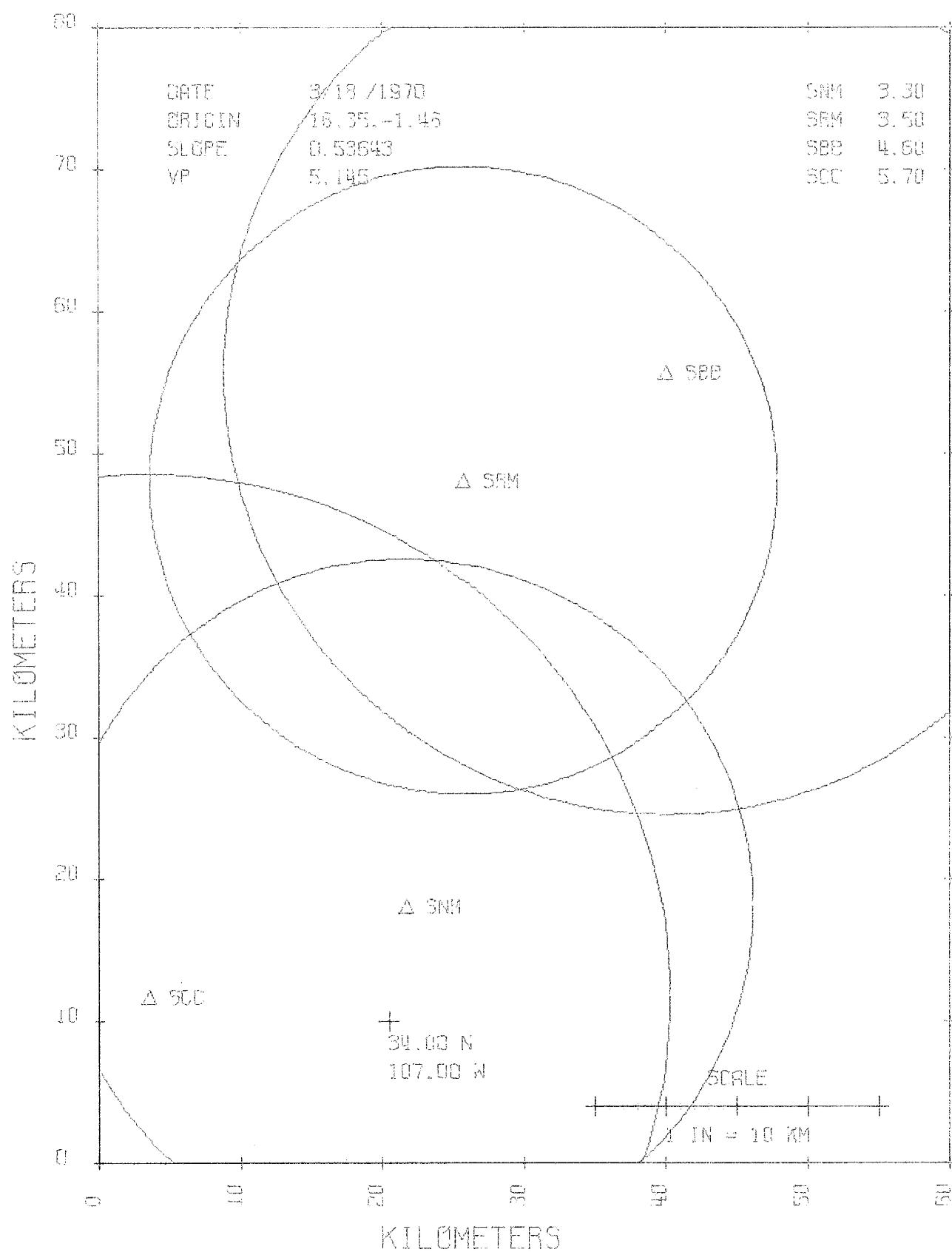


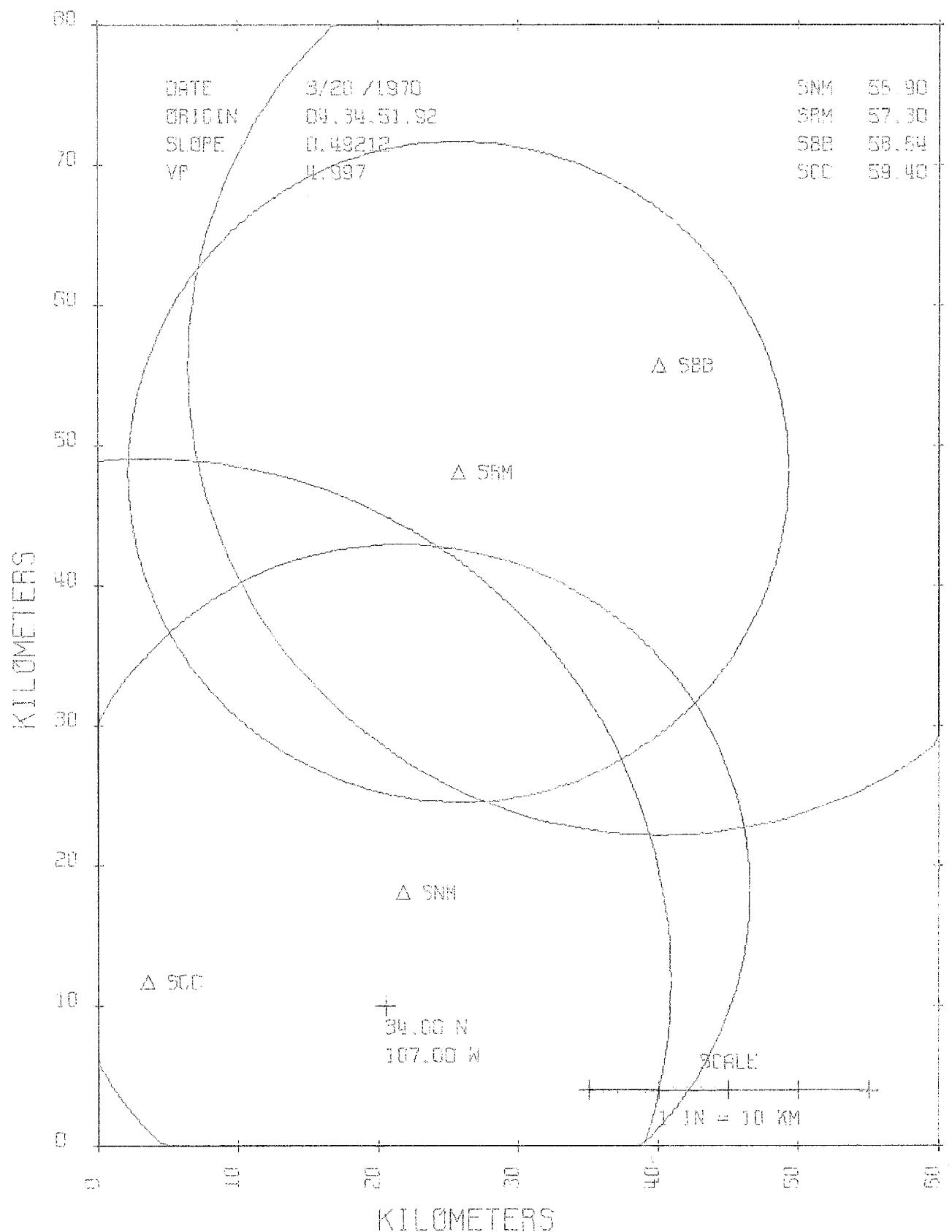


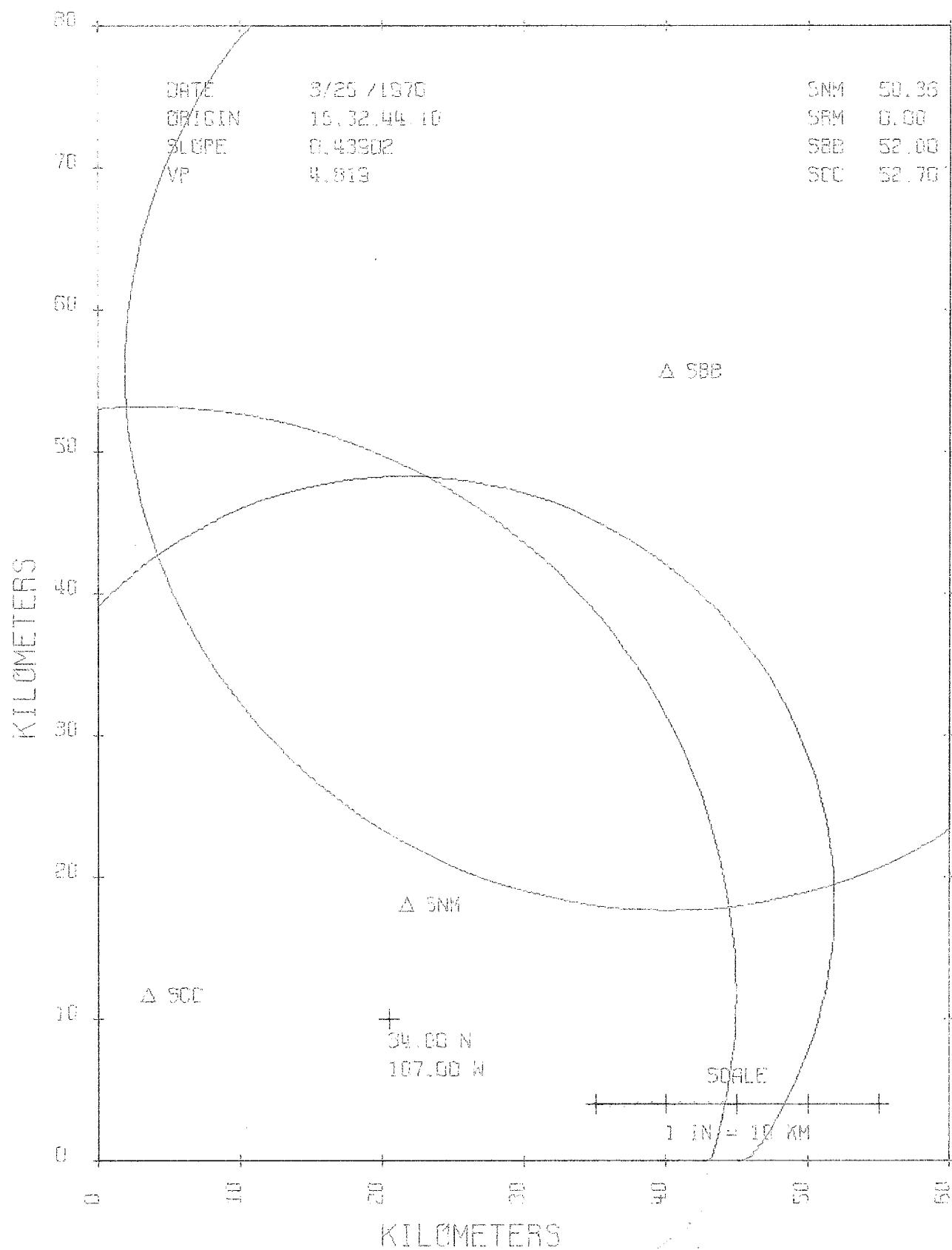


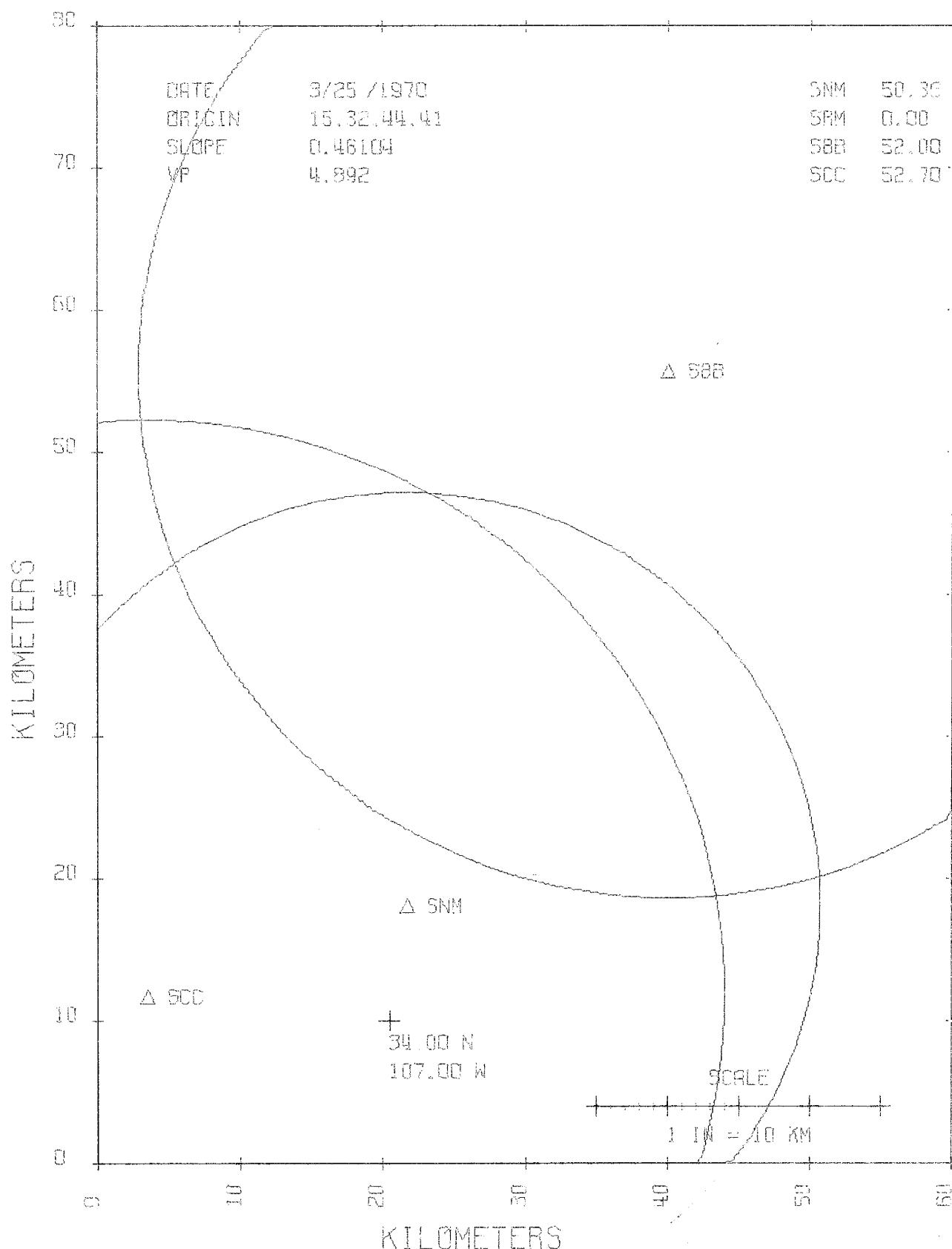


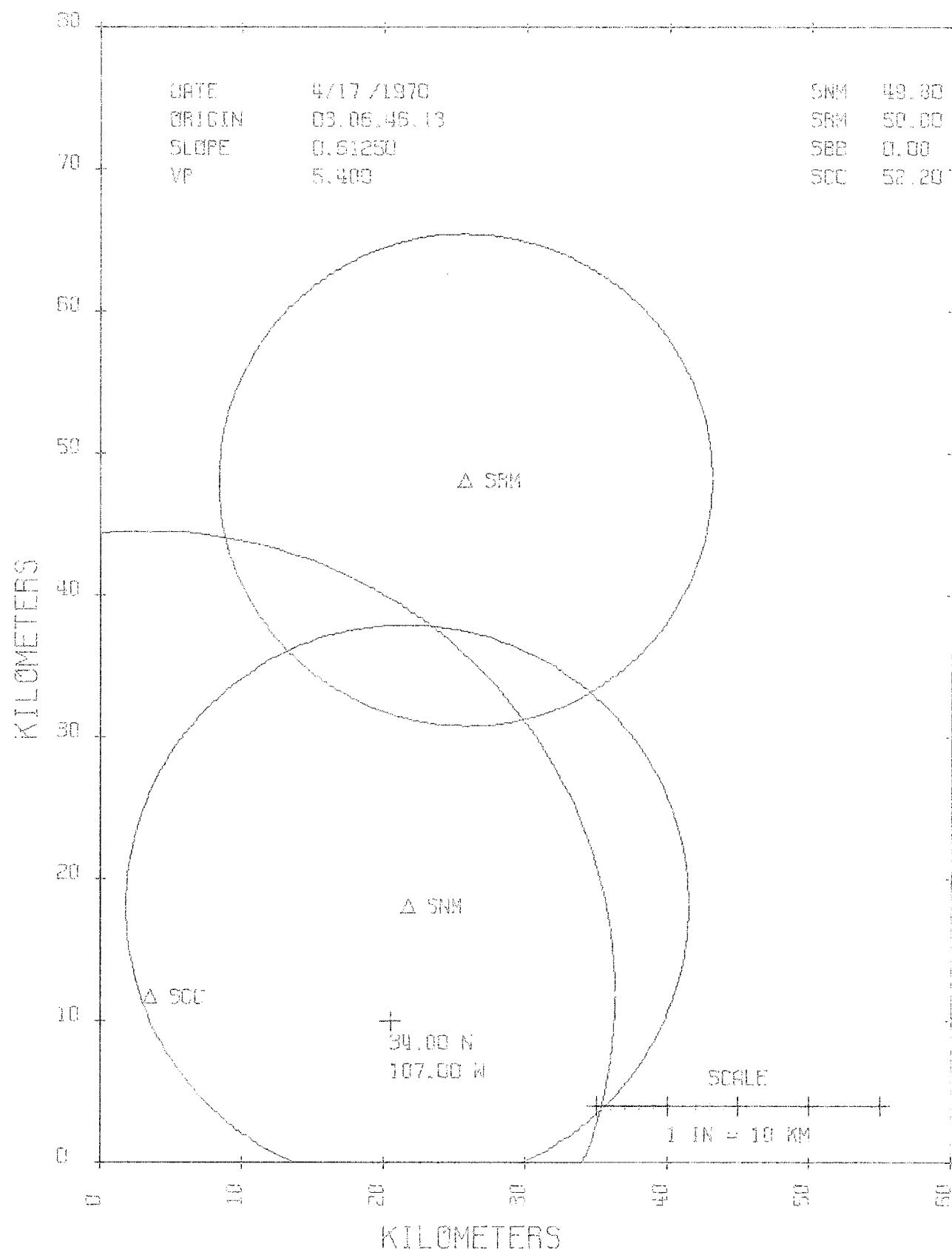


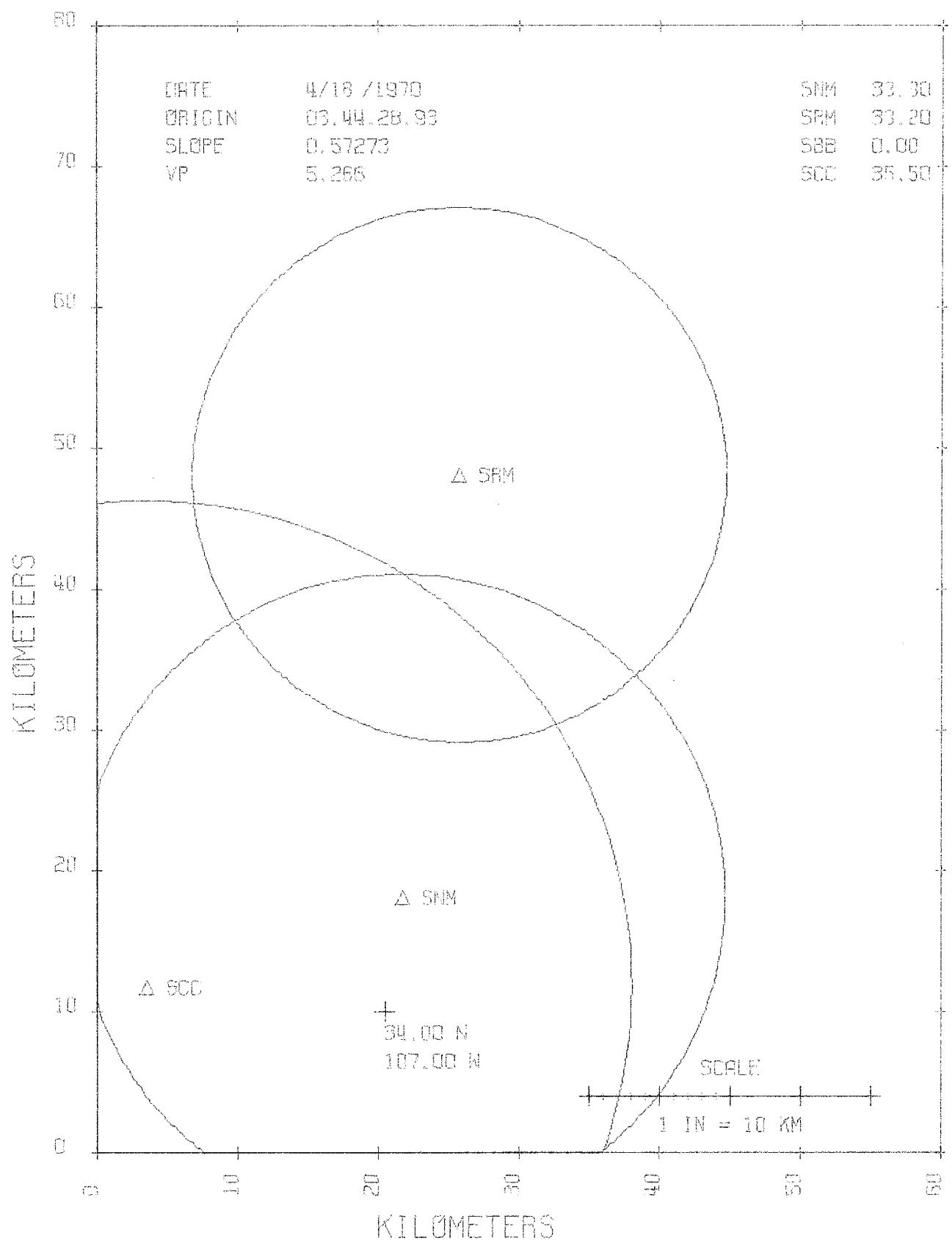


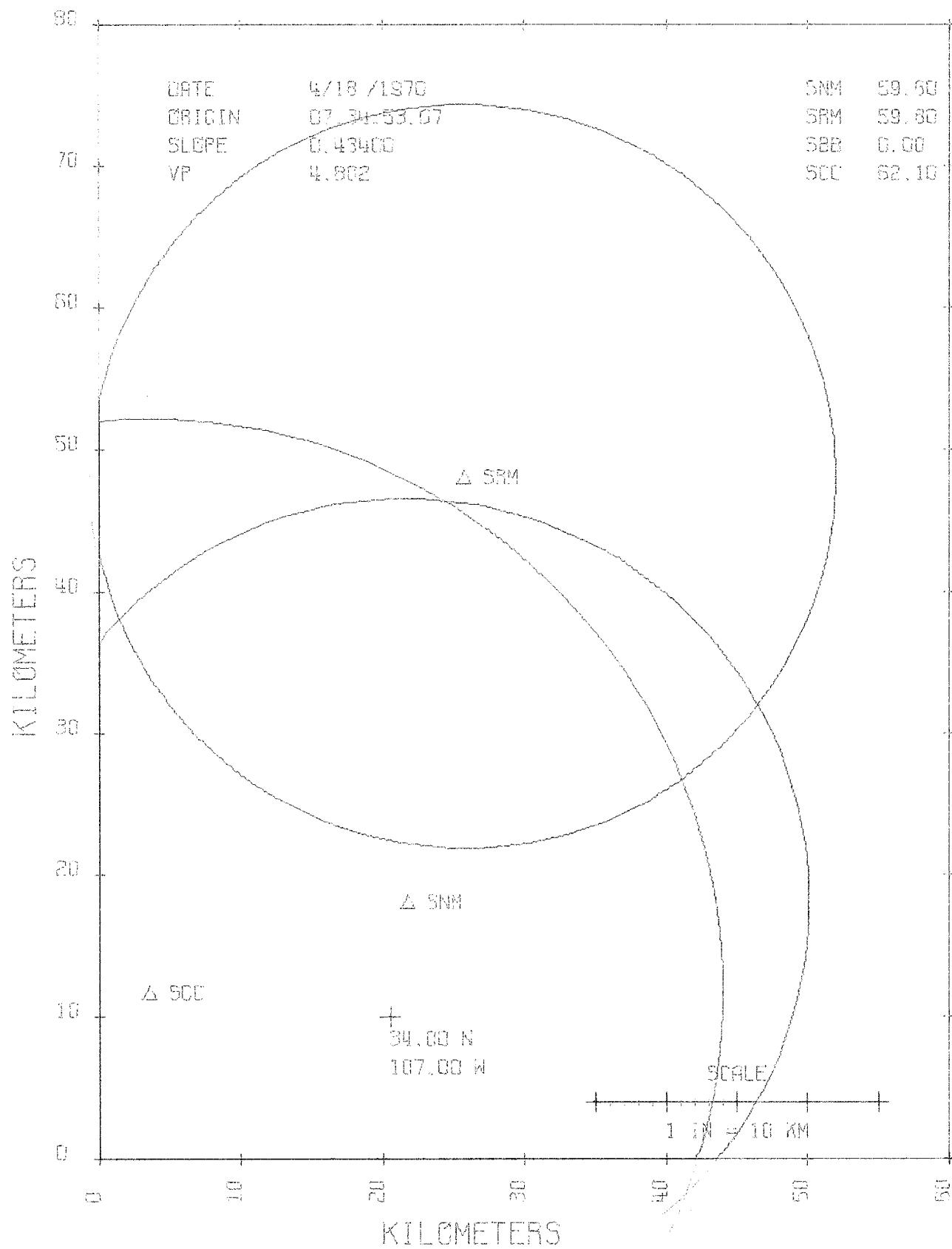


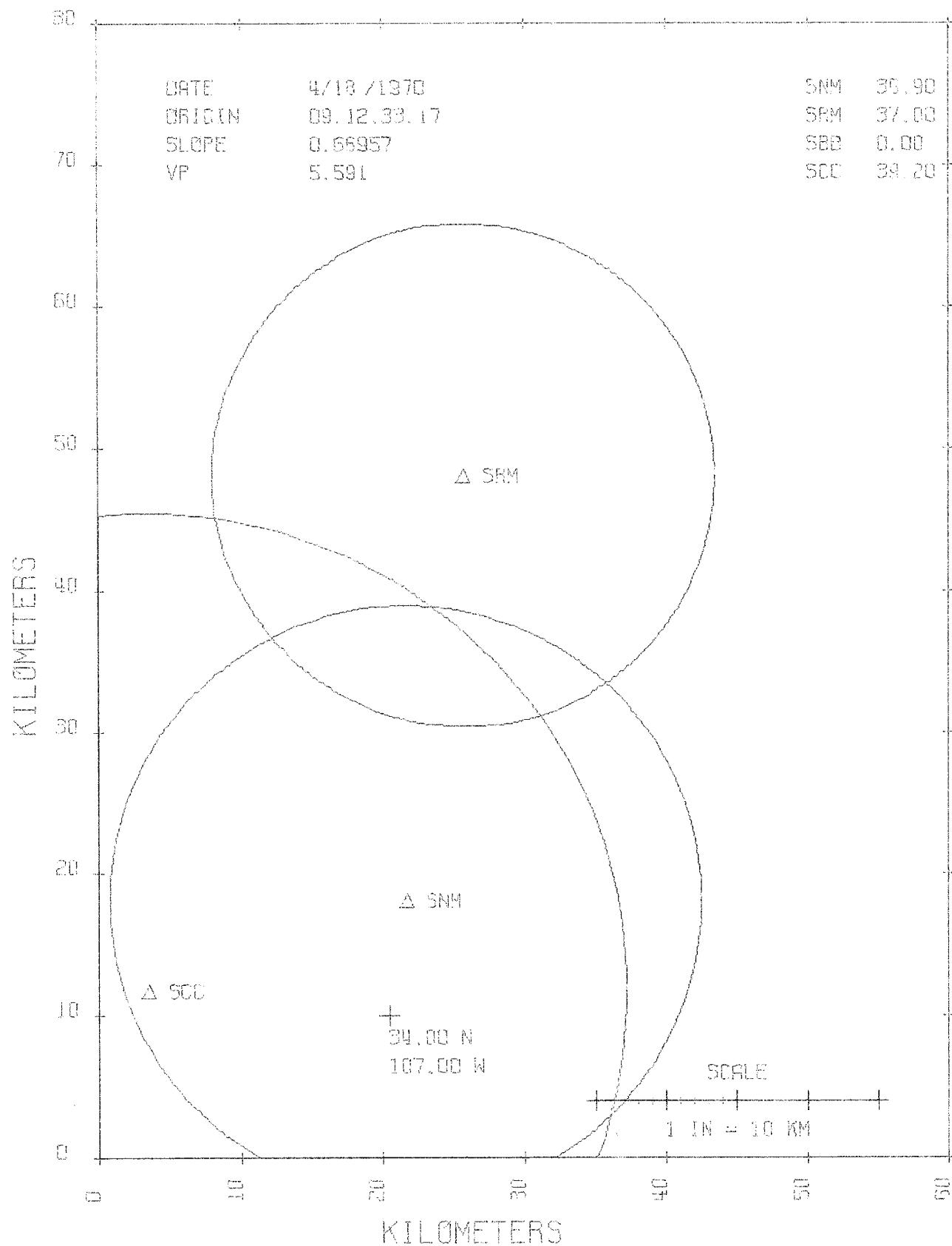


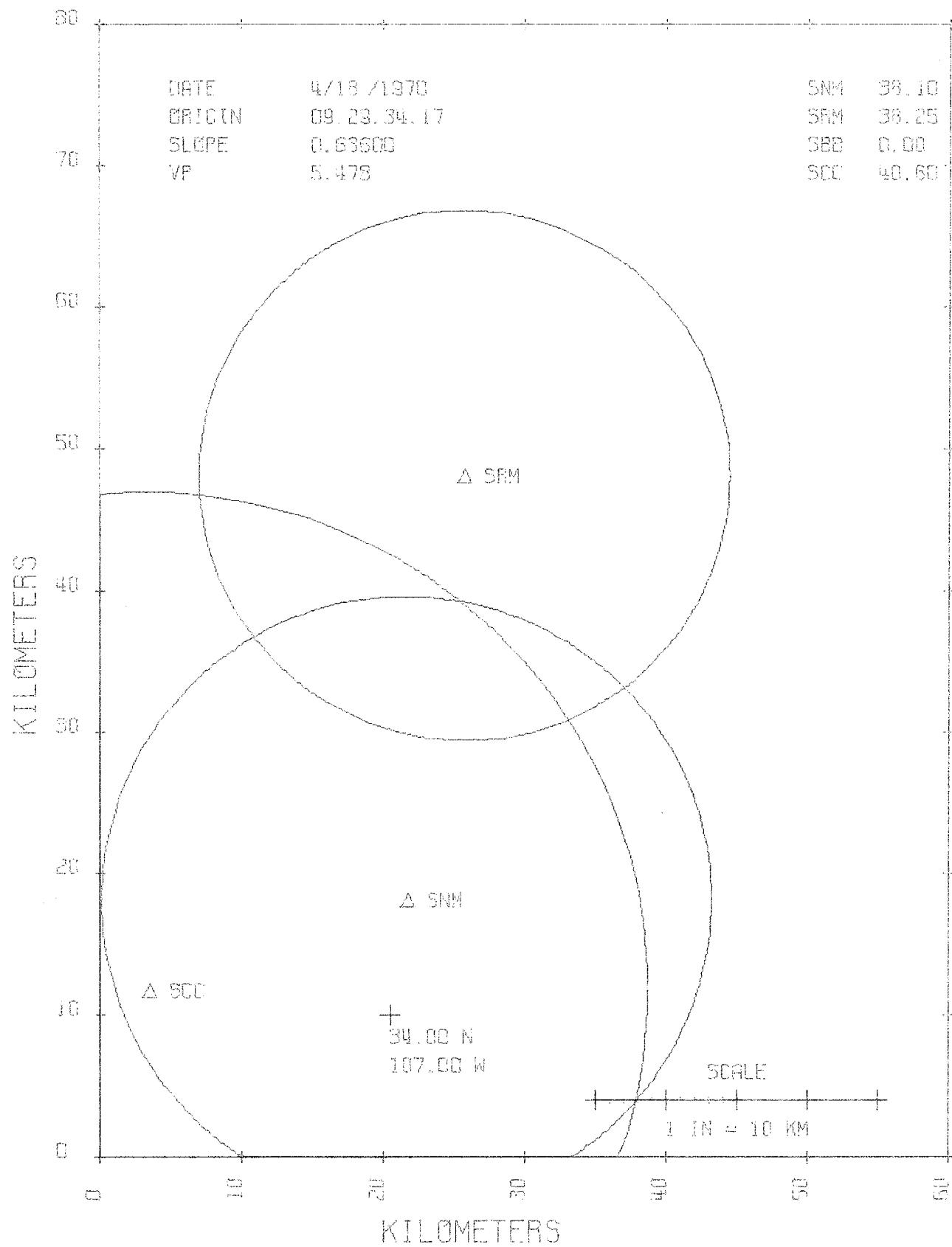


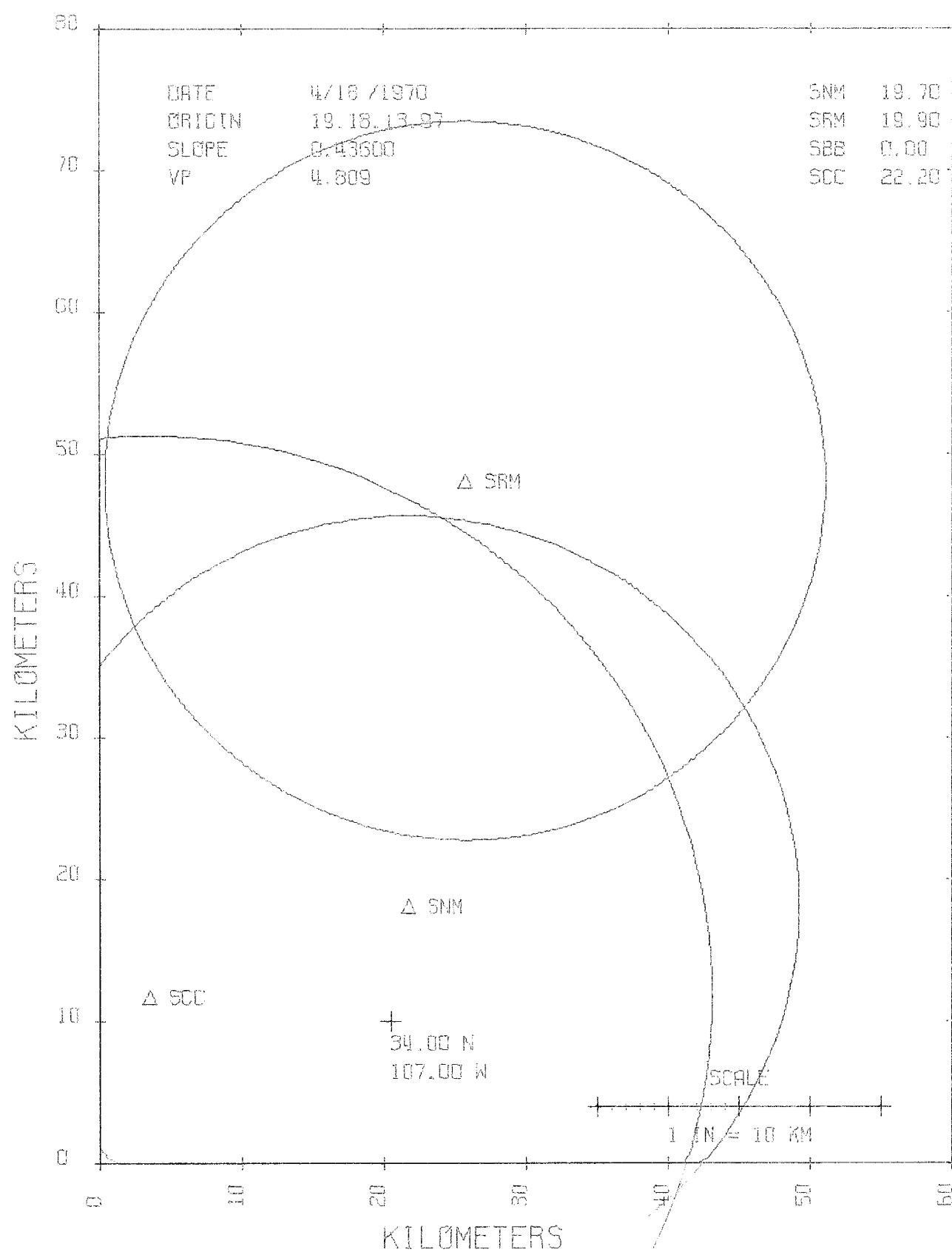


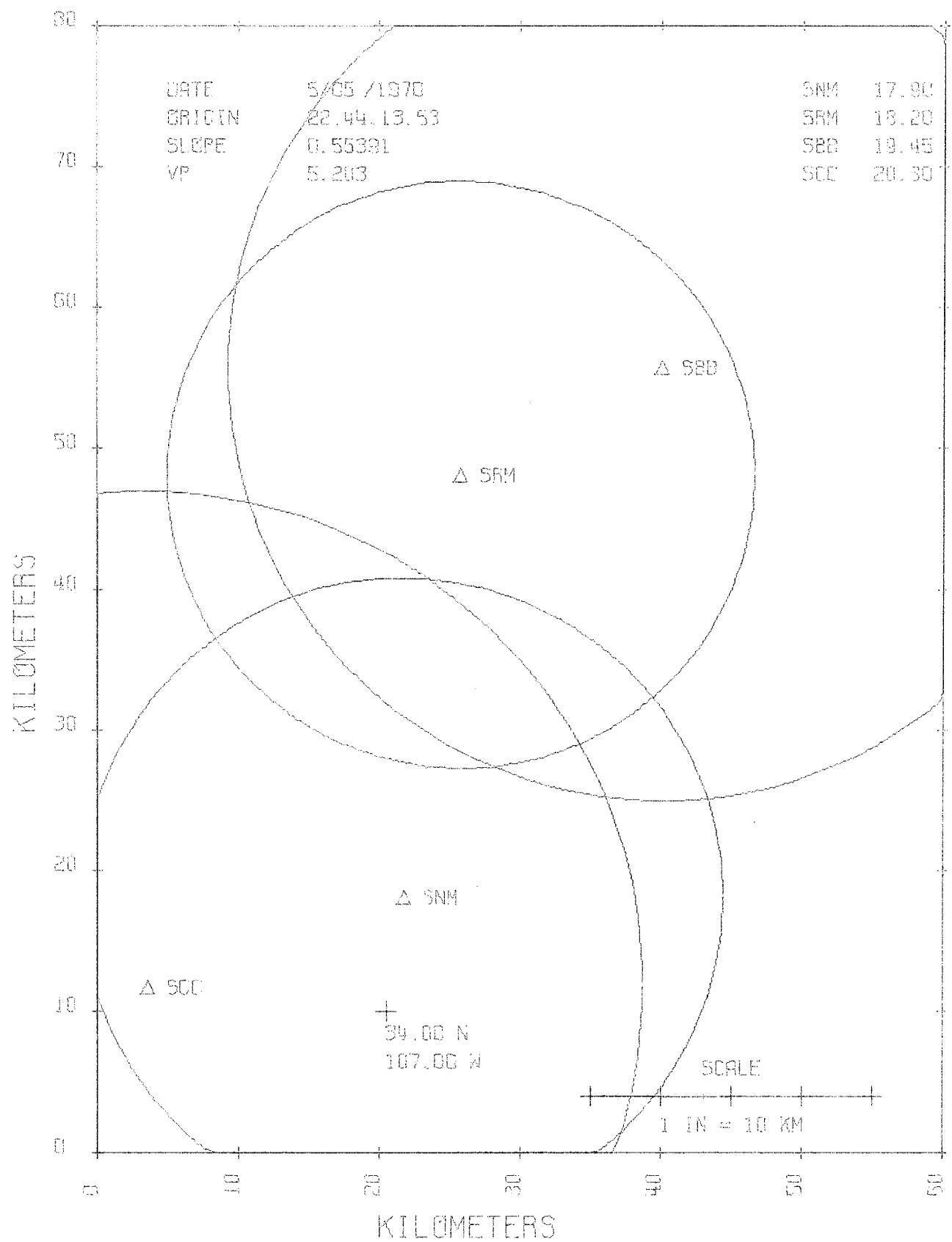


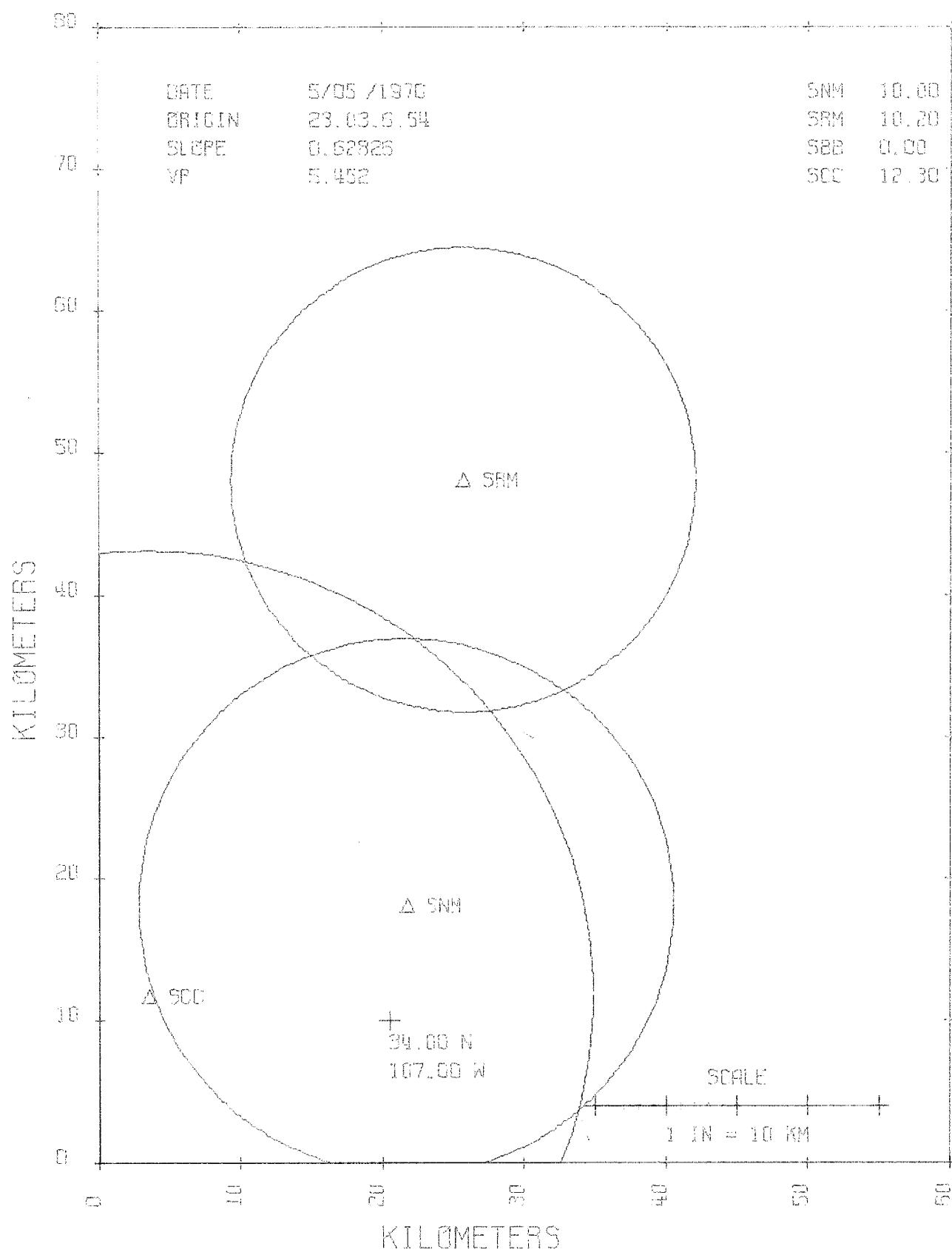


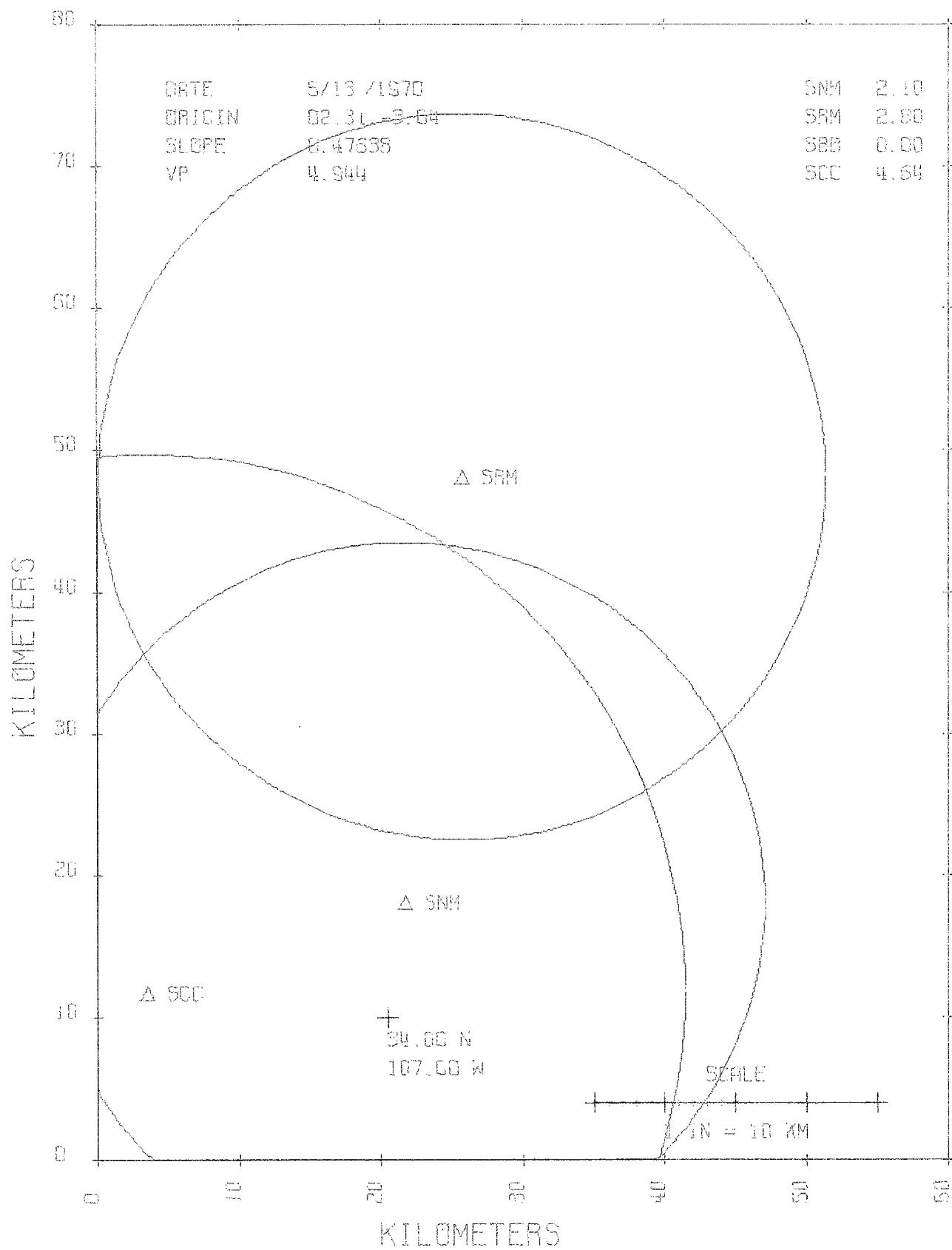


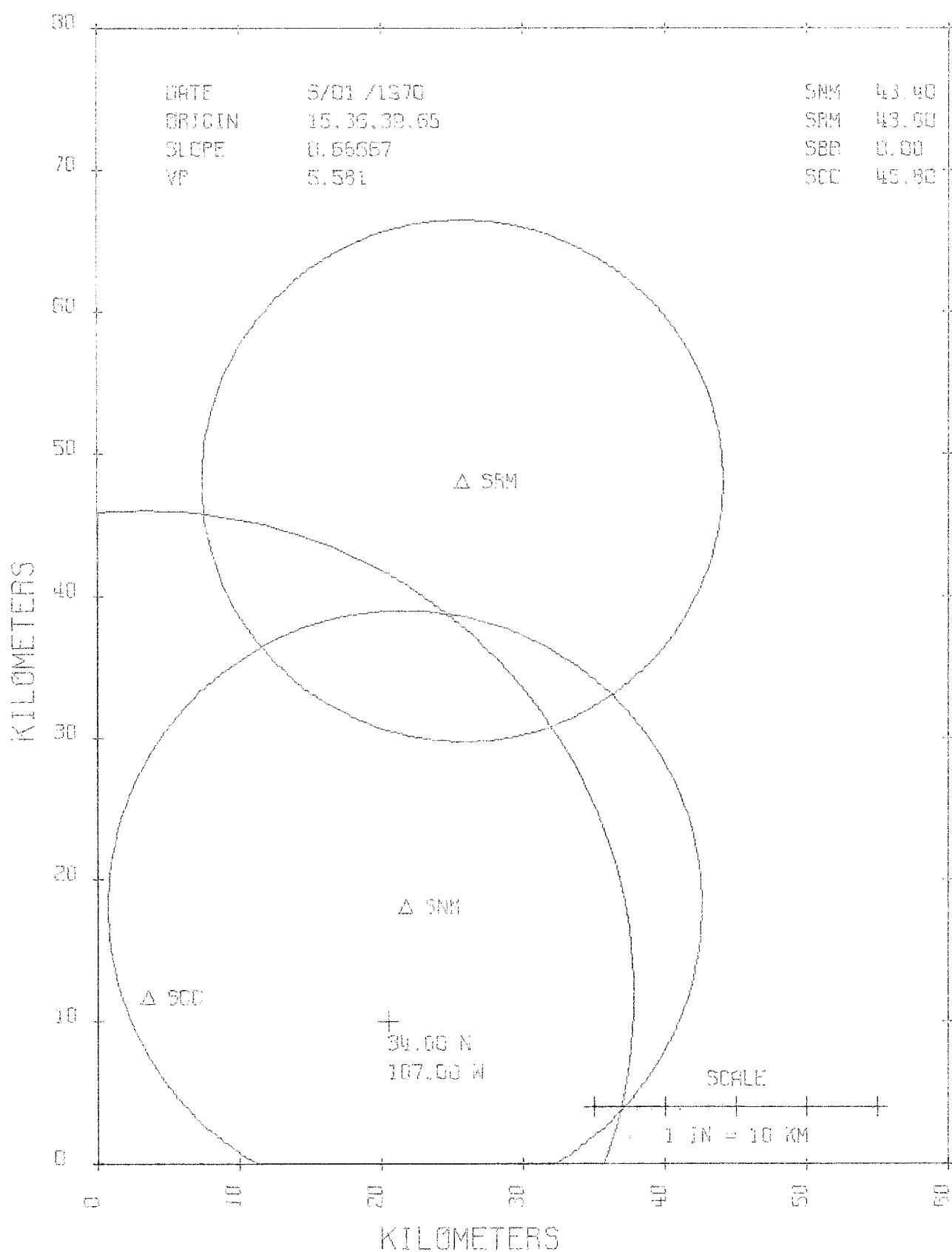


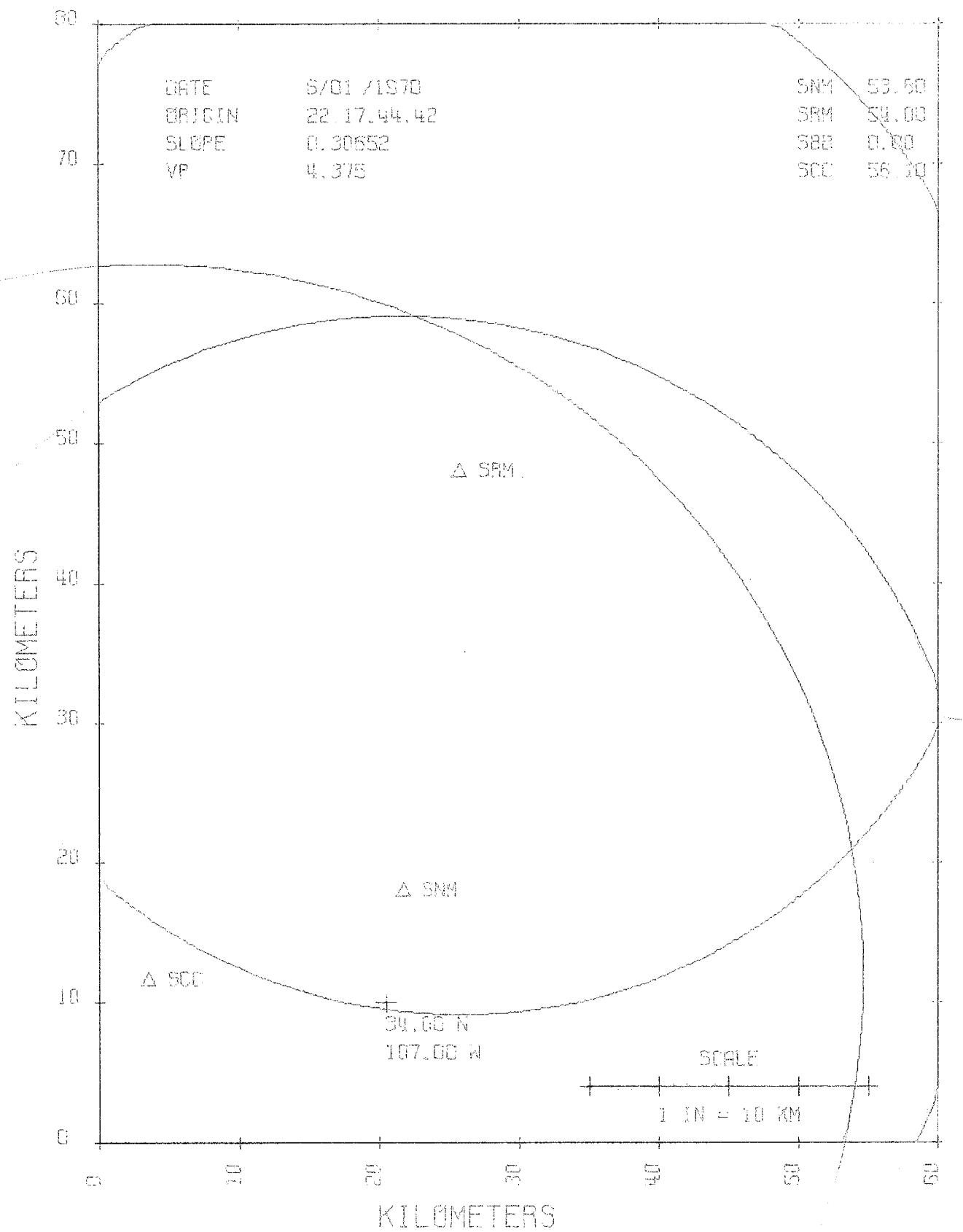


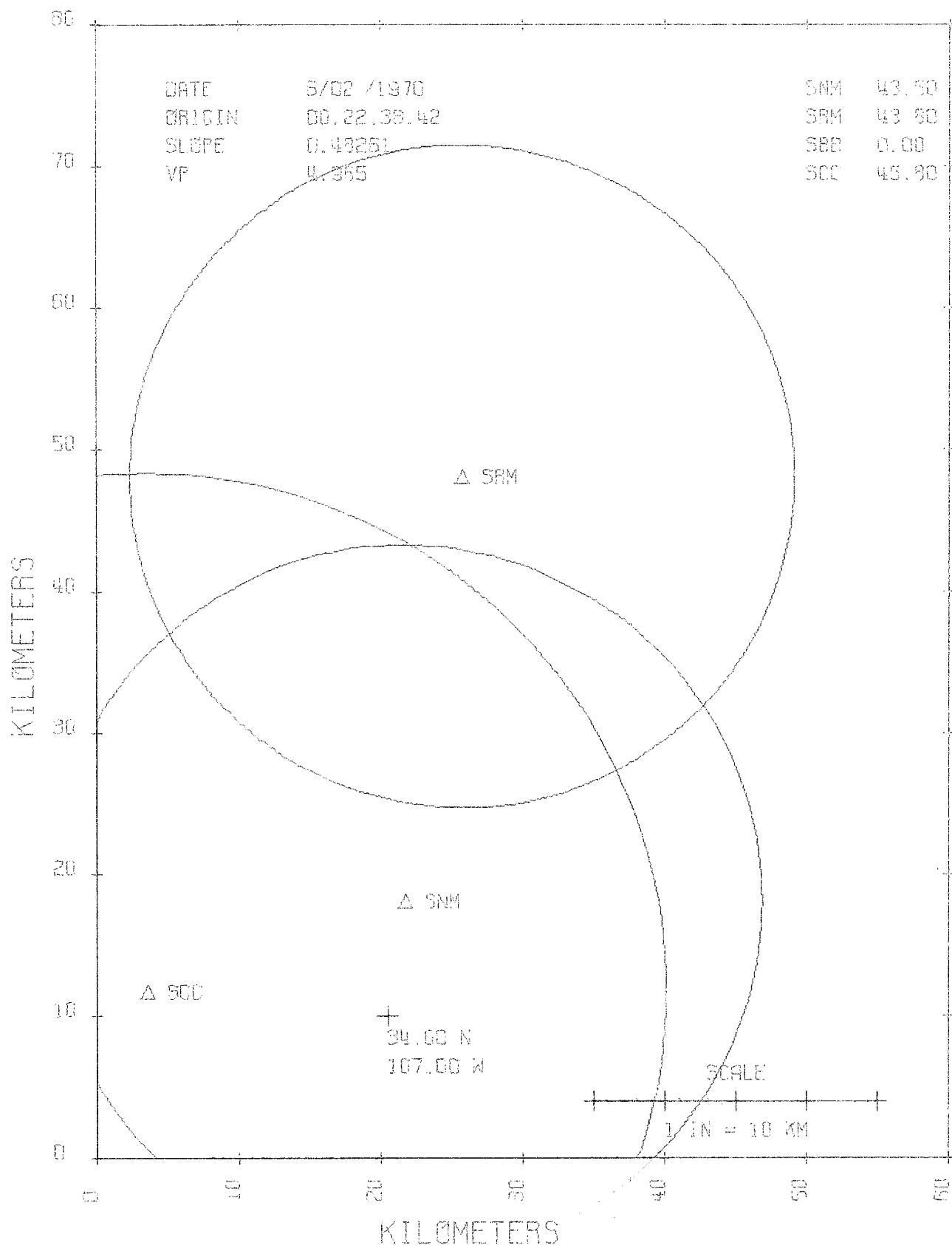


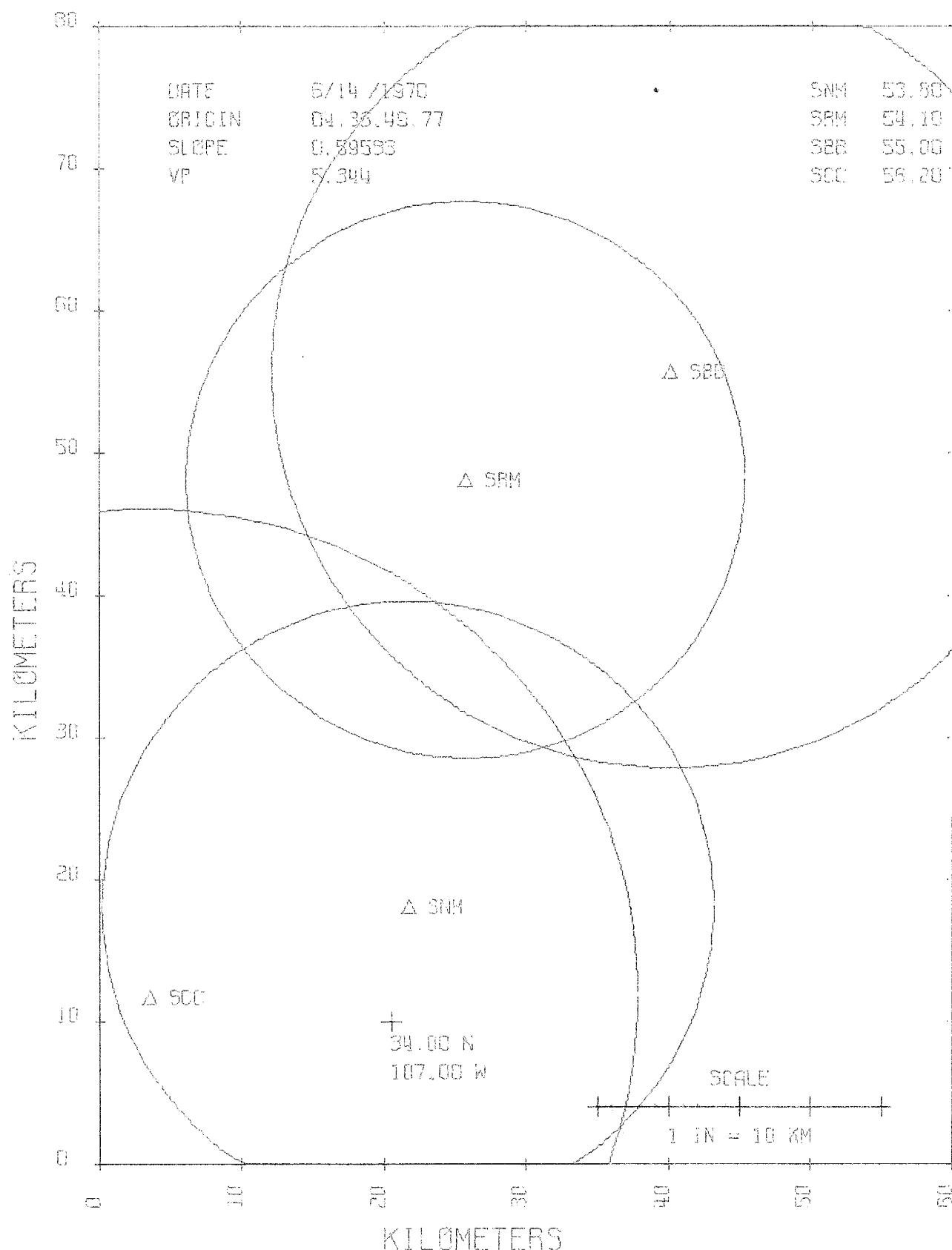


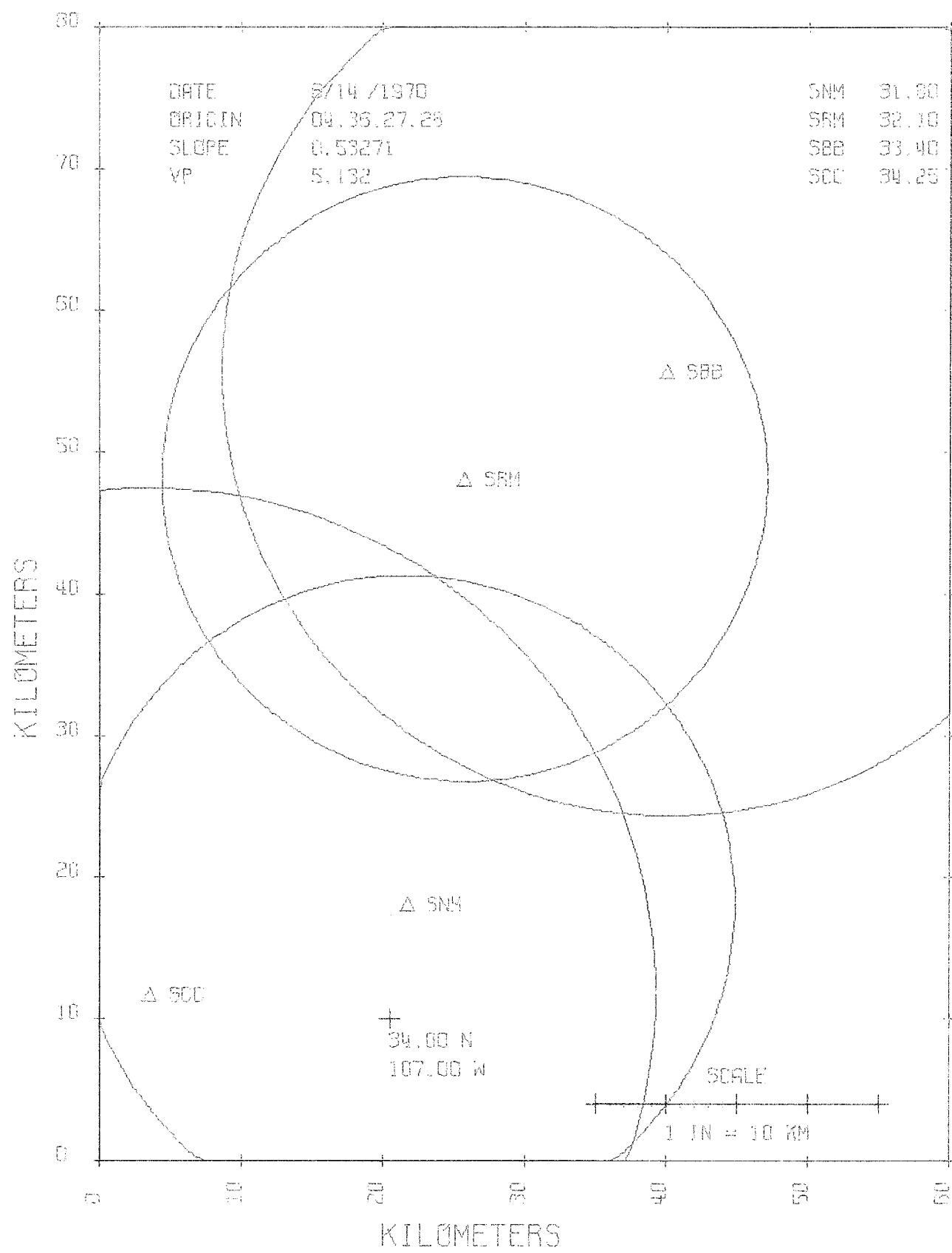


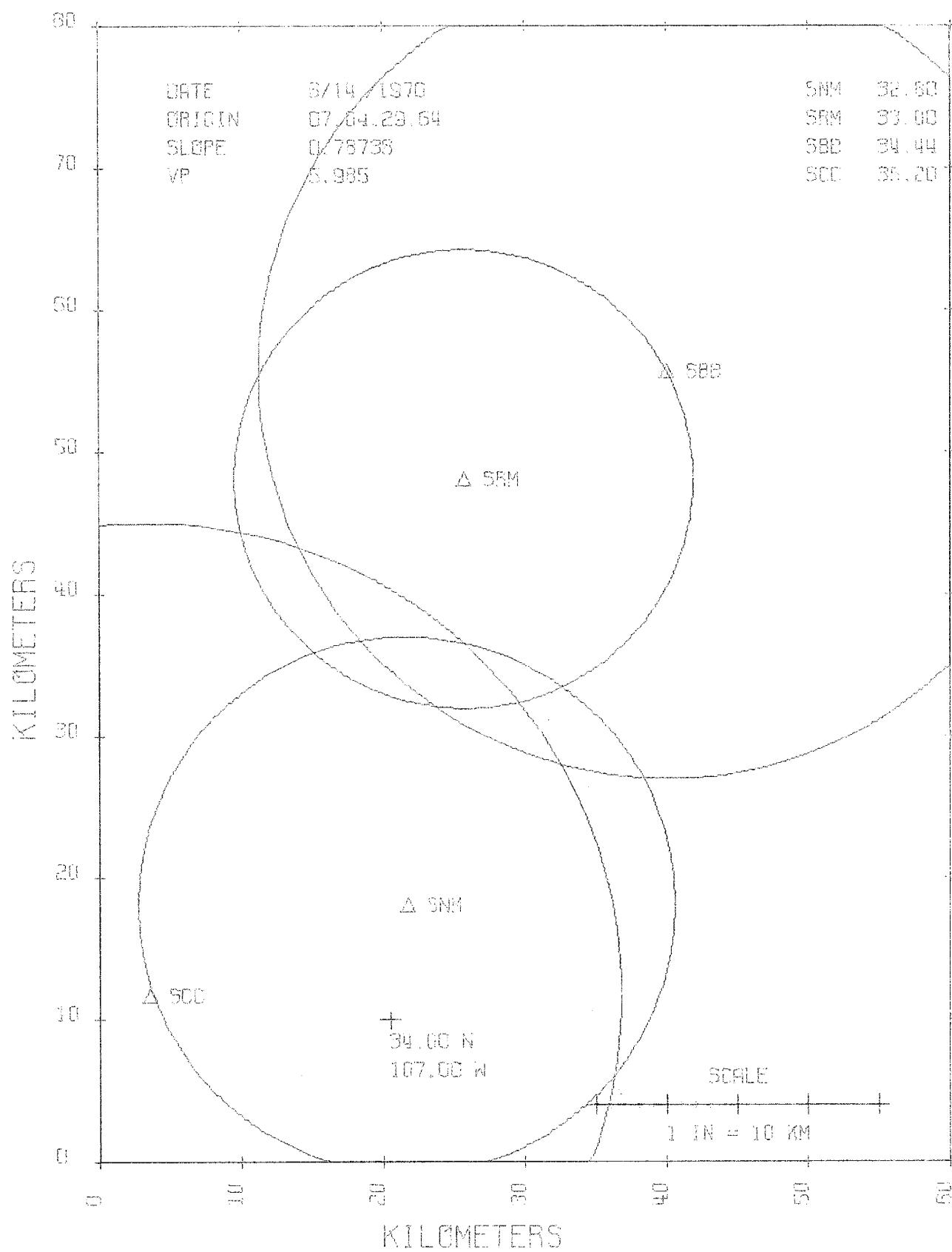


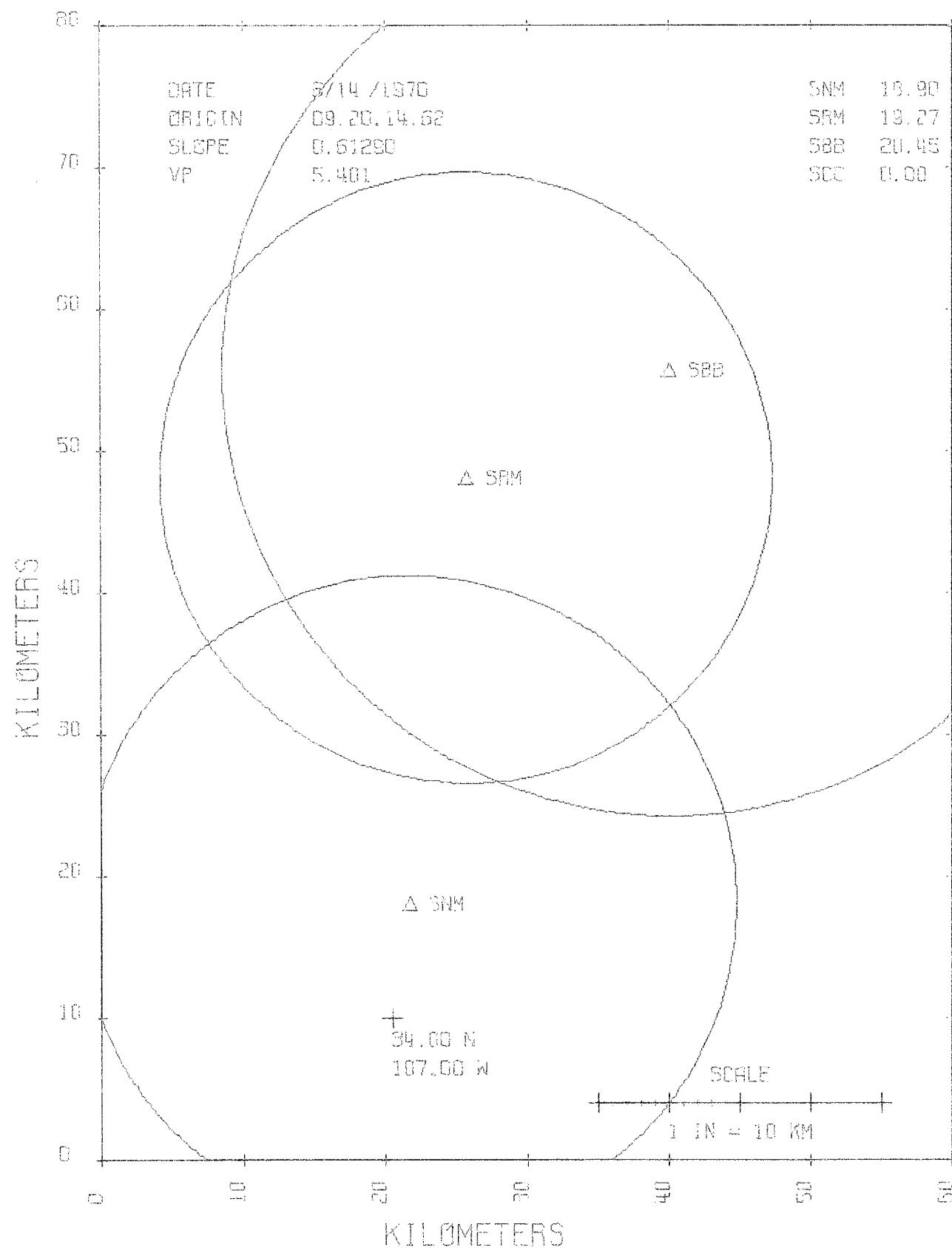


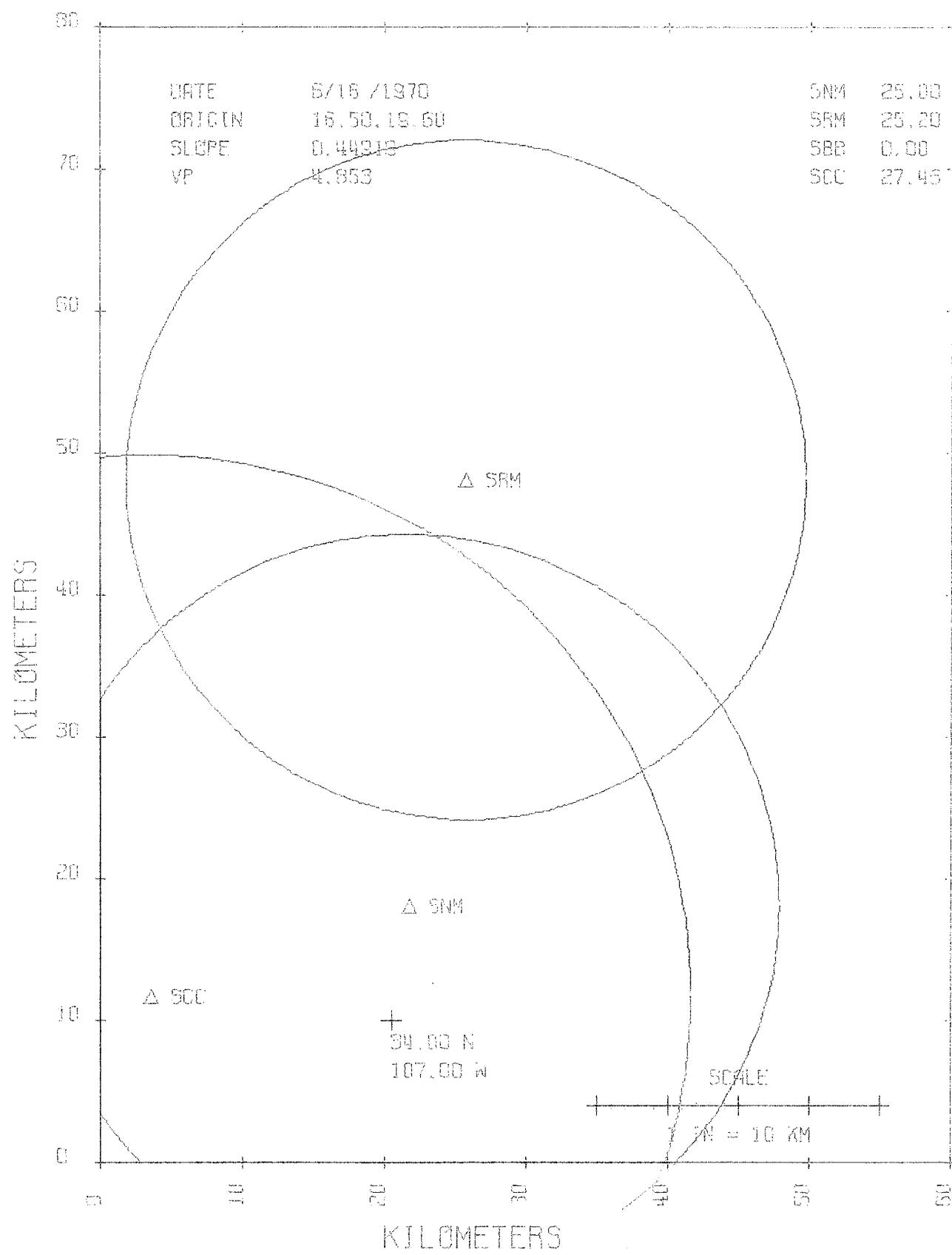


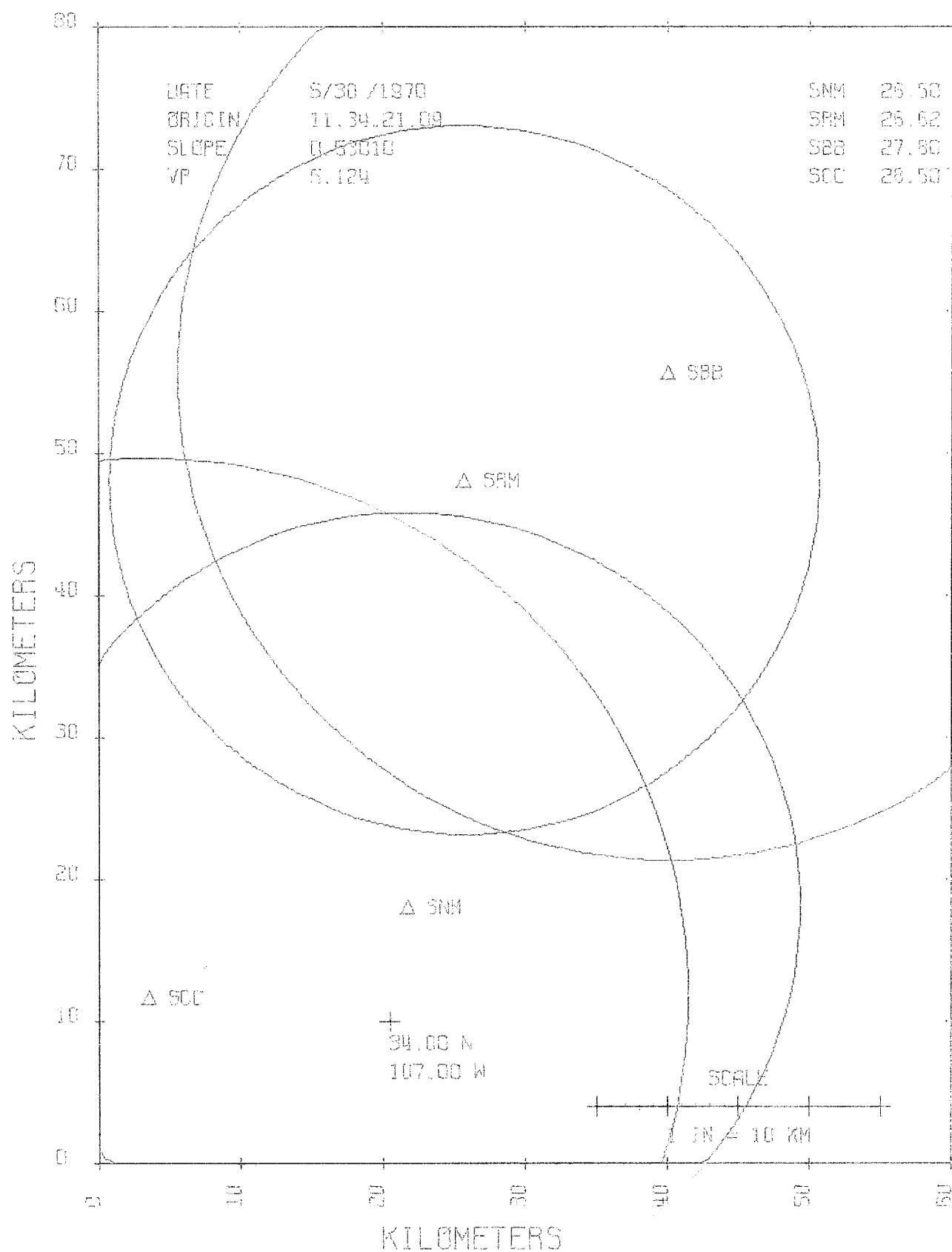


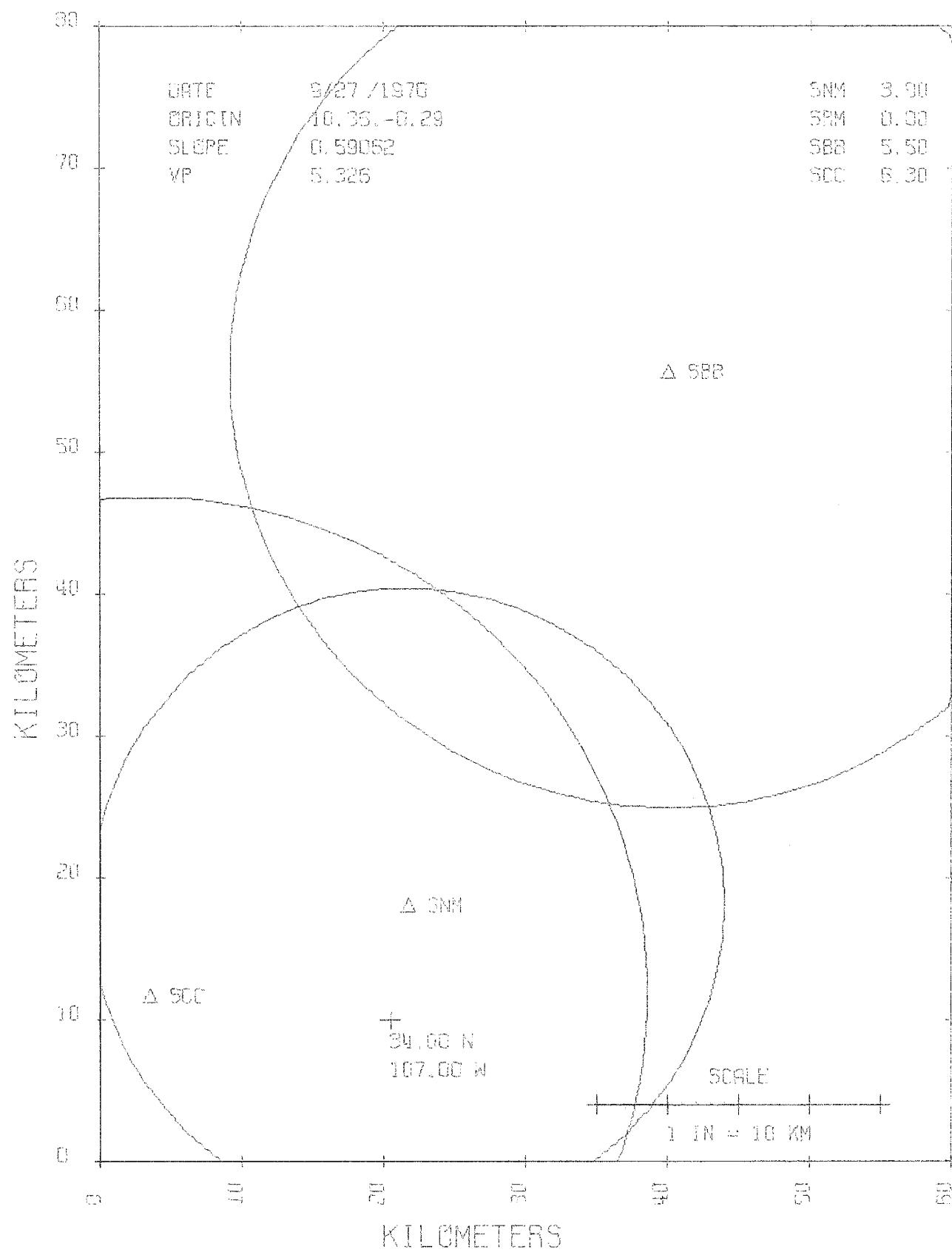


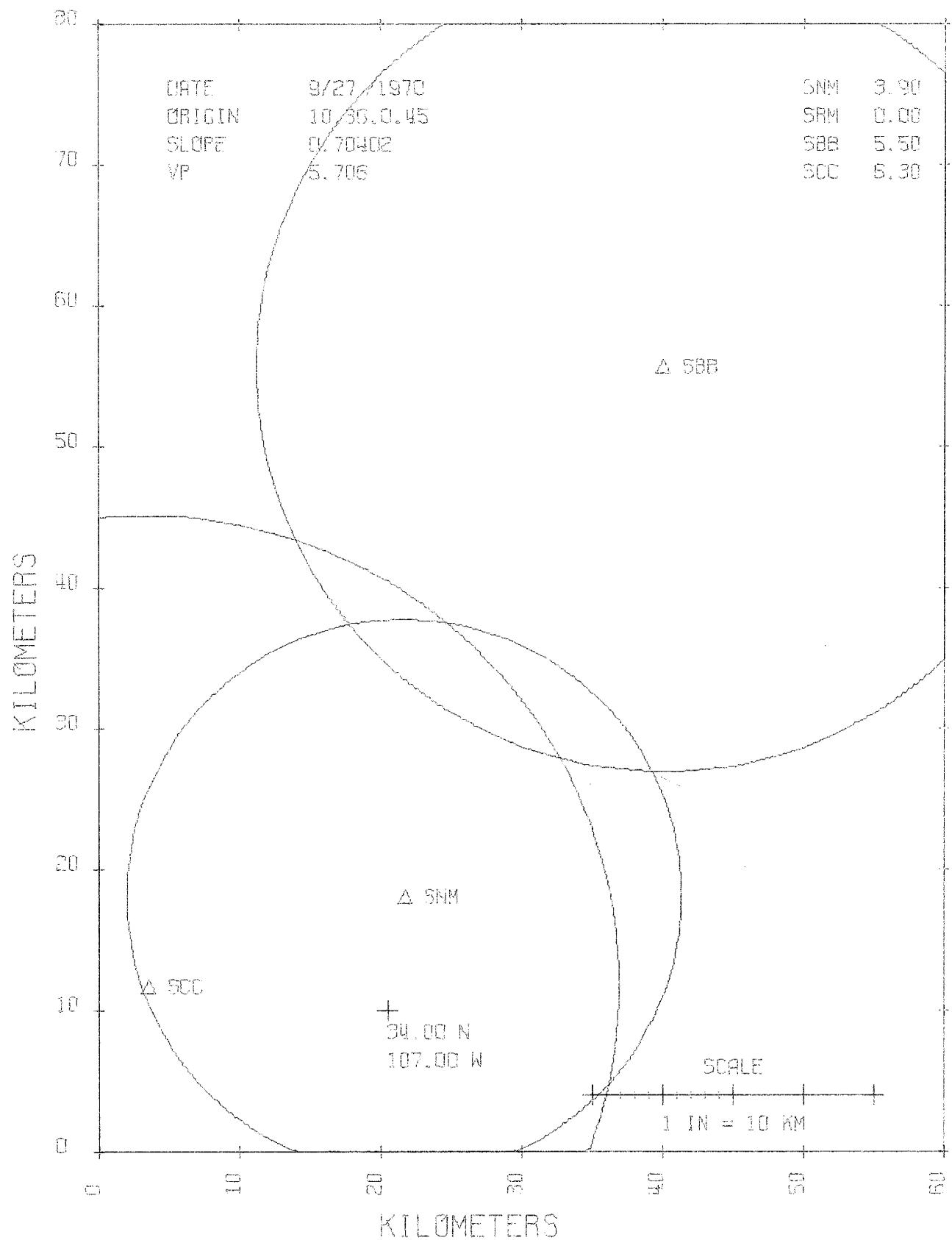












BIBLIOGRAPHY

1. Aggarival, Yash P.; Sykes, Lynn C.; Archibuster, John; and Sbar, Marc L., (1973), Premonitory changes in seismic velocities and prediction of earthquakes: *Nature*, v. 241, pp. 101-104.
2. Gregory, A. R., (1962), Shear wave velocity measurements of sedimentary rock samples under compression: Paper presented at the Fifth Symposium on Rock Mechanics, University of Minnesota, May, 1962, pp. 439-467.
3. Hammond, Allen L., (1973), Earthquake predictions: Breakthrough in theoretical insight? *Science*, v. 180, pp. 851-853.
4. Nur, Amos; and Simmons, Gene, (1969), The effect of saturation on velocity in low porosity rocks: *Earth and Planetary Science Letters*, v. 7, pp. 183-193.
5. Sanford, A. R.; Budding, A. J.; Hoffman, J. P.; Alptekin, O.S.; Rush, G. A.; and Topozada, T. R., (1972), Seismicity of the Rio Grande Rift in New Mexico: New Mexico State Bureau of Mines and Mineral Resources, Cir. 120, 19 pages.
6. Semenov, A. M., (1960), Variations in the travel time of transverse and longitudinal waves before violent earthquakes: *Izvestiya [Physics of the Solid Earth]*, v.5, pp. 245-248.
7. Whitcomb, James H.; Germany, Jan D.; and Anderson, Don L., (1973), Earthquake prediction: Variation of seismic velocities before the San Francisco Earthquake: *Science*, v. 180, pp. 632-635.

APPENDIX 1

Programs I, II, and III are the computer programs that were used in calculating the vp/vs ratio and in plotting the graphs.

Program I uses the data of P arrival time and the S-P interval to plot P arrival vs. S-P interval and to calculate the P wave velocity and the origin time. From this the epicenters are plotted.

Program II calculates the differences in P arrival times to check for consistency.

Program III plots vp/vs with the time and magnitude of the events.

P R O G R A M I

```

      IMPLICIT *FALS*G(A-H,O-Z), INTEGER(I-N)
      INTEGER STA(4), IDEN(4,4), NSTA(4)
      DIMENSION X(4), Y(4), U(4), V(4), ZX(4), ZY(4), G(4)

C
C
C               READ DATA
C
C
C       READ (5,106) ((STA(I),U(I),V(I)),I=1,4)
C       WRITE (6,107)((STA(I),U(I),V(I)),I=1,4)
C       PRINT 216
C
C       106 FORMAT ((A3,2F5.3))
C       107 FORMAT (15X,A3,2(5X,F5.3)))
C
C       DO 200 I = 1,4
C         U(I) = 0.635 * U(I)
C         V(I) = 0.635 * V(I) + 1.0
C 200 CONTINUE
C
C       LAP = 0
C
C       5 WRITE(6,1)
C       1 FORMAT (//)
C
C
C       DO 250 I = 1,4
C         NSTA(I) = 0.0
C         X(I) = 0.0
C         Y(I) = 0.0
C 250 CONTINUE
C
C       DO 10 I=1,5
C         READ (5,2,END=3)(IDEN(I,J),J=1,4),NSTA(I),Y(I),X(I),G(I),JJJ
C         2 FORMAT (A4,1X,2(A2,1X),A3,I1,1X,3F9.6,36X,I1)
C 10 CONTINUE
C       3 IF(JJJ)50,4,50
C
C       4 NUMB = I-2
C       DO 11 I=1,NUMB
C         WRITE (6,6) ( IDEN(I,J),J=1,4),X(I),Y(I)
C         6 FORMAT (5X,4A4,2F11.4)
C 11 CONTINUE
C
C
C               CALCULATE A & B IN THE EQN   Y = AX + B
C
C
C       SUMX = 0.
C       SUMY = 0.
C       SUMXS = 0.
C       SUMYS = 0.
C       SUMXY = 0.
C
C       DO 12 I=1,NUMB
C         SUMX = SUMX + X(I)
C         SUMY = SUMY + Y(I)
C         SUMXS = SUMXS + X(I)**2
C         SUMYS = SUMYS + Y(I)**2

```

```

SUMXY = SUMXY + X(1)*Y(1)
12 CONTINUE
  FNUMB = NUMR
  AX=FNUMB*SUMXS-SUMX**2
  AY=FNUMB*SUMYS-SUMY**2
  AXY=FNUMB*SUMXY-SUMX*SUY
  RAX = DSQRT(AX)
  RAY = DSQRT(AY)
  XMEAN = SUMX/FNUMB
  YMEAN = SUMY/FNUMB
  SIGX = DSQRT(AX)/FNUMB
  SIGY = DSQRT(AY)/FNUMB
  A = AXY/AX
  IF (NUMB.EQ.2) GO TO 13
  RXY = AXY/(RAX*RAY)
  R2XY = 1.0-(1.0-RXY**2)*((FNUMB-1.0)/(FNUMB-2.0))
  Q=(SUMYS-FNUMB*YMEAN*YMEAN)/(FNUMB-1.0)*(1.-RXY**2)
  QQ = DABS(Q)
  SYX = DSQRT(QQ)
  GU TO 14
13 RXY = 1.0
  SYX = 0.0
14 B = (SUMY*SUMXS-SUMX*SUMXY)/AX
C
C      *****
C
C      LAP = LAP + 1
  IF (LAP.EQ.6) PRINT 216
  IF (LAP.EQ.6) LAP = 0
C
  SLOPF = A
  XINT = - B/A
  VP =(A+1.0)*B*8/SQRT(3.0)
C
  DO 301 I = 1,4
  ZX(I) = 0.0
  ZY(I) = 0.0
301 CONTINUE
  DO 302 I = 1,4
  J = NSTA(I)
  IF (J.EQ.0) GO TO 302
  ZX(J) = X(I)
  ZY(J) = Y(I)
302 CONTINUE
  DO 303 I = 1,4
  X(I) = ZX(I)
  Y(I) = ZY(I)
303 CONTINUE
C
C      WRITE OUTPUT
C
  WRITE (6,210) (IDEN(1,J),J=1,3),XINT
  PRINT 215
C
  DO 220 I = 1,4
  IN = Y(I)

```

```

TRTIM = 0.0
R = 0.0
FD = 0.0
IF (IN.EQ.0.AND.I.EQ.2) GO TO 202
IF (IN.EQ.0) GO TO 220
TRTIM = X(I) - XINT
IF (I.EQ.2) TRTIM = X(I) - XINT - 0.66
R = VP * TRTIM
IRG = (R*R)-(G(1)*G(1))
IF (IRG.LT.0.0R.IRG.EQ.0) FD = 0.0
IF (IRG.LT.0.0R.IRG.EQ.0) GO TO 199
FD = DSQRT((R*R)-(G(1)*G(1)))
199 GO TO (201,202,203,204),I
201 WRITE (6,211) IDFN(I,4),X(I),TRTIM,R,Y(I),FD
GO TO 220
202 WRITE (6,212) STA(I),X(I),TRTIM,R,Y(I),VP
GO TO 220
203 WRITE (6,213) STA(I),X(I),TRTIM,R,Y(I),RXY
GO TO 220
204 WRITE (6,214) STA(I),X(I),TRTIM,R,Y(I),SYX
220 CONTINUE

```

```

C
C
210 FORMAT (/10X,'DATE *',2X,A4,'/1970', 7X,'ORIGIN TIME *',2X,A2,'/*'
$,A2,'/*',F5.2)
211 FORMAT (10X,A3,2X,'*',4(2X,F5.2),2X,'*' FD',2X,F5.2)
212 FORMAT (10X,A3,2X,'*',4(2X,F5.2),2X,'*' VP',2X,F5.2)
213 FORMAT (10X,A3,2X,'*',4(2X,F5.2),2X,'*' UC',2X,F5.2)
214 FORMAT (10X,A3,2X,'*',4(2X,F5.2),2X,'*' EE',2X,F5.2)
215 FORMAT (20X,'PT',6X,'TT',6X,'R',5X,'S-P')
216 FORMAT (1H1)

```

```

C
C
C     CALL BORDER (IDEN,XINT,A,VP)
C     CALL EPIPLT (X,Y,STA,XINT,VP,U,V)
C     CALL BORDER (IDEN,XINT,A,VP)
C     CALL GRAPH (X,Y,SLOPE,XINT,STA)
C
      GOTO 5
50 CONTINUE
      PRINT 216
C     CALL PLOT (8.0,0.0,3)
      STOP
      END

```

MEMORY REQUIREMENTS 001008 BYTES

```

SUBROUTINE BORDER (IDEN,XINT,A,VP)
IMPLICIT REAL*8(A-H,O-Z), INTEGER(I-N)
INTEGER STA(4), IDEN (4,4)

```

```

C
C
C           DRAW OUTLINE OF PLOT & LABEL THE AXIS
C
C           OUTLINE PAGE 18.5IN.X11.0IN.)
CALL PLOT (0.0,0.0,999)

```

```

C      CALL PLOT (8.0,-2.51,-3)
      OUTLINE PAGE (8.5IN,11.0IN.)
CALL PLOT (-.5,0.0, 3)
CALL PLOT (-.5,11.0, 2)
CALL PLOT (8.0,11.0,2)
CALL PLOT (8.0,0.0, 2)
CALL PLOT (-.5,0.0, 2)
CALL SYMBOL (-.3,9.5,0.07,'RUN # 2',90.0,7)
CALL SYMBOL (2.0,10.0,0.1,'DATE',0.0,4)
CALL SYMBOL (3.0,10.0,0.1,1DEN(1,1),0.0,4)
CALL SYMBOL (3.4,10.0,0.1,'/1970',0.0,5)
CALL SYMBOL (2.0,09.8,0.1,'ORIGIN',0.0,6)
CALL SYMBOL (3.0,09.8,0.1,1DEN(1,2),0.0,2)
CALL SYMBOL (-0.,-0.,-0.,1.,0.0,1)
CALL SYMBOL (-0.,-0.,-0.,1.,0.0,2)
CALL SYMBOL (-0.,-0.,-0.,1.,0.0,1)
CALL NUMBER (-0.,-0.,-0.,XINT,0.0,2)
CALL SYMBOL (2.0,09.6,0.1,'SLOPE',0.0,5)
CALL NUMBER (3.0,09.6,0.1,A,0.0,5)
CALL SYMBOL (2.0,09.4,0.1,'VP',0.0,2)
CALL NUMBER (3.0,09.4,0.1,VP,0.0,3)

C      OUTLINE PLOT AND ESTABLISH NEW REFERENCE
CALL PLOT (1.5,2.5,-3)
CALL PLOT (0.0,8.0,2)
CALL PLOT (6.0,8.0,2)
CALL PLOT (6.0,0.0,2)
CALL PLOT (0.0,0.0,2)

C      RETURN
END

```

MEMORY REQUIREMENTS 000594 BYTES

```

SUBROUTINE EPIPLT (X,Y,STA,XINT,VP,U,V)
IMPLICIT REAL*8(A-H,D-Z), INTEGER(I-N)
INTEGER STA(4)
DIMENSION X(4), Y(4), U(4), V(4)

C      LABEL THE AXIS

C      DO 31 I = 1,7
X1 = I - 1
X2 = X1 * 10.0
CALL NUMBER (X1,-0.30,0.10,X2,90.0,-1)
CALL SYMBOL (X1,0.0,0.07,3,0.0,-1)
31 CONTINUE

C      DO 32 I = 1,9
Y1 = I-1
Y2 = Y1 * 10.0
CALL NUMBER (-0.30,Y1,0.10,Y2,00.0,-1)
CALL SYMBOL (0.0,Y1,0.07,3,0.0,-1)
32 CONTINUE

C      DO 33 I = 1,7
X1 = I - 1
X2 = X1 * 10.0

```

```

CALL SYMBOL ( XI,8.0,0.07,3,0.0,-1)
33 CONTINUE
C
DO 34 I = 1,9
Y1 = I - 1
Y2 = Y1 * 10.0
CALL SYMBOL (6.0,Y1,0.07,3,0.0,-1)
34 CONTINUE
C
XY = 7.5
DO 35 I = 1,4
CALL SYMBOL (5.0,XY,0.1,STA(I),0.0,3)
CALL NUMBER (5.5,XY,0.1,X(I),0.0,2)
XY = XY - 0.2
35 CONTINUE
C
DRAW SCALE
C
CALL SYMBOL (4.3,0.55,0.1,'SCALE',0.0,5)
CALL SYMBOL (4.0,0.15,0.1,'1 IN = 10 KM',0.0,12)
DO 36 I = 1,11
XI = I - 1
XI = XI / 10.0 + 3.5
CALL SYMBOL (XI,0.40,0.04,3,0.0,-1)
36 CONTINUE
C
CALL PLOT (4.0,0.4,3)
DO 37 I = 1,5
XI = I - 1
XI = XI / 2.0 + 3.5
CALL SYMBOL (XI,0.40,0.14,3,0.0,-2)
37 CONTINUE
C
CALL SYMBOL (-.45,3.00,0.15,'KILOMETERS',90.0,10)
CALL SYMBOL (2.0,-.6,0.15,'KILOMETERS',0.0,10)
C
CALL SYMBOL (2.05,1.0,0.15,3,0.0,-1)
CALL SYMBOL (2.05,0.8,0.1,'34.00 N',0.0,7)
CALL SYMBOL (2.05,0.6,0.1,'107.00 W',0.0,8)
C
DO 110 M = 1,4
MN = Y(M)
IF (MN.EQ.0) GO TO 110
TRTIM = X(M) - XINT
IF (M.EQ.2) TRTIM = X(M)-XINT-0.66
R = VP * TRTIM
C
CALL EPICTR (STA,U,V,R,M)
C
110 CONTINUE
C
CALL PLOT (0.0,0.0,3)
CALL PLOT (0.0,0.0,999)
C
RETURN
END

```

```

SUBROUTINE EPICTR(STA,X,Y,R,M)
IMPLICIT REAL*8(A-H,O-Z), INTEGER(I-N)
INTEGER STA(4), IDEN(4,4)
DIMENSION X(4),Y(4),XR(361),YR(361)

C
C
C          PLOTS STATIONS & DRAWS CIRCLES
C

XXI = X(M) + 0.15
XXII = XXI - 0.15
YYI = Y(M) - 0.05
YYII = YYI + 0.05
CALL PLOT (XXI,YYI,3)
CALL SYMBOL(XXI,YYI,.10,STA(M),0.0,3)
PTX1 = XXII -.05
PTX2 = XXII + .05
PTY1 = YYII -.05
PTY2 = YYII + .05
CALL PLOT(PTX1,PTY1,3)
CALL PLOT(PTX2,PTY1,2)
CALL PLOT(XXII,PTY2,2)
CALL PLOT(PTX1,PTY1,2)
CALL CIRC (R,XR,YR)
DO 150 K=1,181
XR(K) = X(M) + XR(K)
YR(K) = Y(M) + YR(K)
IF(XR(K).GT.06.0)XR(K)=6.0
IF(XR(K).LT.-6.0)XR(K)=0.0
IF(YR(K).GT.08.0)YR(K)=8.0
IF(YR(K).LT.-8.0)YR(K)=0.0
IF(K.GT.1)GO TO 160
CALL PLOT(XR(K),YR(K),3)
GO TO 150
160 CONTINUE
CALL PLOT(XR(K),YR(K),2)
150 CONTINUE
RETURN
END

```

MEMORY REQUIREMENTS 001C44 BYTES

```

SUBROUTINE CIRC (R,XCR,YCR)
IMPLICIT REAL*8(A-H,O-Z), INTEGER(I-N)
DIMENSION XCR(361),YCR(361)
DELTA = 0.0
PI=3.14159265
KKK = 181
STP=(2.0*PI)/180.0
R = R * 0.1
DO 1 J=1,KKK
XCR(J)= R*DCOS(DELTA)
YCR(J)= R*DSIN(DELTA)
1 DELTA = DELTA + STP
RETURN
END

```

MEMORY REQUIREMENTS 000294 BYTES

```
SUBROUTINE GRAPH (X,Y,SLOPE,XINT,STA)
IMPLICIT REAL*8(A-H,D-Z), INTEGER(I-N)
INTEGER STA(4), IDEN(4,4)
DIMENSION X(4),Y(4)

C
C
C          PLOTS P ARRIVAL VS S-P
C
C
CALL SYMBOL (-0.55,2.0,0.15,'S - P IN SECONDS',90.0,16)
CALL SYMBOL (2.0,-0.7,0.15,'P ARRIVAL TIME',0.0,14)
C
C          LABEL STATIONS
C
XY = 7.5
DO 5 I = 1,4
J = I - 1
CALL SYMBOL (5.0,XY,0.1,STA(I),0.0,3)
CALL SYMBOL (5.5,XY,0.1,J,0.0,-1)
XY = XY - 0.2
5 CONTINUE

C          PLOT POINTS
C
DO 10 I = 1,4
MN = X(I)
IF (MN.EQ.0) GO TO 10
J = I - 1
XX = XINT
XX = X(I) - XX
YY = Y(I)
XX = XX * 0.5
YY = YY * 0.5
IF (XX.GT.6.0) GO TO 10
IF (YY.GT.6.0) GO TO 10
CALL SYMBOL (XX,YY,0.1,J,0.0,-1)
10 CONTINUE

C          CALL PLOT (0.0,0.0,3)

C          PLOT LINE
C
DELX = 0.01
XX = 0.0
DO 20 I = 1,600
YY = XX * SLOPE
XX = XX + DELX
IF (XX.GT.6.0) GO TO 20
IF (YY.GT.6.0) GO TO 20
CALL PLOT (XX,YY,2)
20 CONTINUE

C          LABEL THE AXIS
C
CALL NUMBER (0.0,-0.45,0.10,XINT,90.0,2)
```

```

CALL SYMBOL (0.0,0.0,0.07,3,0.0,-1)
IJK = 0
DO 30 I = 1,4
MN = X(I)
IF (MN.EQ.0) GO TO 30
XX = XINT
XX = X(I) - XX
YY = Y(I)
XX = XX *0.5
YY = YY * 0.5
IF (XX.GT.6.0) GO TO 25
IF (YY.GT.6.0) GO TO 25
CALL NUMBER (XX,-0.45,0.10,X(I),90.0,2)
CALL SYMBOL (XX,0.0,0.07,3,0.0,-1)
GO TO 30
25 CONTINUE
IF (IJK.EQ.1) GO TO 30
IJK = 1
XY = 7.5
DO 27 J = 1,4
CALL NUMBER (3.0,XY,0.1,X(J),0.0,2)
CALL NUMBER (4.0,XY,0.1,Y(J),0.0,2)
XY = XY -0.2
27 CONTINUE
30 CONTINUE
C
DO 40 I = 1,4
MN = X(I)
IF (MN.EQ.0) GO TO 40
YY = Y(I)
YY = YY * 0.5
IF (YY.GT.6.0) GO TO 40
CALL NUMBER (-0.45,YY,0.10,Y(I),0.0,2)
CALL SYMBOL (0.0,YY,0.07,3,0.0,-1)
40 CONTINUE
C
C      DRAW SCALE
C
CALL SYMBOL (4.1,0.55,0.1,'SCALE',0.0,5)
CALL SYMBOL (3.7,0.15,0.1,'1 IN = 2 SEC',0.0,12)
C
DO 50 I = 1,11
XI = I - 1
XI = XI/10.0 + 3.5
CALL SYMBOL (XI,0.4,0.04,3,0.0,-1)
50 CONTINUE
C
CALL PLOT (4.0,0.4,3)
DO 60 I = 1,5
XI = I - 1
XI = XI/02.0 + 3.5
CALL SYMBOL (XI,0.4,0.14,3,0.0,-2)
60 CONTINUE
C
CALL PLOT (0.0,0.0,999)
C
RETURN
END

```

P R O G R A M XI

```

      INTEGER IDEN(50,4)
      DIMENSION S(50,4), DIF(50,6)

C
      PRINT 14
      PRINT 16
      PRINT 17

C
      I=1
 2 READ (5,1,END=50) (IDEN(I,J),J=1,4), (S(I,J),J=1,4)
      WRITE (6,3)      (IDEN(I,J),J=1,4), (S(I,J),J=1,4)
      I = I + 1
      GO TO 2
 1 FORMAT (4A4,4(3X,F4.1))
 3 FORMAT ((20X,4A4,4(2X,F4.1)))

C
 50 CONTINUE
      PRINT 14
      PRINT 15

C
      NUMB = I - 1

C
      DO 10 I = 1,NUMB

C
      DIF(I,1) = S(I,2) - S(I,1)
      DIF(I,2) = S(I,3) - S(I,1)
      DIF(I,3) = S(I,4) - S(I,1)
      DIF(I,4) = S(I,3) - S(I,2)
      DIF(I,5) = S(I,4) - S(I,2)
      DIF(I,6) = S(I,4) - S(I,3)

C
      IF (S(I,2).EQ.0.0.DR.S(I,1).EQ.0.0)DIF(I,1) = 0.0
      IF (S(I,3).EQ.0.0.DR.S(I,1).EQ.0.0)DIF(I,2) = 0.0
      IF (S(I,4).EQ.0.0.DR.S(I,1).EQ.0.0)DIF(I,3) = 0.0
      IF (S(I,3).EQ.0.0.DR.S(I,2).EQ.0.0)DIF(I,4) = 0.0
      IF (S(I,4).EQ.0.0.DR.S(I,2).EQ.0.0)DIF(I,5) = 0.0
      IF (S(I,4).EQ.0.0.DR.S(I,3).EQ.0.0)DIF(I,6) = 0.0

C
      WRITE (6,20) (IDEN(I,J),J=1,4), (DIF(I,L),L=1,6)

C
 14 FORMAT (1H1)
 15 FORMAT (13X,'DATE',12X,'S2-1    S3-1    S4-1    S3-2    S4-2    S4-3 /)
 16 FORMAT (22X,'DATE',17X,'P ARRIVAL TIME')
 17 FORMAT (39X,'SNM    SRM    S88    SCC')
 20 FORMAT ((10X,4A4,6(2X,F5.1)))

C
 10 CONTINUE
      PRINT 14
      STOP
      END

```

MEMORY REQUIREMENTS 001100 BYTES

HIGHEST SEVERITY CODE WAS 0

GRADE

00.00.07

HIGHEST SEVERITY WAS 0 -- EXECUTION

P R O G R A M III

```

      CALL BORDER
C
      K = 1
      CALL PLOT (0.0,4.0,-3)
C
      1 READ (5,10,END=2) XMO,DA,HR,XMIN,SEC,VP,JJJ,XMAG
      WRITE (6,10) XMO,DA,HR,XMIN,SEC,VP,JJJ,XMAG
      10 FORMAT (5(1X,F4.1),1X,F4.2,2X,11.3X,F4.2)
C
C
      IF (JJJ.EQ.0) PRINT 12
      12 FORMAT ('JJJ = 0')
C
      IF (JJJ) 3,4,3
      3 X =(XMO*30. + DA + HR/24. + XMIN/1440. + SEC/86400.)*6./60.
      Y =(VP * SQRT(3.0)/5.8*2.0) -1.5
      WRITE (6,11) X,Y
      11 FORMAT (2(2X,F4.2))
      GO TO (20,30),JJJ
      20 CALL SYMBOL(X,Y,0.07,3,0.0,-K)
C
      IF (XMAG.LT.0.1) GO TO 25
      X1 = X + 0.1
      YMAG = XMAG
      XMAG = XMAG / 2.0
      IF (YMAG.LT.0.3) GO TO 24
      CALL NUMBER (X1,XMAG,0.07,YMAG,0.0,1)
      24 CALL PLOT (X,0.0,3)
      CALL PLOT (X,XMAG,2)
      CALL PLOT (X,Y,3)
C
      25 K = 2
      GO TO 2
      30 CALL PLOT (0.0,-4.0,-3)
      IF (XMAG.LT.0.1) GO TO 35
      X1 = X + 0.1
      YMAG = XMAG
      XMAG = XMAG / 2.0
      IF (YMAG.LT.0.3) GO TO 34
      CALL NUMBER (X1,XMAG,0.07,YMAG,0.0,1)
      34 CALL PLOT (X,0.0,3)
      CALL PLOT (X,XMAG,2)
      35 CALL PLOT (X,Y,3)
      CALL SYMBOL(X,Y,0.07,3,0.0,-2)
      2 IF (JJJ) 1,4,1
      4 CALL PLOT (0.0,0.0,999)
      STOP
      END

```

MEMORY REQUIREMENTS 000568 BYTES

```

SUBROUTINE BORDER
CALL PLOT (0.0,0.0,999)
CALL PLOT (0.0,0.0,3)
CALL PLOT (0.0,11.0,2)
CALL PLOT (8.5,11.0,2)
CALL PLOT (8.5,0.0,2)

```

```

      CALL PLOT (0.0,0.0,0,2)
      CALL PLOT (2.0,2.5,-3)
      CALL PLOT (0.0,8.0,2)
      CALL PLOT (6.0,8.0,2)
      CALL PLOT (6.0,0.0,2)
      CALL PLOT (10.0,0.0,2)
      CALL PLOT (0.0,4.0,3)
      CALL PLOT (6.0,4.0,2)
      CALL PLOT (0.0,0.0,3)

C
C
C
C
      DO 10 I = 1,2
      Y = I
      YY = Y * 2.0 - 1.5
      CALL NUMBER (-0.3,YY,0.1,Y,0.0,-1)
      CALL SYMBOL (0.0,YY,0.07,3,0.0,-1)
      XY = YY + 1.0
      IF (I.EQ.1) CALL SYMBOL (0.0,XY,0.07,3,0.0,-1)
10 CONTINUE

C
C
      DO 15 I = 1,2
      Y = I
      YY = Y * 2.0 - 1.5
      YY = YY + 4.0
      CALL NUMBER (-0.3,YY,0.1,Y,0.0,-1)
      CALL SYMBOL (0.0,YY,0.07,3,0.0,-1)
      XY = YY + 1.0
      IF (I.EQ.1) CALL SYMBOL (0.0,XY,0.07,3,0.0,-1)
15 CONTINUE

C
C
      YY = -0.3
      DO 20 I = 1,4
      DO 20 J = 1,6
      X = J - 1
      XX = X / 2.0
      X = X * 5.0
      IF (I.EQ.2 .OR. I.EQ.4) XX = XX + 3.0
      IF (I.EQ.3 .OR. I.EQ.4) YY = 3.7
      CALL NUMBER (XX,YY,0.1,X,0.0,-1)
20 CONTINUE

C
C
      YY = 0.0
      DO 25 I = 1,2
      IF (I.EQ.2) YY = 4.0
      DO 25 J = 1,61
      X = J - 1
      XX = X / 10.0
      CALL SYMBOL (XX,YY,0.07,3,0.0,-1)
25 CONTINUE

C
C
      DO 40 I = 1,4
      GO TO (31,32,33,34),I
31 CALL SYMBOL (1.0,-0.6,0.15,'MAY',0.0,3)
      GO TO 40

```

32 CALL SYMBOL (4,0,-0.6,0.15,'JUNE',0,0,4)
GO TO 40
33 CALL SYMBOL (1,0,3,4,0.15,'MARCH',0,0,5)
GO TO 40
34 CALL SYMBOL (4,0,3,4,0.15,'APRIL',0,0,5)
40 CONTINUE

C
C

X = 1.8
DO 50 I = 1,2
IF (I.EQ.2) X = X + 4.0
CALL SYMBOL (-0.6, X, 0.15, 'V', 90, 0, 1)
CALL SYMBOL (-0.6,-0.,0.07,'P',90,0,1)
CALL SYMBOL (-0.6,-0.,0.15,'/V',90,0,2)
CALL SYMBOL (-0.6,-0.,0.07,'S',90,0,1)
50 CONTINUE

C
C

RETURN
END

MEMORY REQUIREMENTS 0003F0 BYTES

HIGHEST SEVERITY CODE WAS 0

00,00,12

| Date | S _{RM} | S _{Bm} | S _{BB} | S _{CC} | S _{NN} | S _{RM} | S _{Bm} |
|--------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| 7/7 - 13:35 | 2.85 | F | 3.16 | P | | 7.215 | 5.95 |
| 7/11 - 20:40 | 2.12 | P | 2.56 | P | | 4.115 | 5.95 |
| 7/12 - 05:17 | 2.20 | P | 1.78 | F | 2.34 P | 5.00 | 3.11 |
| 7/13 - 08:36 | 2.50 | F | 2.875 F | 3.54 F | | 7.50 | 4.95 |
| 7/12 - 11:35 | 2.25 | P | 2.89 | F | 3.53 P | 6.15 | 4.66 |
| 7/17 - 06:40 | 2.325 | F | 2.80 | F | 3.61 F | 7.00 | 4.13 |
| 7/17 - 08:39 | 2.25 | F | 2.81 | F | 3.36 P | 3.54 F | 7.00 |
| 7/17 - 11:05 | 2.25 | F | 3.82 | F | 3.33 F | 3.59 P | 9.00 |
| 7/18 - 07:20 | 2.25 | G | 2.89 | G | 3.84 P | 3.55 P | 9.125 |
| 7/18 - 16:35 | 2.375 | F | 3.85 | F | 3.64 F | 3.63 F | 7.35 |
| 7/20 - 04:34 | 2.4125 | F | 2.80 | F | 3.43 G | 3.59 G | 9.25 |
| 7/25 - 15:32 | 2.75 | F | | | 3.47 G | 3.84 G | 7.125 |
| 7/28 - 07:02 | 2.20 | F | 2.82 | F | 2.2 P | | 9.00 |
| 7/30 - 02:51 | 3.25 | F | 1.96 | P | 3.40 P | | 6.25 |
| 7/31 - 06:29 | 3.80 | P | 1.94 | P | | | 4.13 |

Date Sym Sym Sym Sym Sym Sym Sym

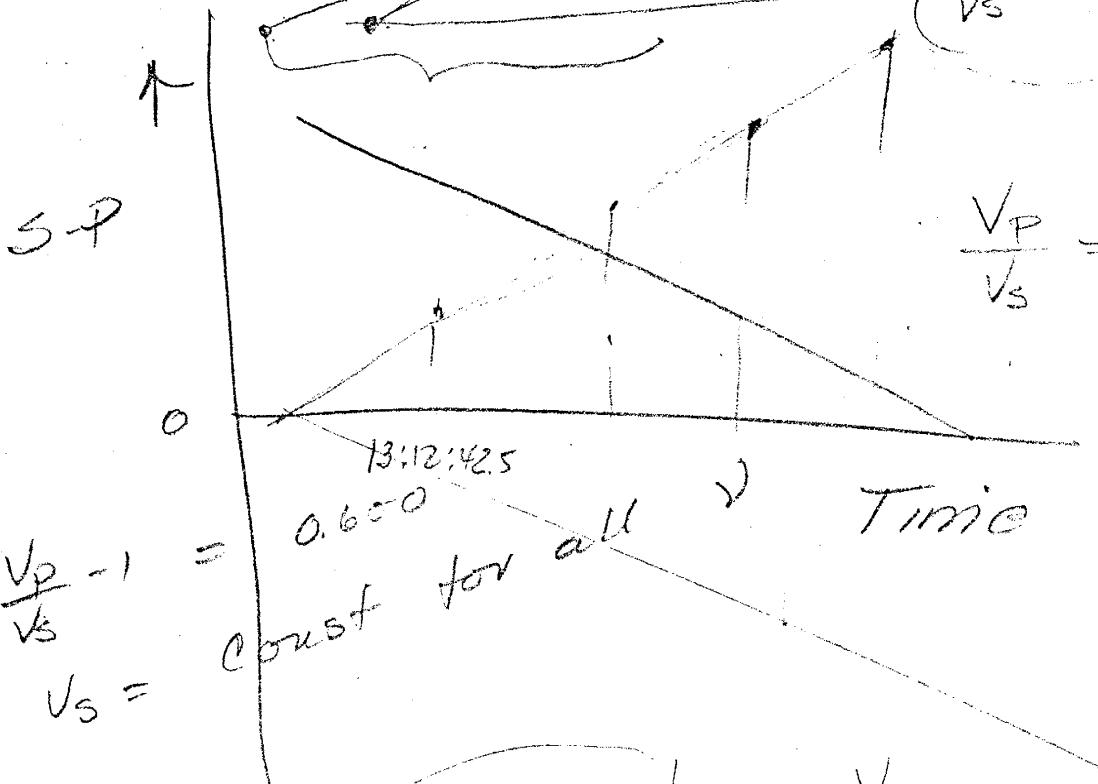
| | | | | | | | |
|--------------|---------|--------|--|---------|--------|------|-------|
| 4/17 - 03:06 | 2.25 F | 2.79 F | | 3.72 F | 7.25 | 4.46 | 7.1 |
| 4/18 - 02:44 | 2.50 F | 2.81 F | | 3.76 F | 7.00 | 4.55 | 7.14 |
| 4/18 - 04:11 | 3.00 VP | 2.88 P | | 3.80 F | 7.75 | 4.87 | 7.06 |
| 4/18 - 07:34 | 2.575 G | 2.74 P | | 3.66 G | 7.25 | 4.32 | 7.30 |
| 4/18 - 09:05 | 2.575 G | 2.80 F | | 3.11 VP | 6.19 | 8.8? | |
| 4/18 - 09:12 | 2.50 F | 2.80 F | | 4.04 G | 6.125 | 4.52 | 7.125 |
| 4/18 - 07:29 | 2.50 P | 2.89 P | | 4.09 F | 6.00 | | 6.17 |
| 4/18 - 17:18 | 2.50 P | 2.81 P | | 3.59 | 6.87 | 4.79 | 7.05 |
| 5/5 - 22:44 | 2.30 P | 2.89 P | | 3.62 | 3.53 F | 7.1 | 4.67 |
| 5/5 - 22:44 | 2.50 P | 3.12 F | | 3.33 | 7.25 | 4.89 | 6.92 |
| 5/5 - 23:03 | 2.195 G | 3.10 P | | 3.72 G | 7.00 | 4.25 | 7.05 |
| 5/11 - 08:07 | 3.125 G | 2.85 P | | | 7.00 | 4.67 | |
| 5/13 - 02:31 | 2.45 F | 2.92 F | | 3.66 F | 6.875 | 4.83 | 6.98 |
| 6/1 - 12:23 | 2.425 G | 2.87 P | | | 5.42 | | |
| 6/1 - 15:36 | 2.50 F | 2.83 F | | 4.10 F | 7.50 | 5.42 | 6.88 |

| Date | End | Start | Sec | Sec | Sec | Sec | Sec | Sec |
|--------------|---------|---------------|-------|----------|-------|-------|------|-----|
| 6/1 - 22:19 | 2.345 | P 2.67 F | 3.58 | F 7.175 | 5.375 | 7.14 | | |
| 6/2 - 00:22 | 2.45 | G 2.67 P | 3.56 | G 7.375 | 4.5 | 7.02 | | |
| 6/2 - 12:24 | 2.345 | F 2.86 P | 7.25 | | 4.1 | | | |
| 6/7 - 09:14 | 2.125 | F 2.82 P | 6.875 | | 5.40 | | | |
| 6/14 - 04:23 | 2.475 | F 3.64 P | 3.19 | G 7.125 | 4.61 | 7.07 | | |
| 6/14 - 04:31 | 2.20 | F 2.86 P | . | 7.00 | 4.88 | | | |
| 6/14 - 04:36 | 2.375 | F 2.80 G | 3.36 | G 7.125 | 5.39 | 8.15? | 7.24 | |
| 6/14 - 04:36 | 2.350 | F 2.85 F | 3.21 | G 7.125 | 5.91 | 7.5 | 7.4 | |
| 6/14 - 07:04 | 2.375 | P 3.11 F | 4.15 | G 7.125 | 5.53 | 7.7 | 7.44 | |
| 6/14 - 09:20 | 2.625 | F 3.26 P | 3.575 | G 7.5 | 5.7 | 7.125 | | |
| 6/16 - 05:51 | 2.50 | G 3.79 G | 7.075 | | 7.27 | | | |
| 6/16 - 16:50 | 2.425 | G 2.89 G | 3.53 | G 7.125 | 4.70 | 7.33 | | |
| 6/17 - 18:52 | 2.25 | F 2.92 F | . | 7.00 | 4.78 | | | |
| 6/23 - 01:33 | 2.75 | F 2.39 P | 4.23 | G 7.15 | 3.8 | | 6.74 | |
| 6/26 - 11:34 | 2.80 | F 3.07 G | 3.16 | F 3.80 F | 5.6 | 7.26 | 7.27 | |
| 7/7 - 02:51 | 2.375 | P 3.68 F | 3.71 | F 7.00 | 7.10 | 7.25 | | |
| 7/27 - 10:36 | 2.475 G | 3.42 G 4.21 P | 7.25 | | 6.78 | 7.24 | | |

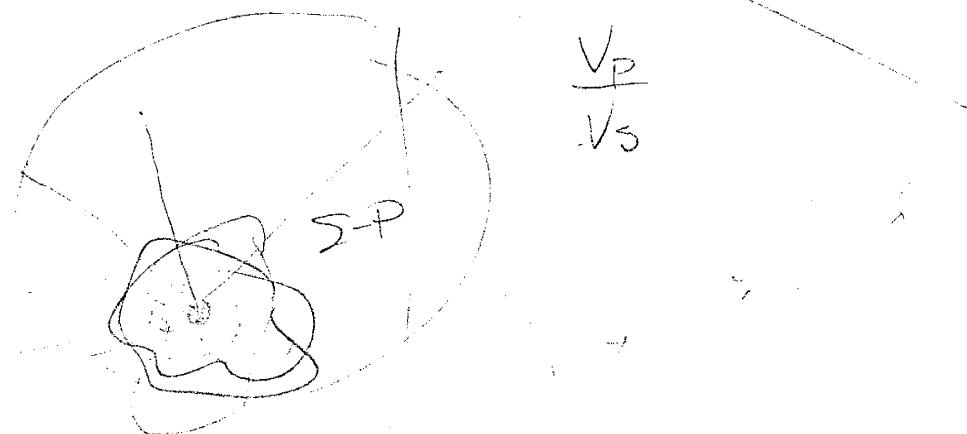
$$\frac{V_p}{V_s} = \sqrt{3}$$

Calculate
Let $V_s = \text{const}$ for all slopes
Calculate V_p for all slopes
 $\frac{V_p}{V_s} = 1.732$

$$J_p = 5.8 \text{ kN}$$

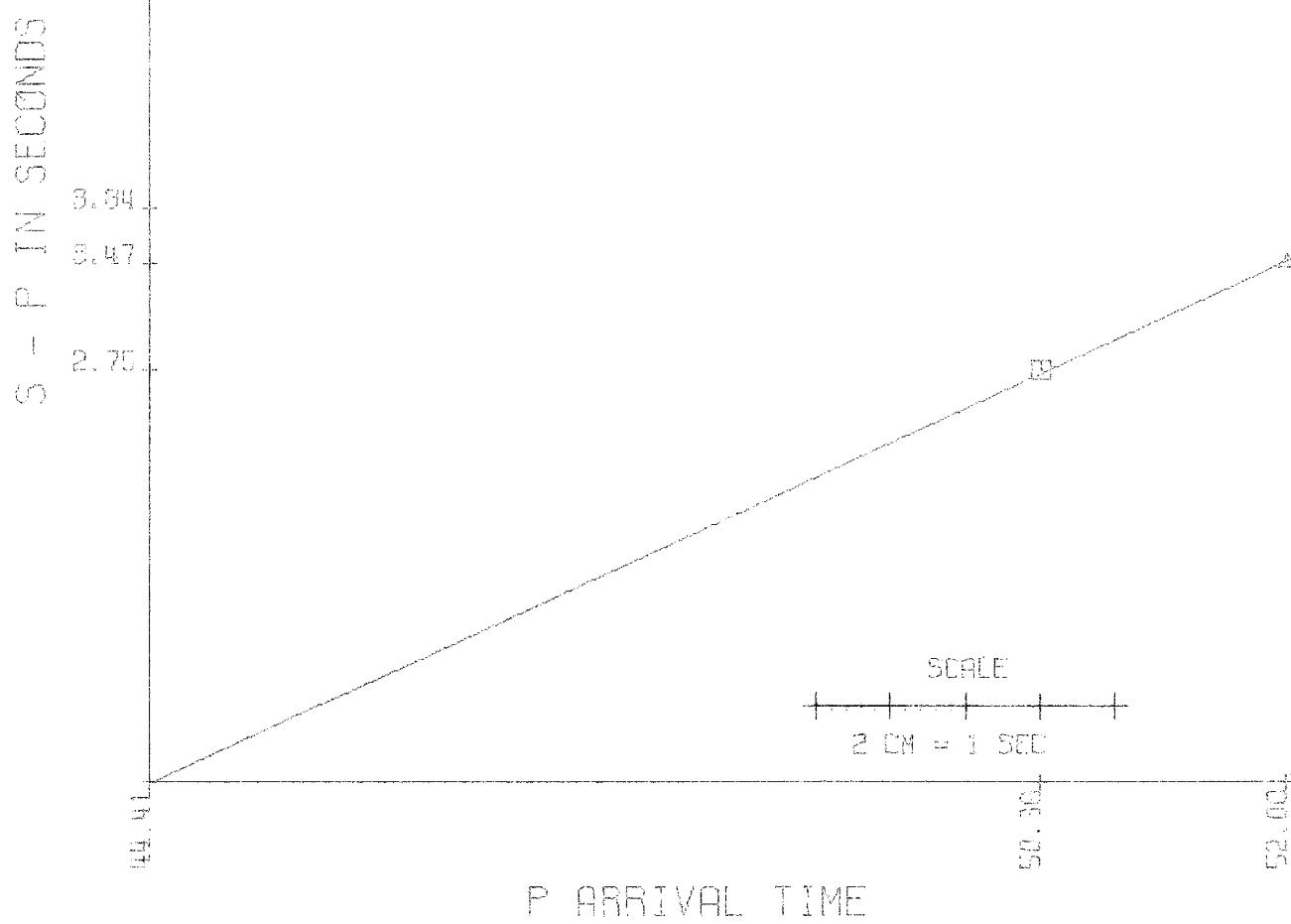


$$\frac{V_p}{V_s} = \boxed{\text{Relation of } V}$$



As

| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 3/25/1970 | 50.30 | 2.75 | SNM | E |
| ORIGIN | 15.32,44.41 | 0.00 | 0.00 | SAM | O |
| SLOPE | 0.46104 | 52.00 | 3.47 | SEB | A |
| VP | 4.392 | 52.70 | 3.84 | SCC | T |



DATE 3/17/1970
ORIGIN 17.05.24.34
SLOPE 0.31301
VF 4.397

SNM E
SRM O
SBB A
SCC +

S = P IN SECONDS

3.82
3.59
3.33

2.25

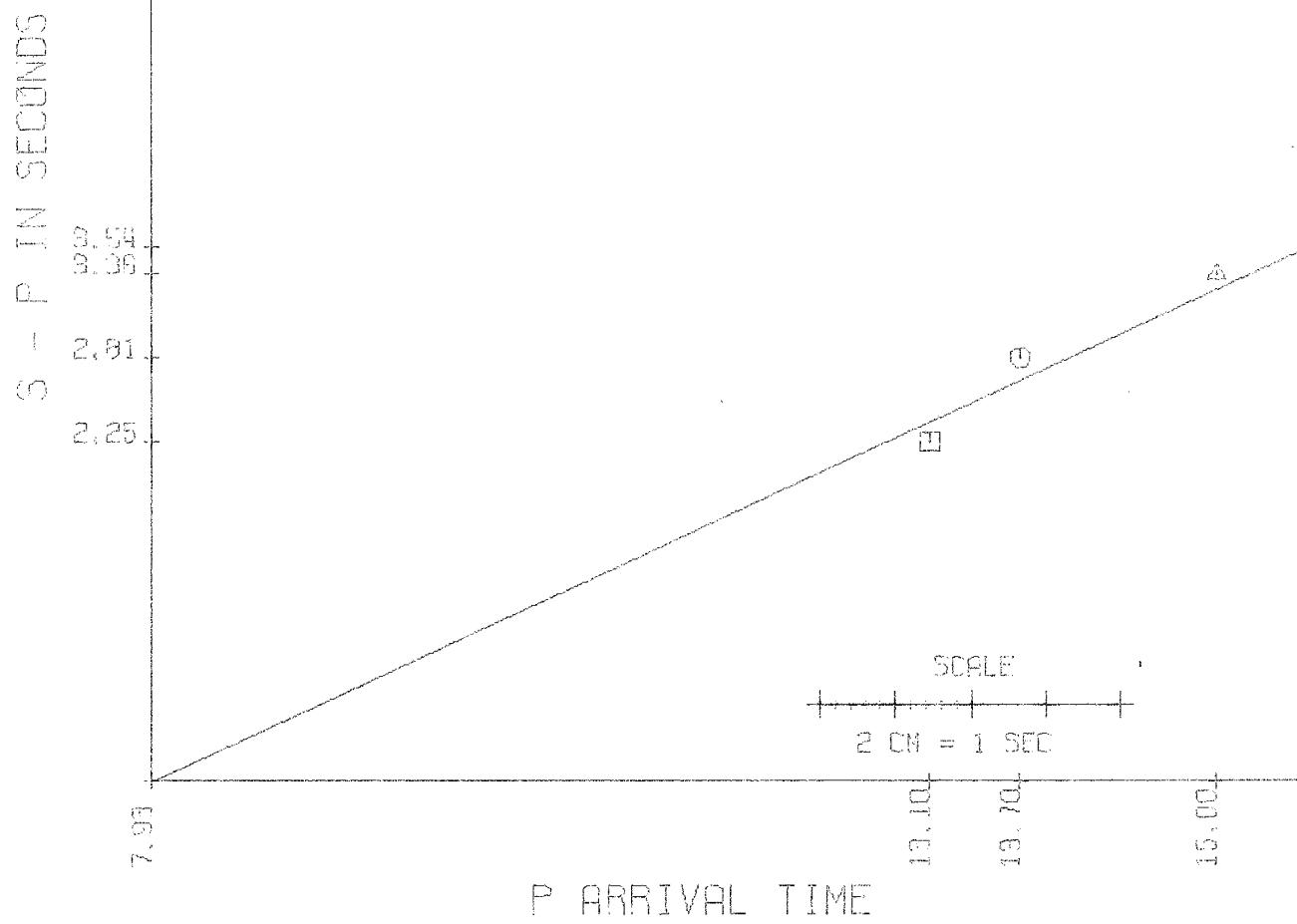
24.34

SCALE
2 CM = 1 SEC

P ARRIVAL TIME

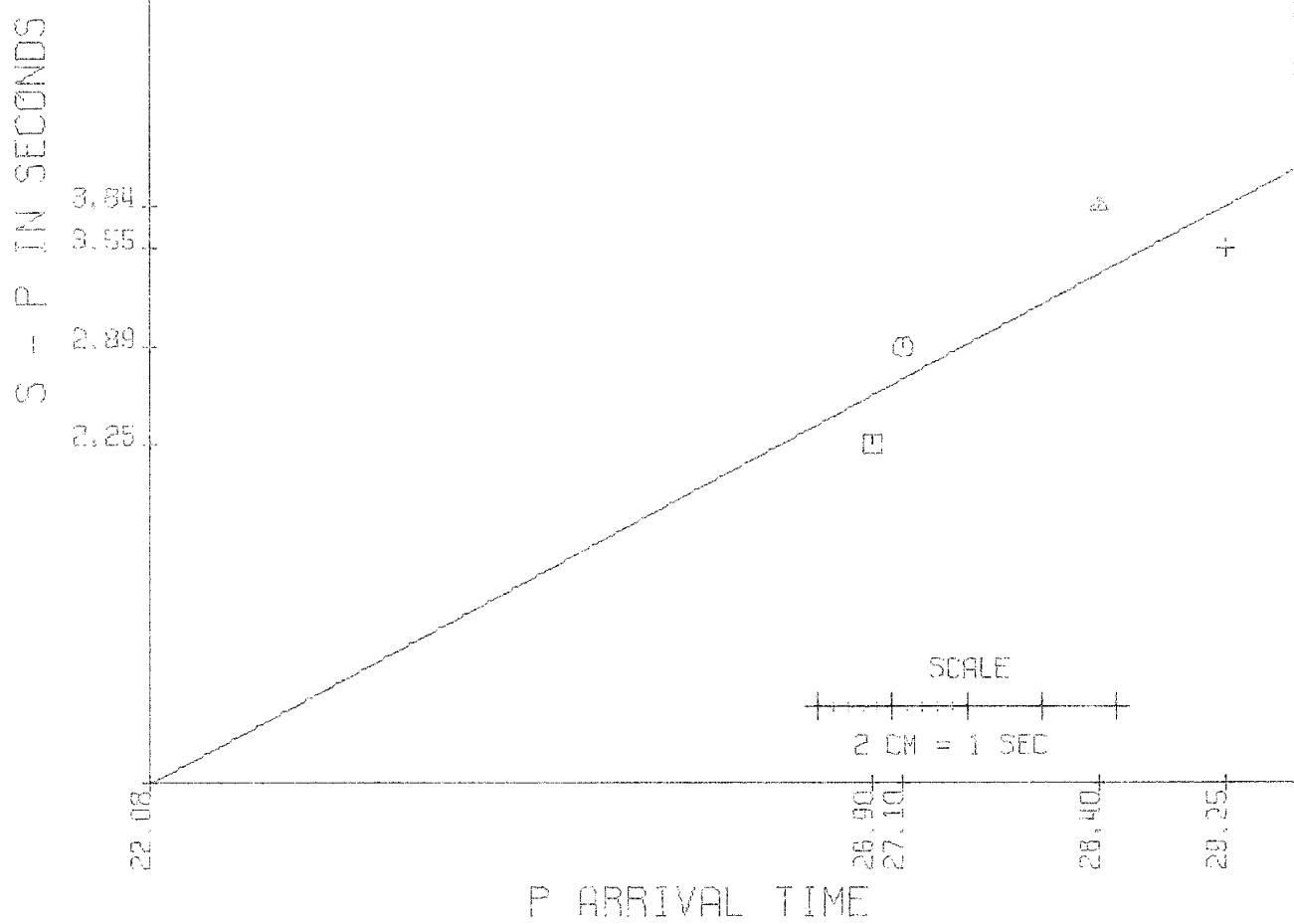
DATE 3/17/1970
ORIGIN 03.39.7.93
SLOPE 0.46222
VP 4.895

SNM
SRM
SRR
SOC
E G D
+



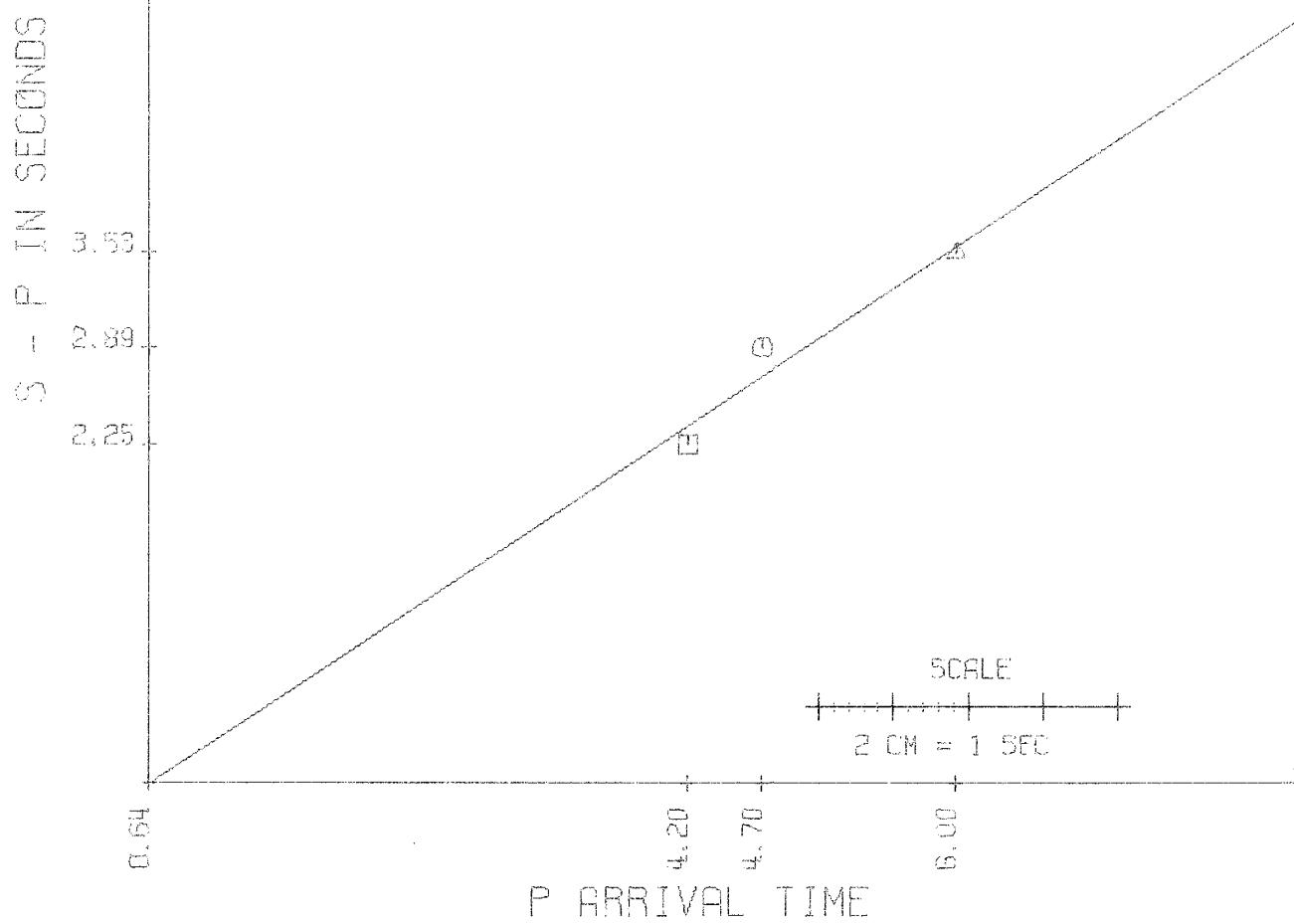
DATE 3/13/1970
ORIGIN 07.20.22.08
SLOPE 0.53716
VP 5.147

SNM
SRM
SBB
SCC
+ PGP

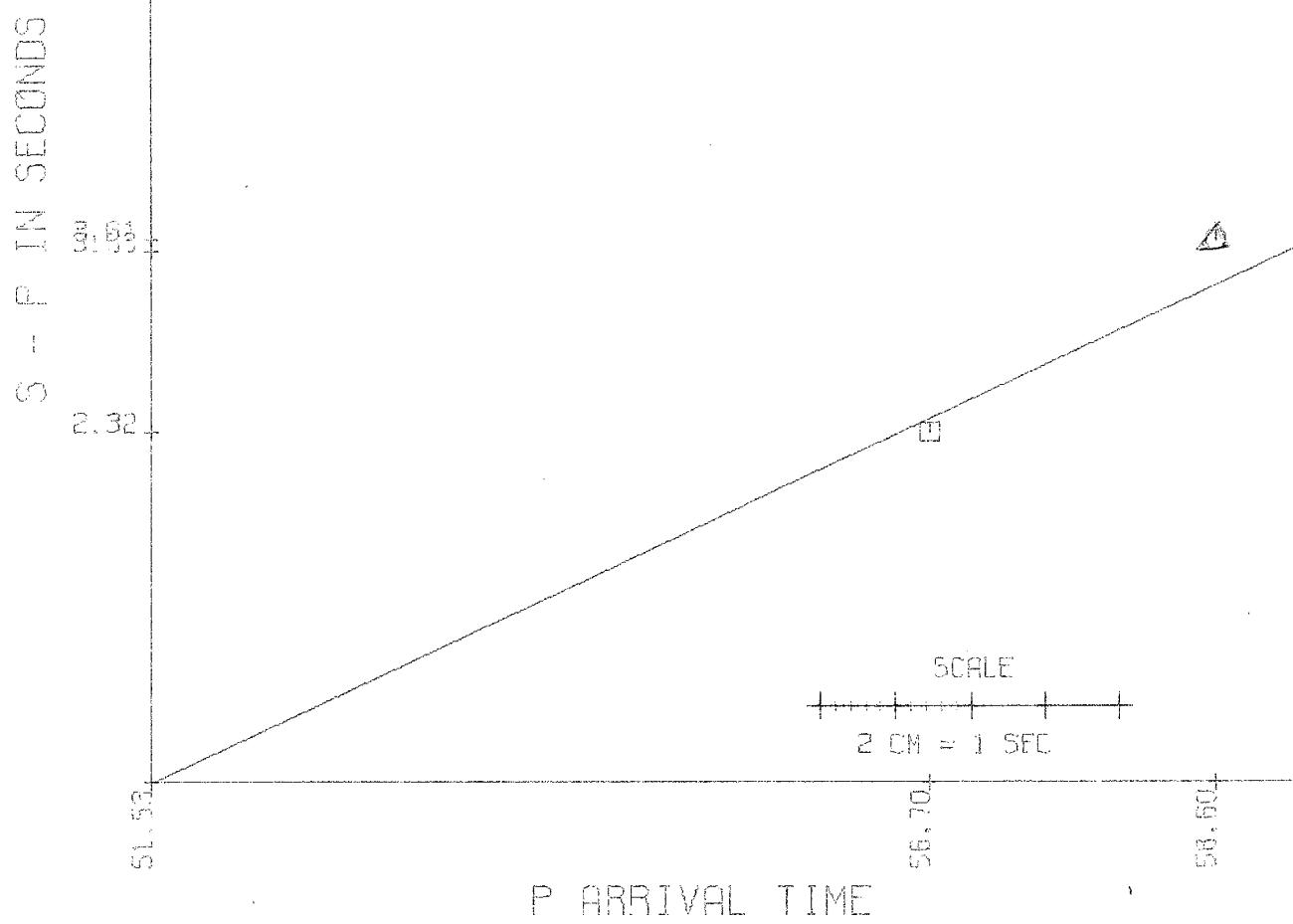


DATE 3/02/1970
ORIGIN 11.35,0.64
SLOPE 0.66718
VF 5.583

SNM E
SRM O
SAB A
SOC +

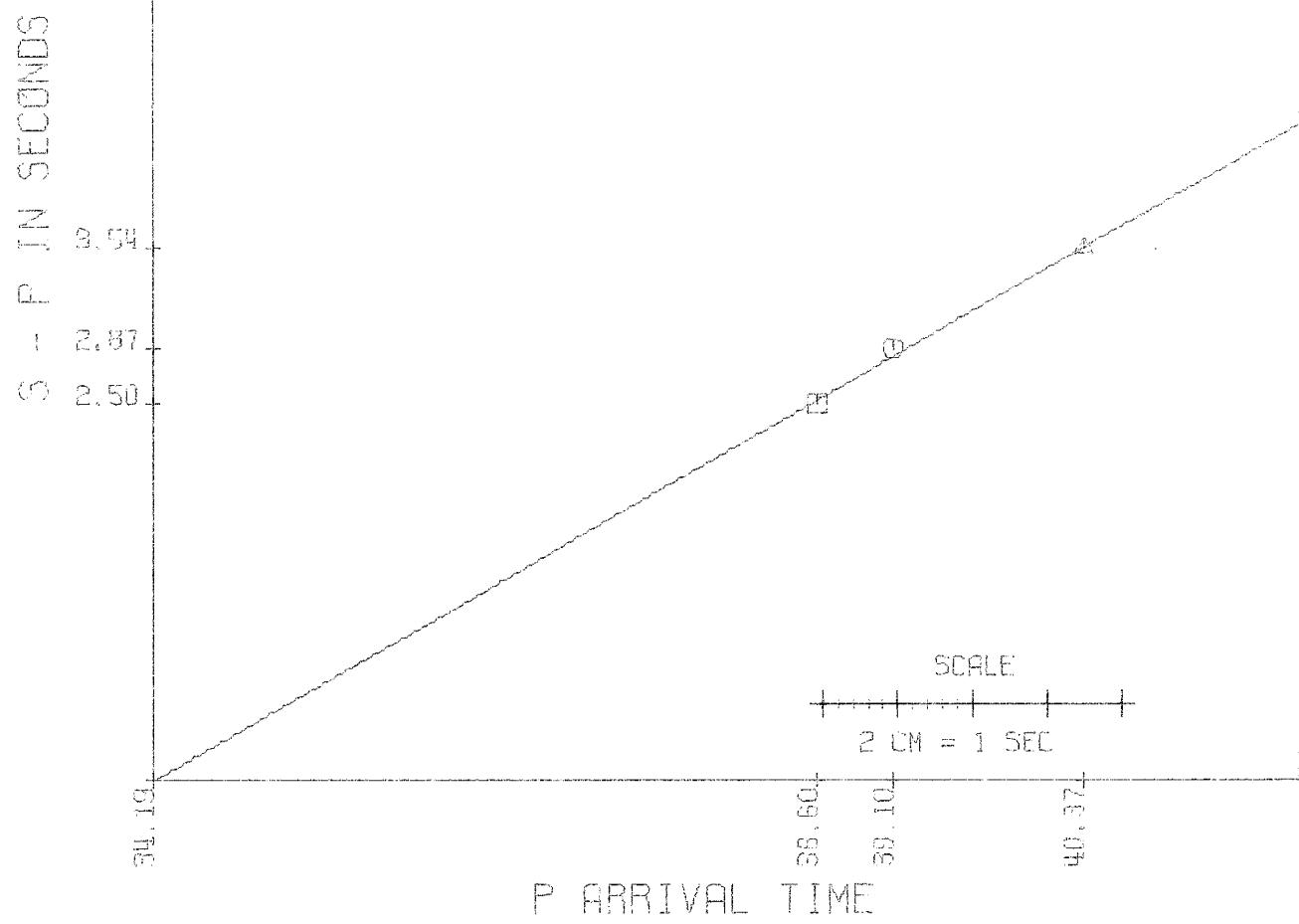


| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 3/17/1970 | 56.70 | 2.32 | SNM | E |
| ORIGIN | 06,40,51.53 | 58.60 | 3.61 | SMM | B |
| SLOPE | 0.46847 | 59.50 | 3.59 | SBB | A |
| VP | 4,917 | 0.00 | 0.00 | SCC | + |



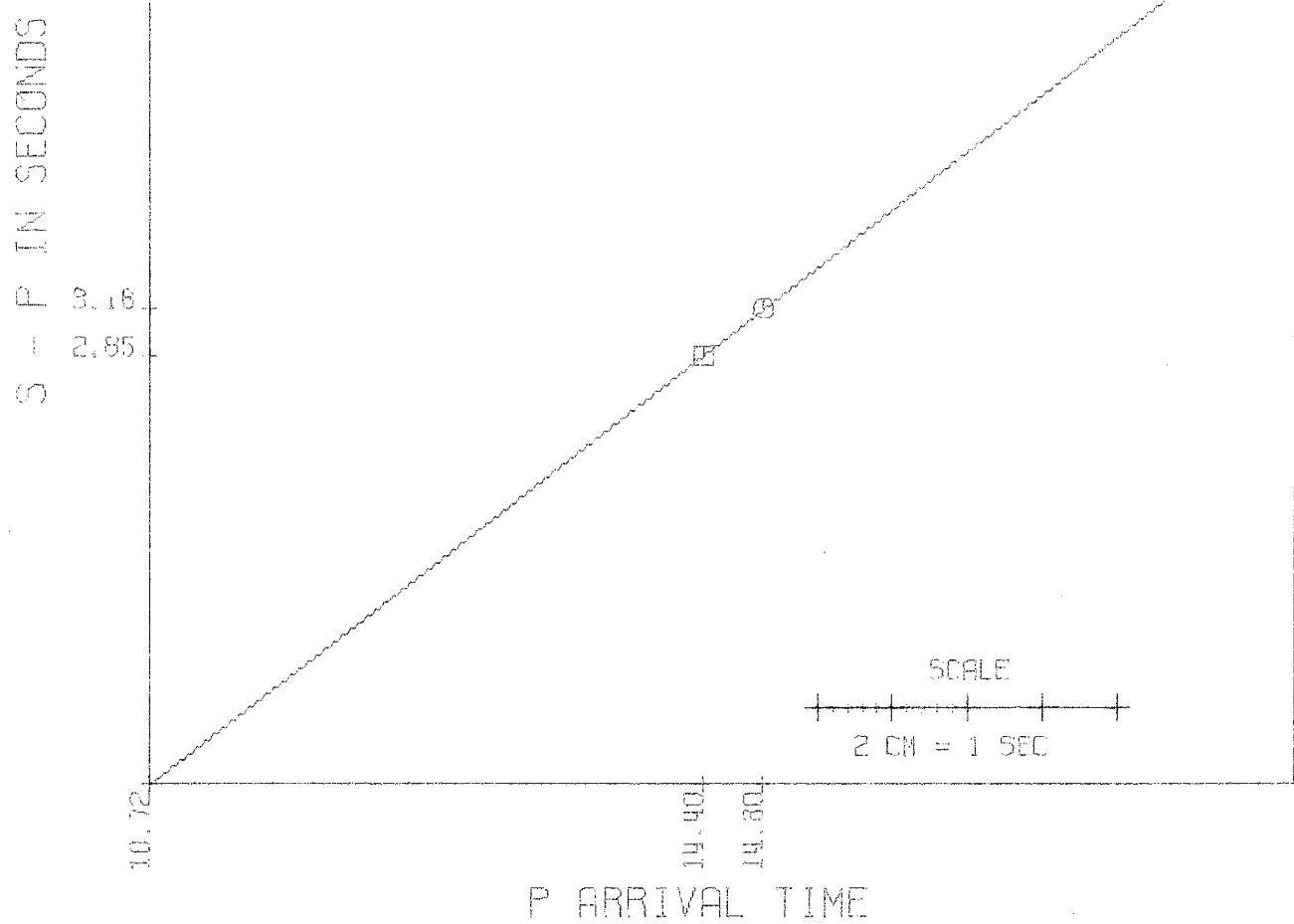
DATE 2/13/1970
ORIGIN 08.36.34.19
SLOPE 0.57505
VP 5.274

SNM P
SRM S
SBE A
SCC +



DATE 1/07/1970
ORIGIN 16.35, 10.72
SLOPE 0.77500
VP 5.944

SNM E
SRM O
S82 A
SOC +



| | | | | | |
|--------|------------|-------|------|-----|---|
| DATE | 1/11/1970 | 18.60 | 2.20 | SNM | E |
| ORIGIN | 20,40,4,82 | 16.85 | 1.78 | SRM | O |
| SLOPE | 0.15229 | 20.50 | 2.34 | SRR | A |
| VP | 3.659 | 0.00 | 0.00 | SCC | + |

S - P IN SECONDS

NO. 2

1.78

4.82

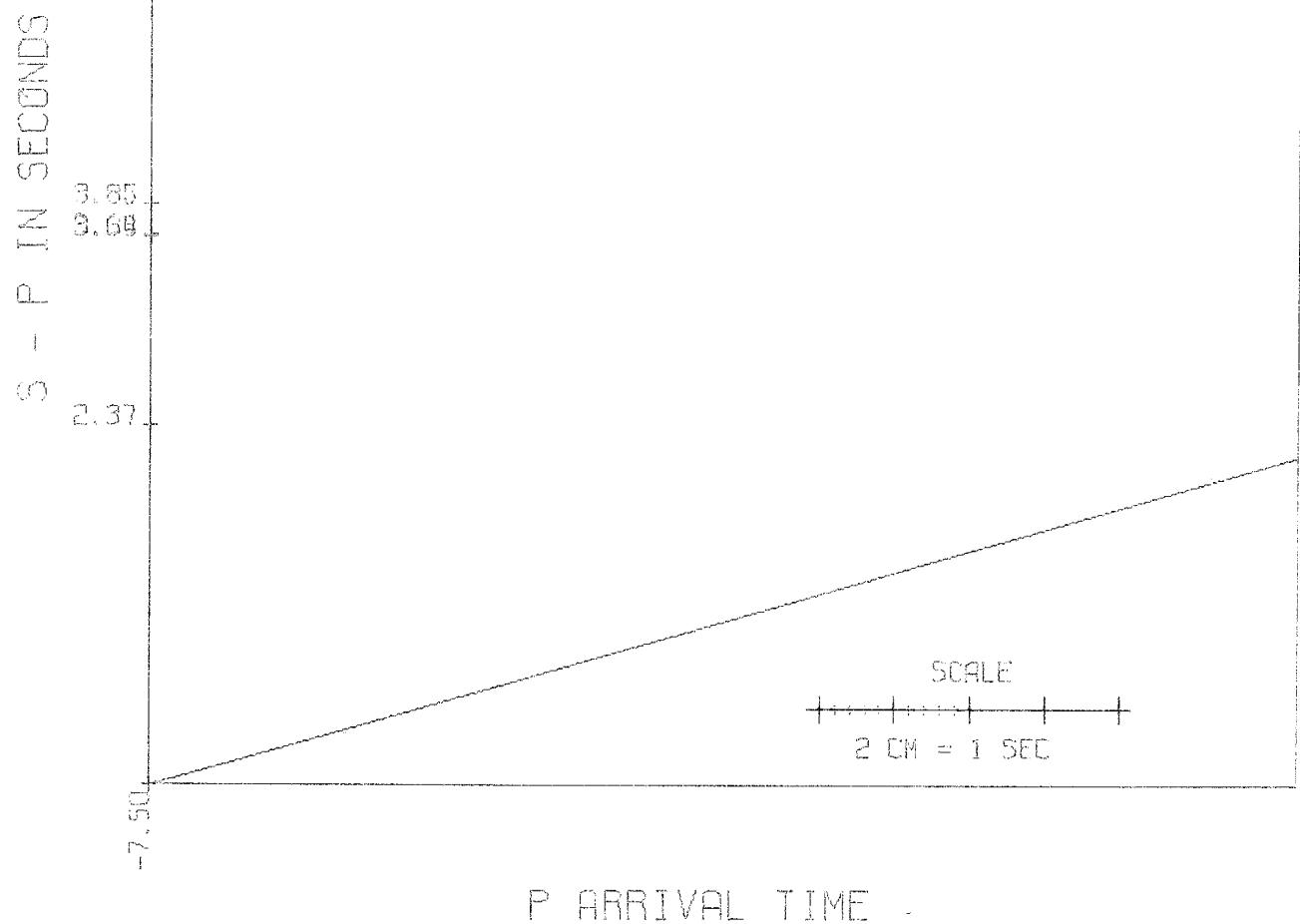


SCRE

2 CM = 1 SEC

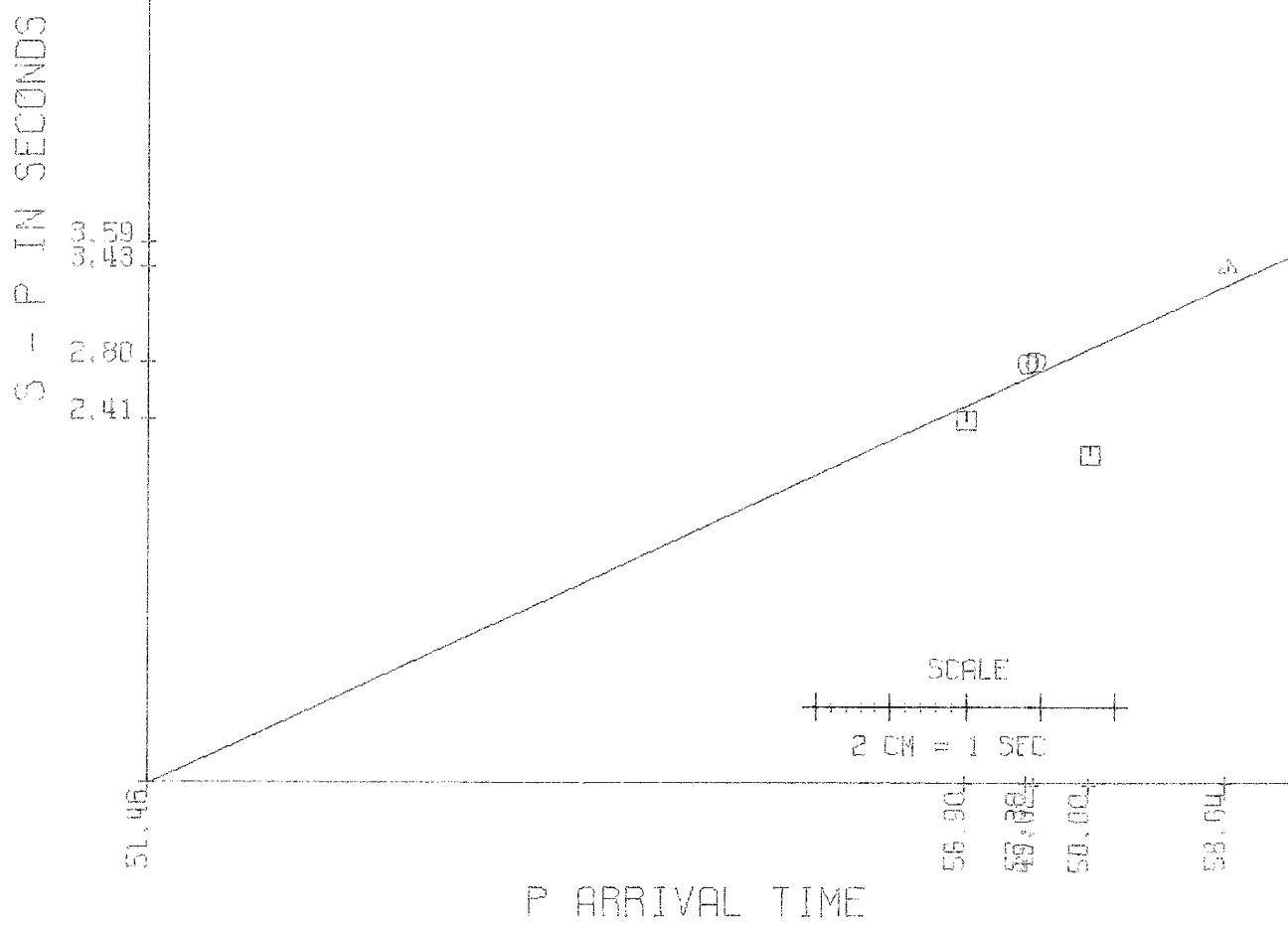
P ARRIVAL TIME

| | | | | | |
|--------|-------------|------|------|-----|---|
| DATE | 3/18/1970 | 3.30 | 2.37 | SNM | m |
| ORIGIN | 16.35,-7.50 | 3.50 | 3.65 | SRM | o |
| SLOPE | 0.28647 | 4.60 | 3.64 | S88 | a |
| VP | 4.308 | 5.70 | 3.63 | SCC | + |



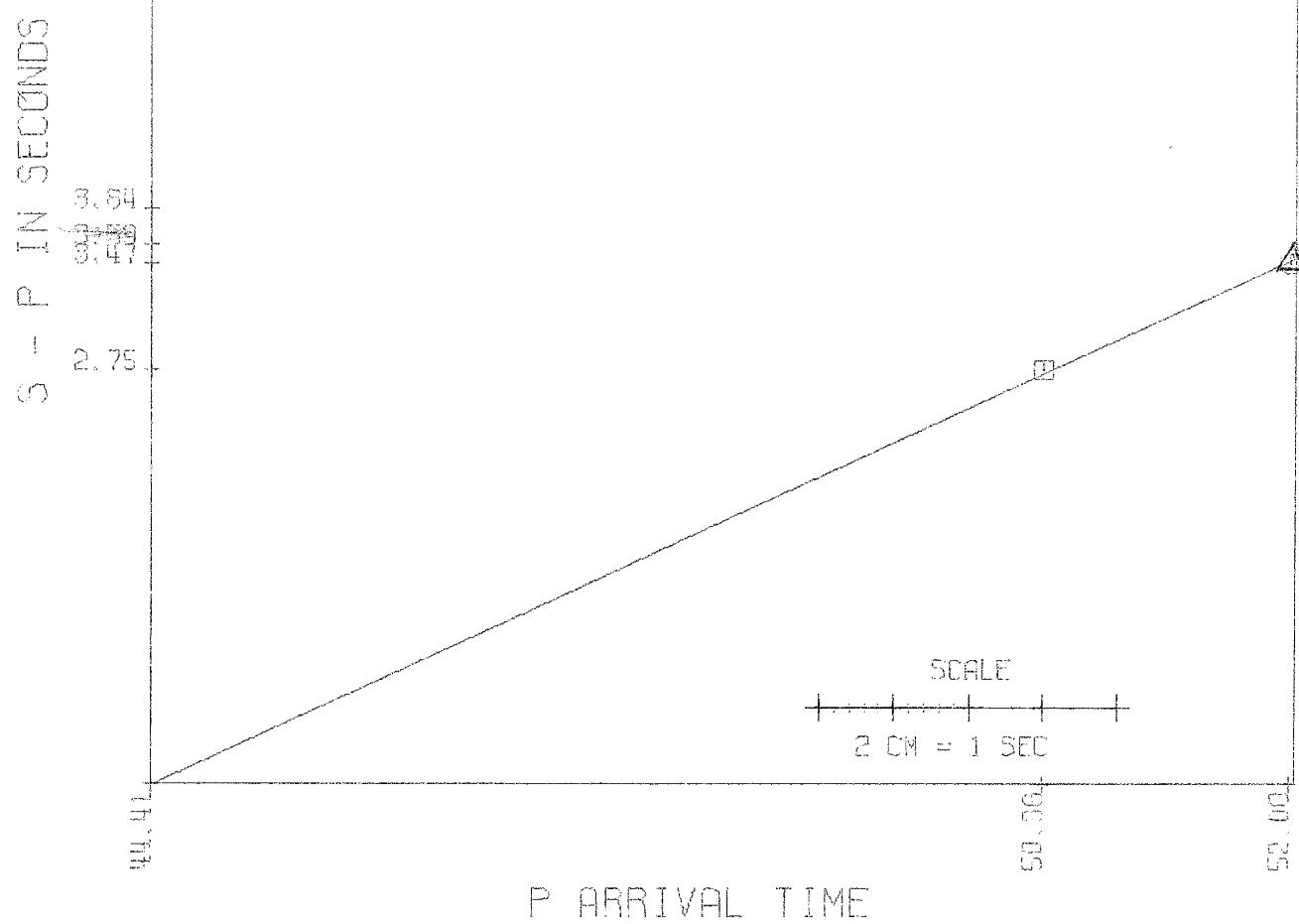
DATE 3/20/1970
ORIGIN 04, 34, 51, 46
SLOPE 0.48251
VP 4, 901

SNM ②
SRM ③
SAB ④
SCC +



DATE 3/25/1970
ORIGIN 15.32, 44.41
SLOPE 0.45104
VP 4.892

SNM E G A +
SRM SBB SDC



DATE 3/26/1970
ORIGIN 09.02.91.99
SLOPE -0.05974
VP 3.149

SNM ②
SRM ③
SBB ④
SCC +

P IN SECONDS

3.59

2.82

2.20

31.98

SCALE
2 CM = 1 SEC

P ARRIVAL TIME

47.70
49.00

55.50
56.25

2.20
1.36

DATE 3/30/1970
ORIGIN 02.51.48.46
SLOPE -4.30000
VP -11.050

SNM
SRM
SBR
SCC

SCALE

2 CM = 1 SEC

S - P IN SECONDS

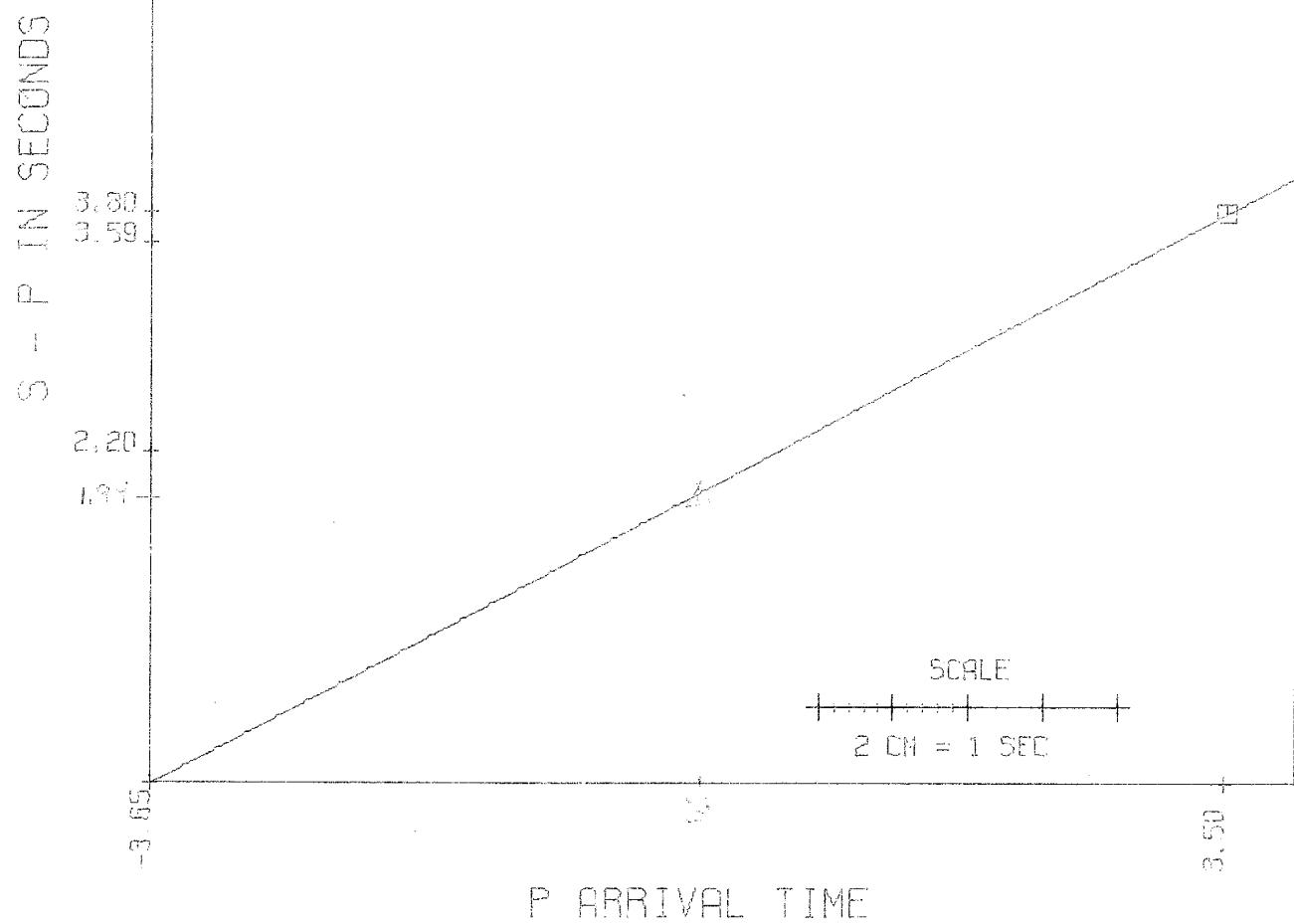
0

b

P ARRIVAL TIME

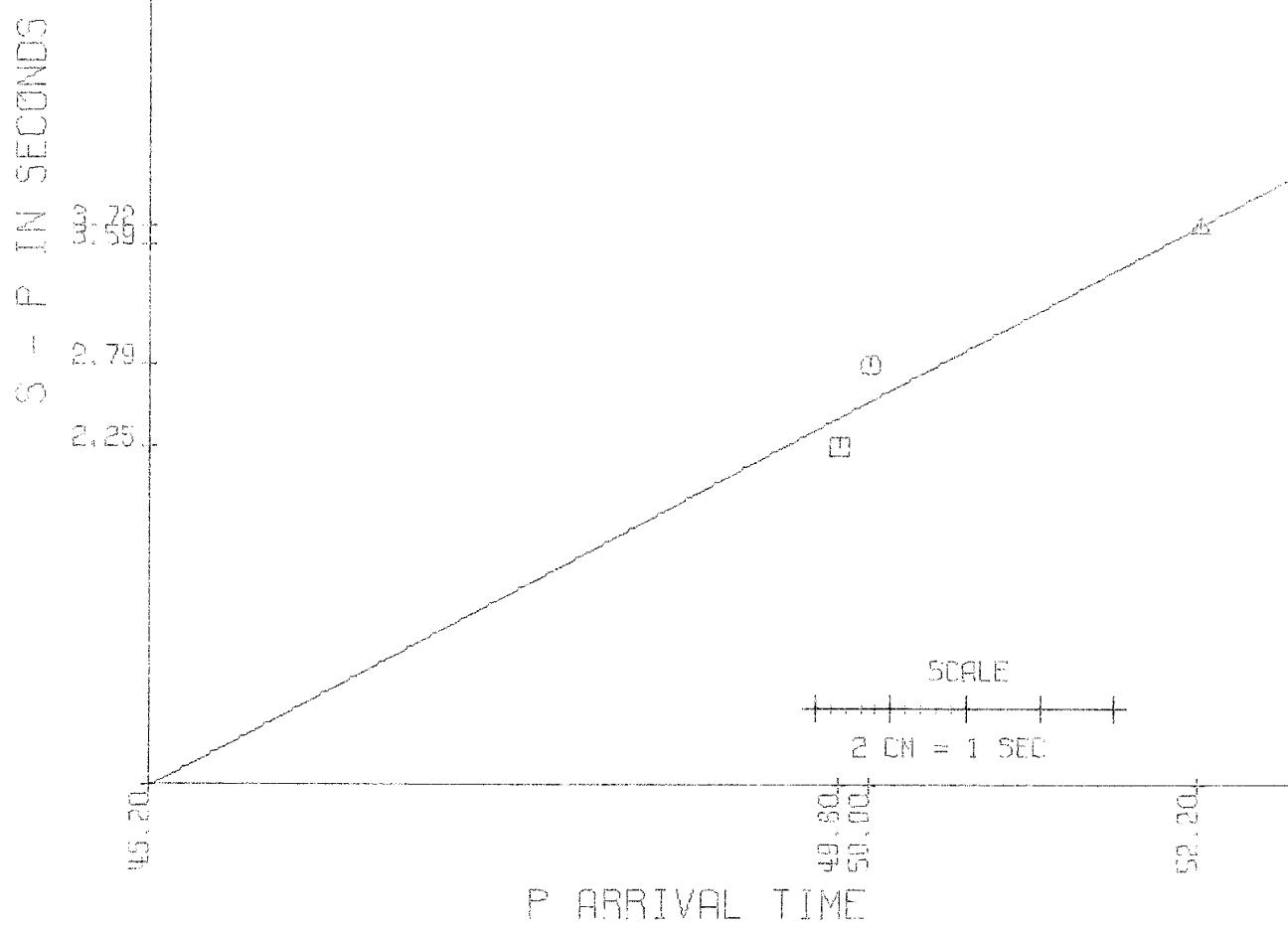
DATE 4/13/1970
ORIGIN 05.29.-3.65
SLOPE 0.53143
VP 5.126

SNM
SRM
SBB
SOC
+ E
④ A
+



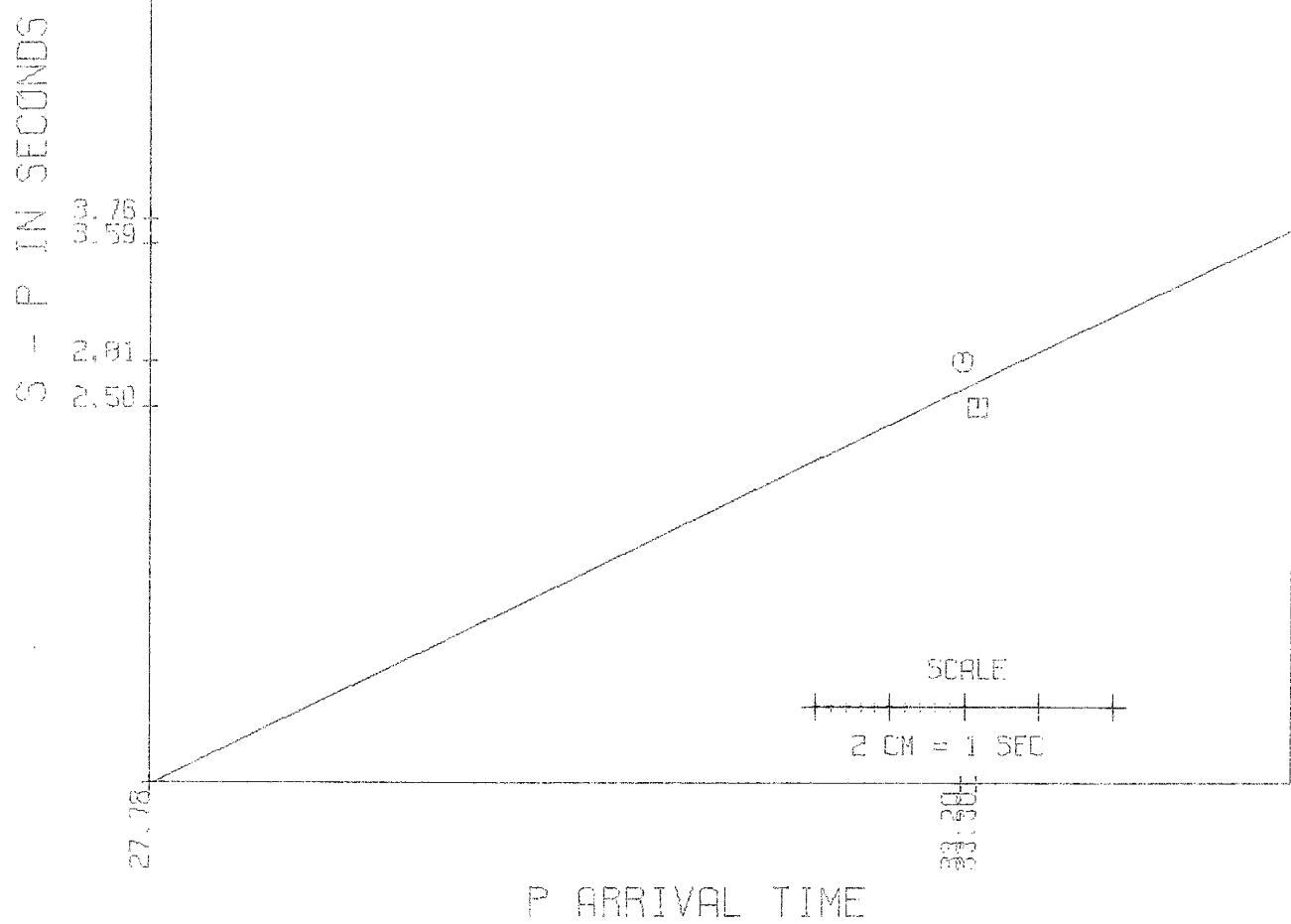
DATE 4/17/1970
ORIGIN 03.06,45.20
SLOPE 0.53402
VP 5.197

SNM
SRM
SAB
SOC
+ E G A



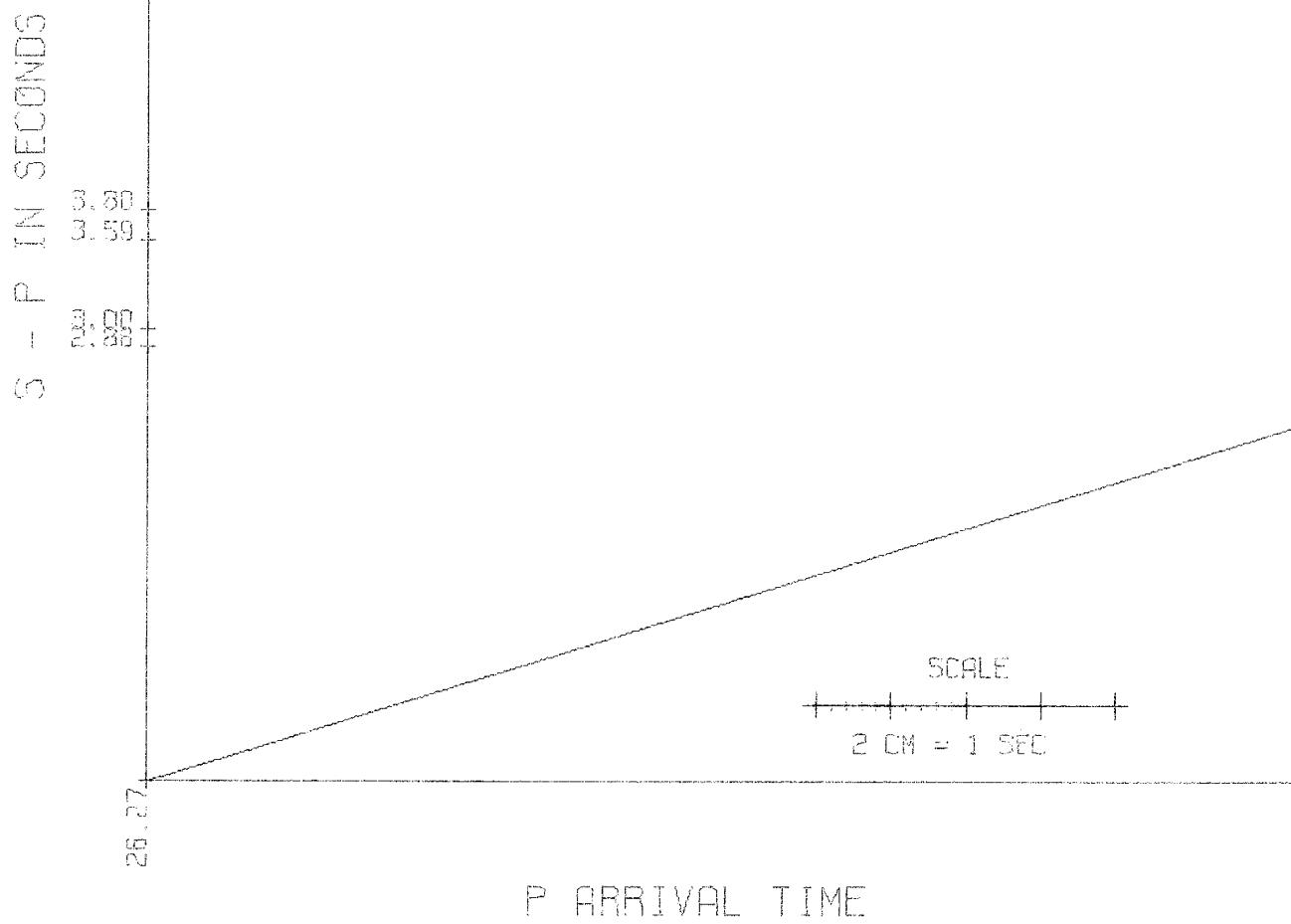
DATE 4/18/1970
ORIGIN 03.44.27.78
SLOPE 0.48580
VP 4.975

SNM D
SRM G
SBB A
SCC +



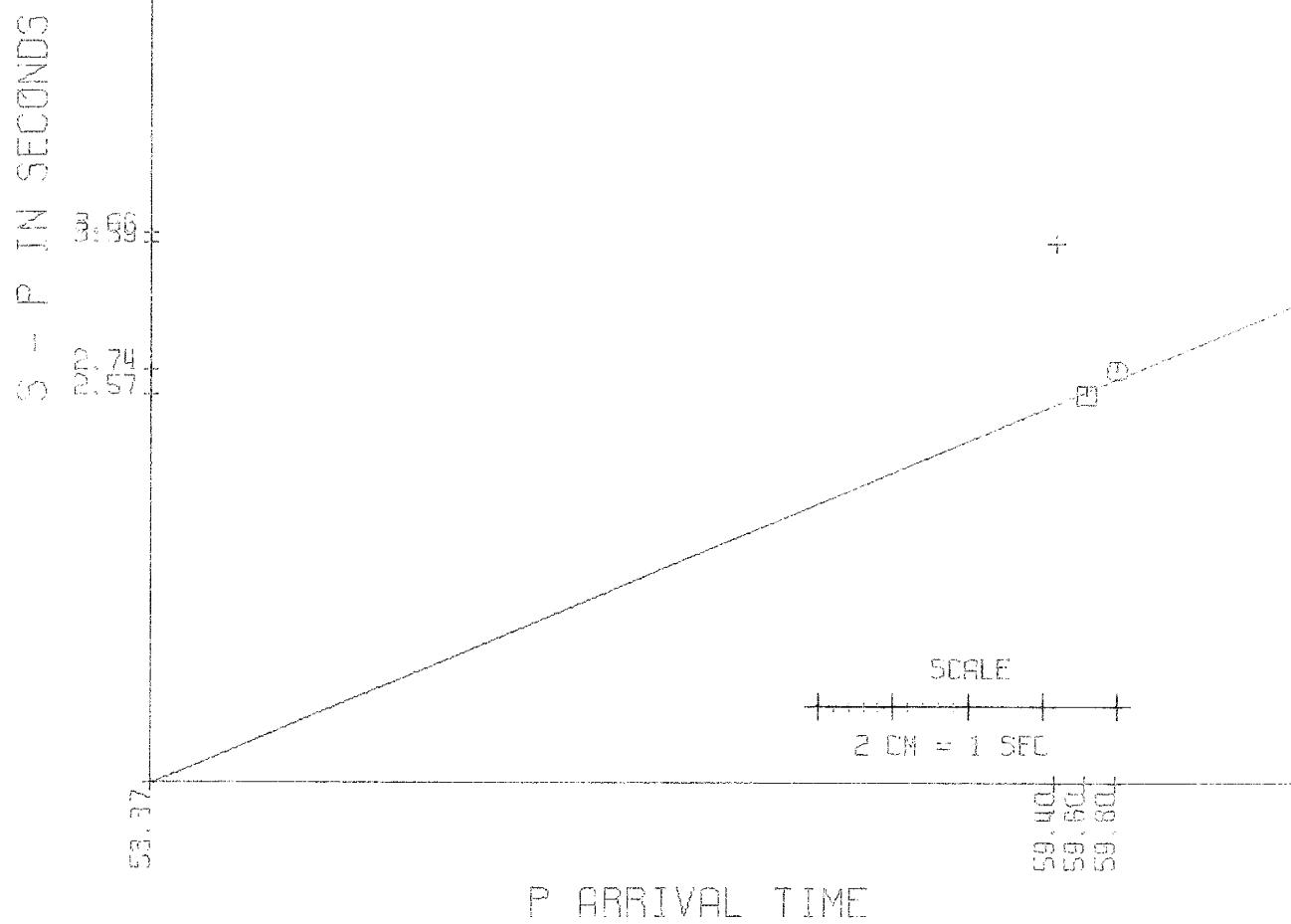
DATE 4/16 /1970
ORIGIN 07.11.26.27
SLOPE 0.31058
VF 4.368

SNM E
SRM G
SBR A
SCC +



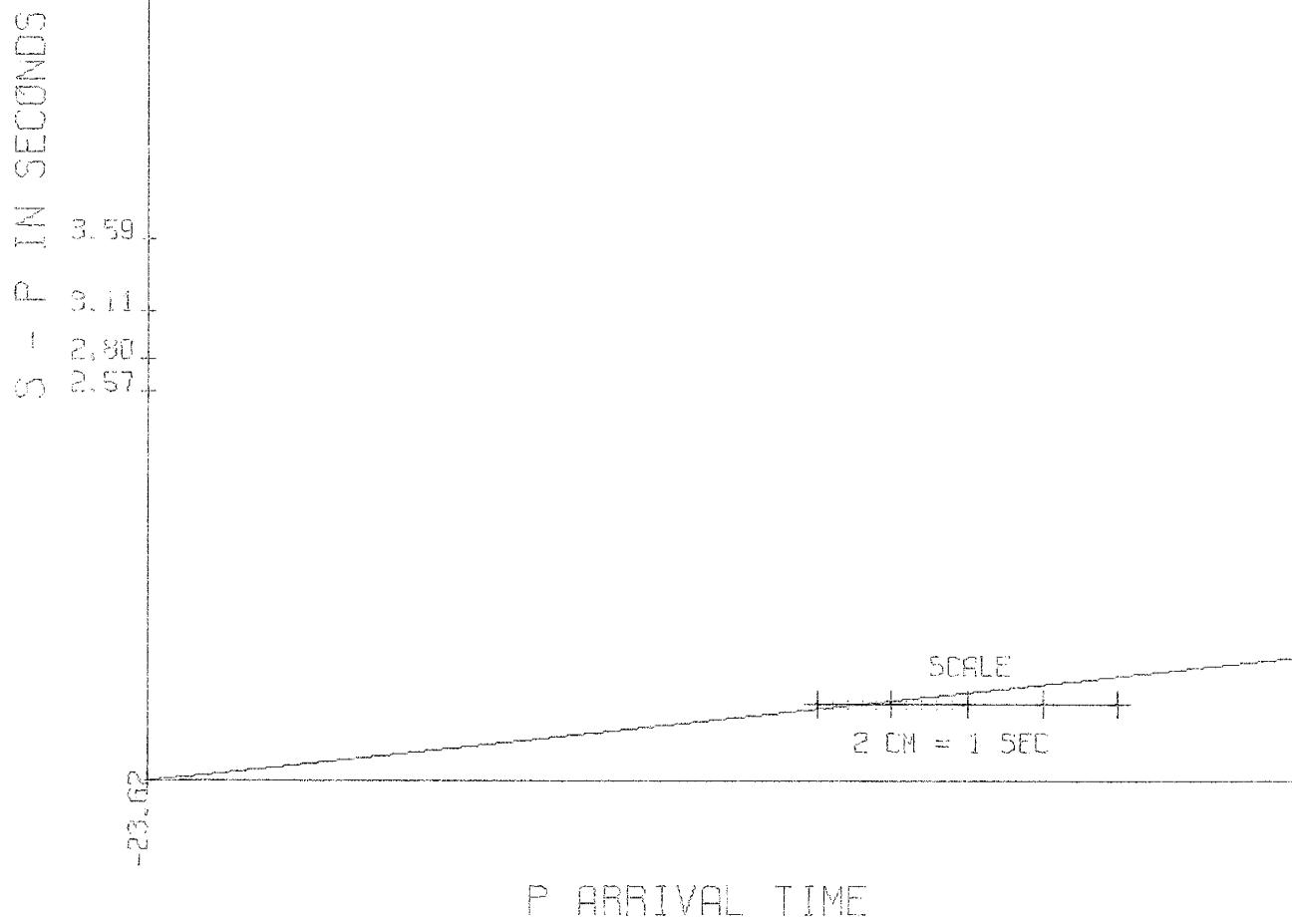
DATE 4/18/1970
ORIGIN 07.34.53.37
SLOPE 0.41982
VP 4.754

SNM 0
SRM 0
SBB 4
SCC 4



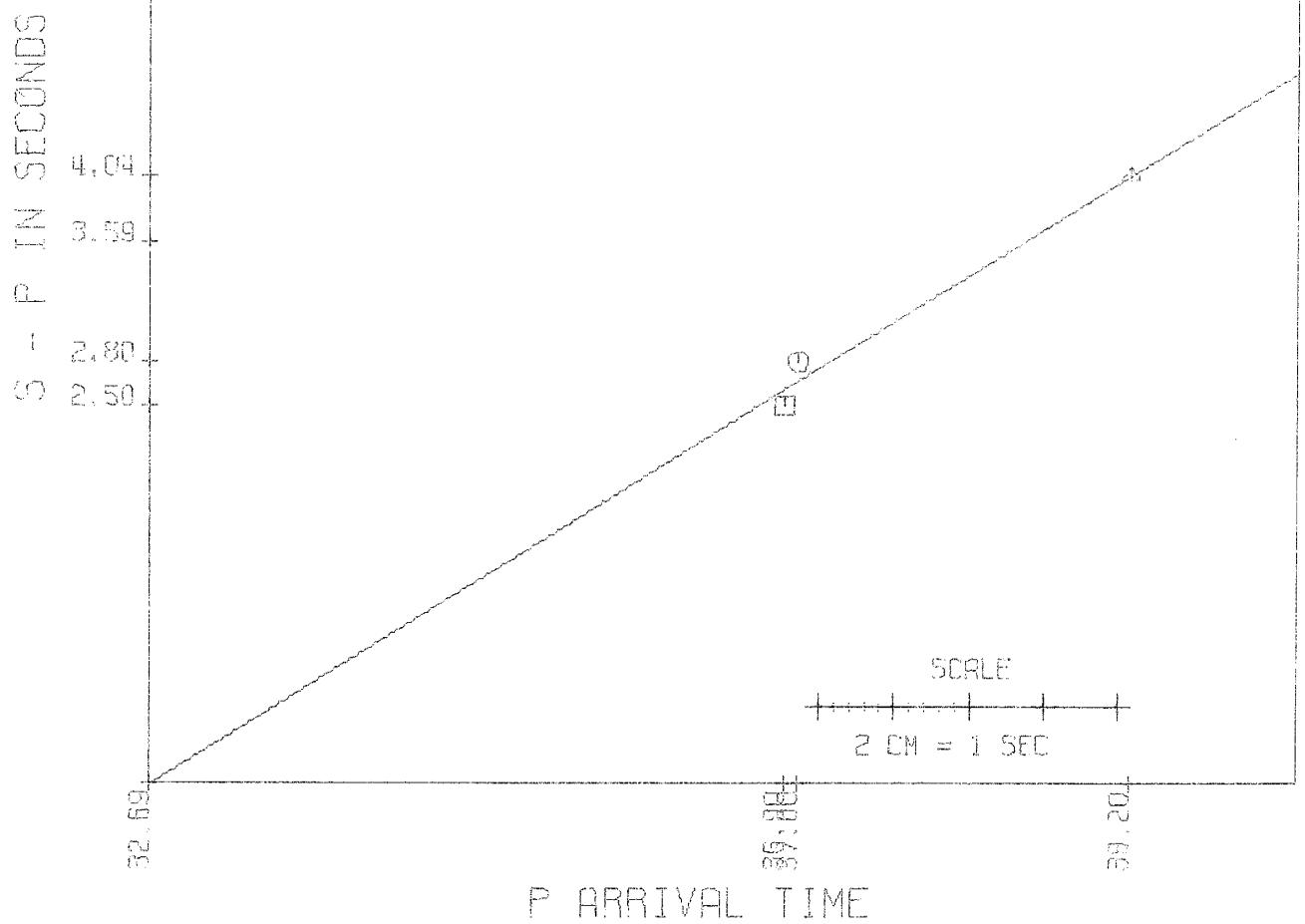
DATE 4/18/1970
ORIGIN 09.05.-23.62
SLOPE 0.10799
VP 3.710

SNM 01
SRM 0
SBB 4
SOC +



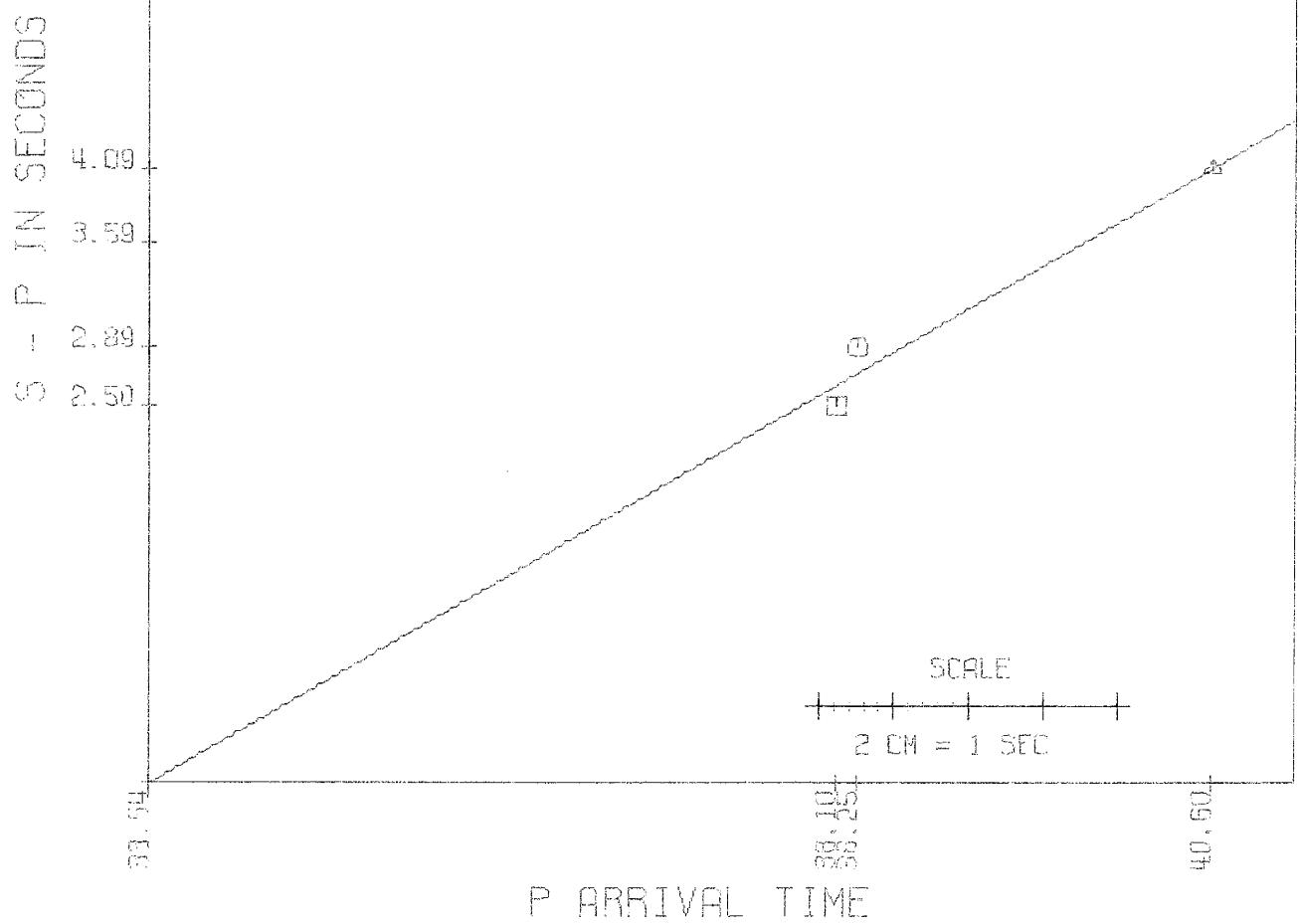
DATE 4/16/1970
ORIGIN 09.12.32.69
SLOPE 0.62130
VP 5.423

SNM E
SRM G
SBB A
SOC +



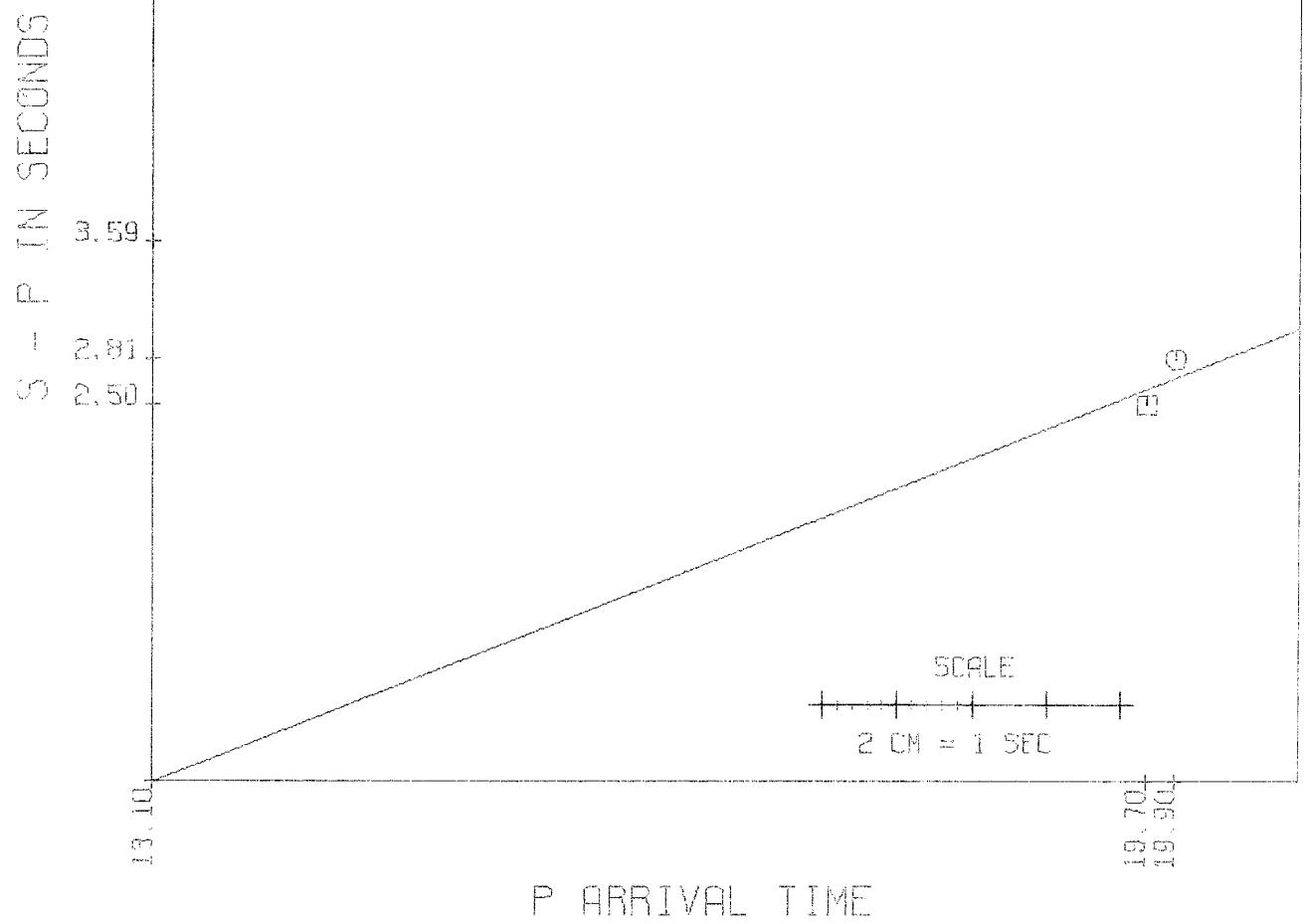
DATE 4/18/1970
ORIGIN 09.29.33.54
SLOPE 0.58105
VP 5.294

SNM □
SRM ○
SBB ▲
SCC +



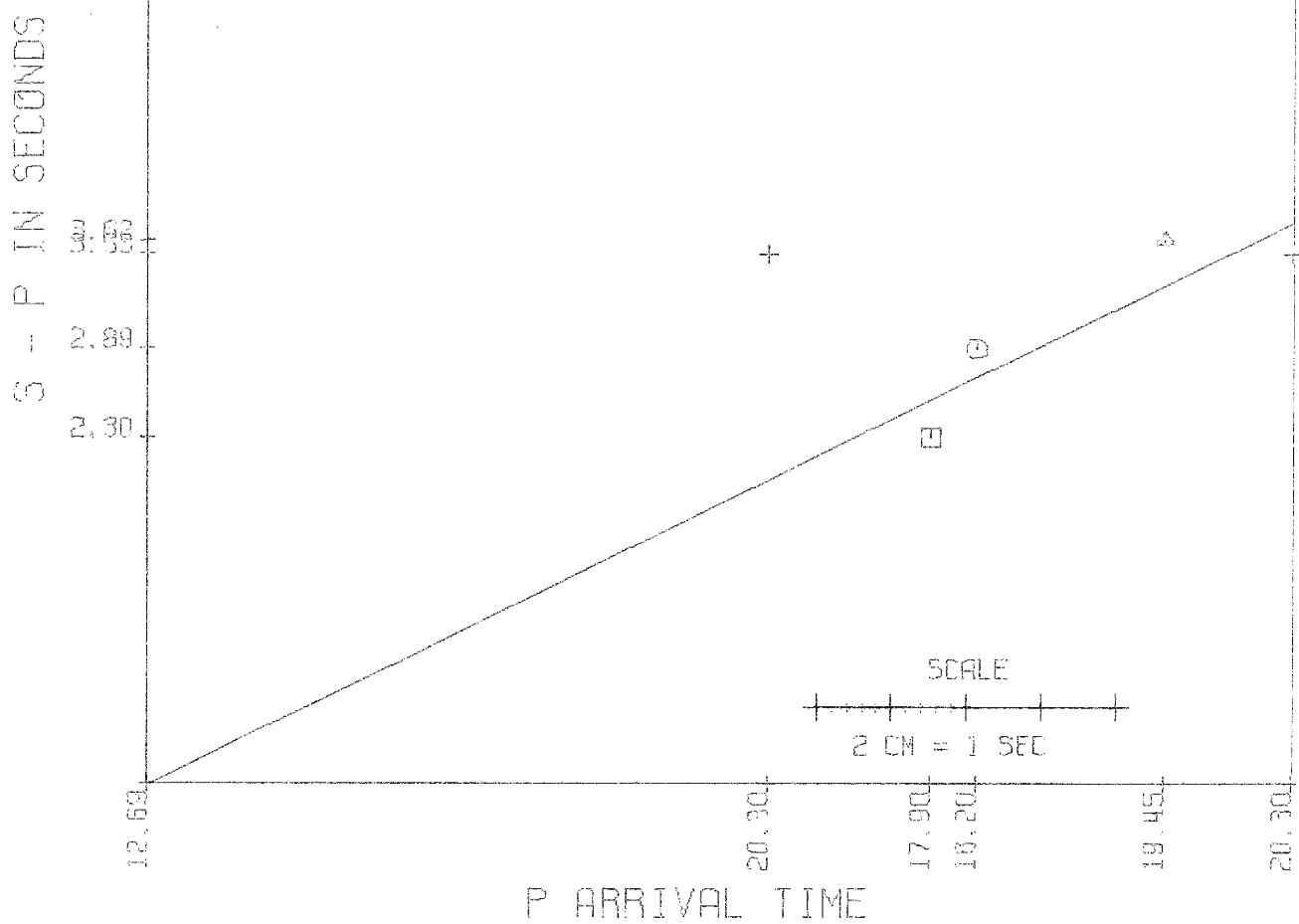
DATE 4/16/1970
ORIGIN 19.18.13.10
SLOPE 0.39560
VP 4.673

SNM □ E
SRM □ G
SBB □ A
SCC +



DATE 5/05/1970
ORIGIN 22.44, 12.69
SLOPE 0.49206
VP 4.996

SNM ④ B
SRM ④ A
SBB ④ +
SOC ④ +



DATE 5/05/1970
ORIGIN 22.44, 40.31
SLOPE 0.20451
VP 4.033

SNM □
SRM ○
S8B ▲
SOC +

P IN SECONDS

3.53
3.33
3.12
2.50
1.88
1.25

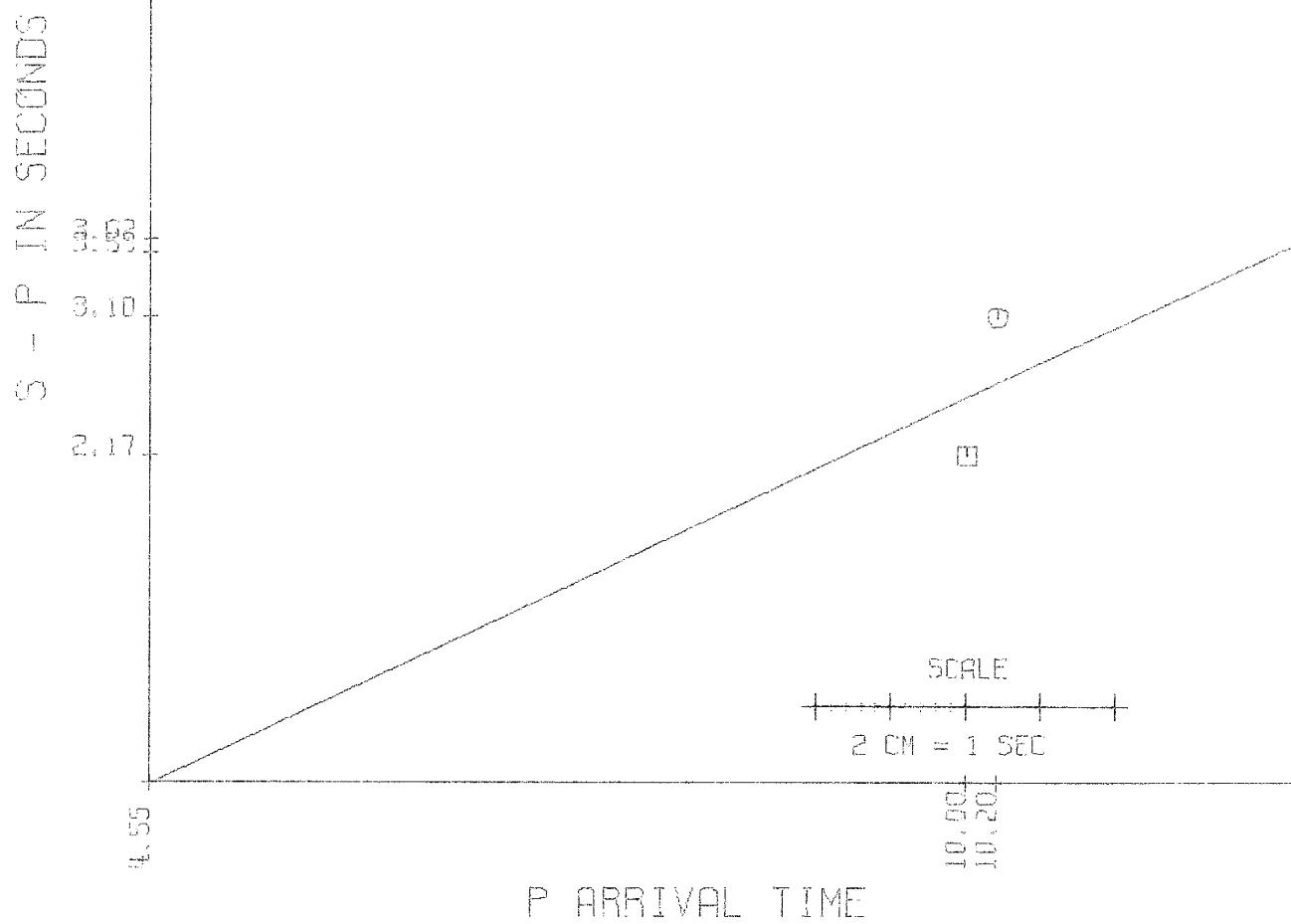
3.53
3.33
3.12
2.50

SCALE
2 CM = 1 SEC

P ARRIVAL TIME

DATE 5/05 /1970
ORIGIN 23.03.4.55
SLOPE 0.47214
VP 4.930

SNM
SRM
SBR
SOC



DATE 5/11/1970
ORIGIN 06.07.55.01
SLOPE -0.91667
VP 0.278

SNM ④
SRM ①
SBB ③
SOC +

S - P IN SECONDS

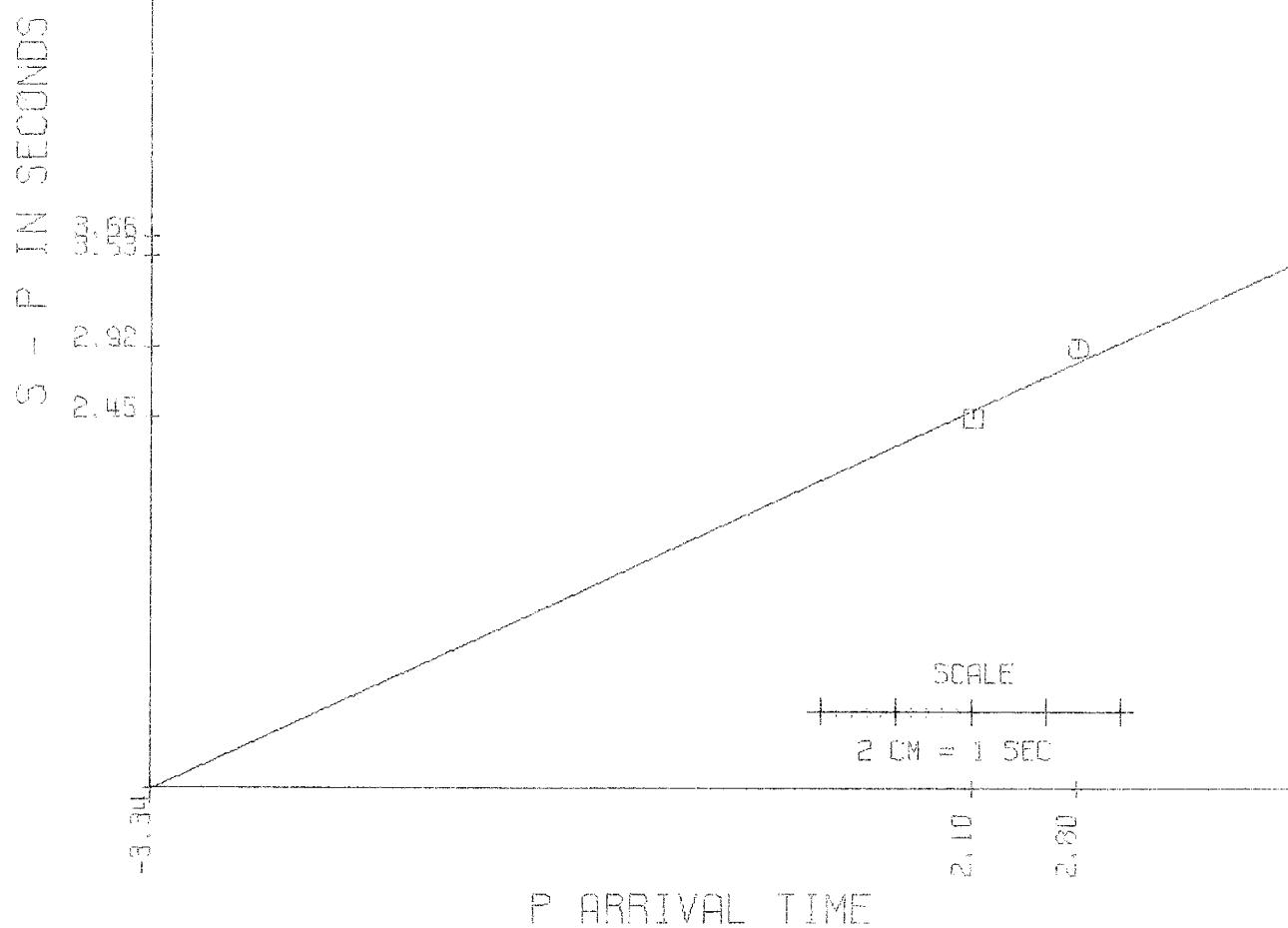
3.00
2.88
2.76
2.64
2.52
2.40
2.28
2.16
2.04
1.92
1.80
1.68
1.56
1.44
1.32
1.20
1.08
0.96
0.84
0.72
0.60
0.48
0.36
0.24
0.12
0.00

SCALE
2 CM = 1 SEC

P ARRIVAL TIME

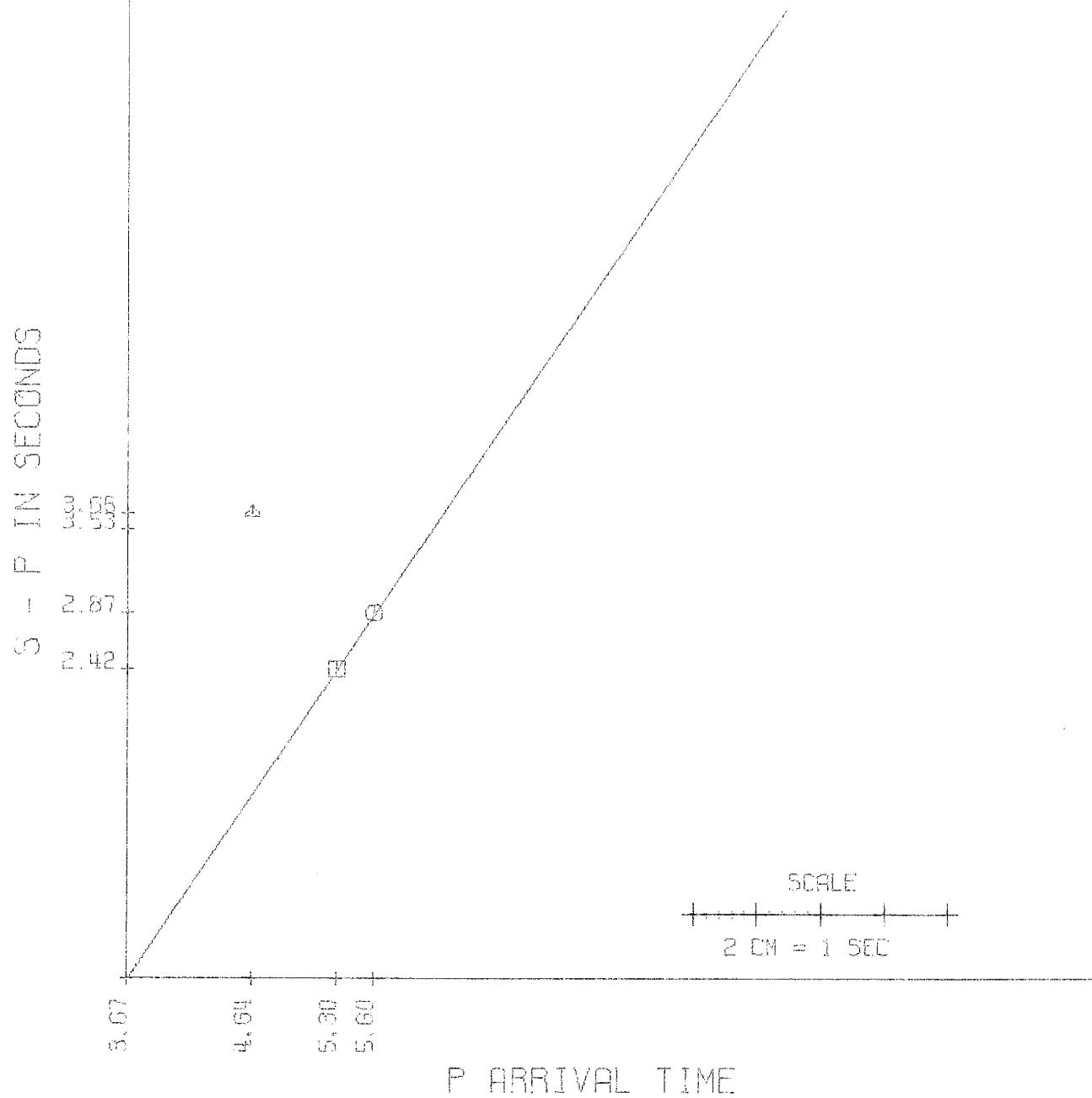
DATE 5/13/1970
ORIGIN 02.31,-3.34
SLOPE 0.46131
VP 4.893

SNM 01
SRM 02
SBB 03
SCC 04



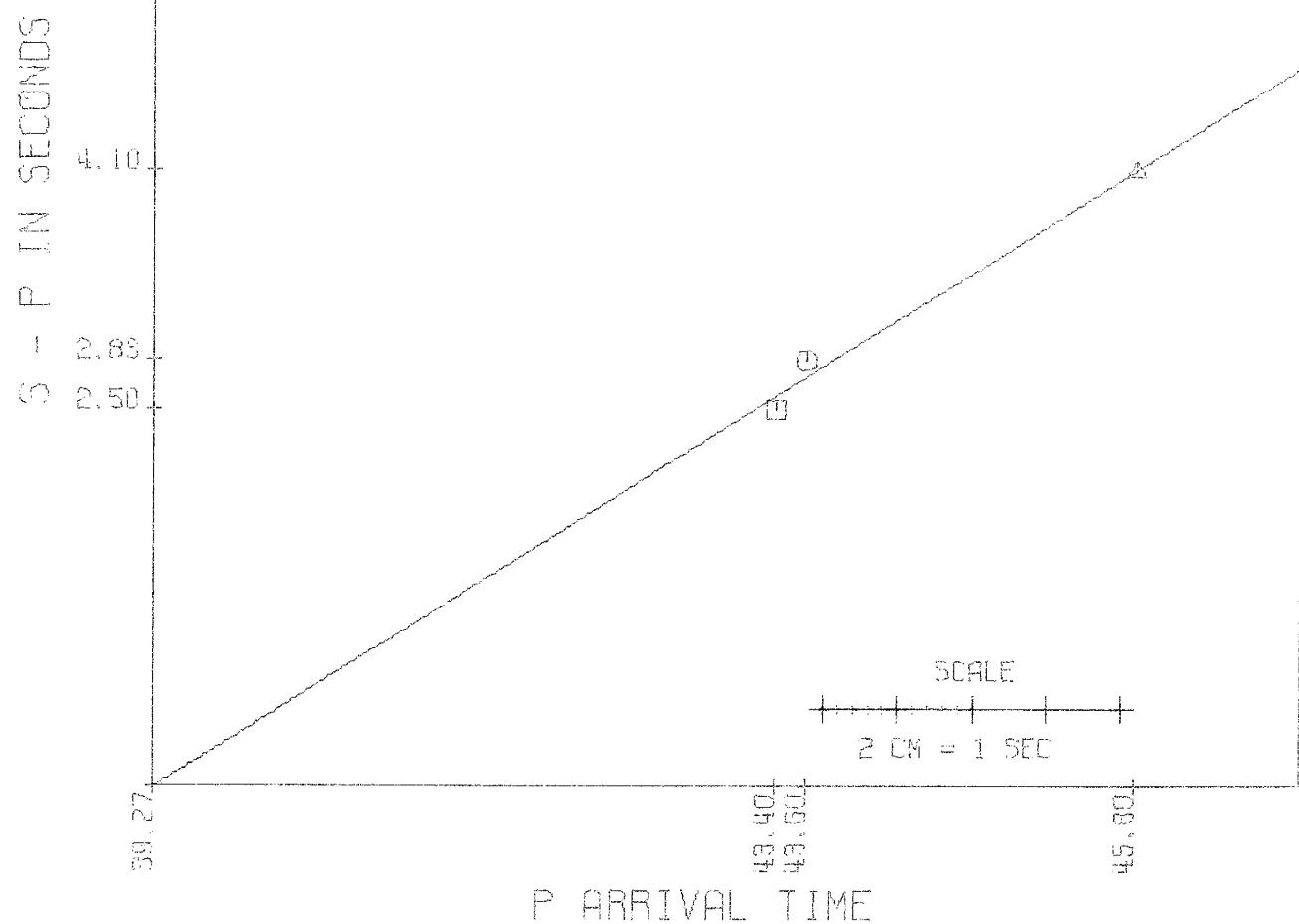
DATE 6/01/1970
ORIGIN 12.23.3.67
SLOPE 1.46333
VP 6.316

SNM □
SPM ○
SBB ▲
SCC +

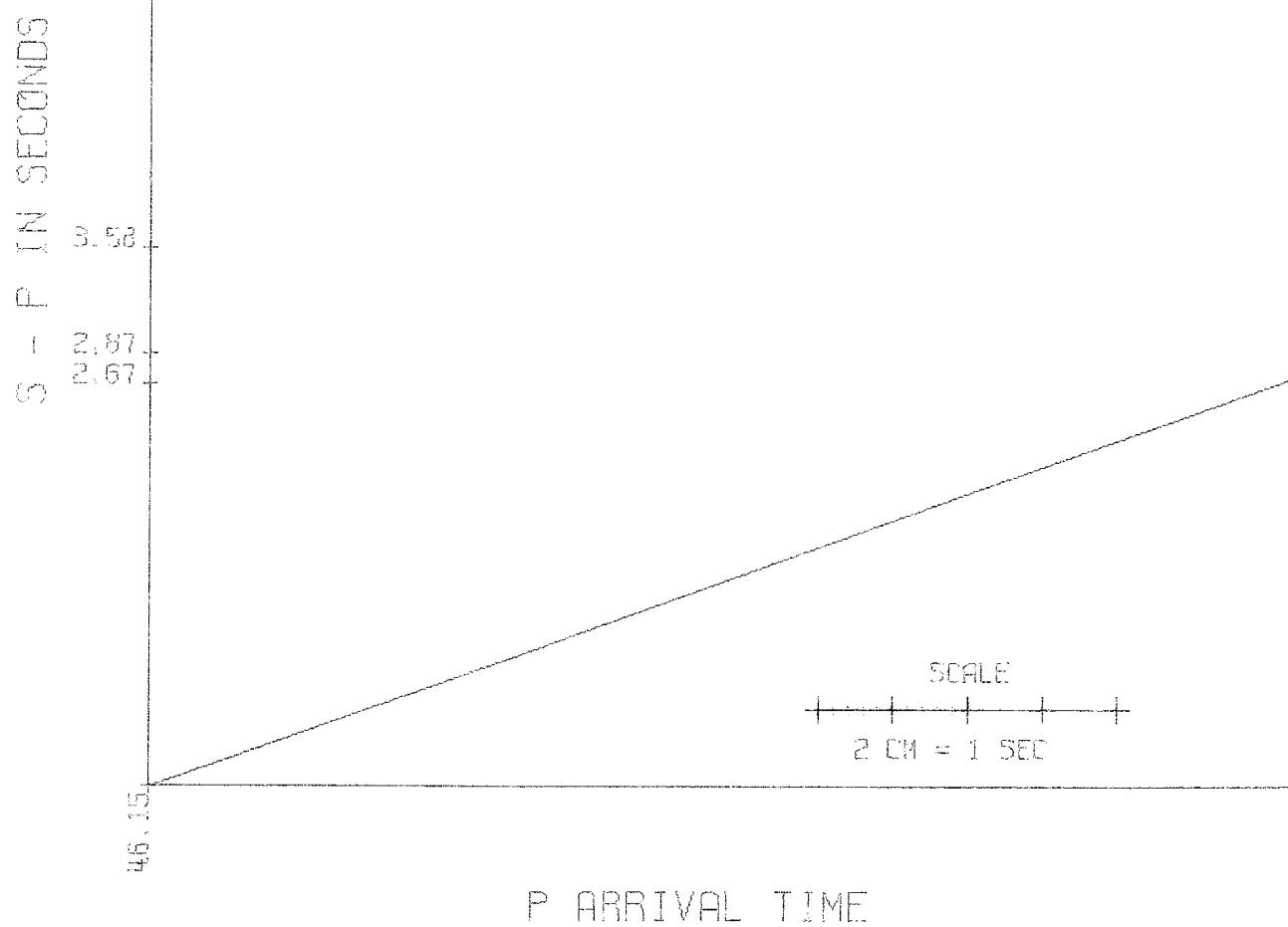


DATE 6/01/1970
ORIGIN 15, 35, 38, 27
SLOPE 0.62970
VP 5.457

SNM
SRM
SBB
SCC
E + P Q E

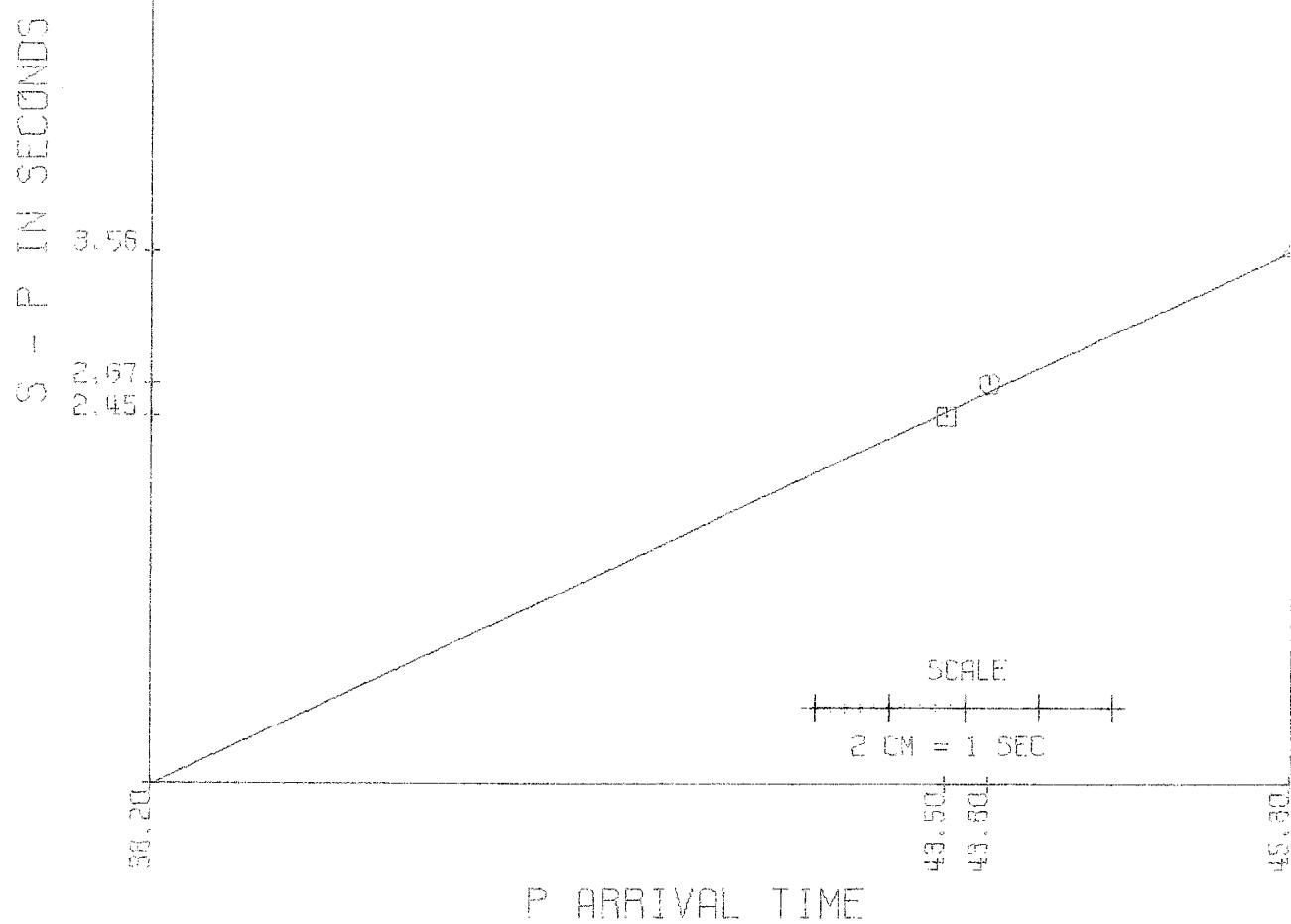


| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 6/01/1970 | 53.60 | 2.87 | SNM | P |
| ORIGIN | 22.17.46.15 | 54.00 | 2.67 | SRM | Q |
| SLOPE | 0.35847 | 56.10 | 3.56 | SBB | A |
| VP | 4.548 | 0.00 | 0.00 | SCC | + |



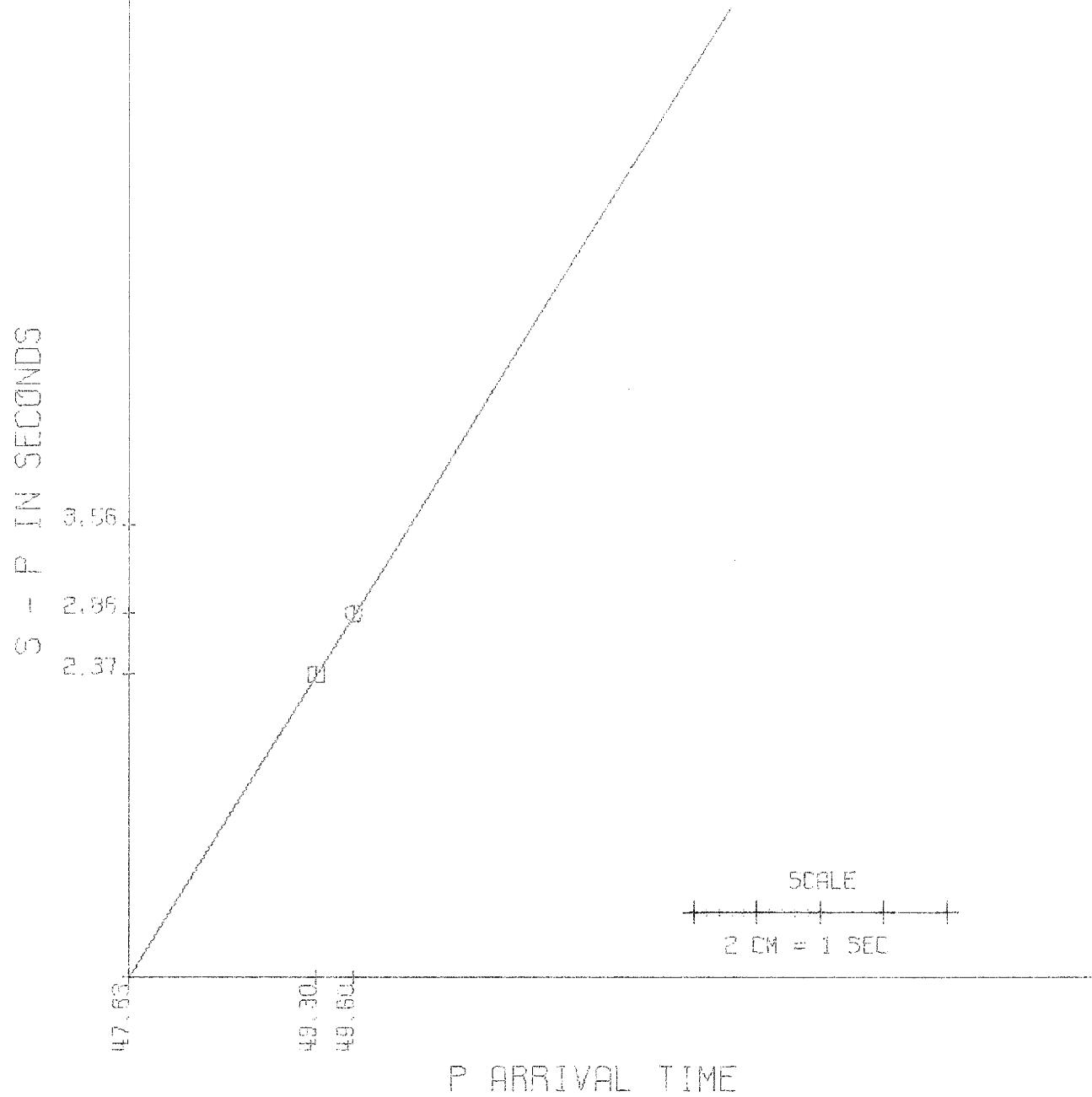
DATE 6/02 /1970
ORIGIN 00.22.38.20
SLCPE 0.46693
VP 4.919

SNM E
SRM E
SBB +
SCC +

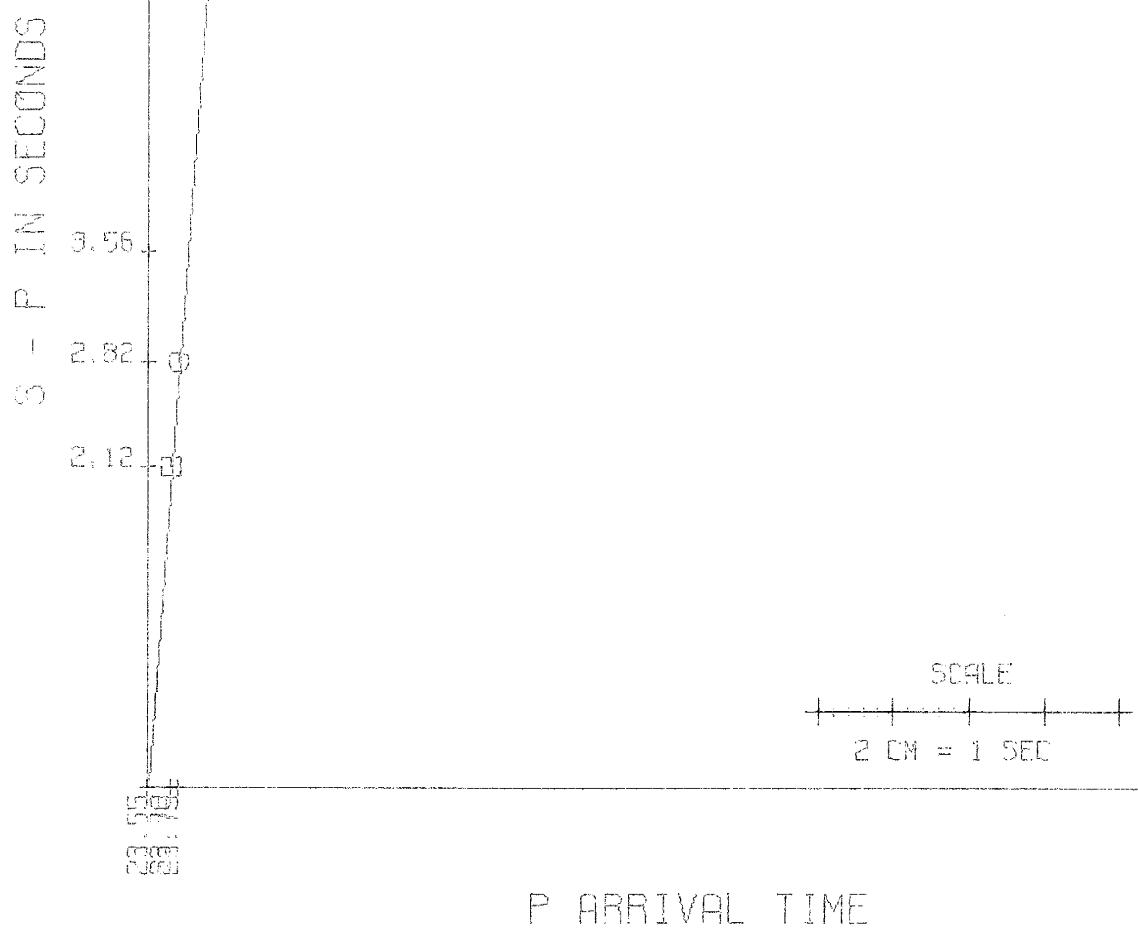


DATE 6/02 /1970
ORIGIN 12.24.47.63
SLOPE 1.61667
VP 3.782

SNM
SRM
SBB
SOC
+ A G E



| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 6/07 /1970 | 23.70 | 2.12 | SNM | ② |
| ORIGIN | 09.14.23.55 | 23.75 | 2.82 | SRM | ③ |
| SLOPE | 13.90000 | 45.80 | 3.56 | SAB | ④ |
| VP | 49.895 | 6.00 | 6.00 | SCC | + |



| | | | | | |
|--------|---------------|-------|------|-----|---|
| DATE | 6/14/1970 | 26.20 | 2.47 | SNM | B |
| ORIGIN | 04.23. -10.78 | 25.60 | 3.04 | SRM | D |
| SLOPE | 0.07394 | 32.60 | 3.19 | SBB | A |
| VP | 3.596 | 0.00 | 0.00 | SCC | + |

G = P IN SECONDS

3.04
2.47

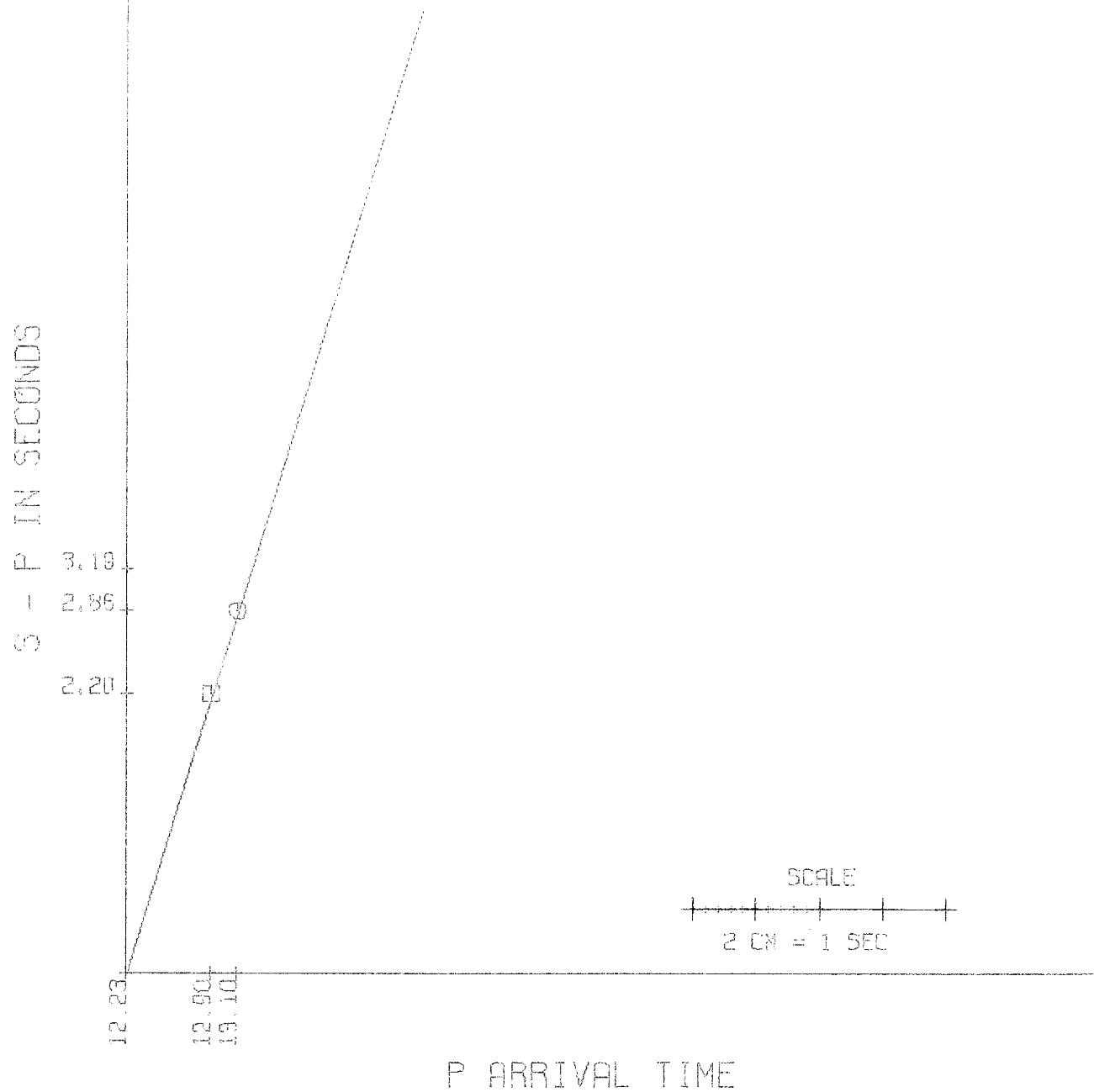
-10.78

SCALE:

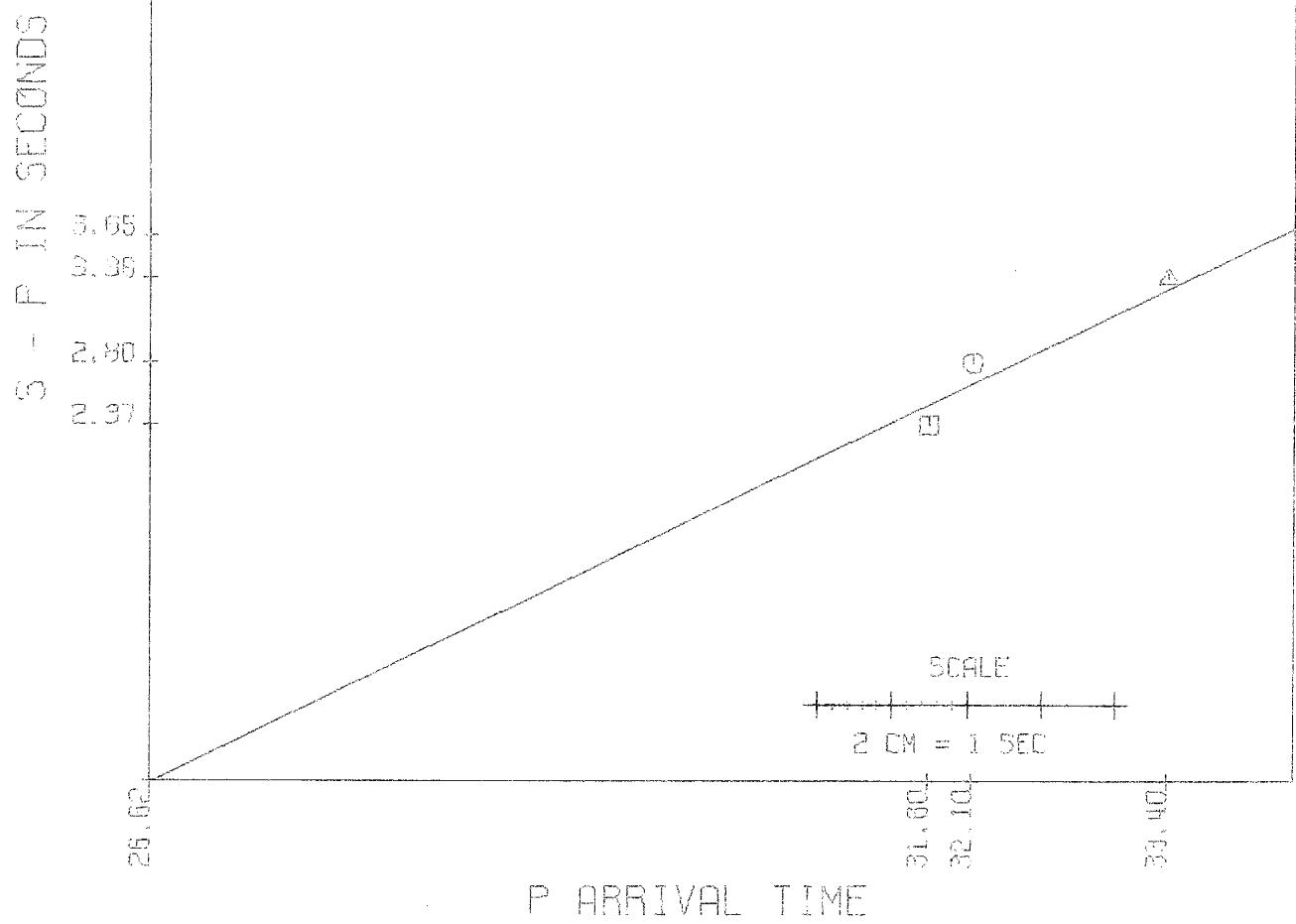
2 CM = 1 SEC

P ARRIVAL TIME

| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 6/14/1970 | 12.90 | 2.20 | SNM | □ |
| ORIGIN | 04.31.12.23 | 13.10 | 2.86 | SRM | ○ |
| SLOPE | 3.30000 | 32.60 | 3.18 | SAB | ▲ |
| VP | 14.399 | 0.00 | 0.00 | SCC | + |

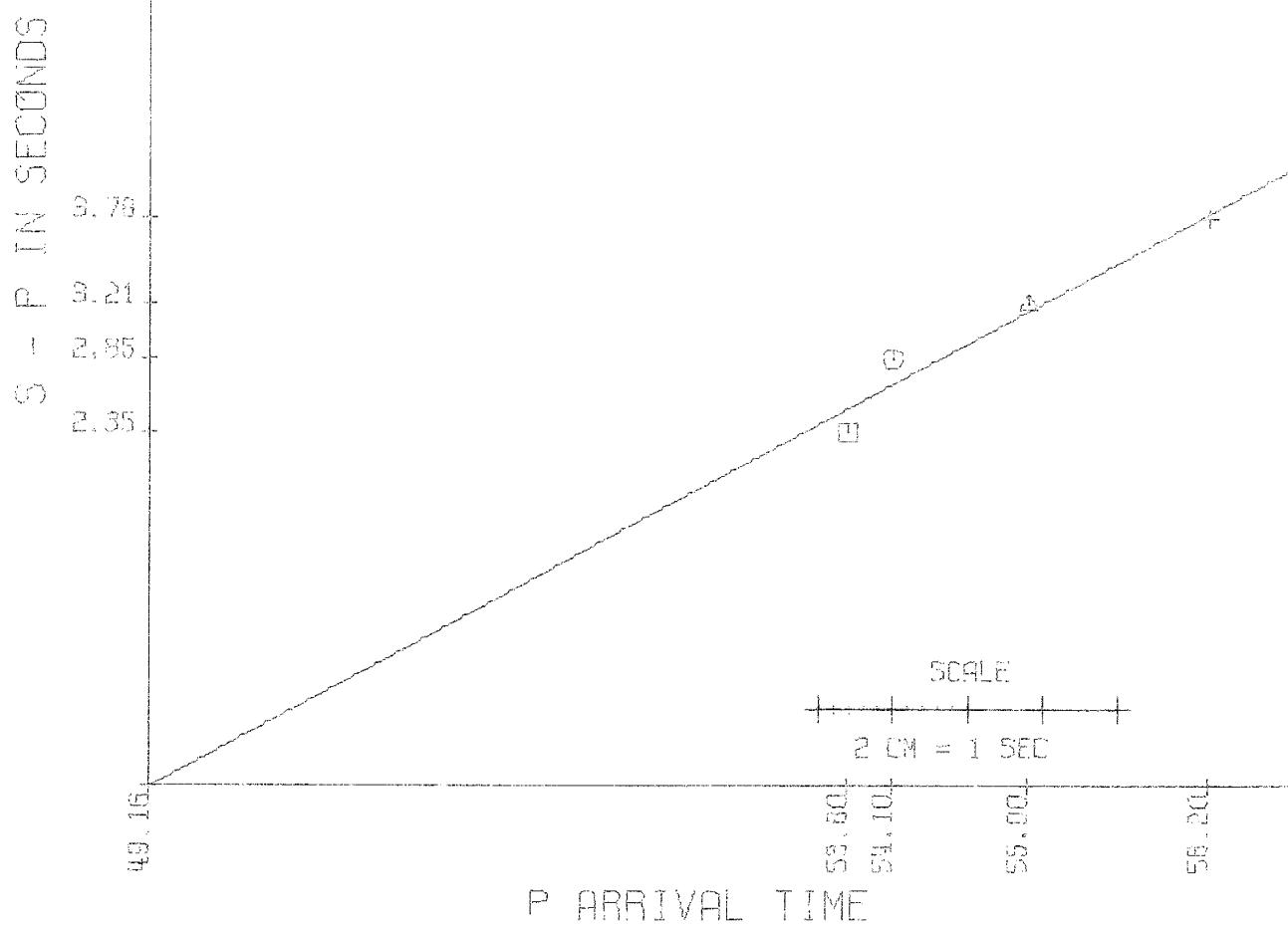


| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 6/14/1970 | 31.60 | 2.37 | SNM | E |
| ORIGIN | 04.36.26.62 | 32.10 | 2.80 | SRM | G |
| SLOPE | 0.48653 | 33.40 | 3.30 | SRR | A |
| VP | 4.977 | 34.25 | 3.65 | SOC | + |



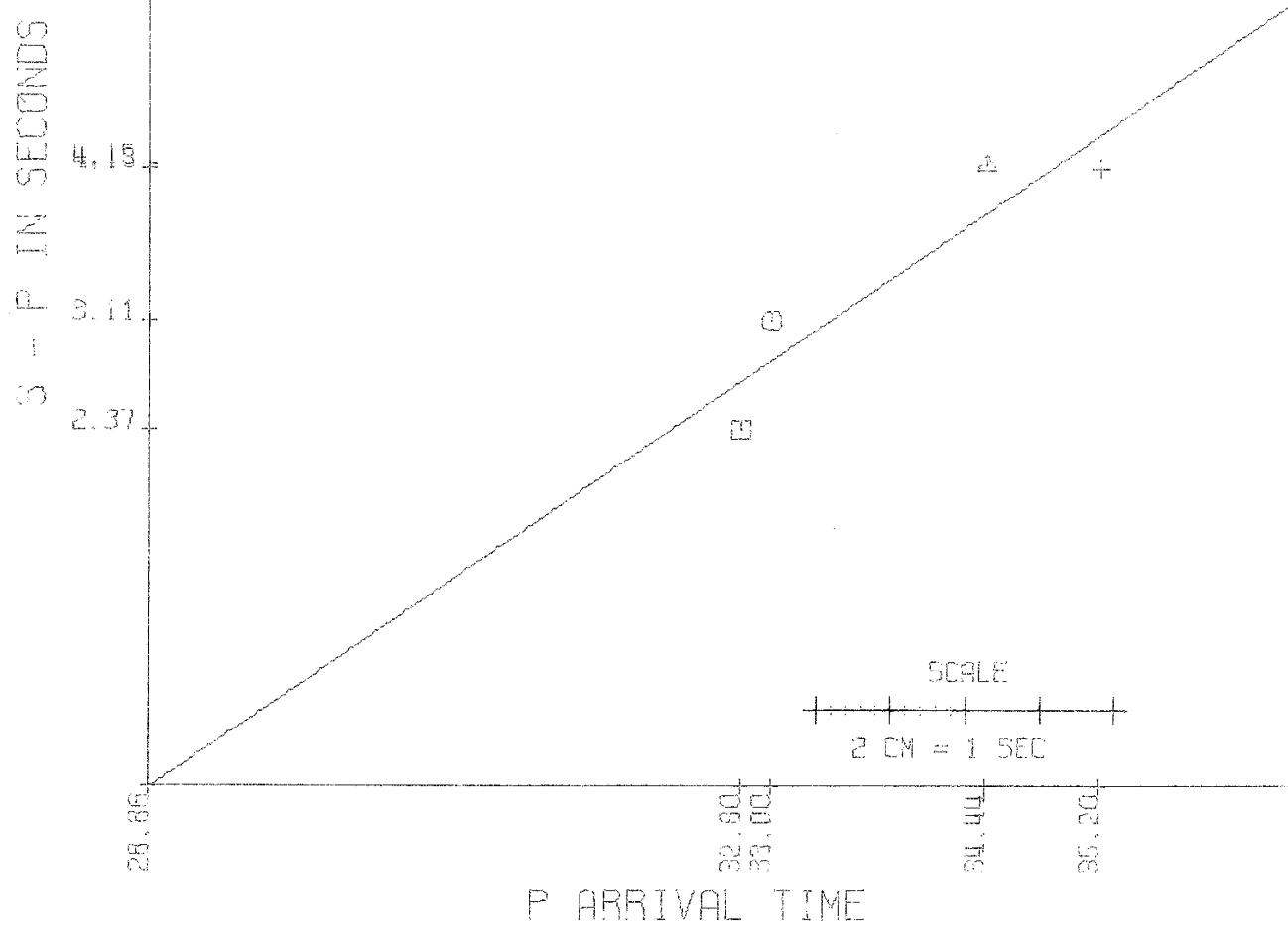
DATE 6/14/1870
ORIGIN 04.36.49.16
SLOPE 0.54301
VP 5.167

SNM E 13
SRM G 4
SBB A +
SCC

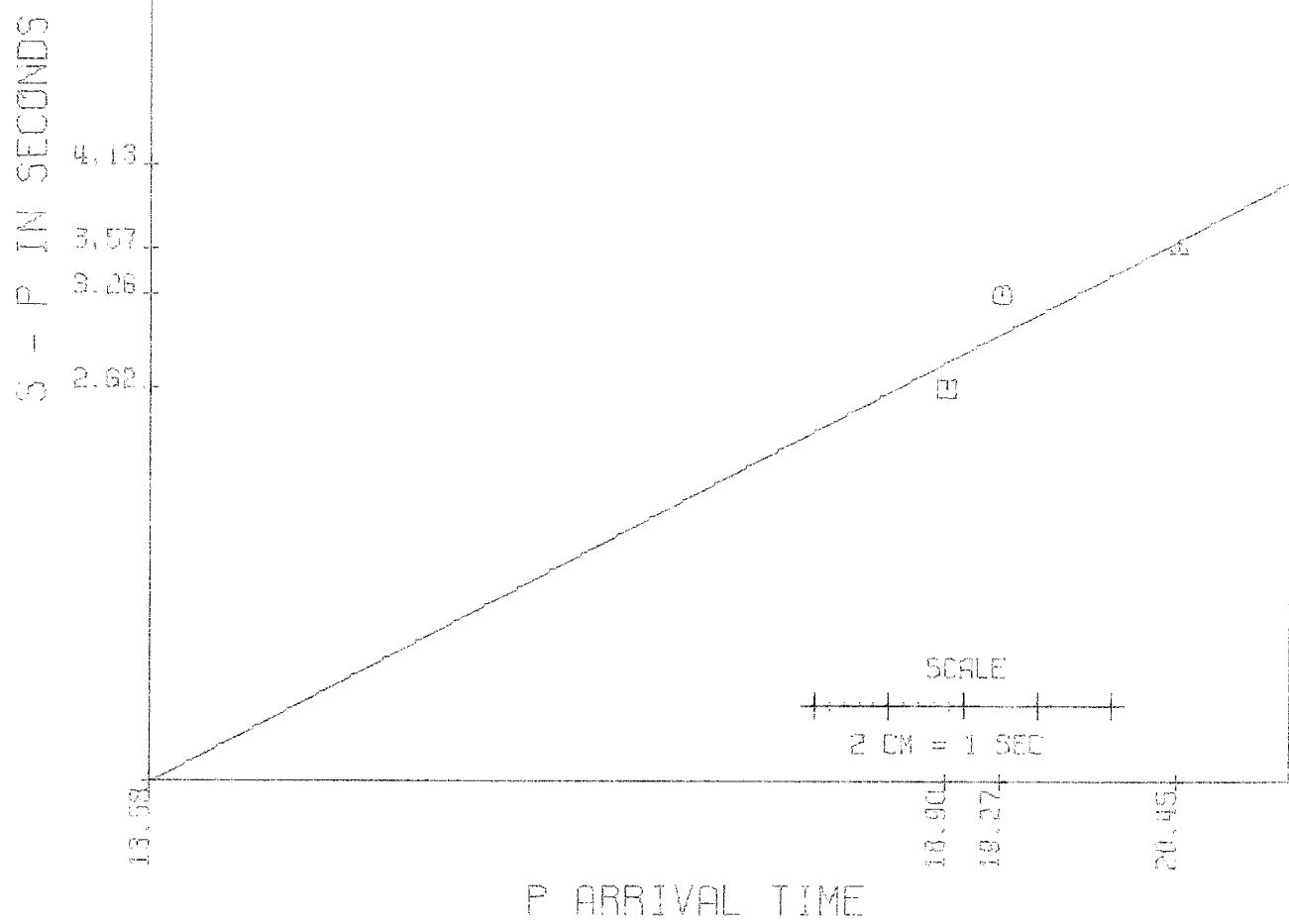


DATE 6/14/1970
ORIGIN 07.04.28.86
SLOPE 0.68810
VP 5.653

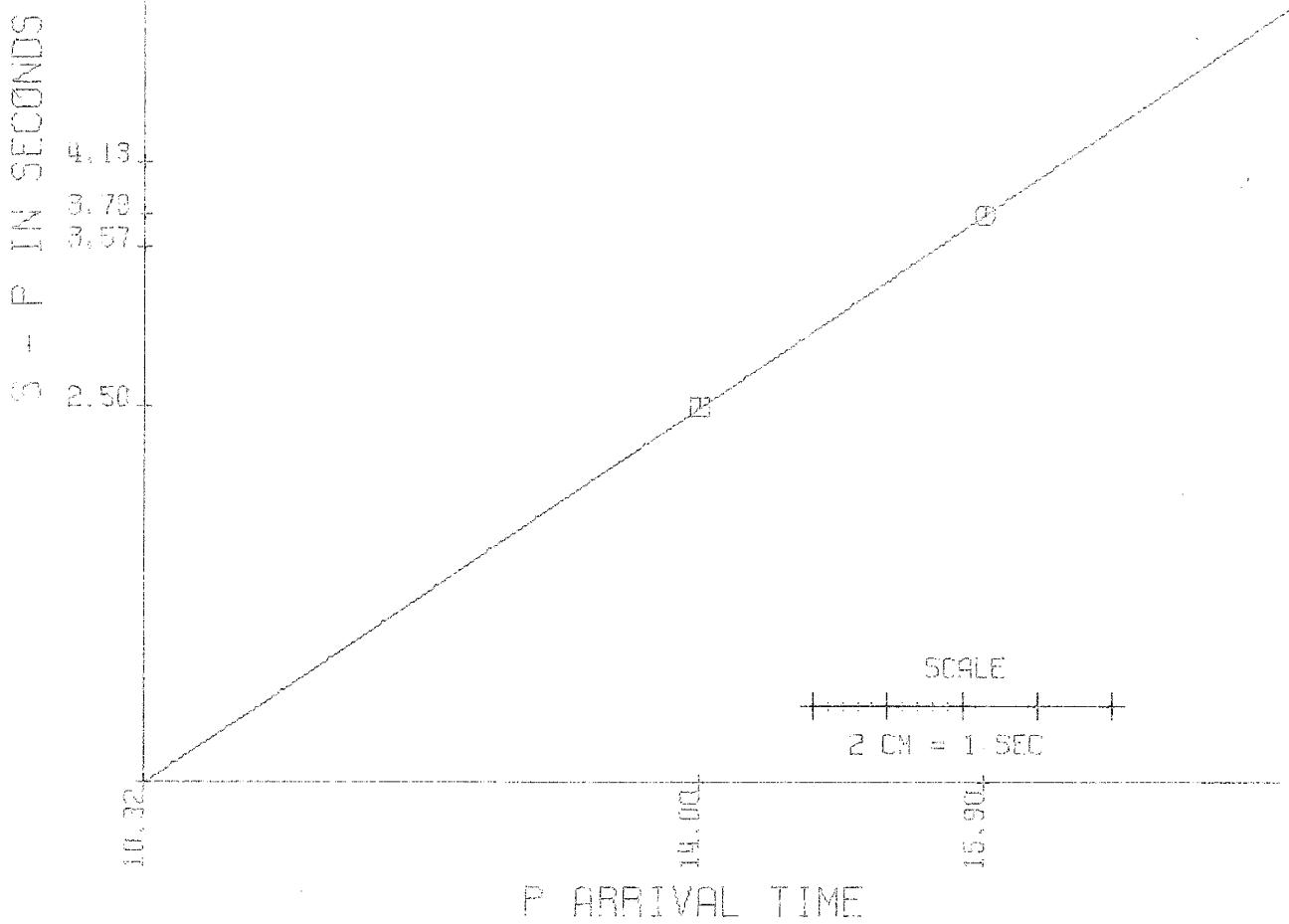
SNM 62
SRM 62
S68 62
S6C 62



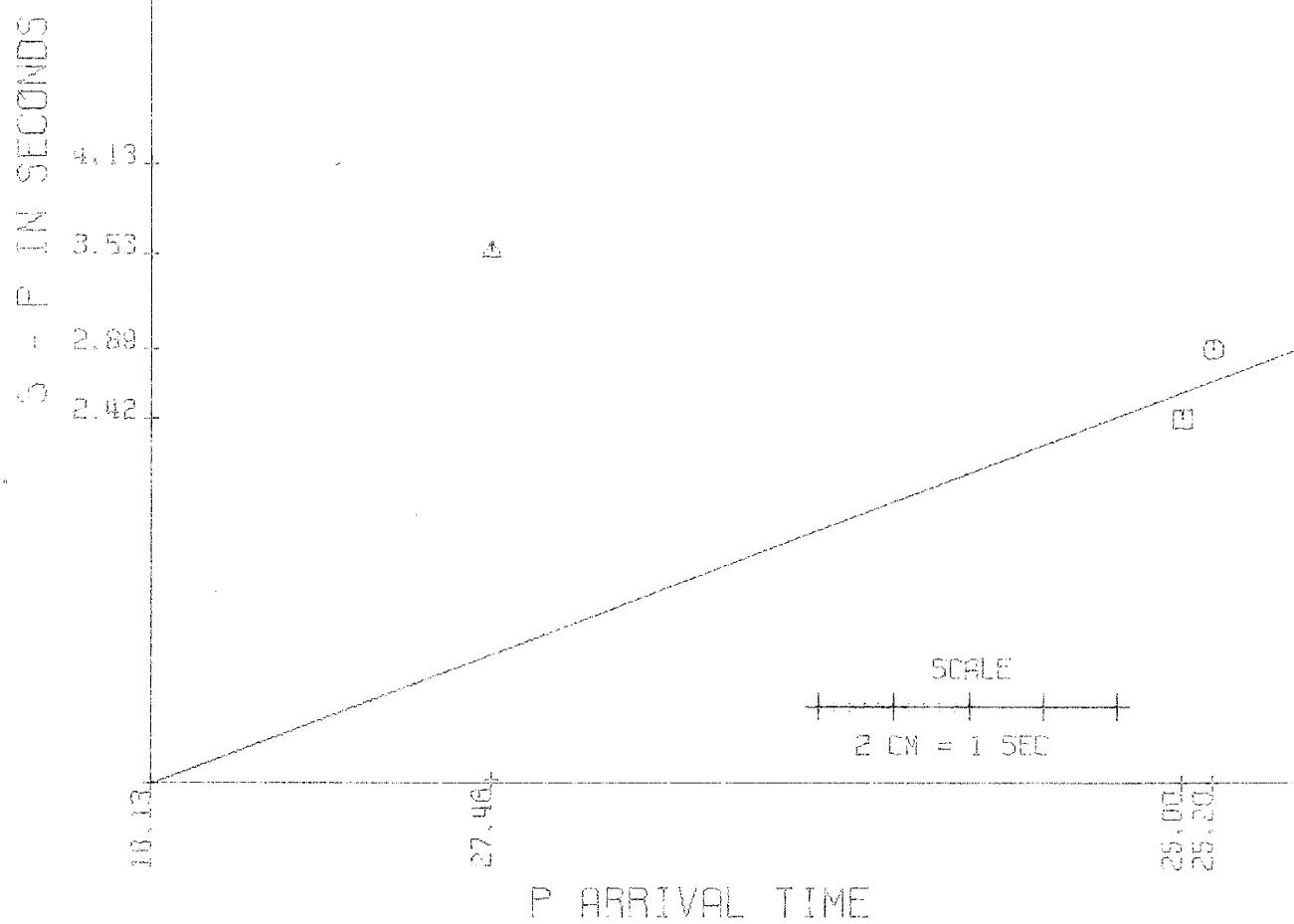
| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 6/14/1970 | 18.90 | 2.62 | SMM | □ |
| ORIGIN | 09.20.13.58 | 18.27 | 3.26 | SMR | ○ |
| SLOPE | 0.52880 | 20.45 | 3.57 | SAB | ▲ |
| VP | 5.113 | 35.20 | 4.13 | SCC | + |



| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 6/16/1970 | 14.00 | 2.50 | SNM | B |
| ORIGIN | 05.51.10.32 | 15.90 | 3.78 | SRM | G |
| SLOPE | 0.67895 | 20.45 | 3.57 | SAB | A |
| VP | 5.622 | 35.20 | 4.13 | SCC | + |

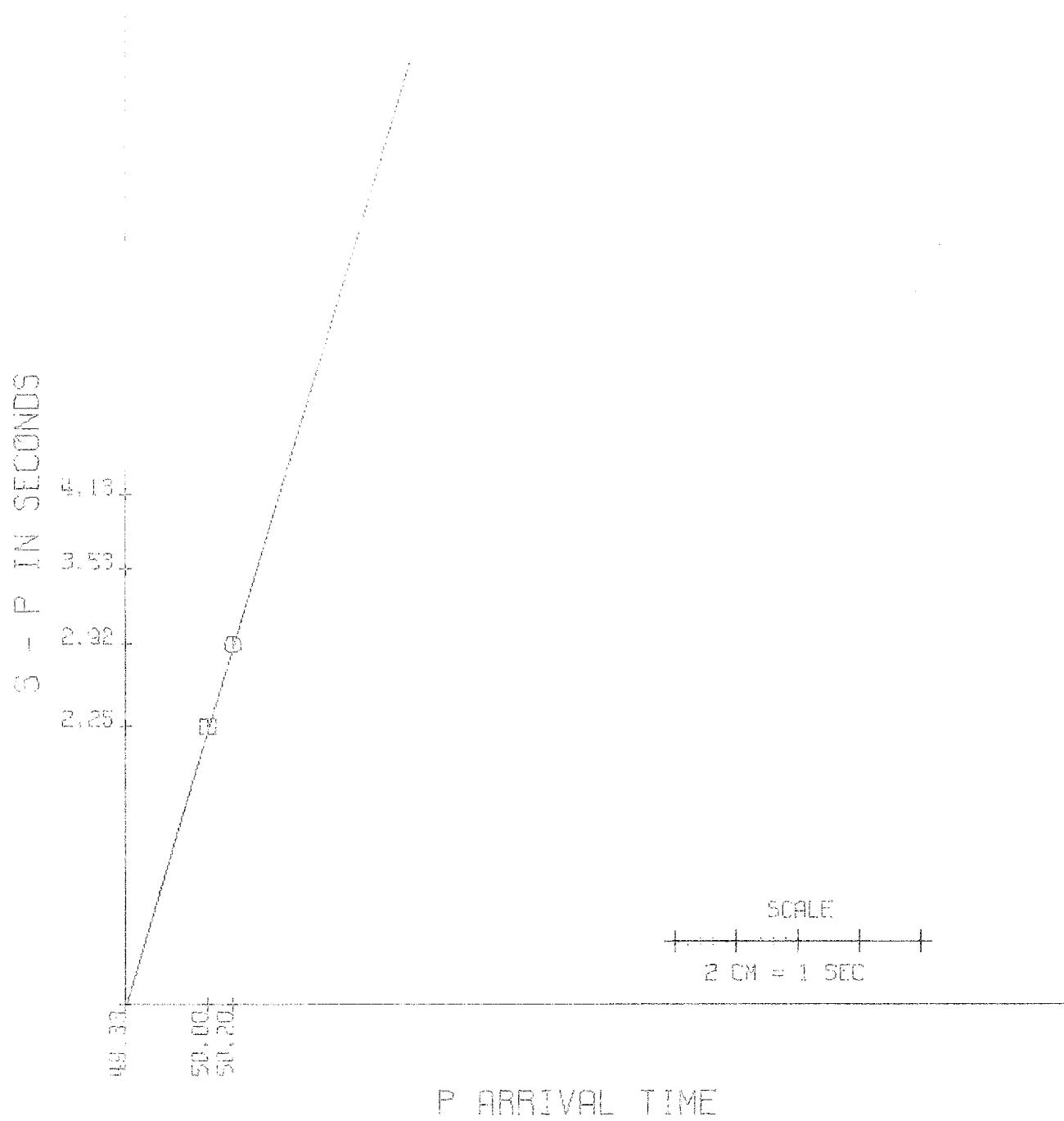


| | | | | | |
|--------|--------------|-------|------|-----|---|
| DATE | 6/16/1970 | 25.00 | 2.42 | SNM | E |
| ORIGIN | 16.50, 18.13 | 25.20 | 2.89 | SRM | O |
| SLOPE | 0.36015 | 27.46 | 3.53 | SAB | A |
| VP | 4.622 | 35.20 | 4.13 | SCC | + |

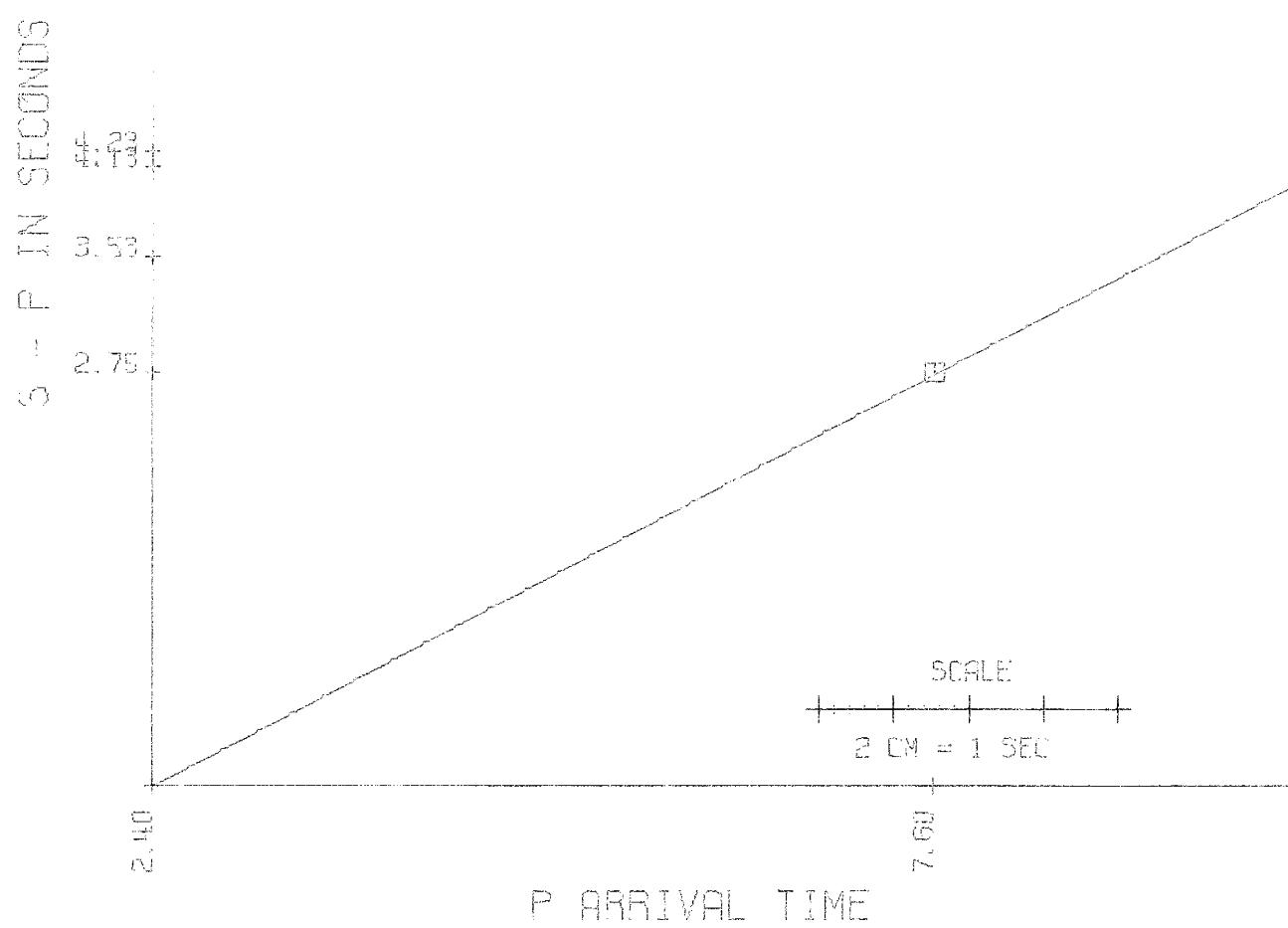


DATE 6/17/1970
ORIGIN 18.52.48.30
SLOPE 3.35000
VP 14.567

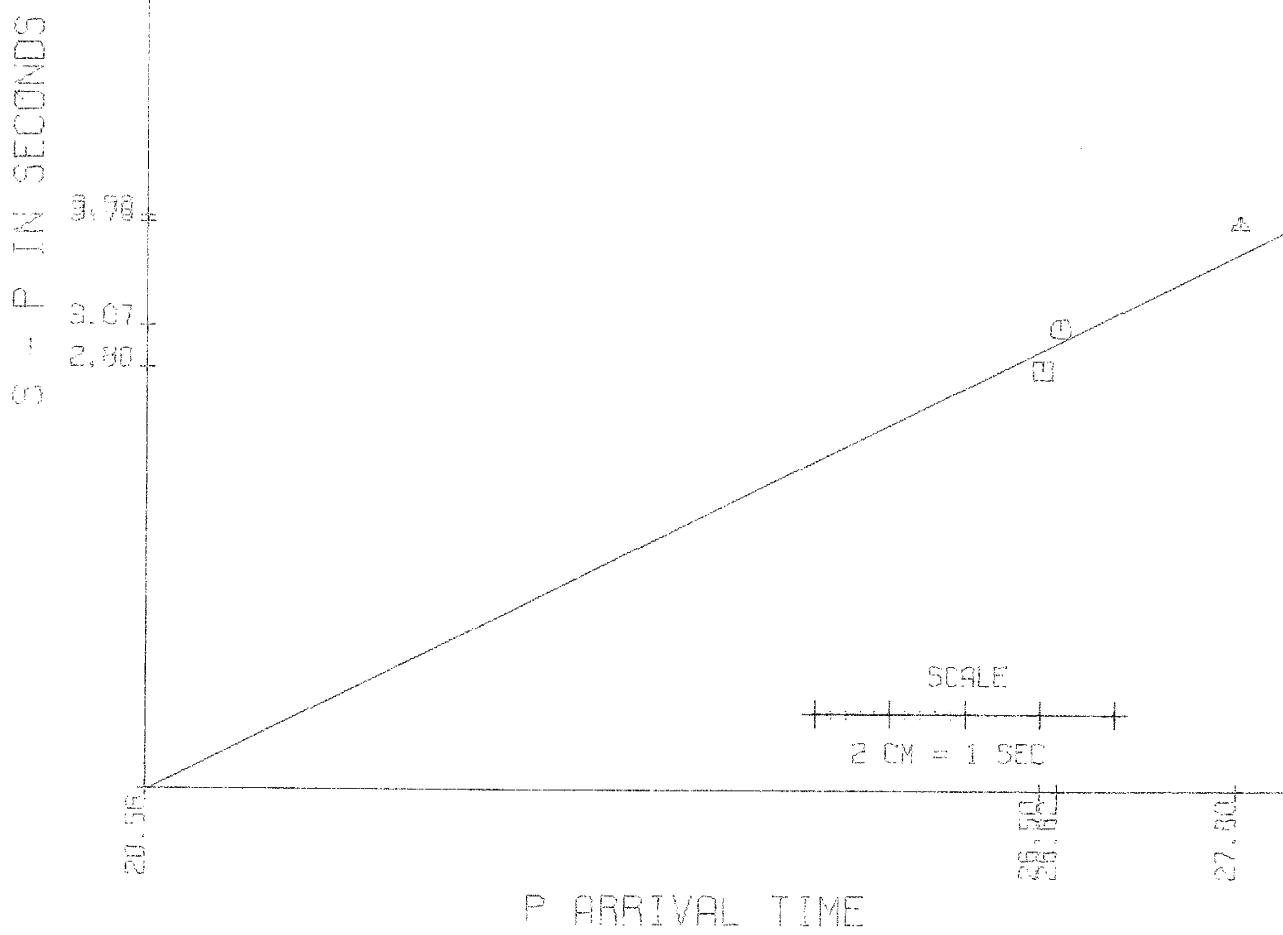
SNM E
SMR O
SBB A
SDC +

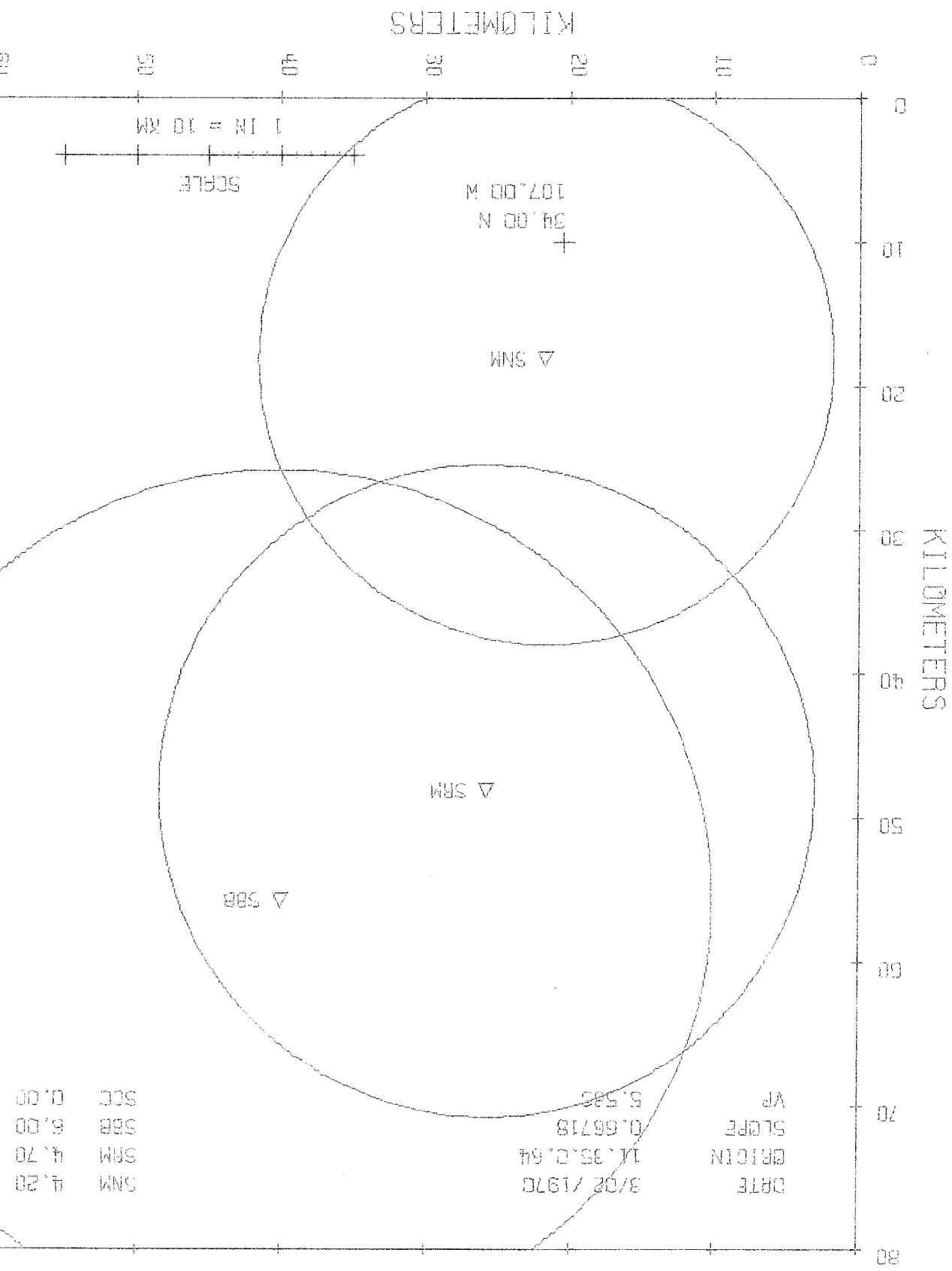


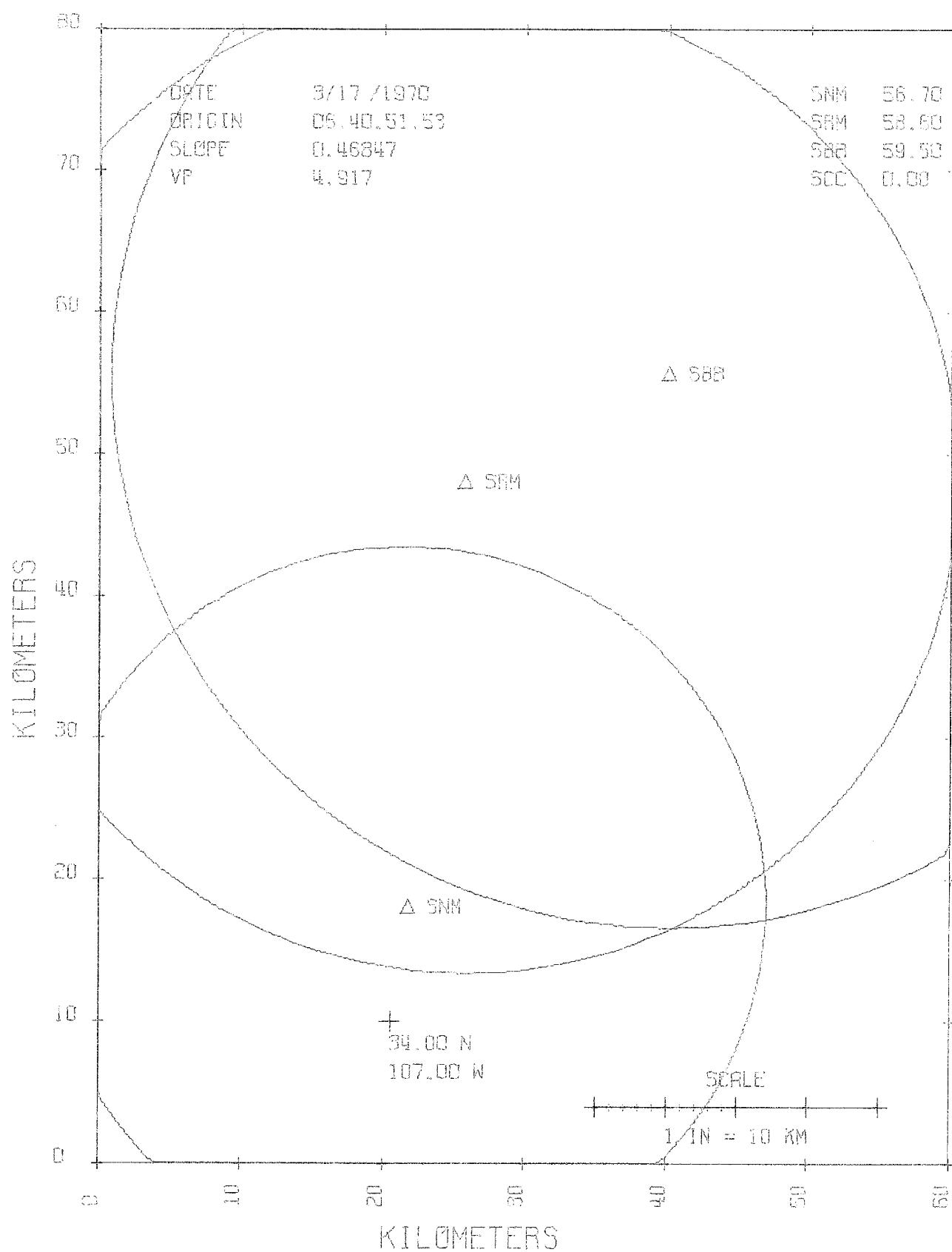
| | | | | | |
|--------|--------------|-------|------|-----|---|
| DATE | 6/23/1970 | 7.60 | 2.75 | SNM | E |
| ORIGIN | 01, 33.2, 40 | 10.40 | 4.23 | SRM | G |
| SLOPE | 0.52657 | 27.46 | 3.53 | SRR | A |
| VP | 5.119 | 35.20 | 4.13 | SOC | + |

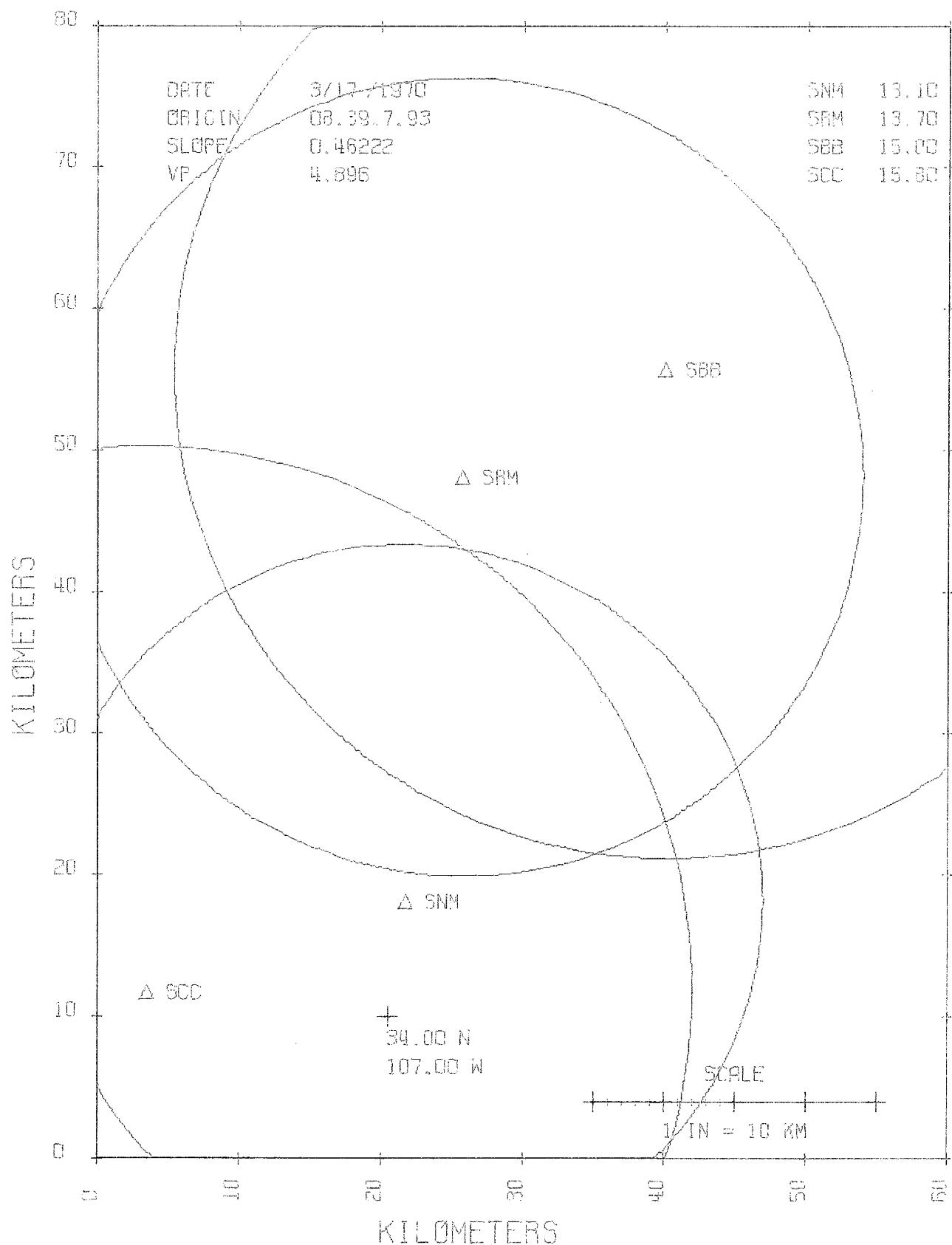


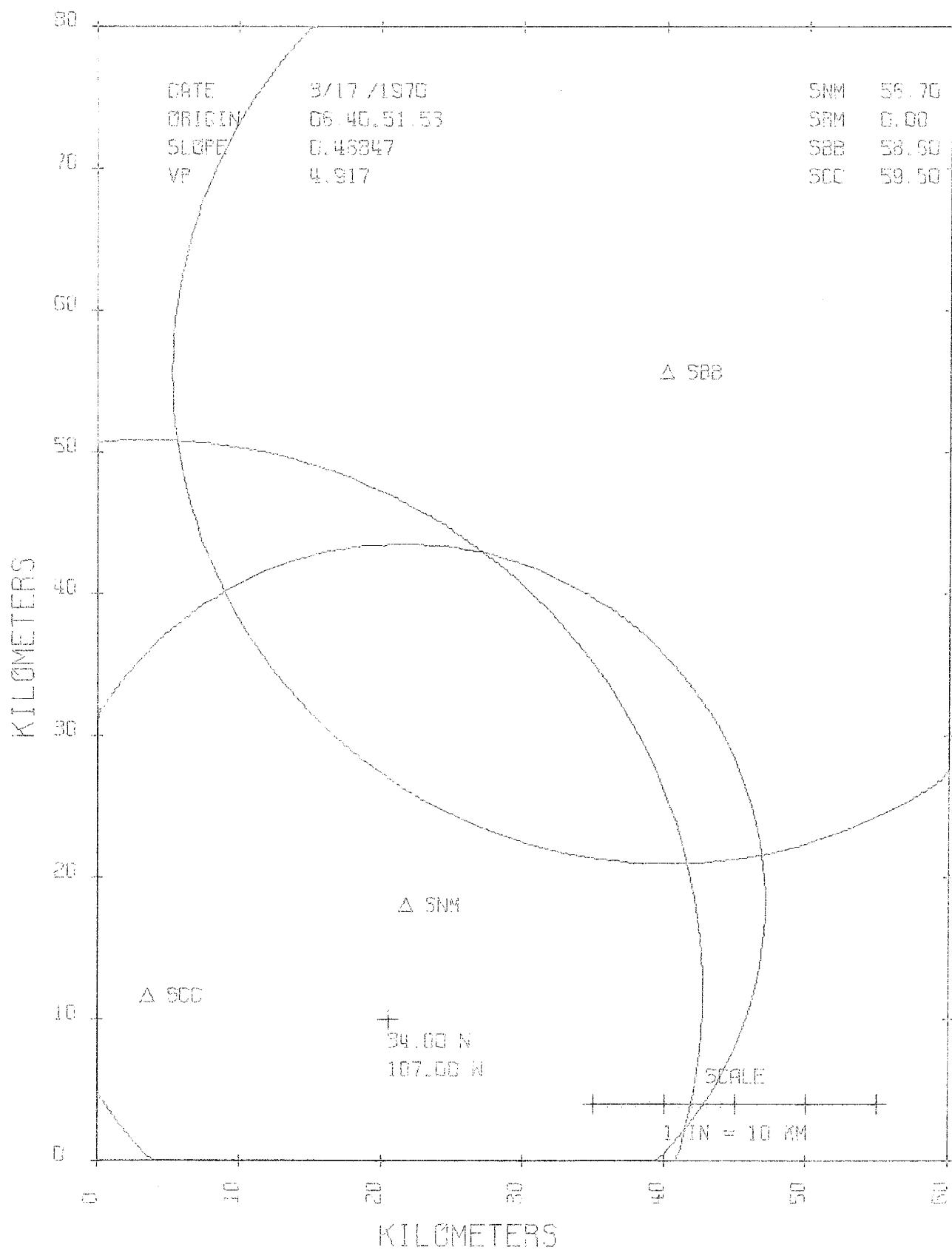
| | | | | | |
|--------|-------------|-------|------|-----|---|
| DATE | 6/30 /1970 | 26.50 | 2.80 | SNM | E |
| ORIGIN | 11.34.20.56 | 26.62 | 3.07 | SRM | S |
| SLOPE | 0.49410 | 27.60 | 3.76 | SBB | A |
| VP | 5.003 | 28.50 | 3.80 | SCC | + |

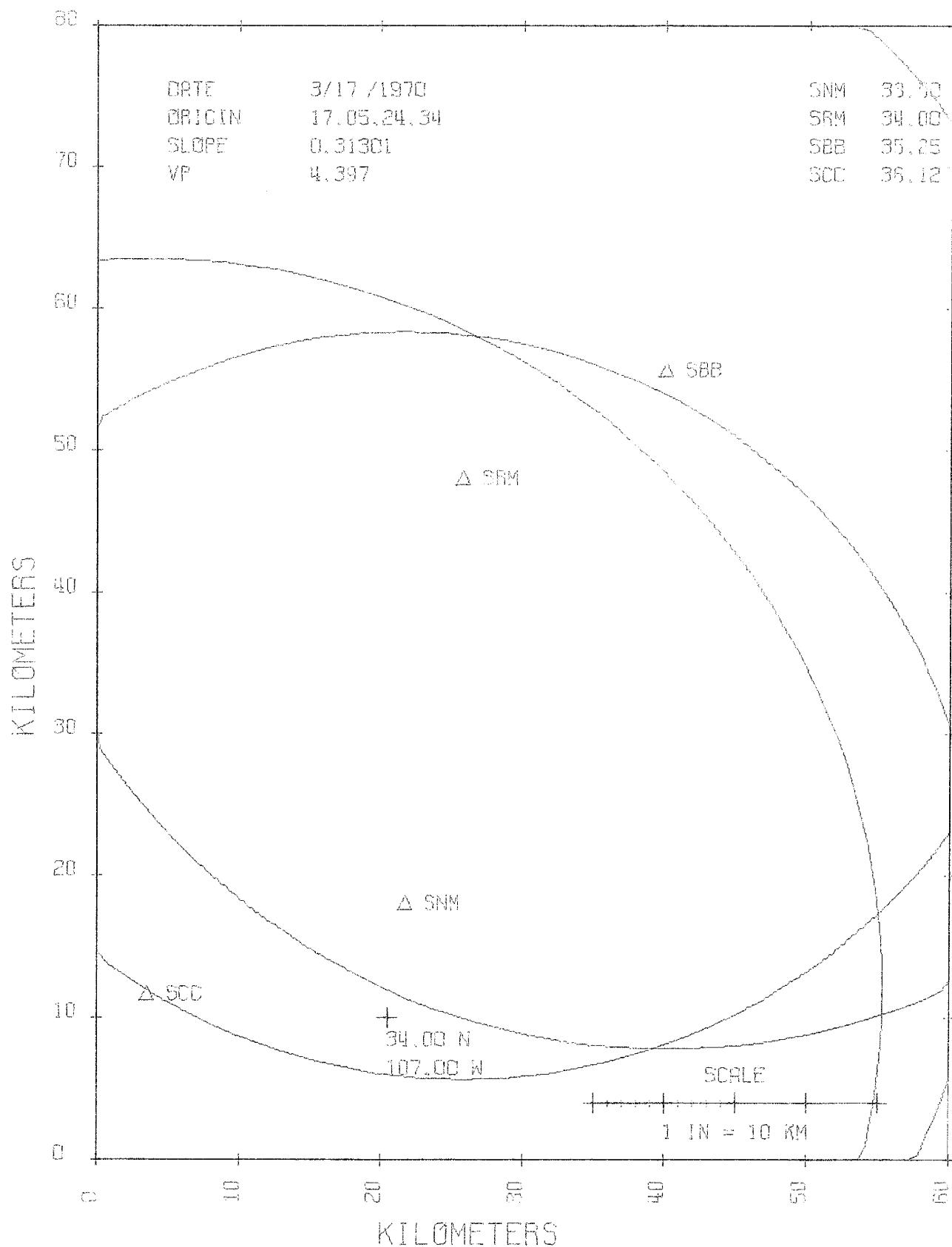


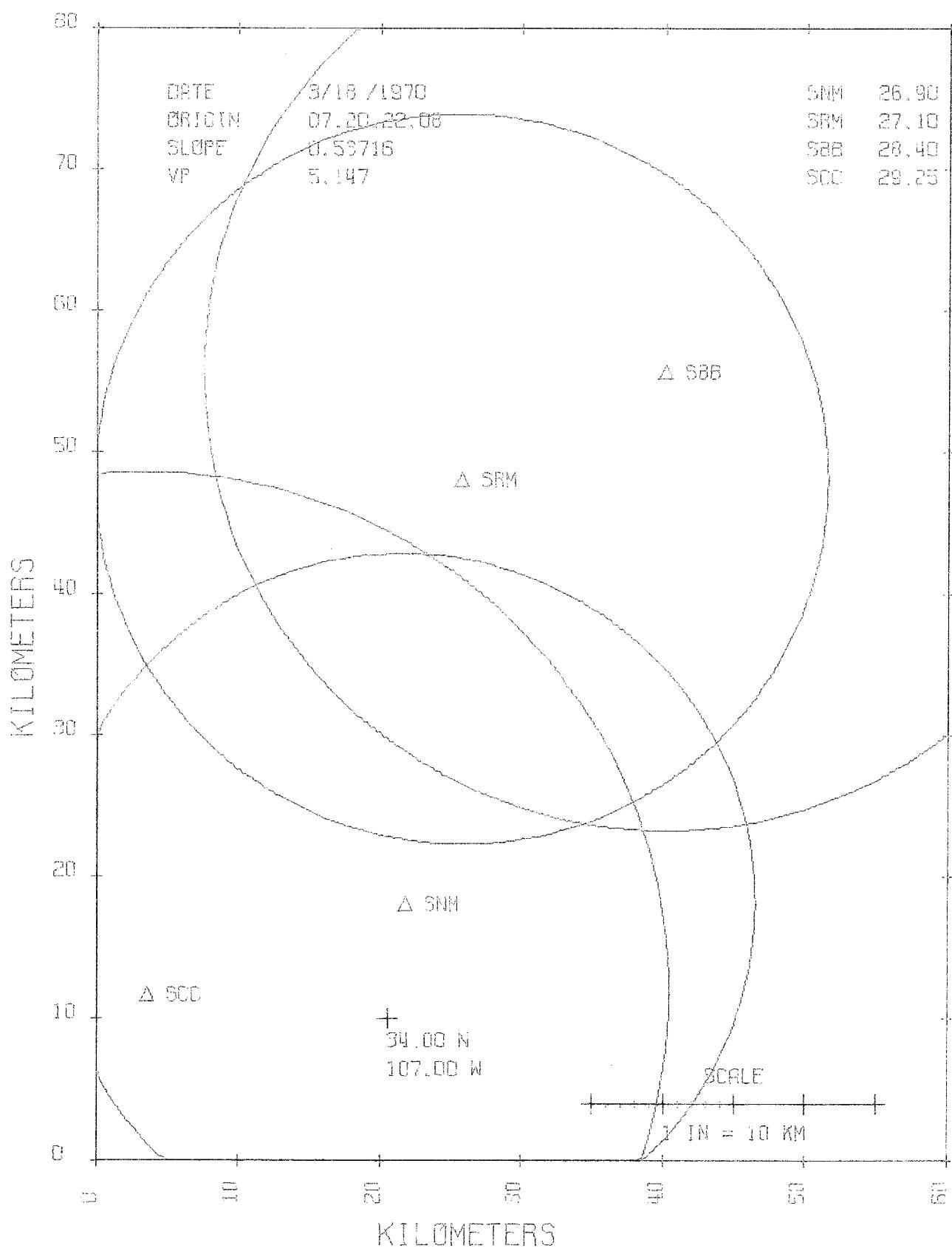


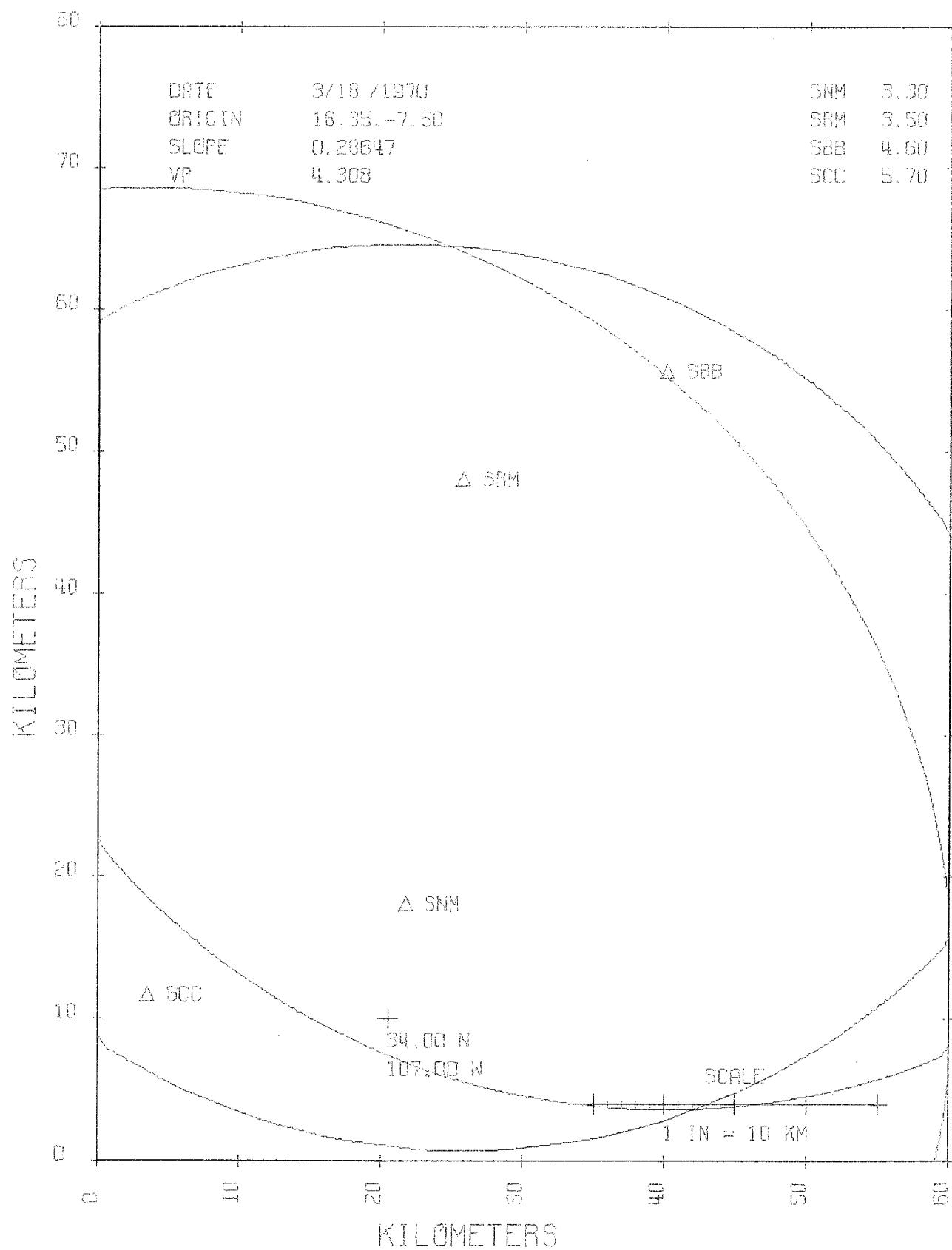


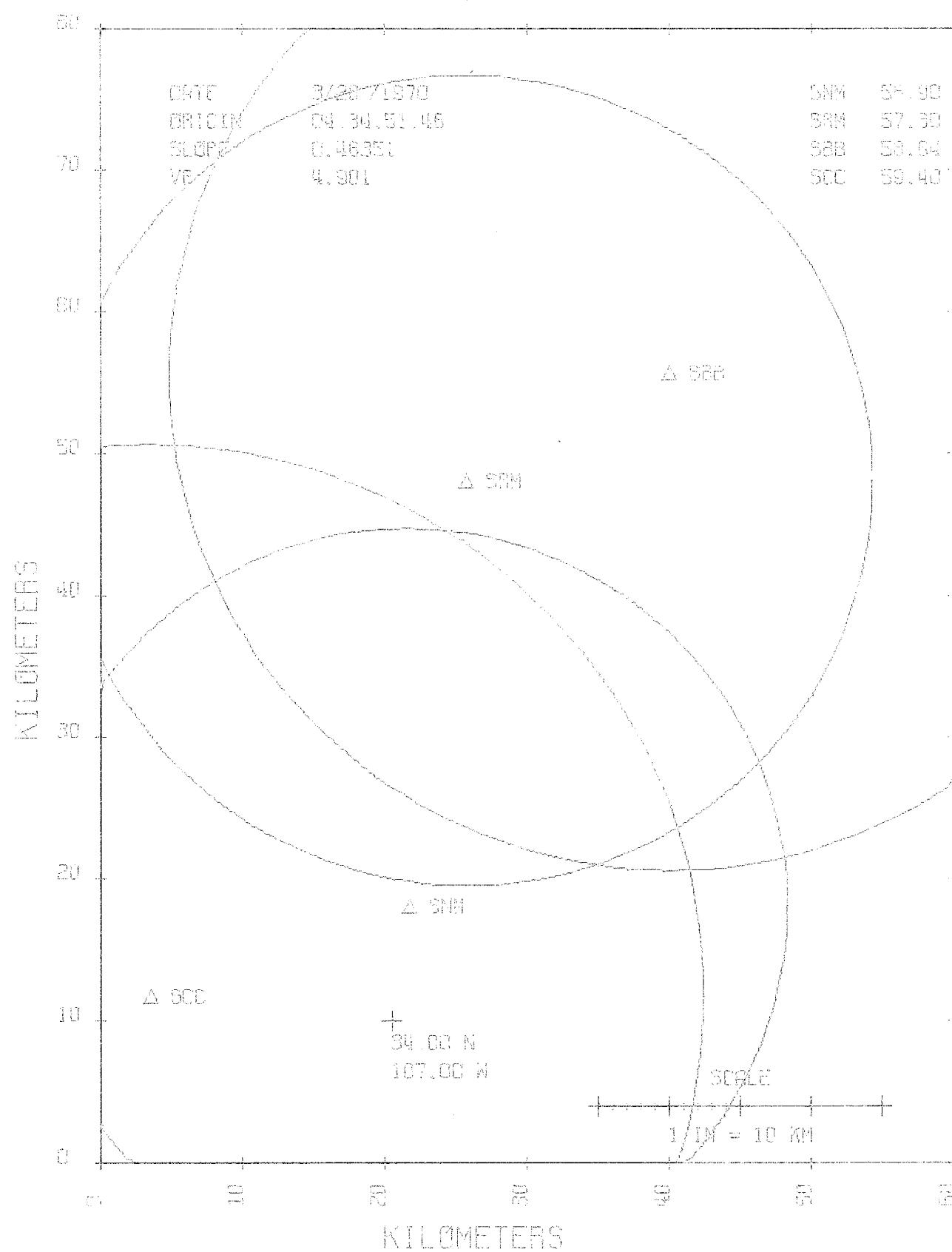


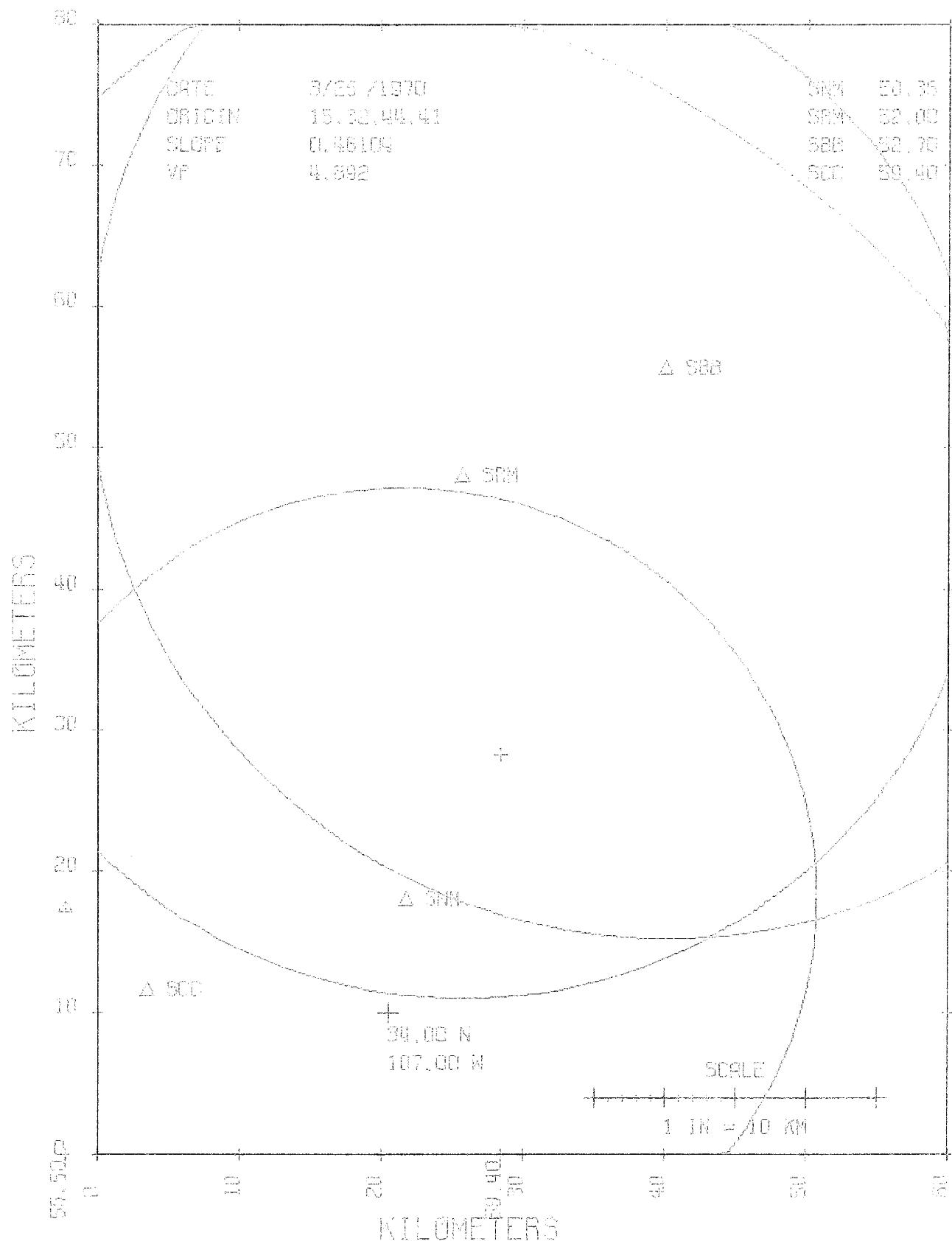


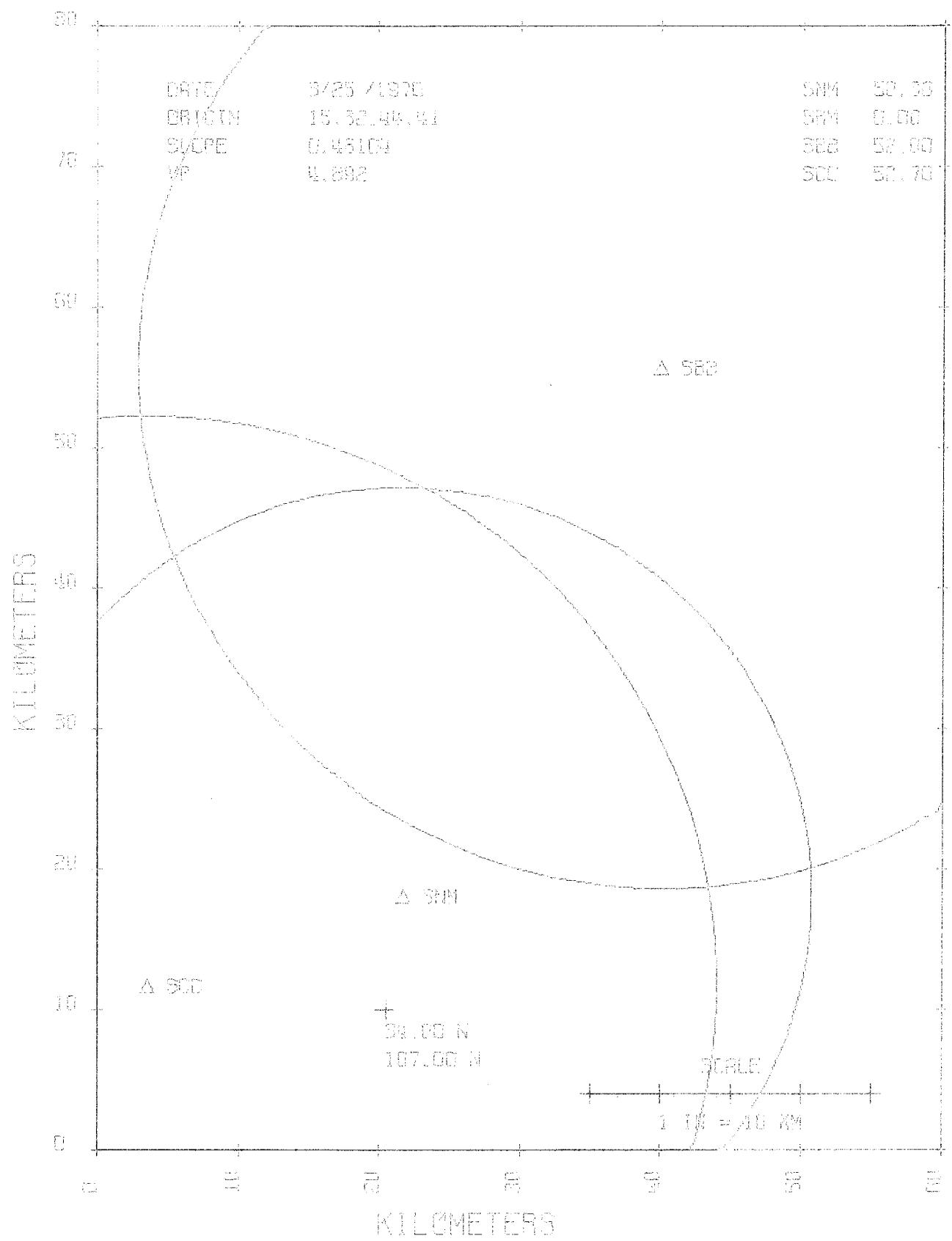


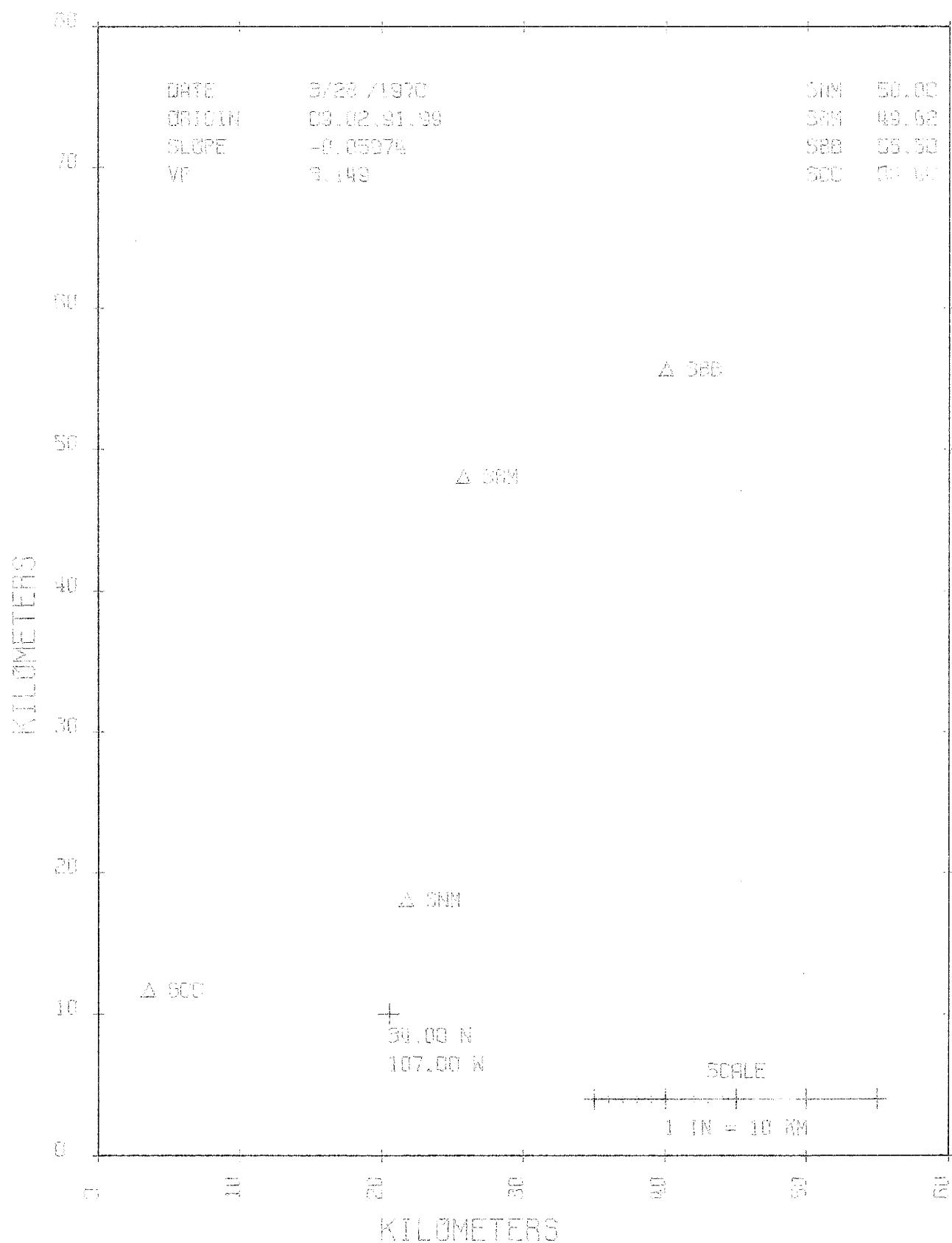


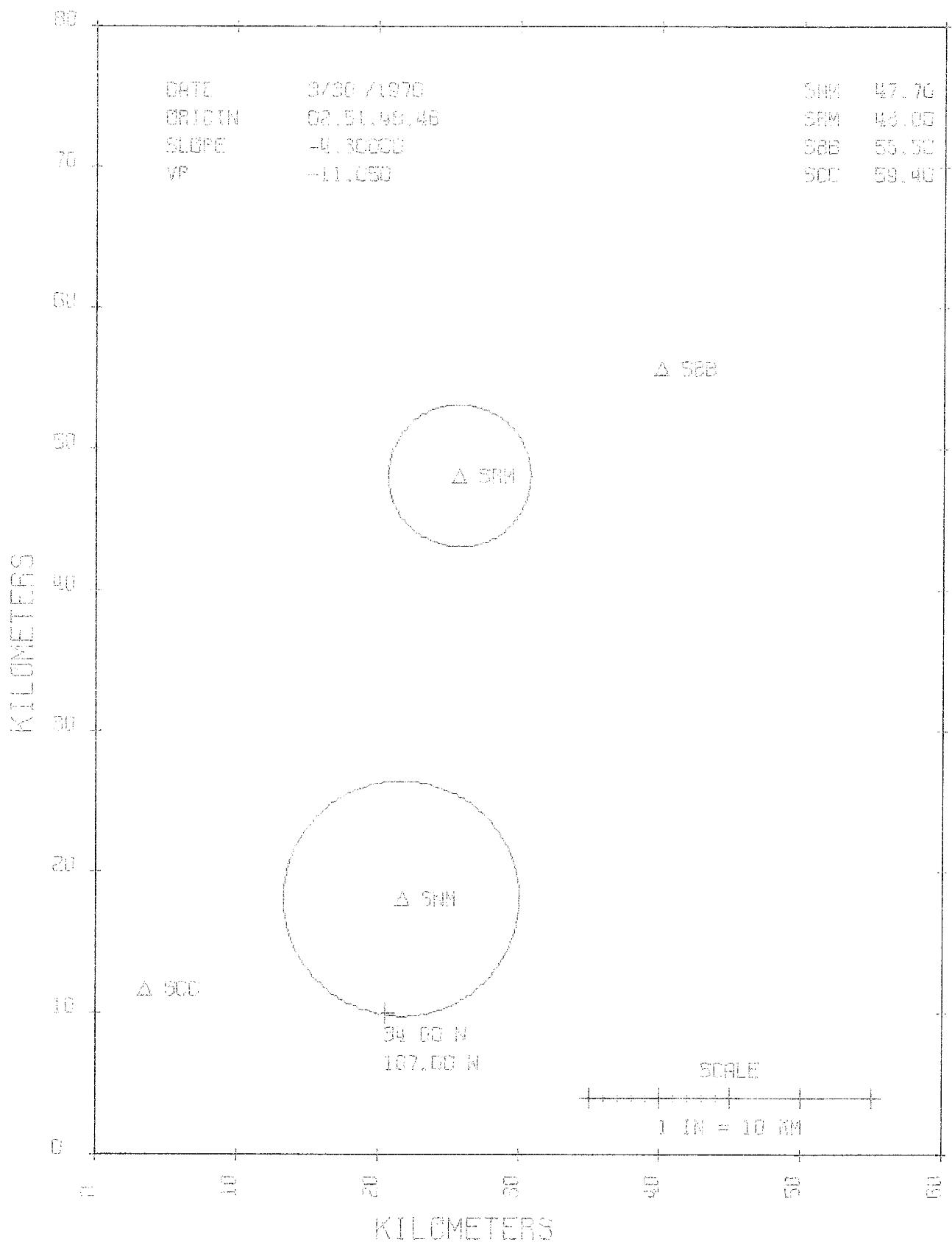


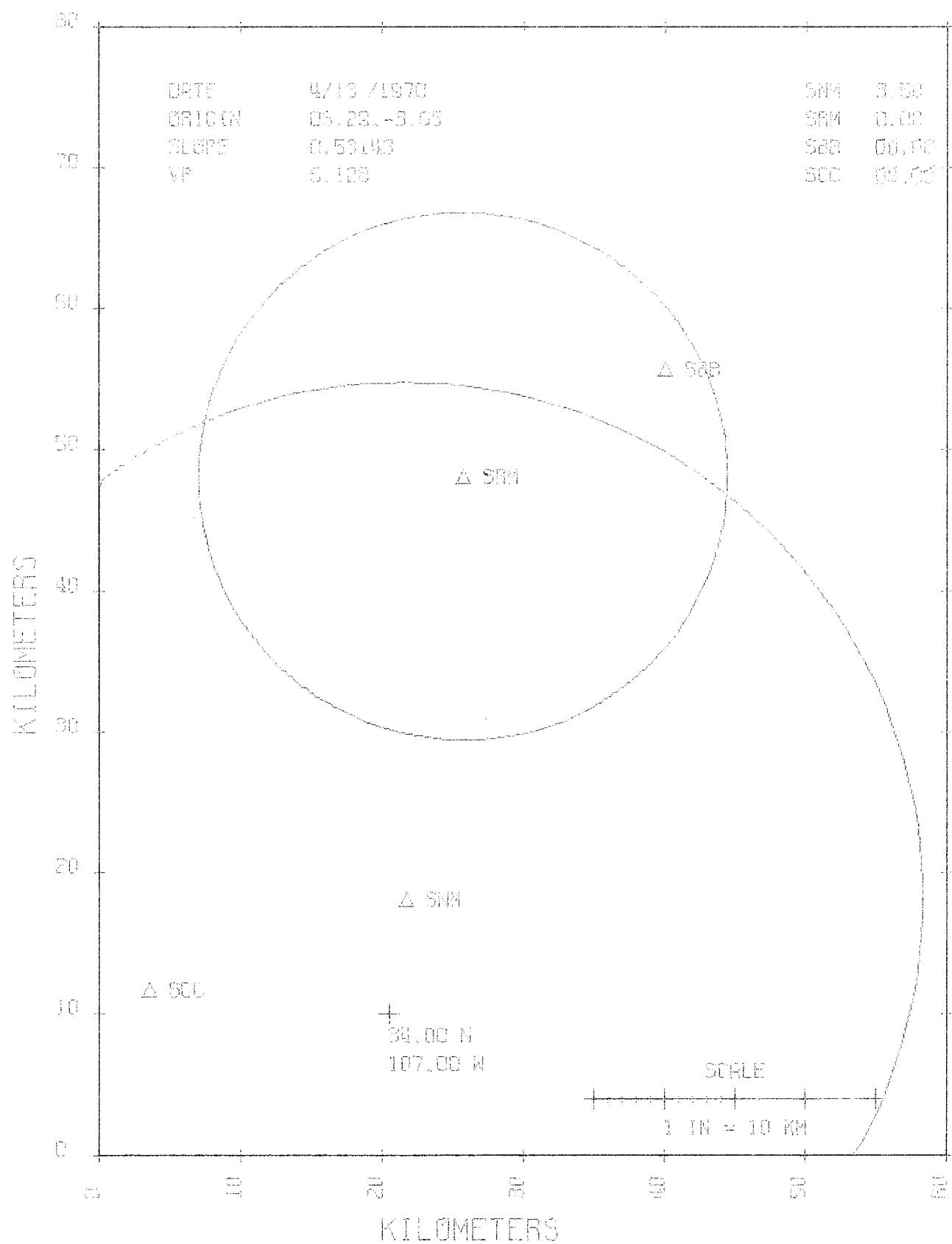


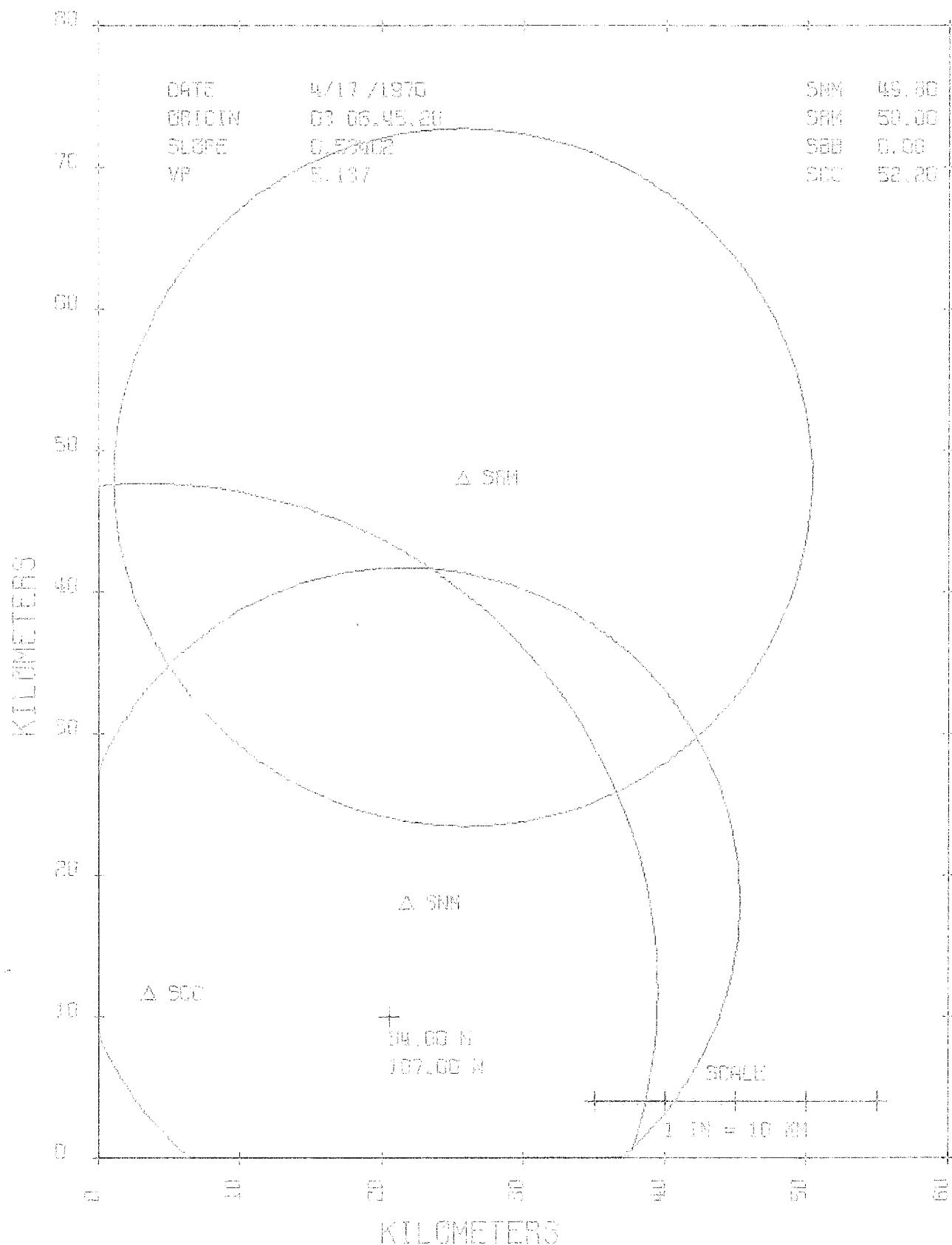


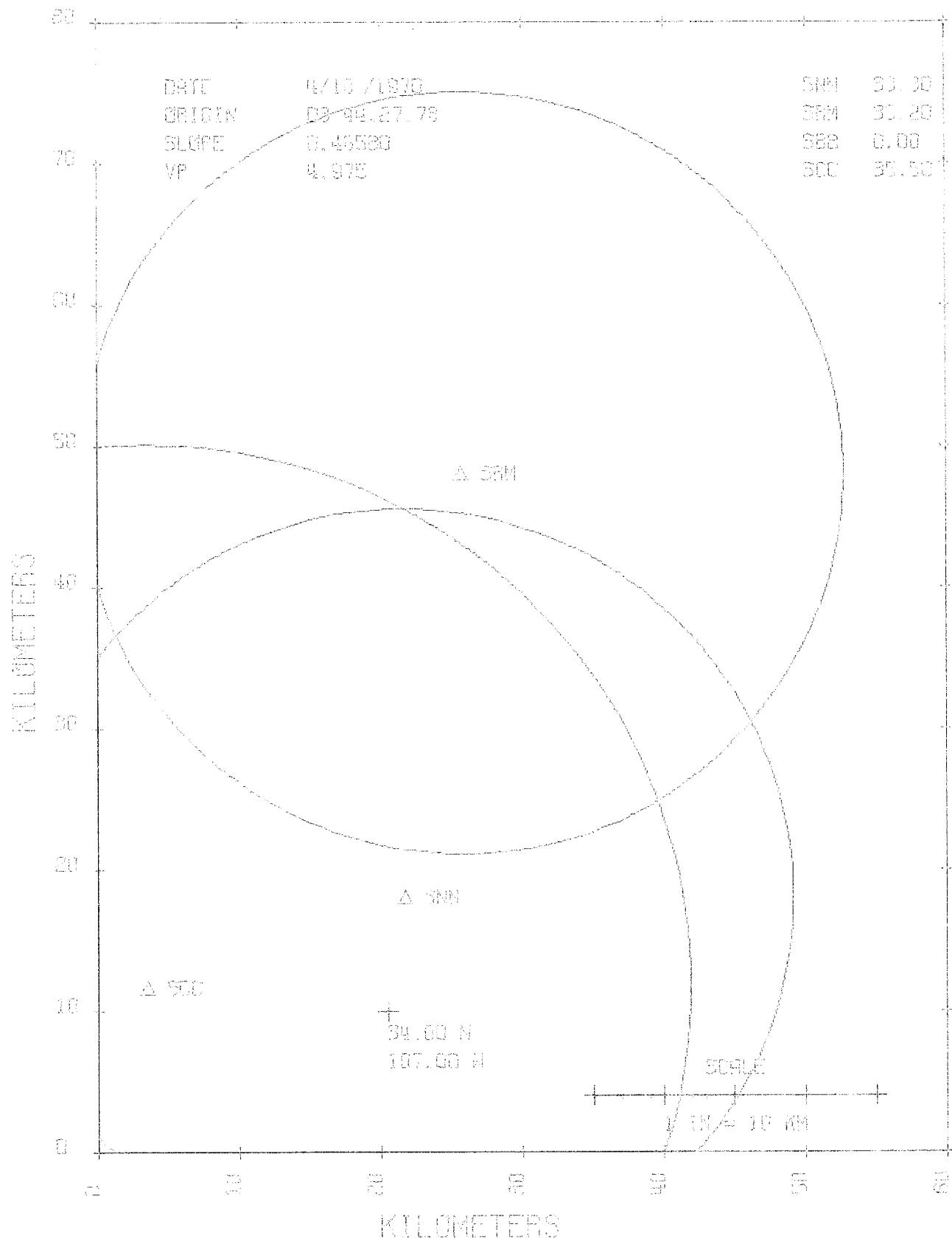


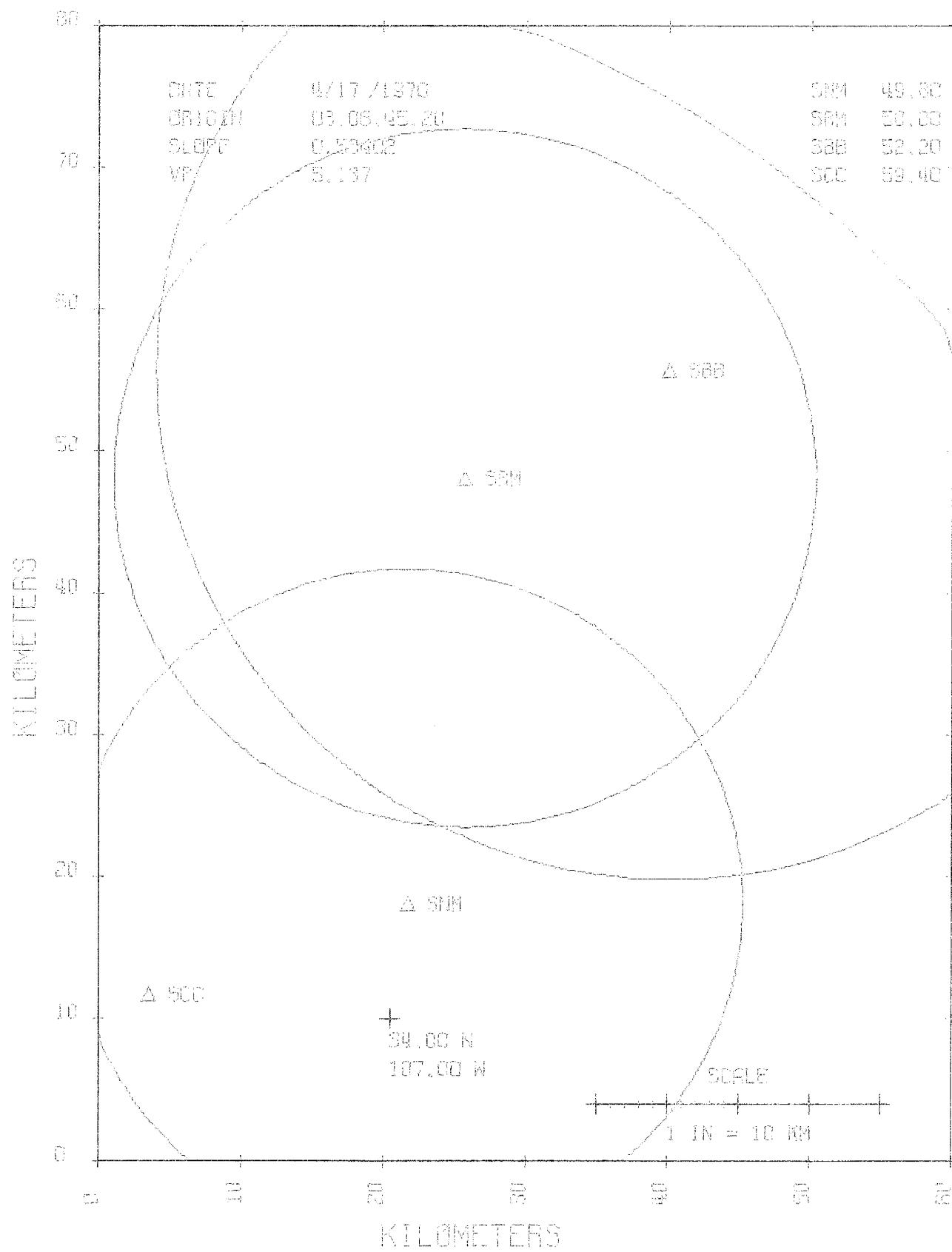


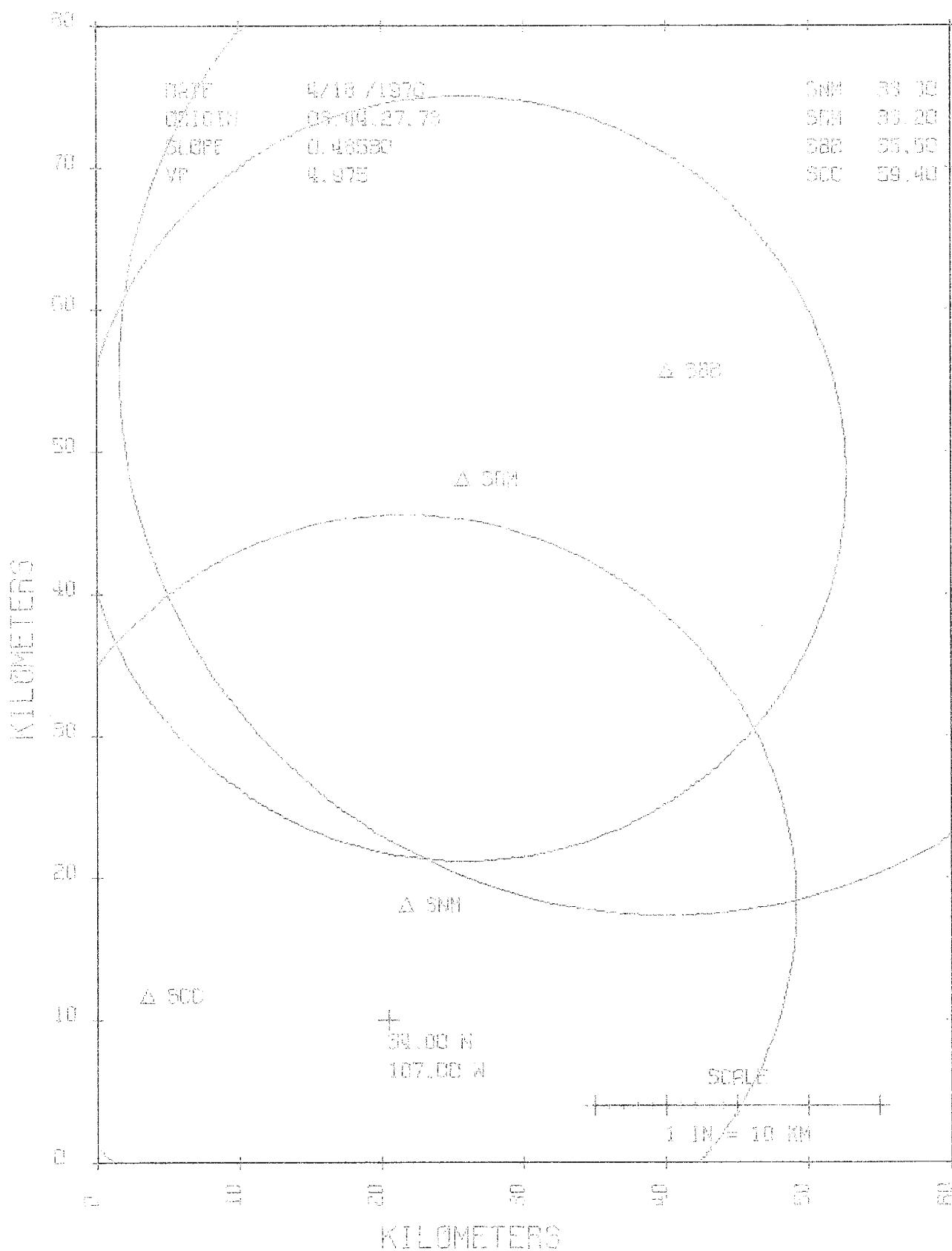


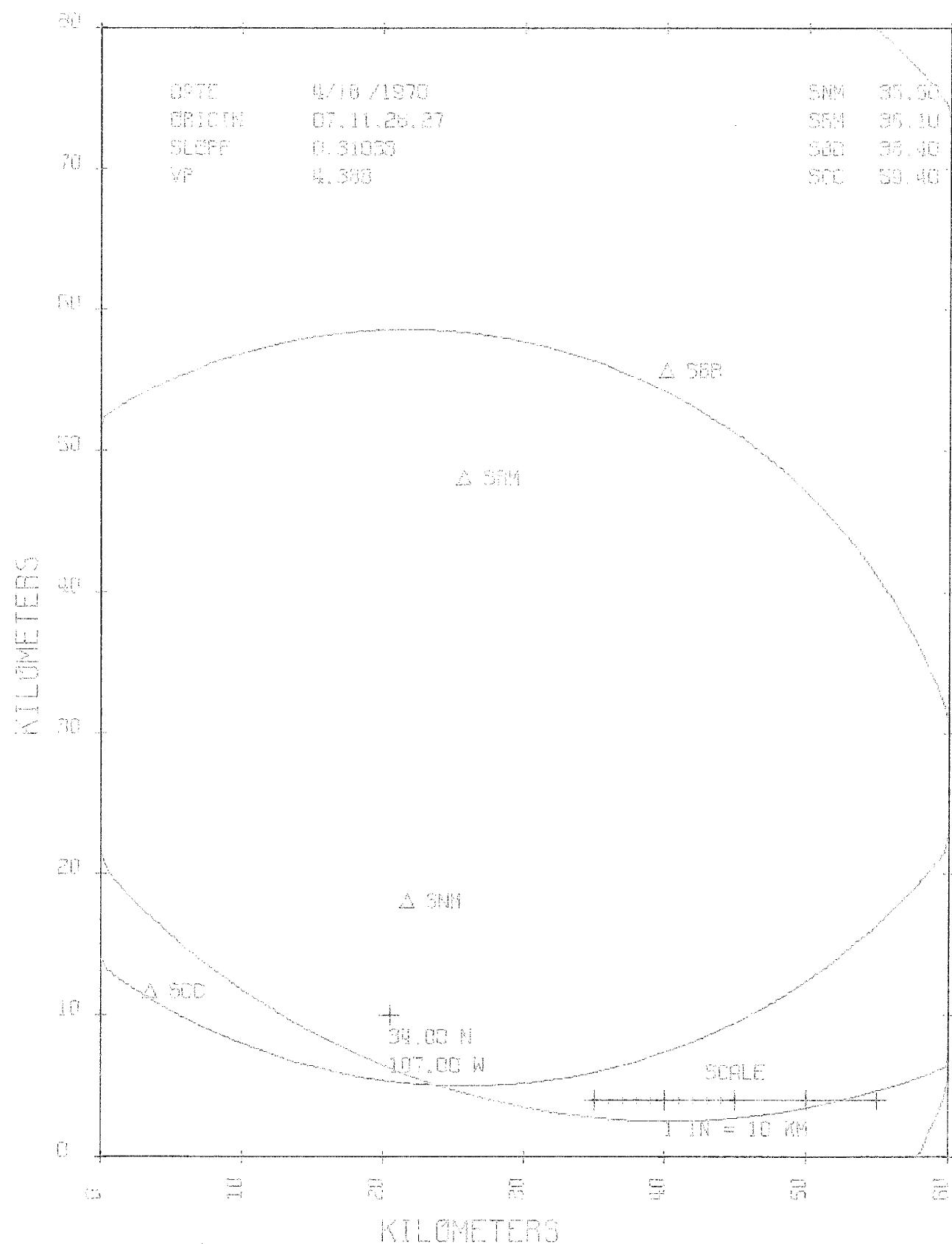


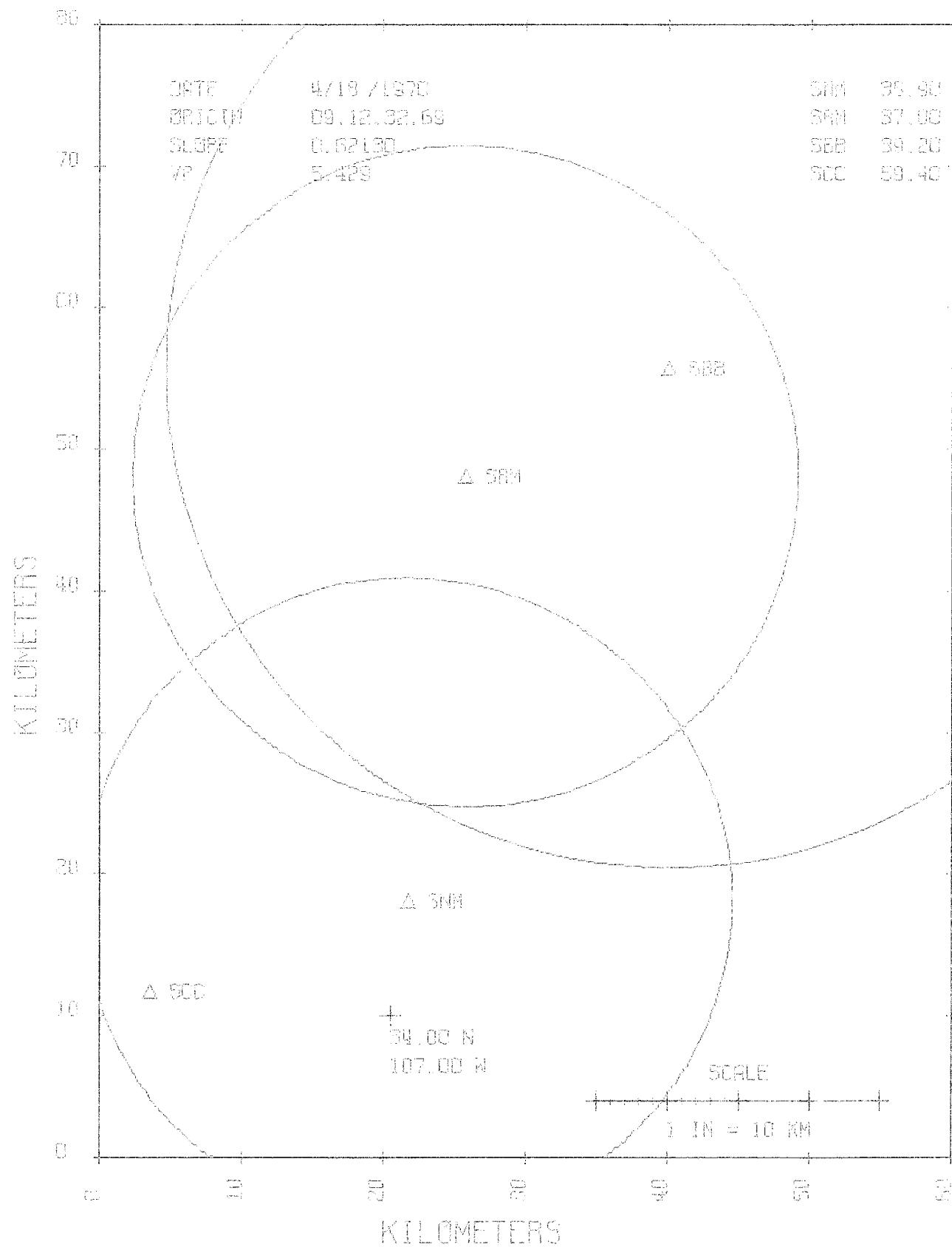


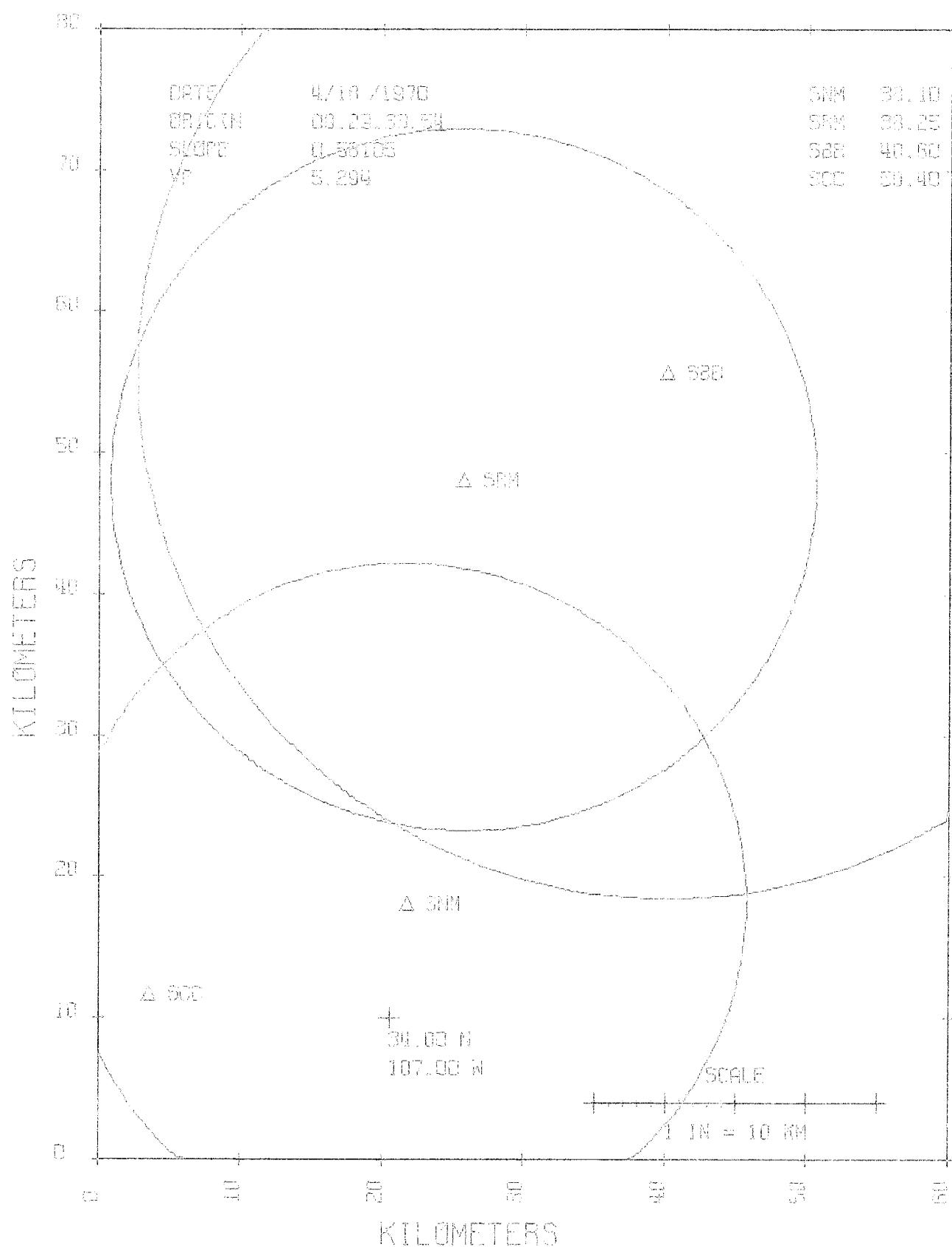


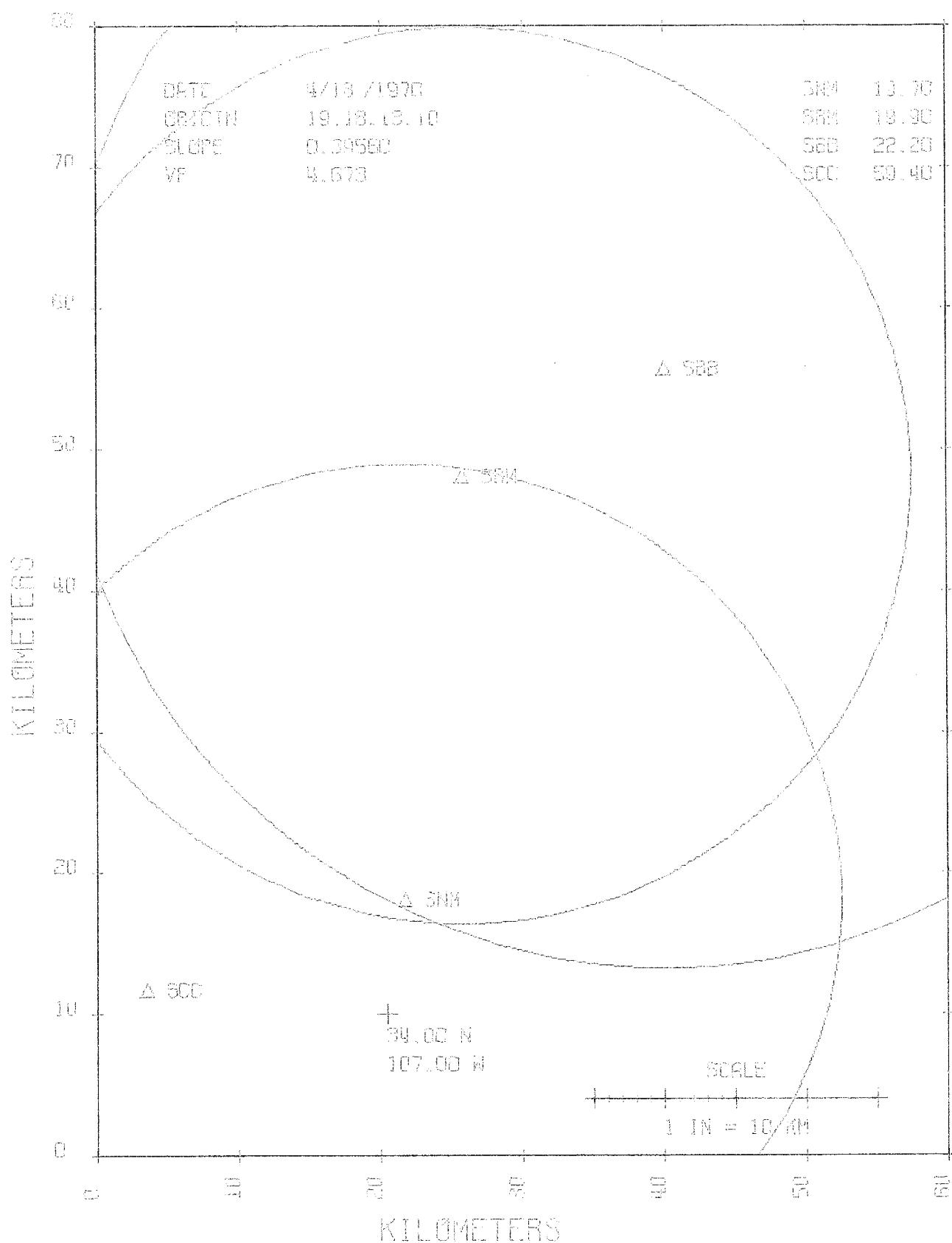


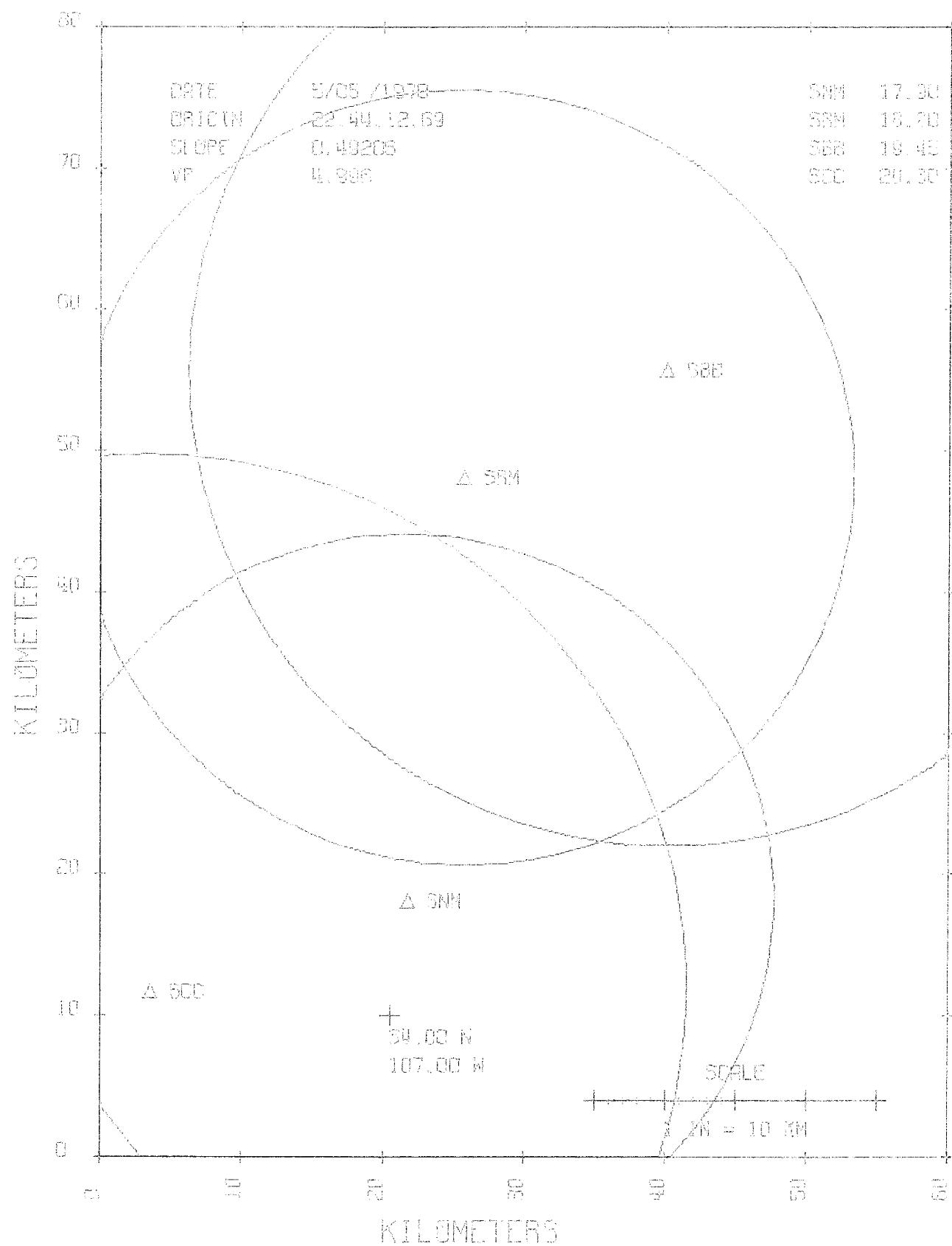


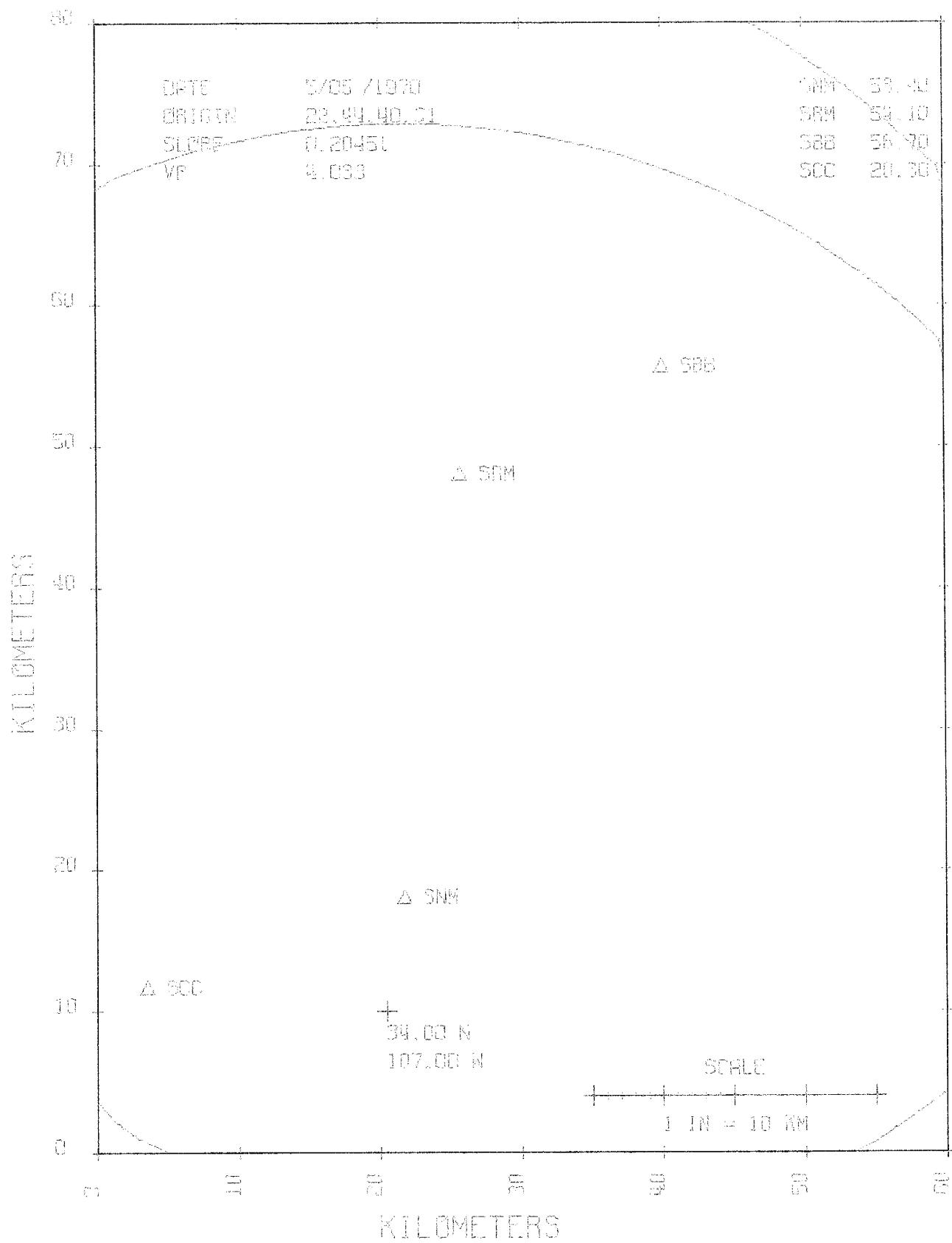


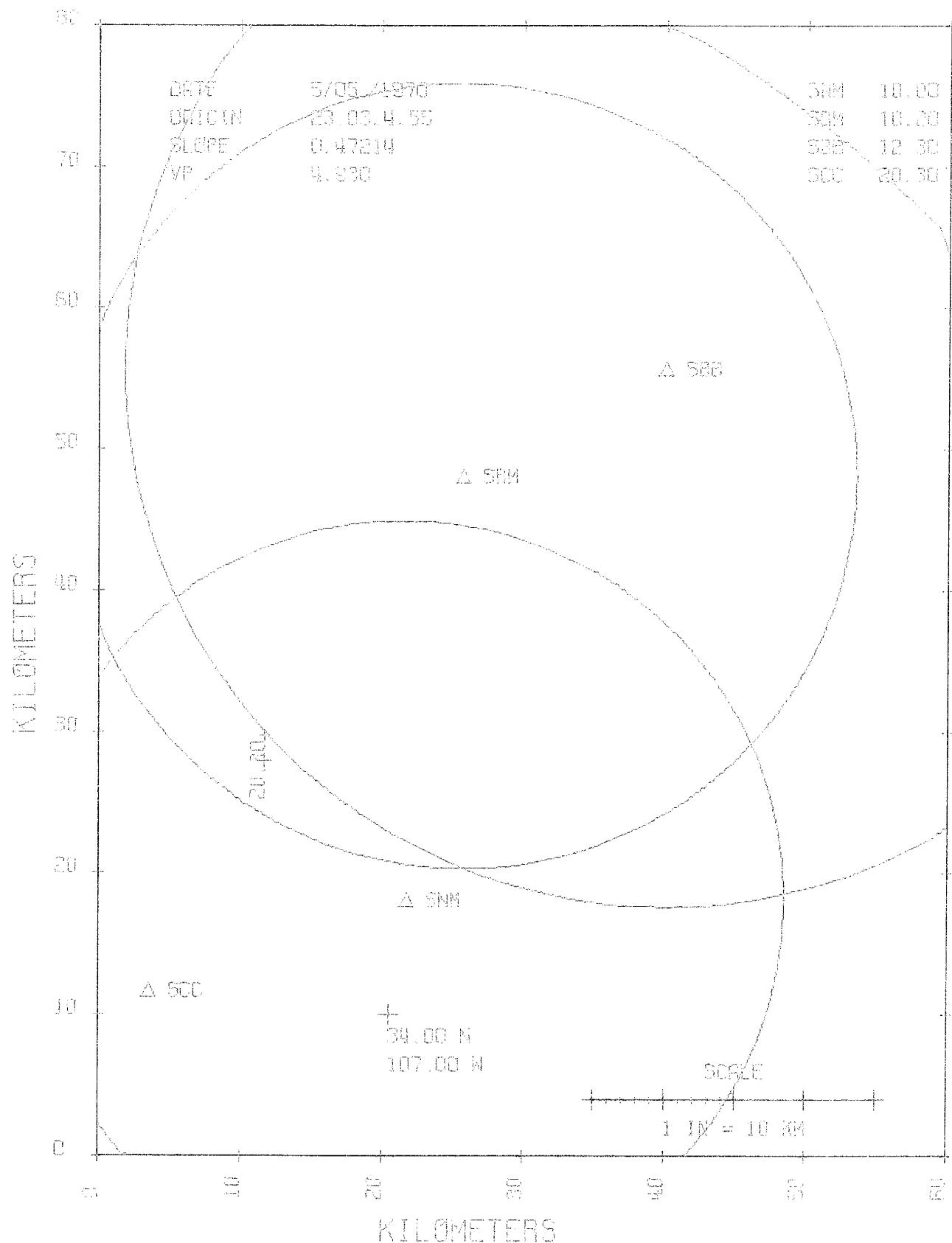


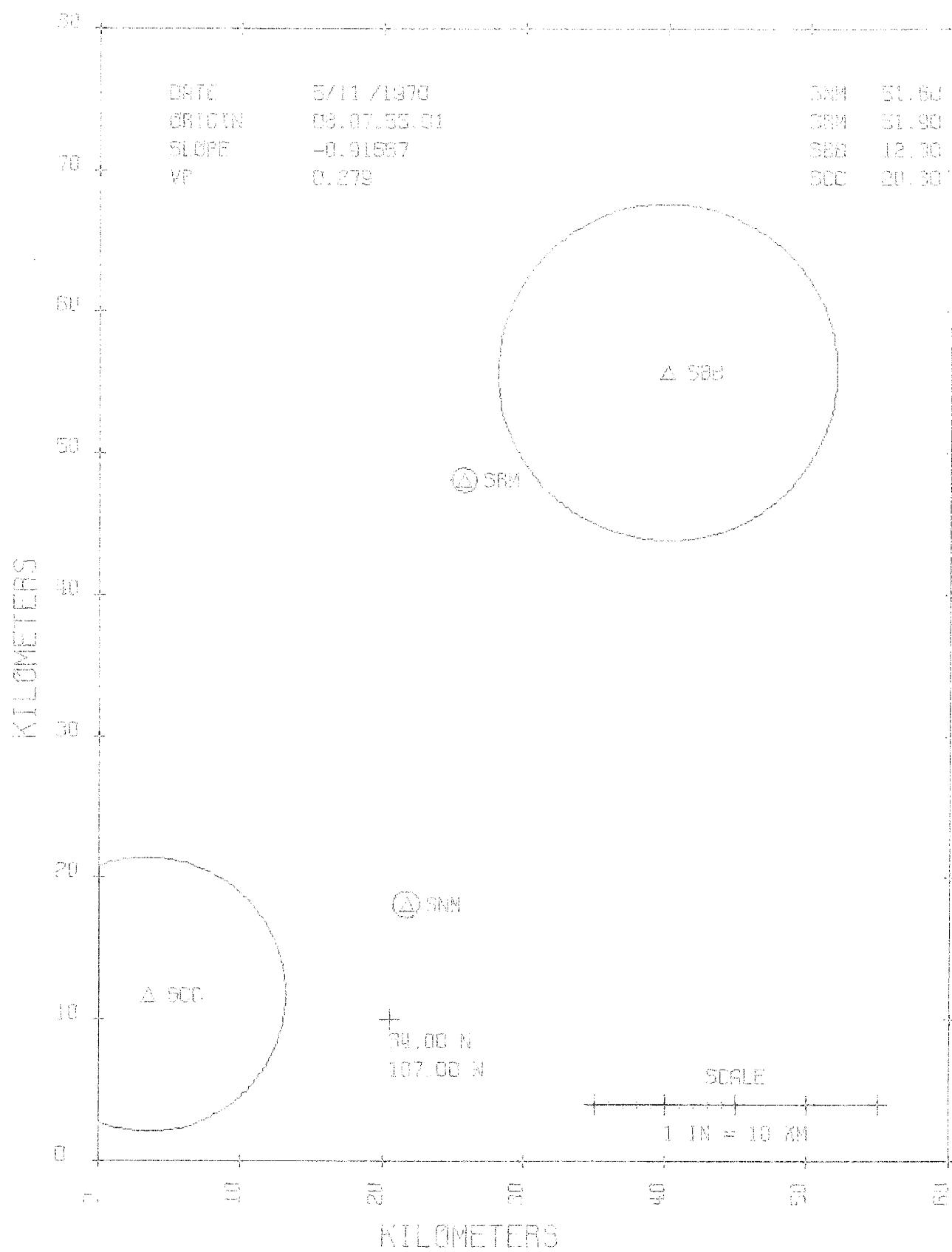


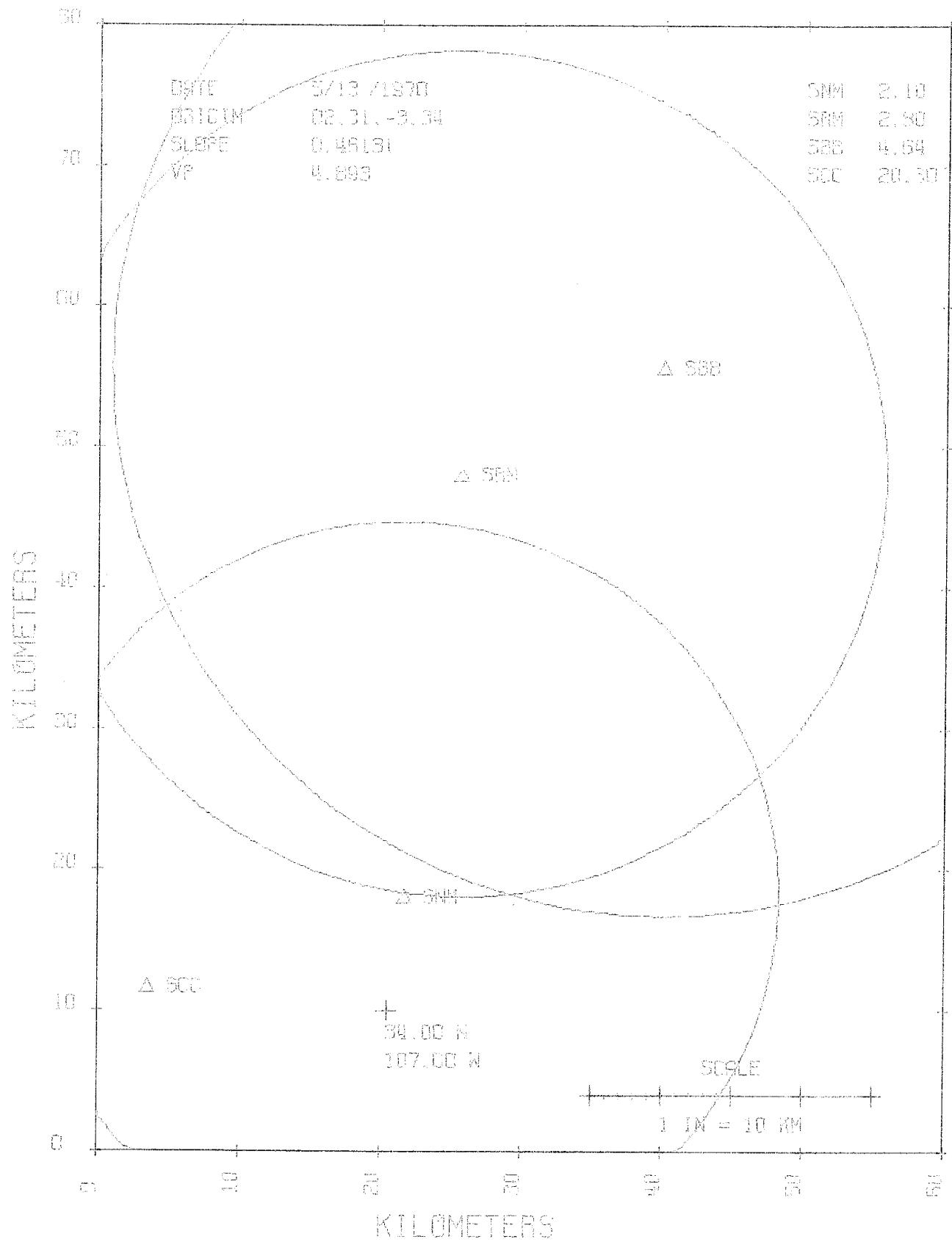


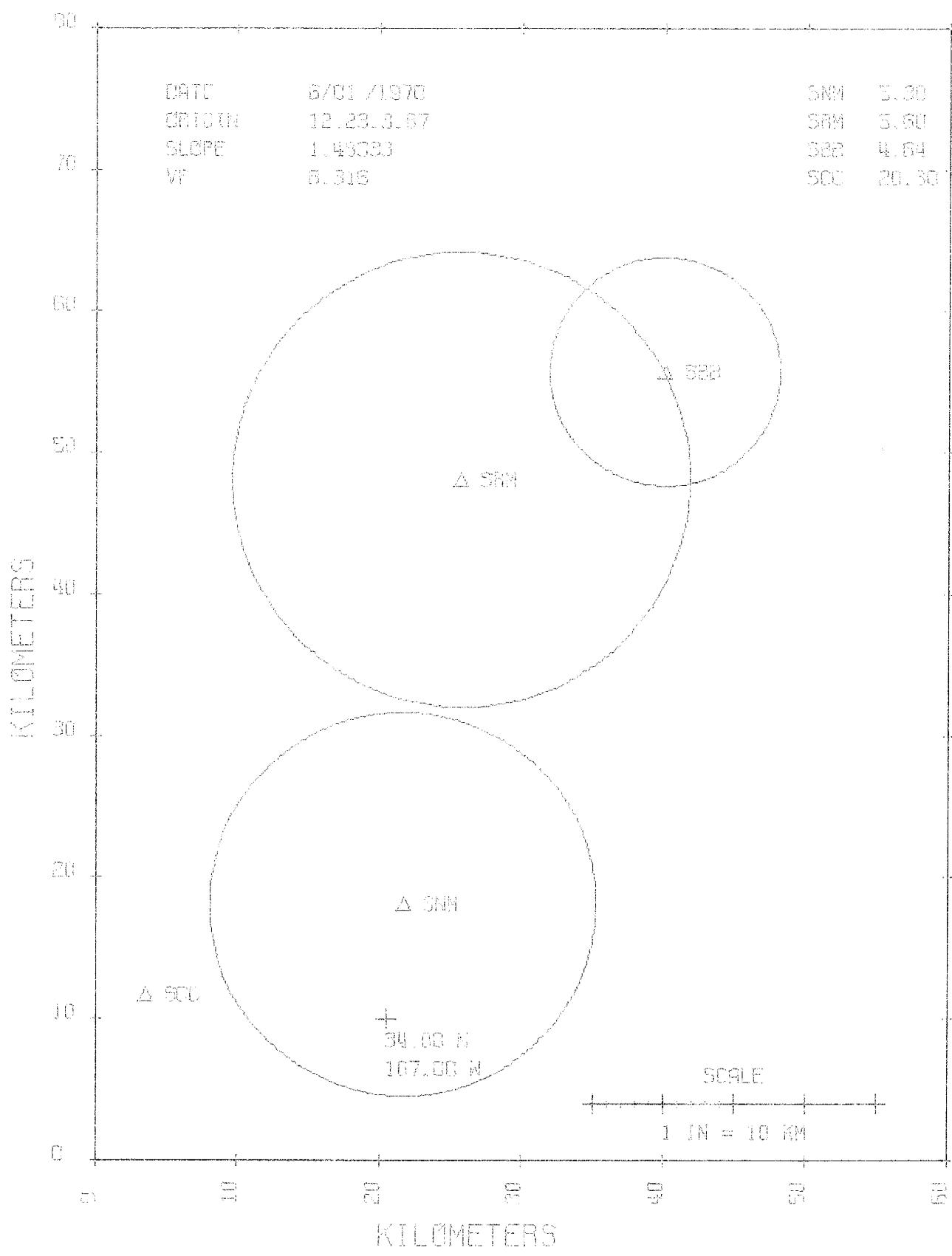


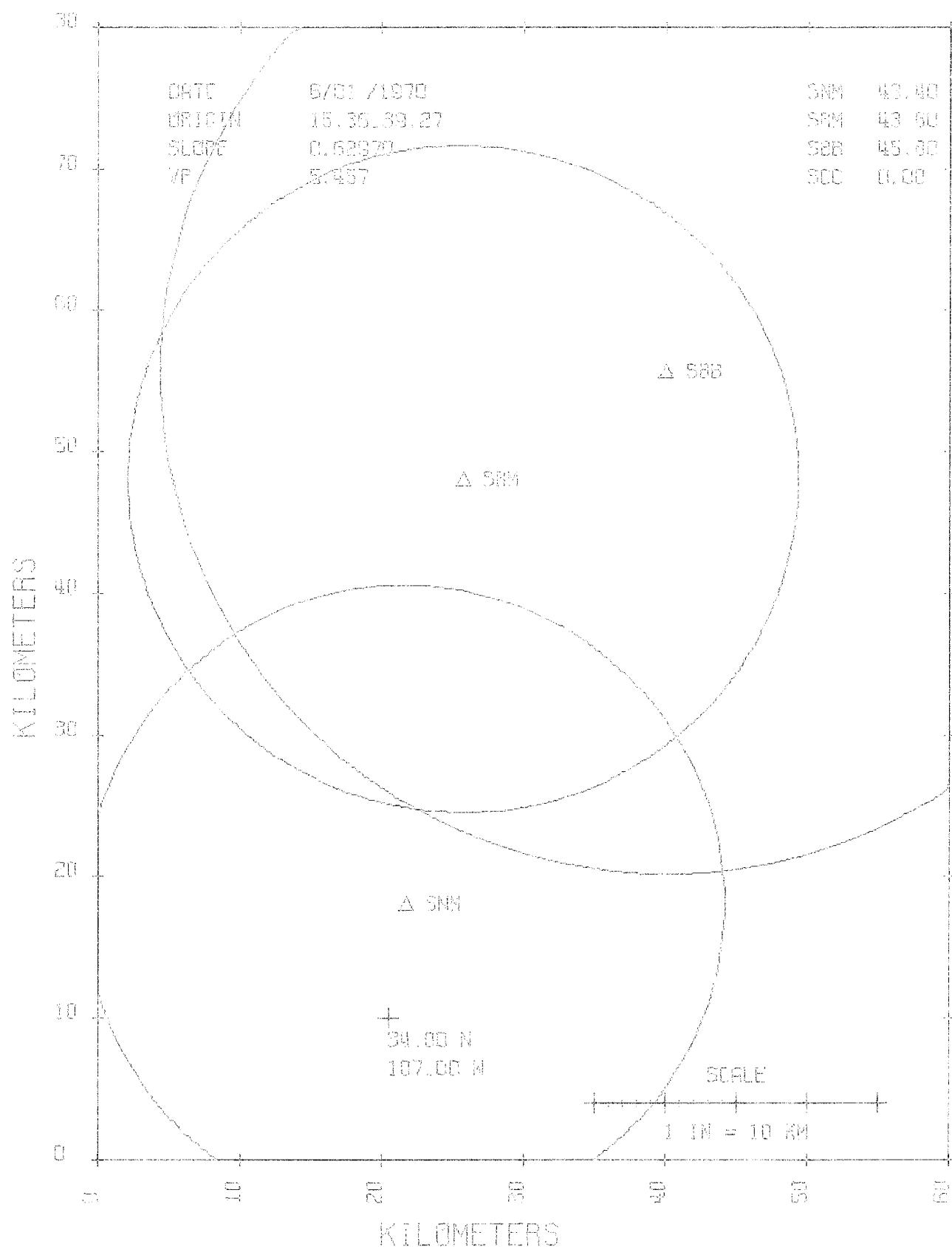


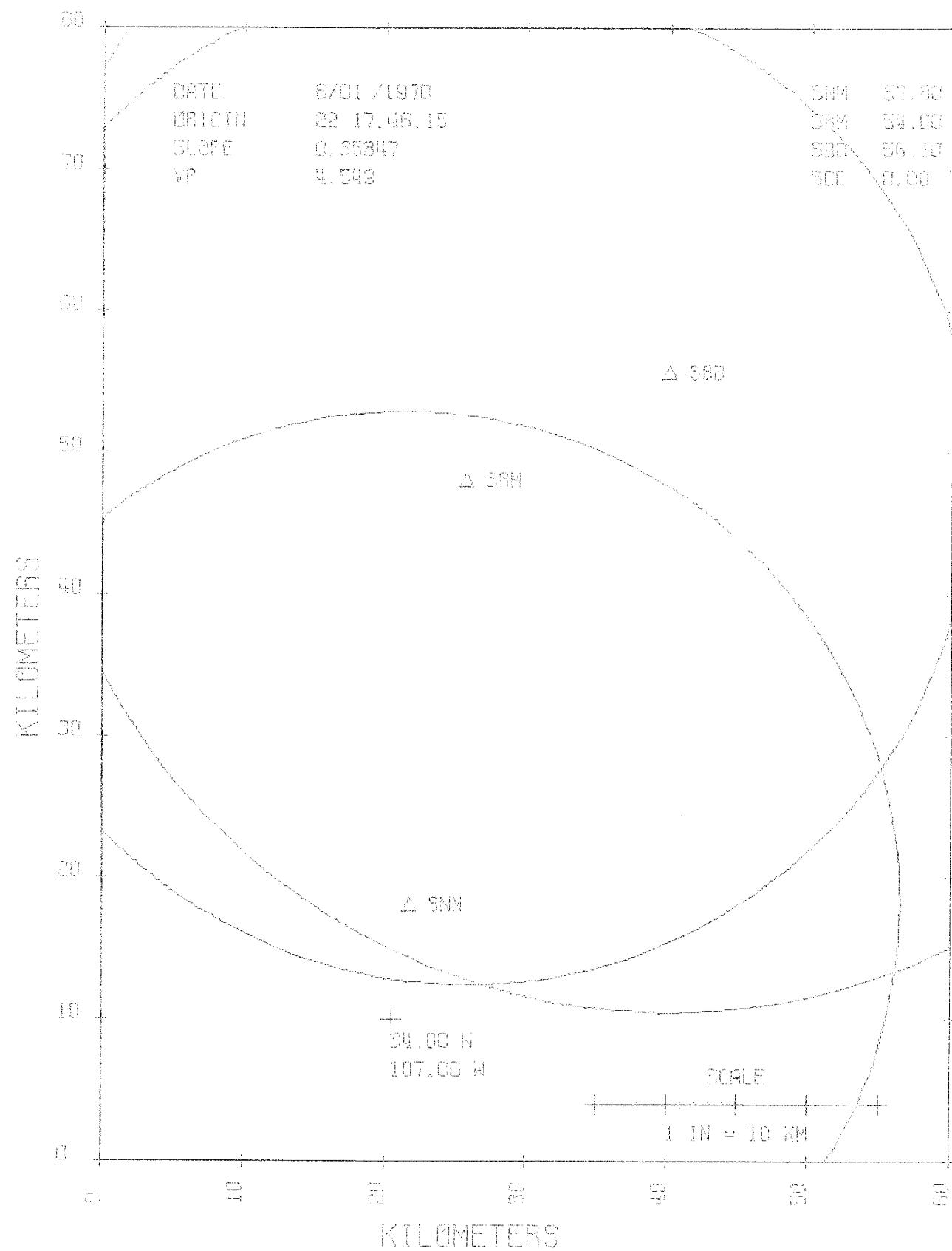


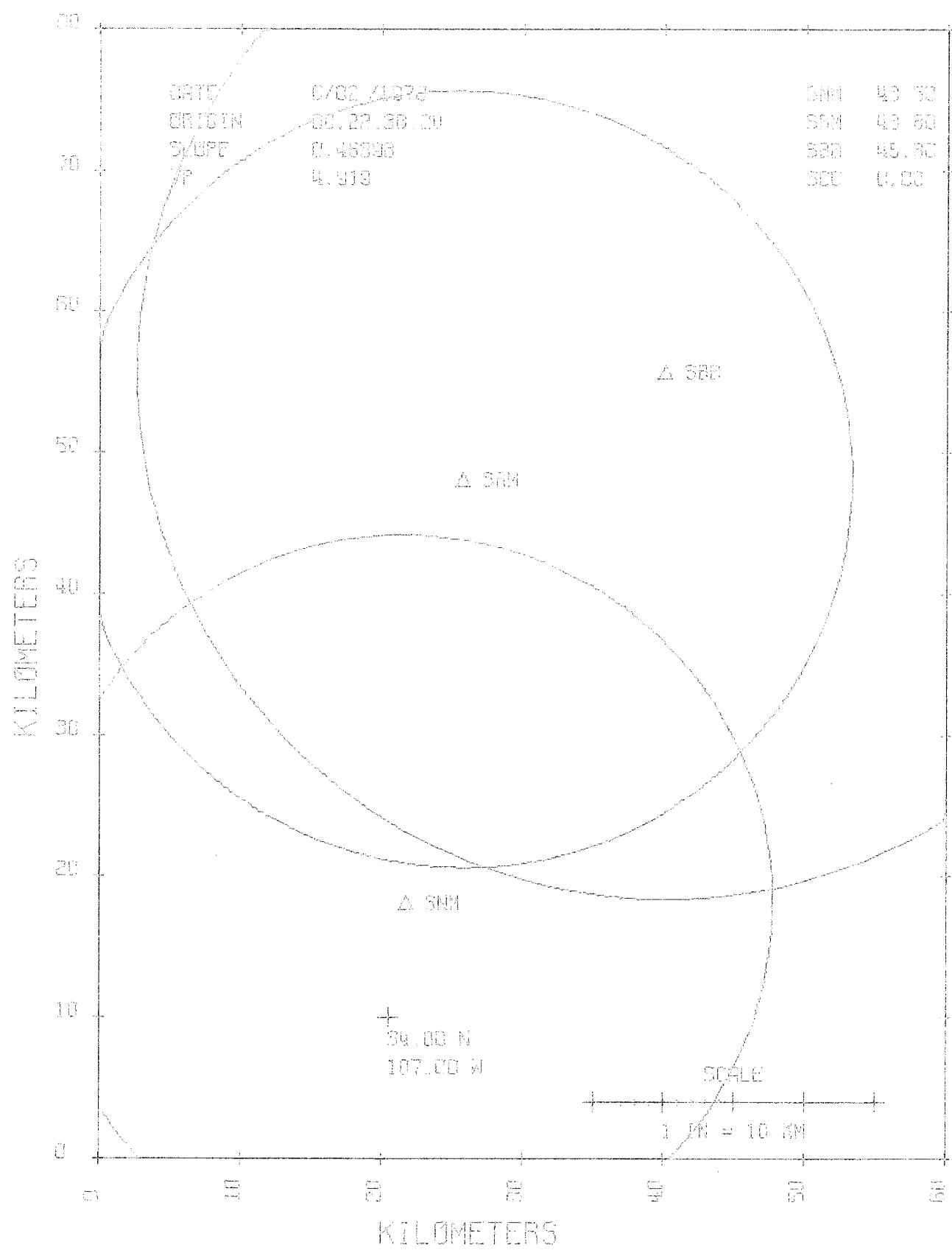


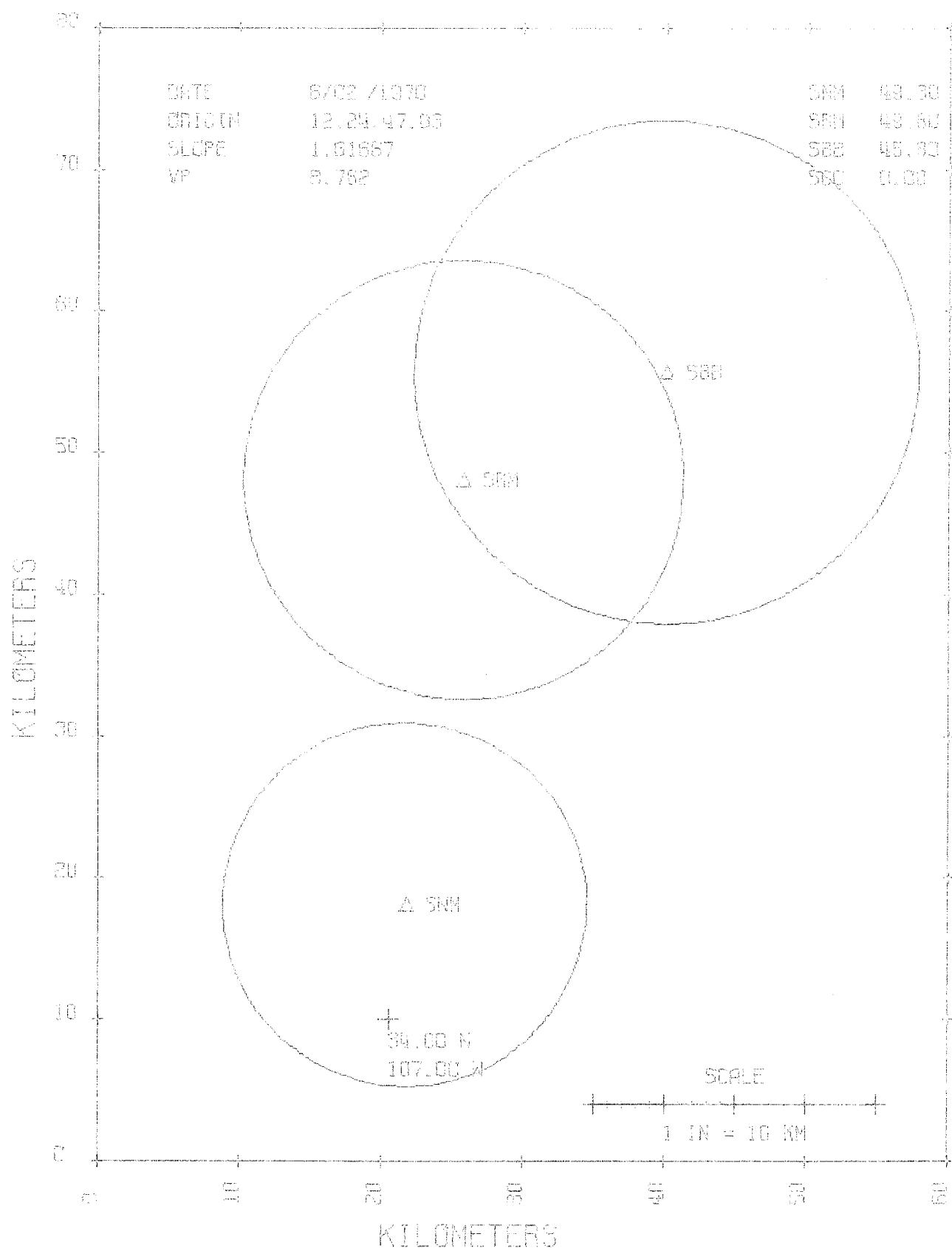


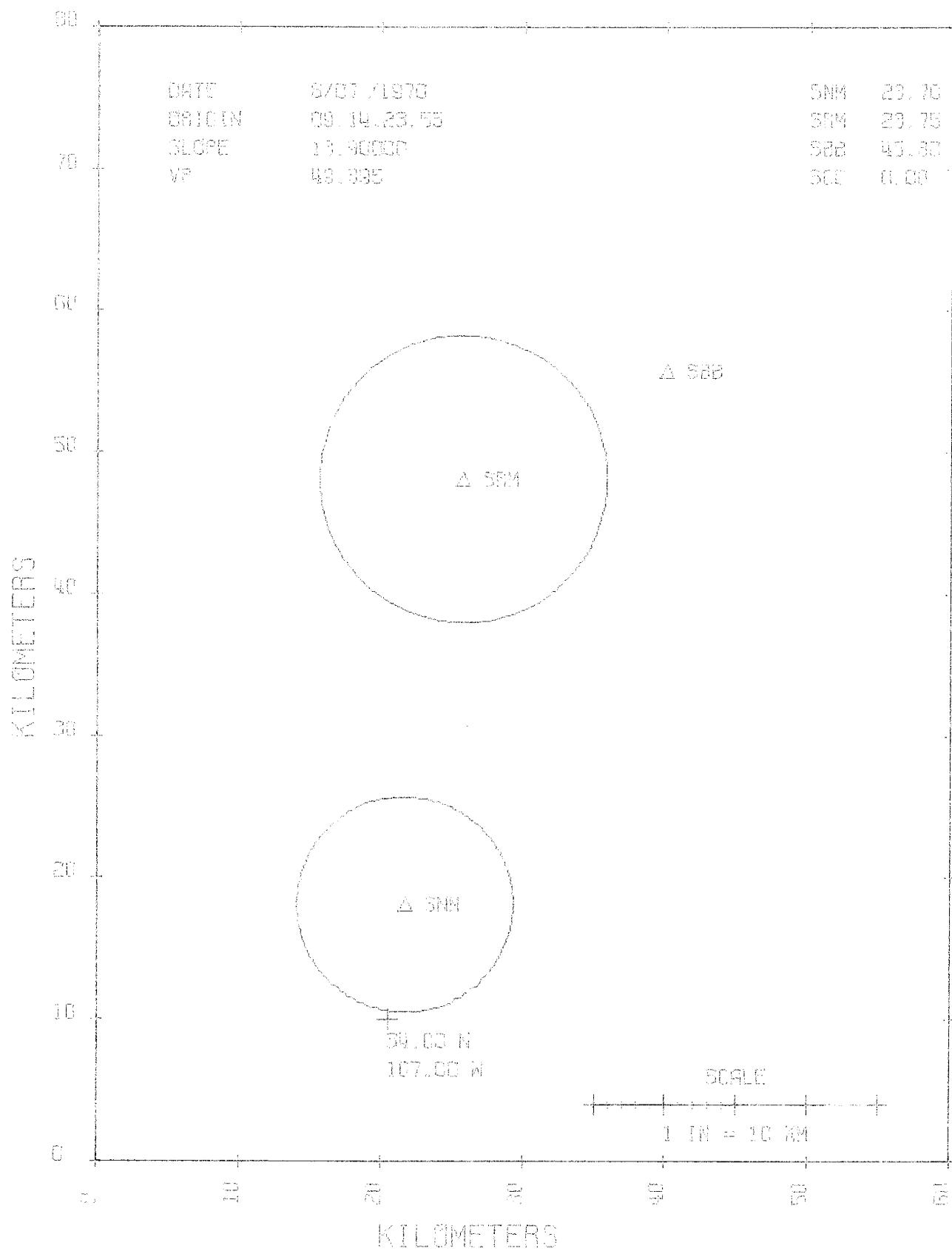


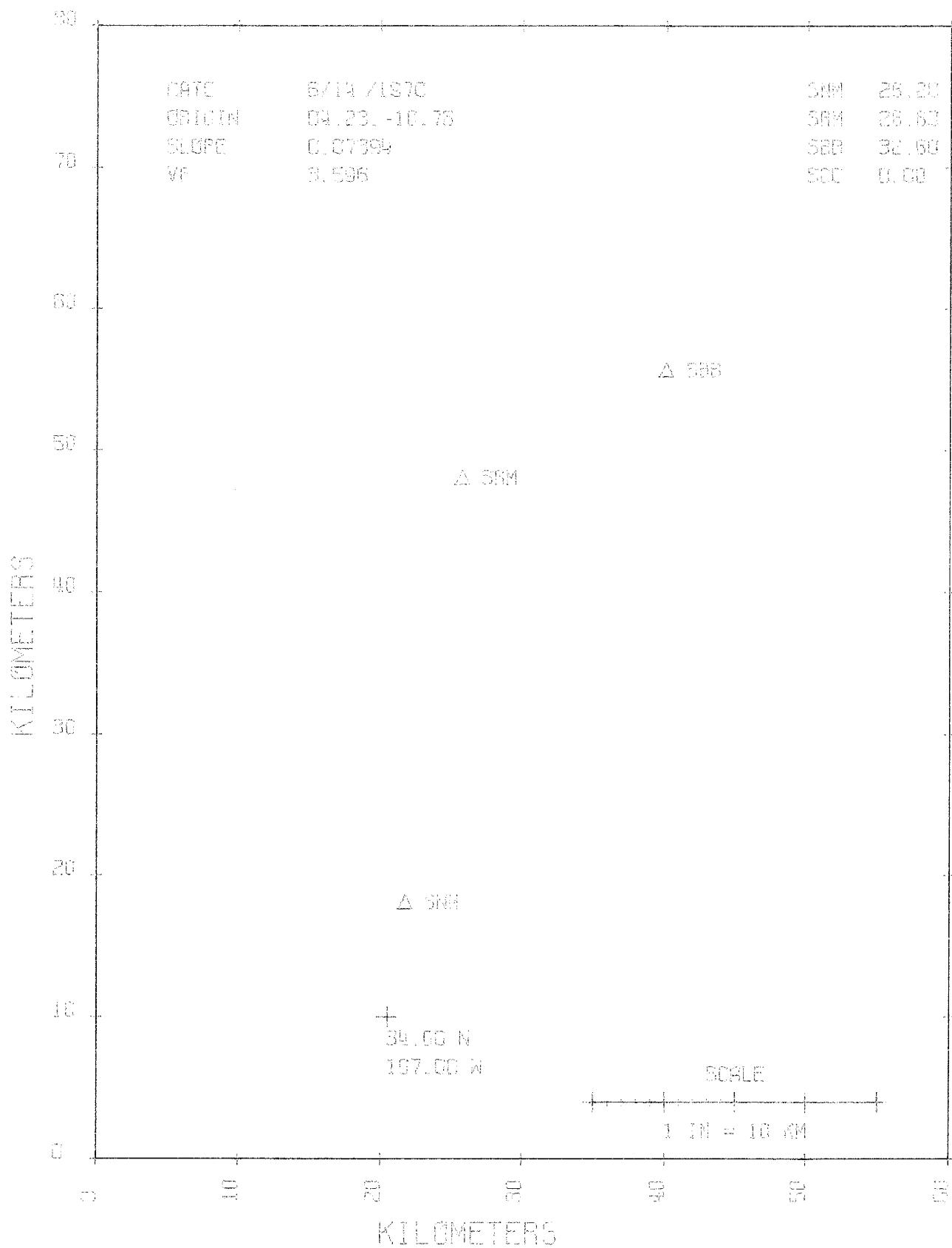


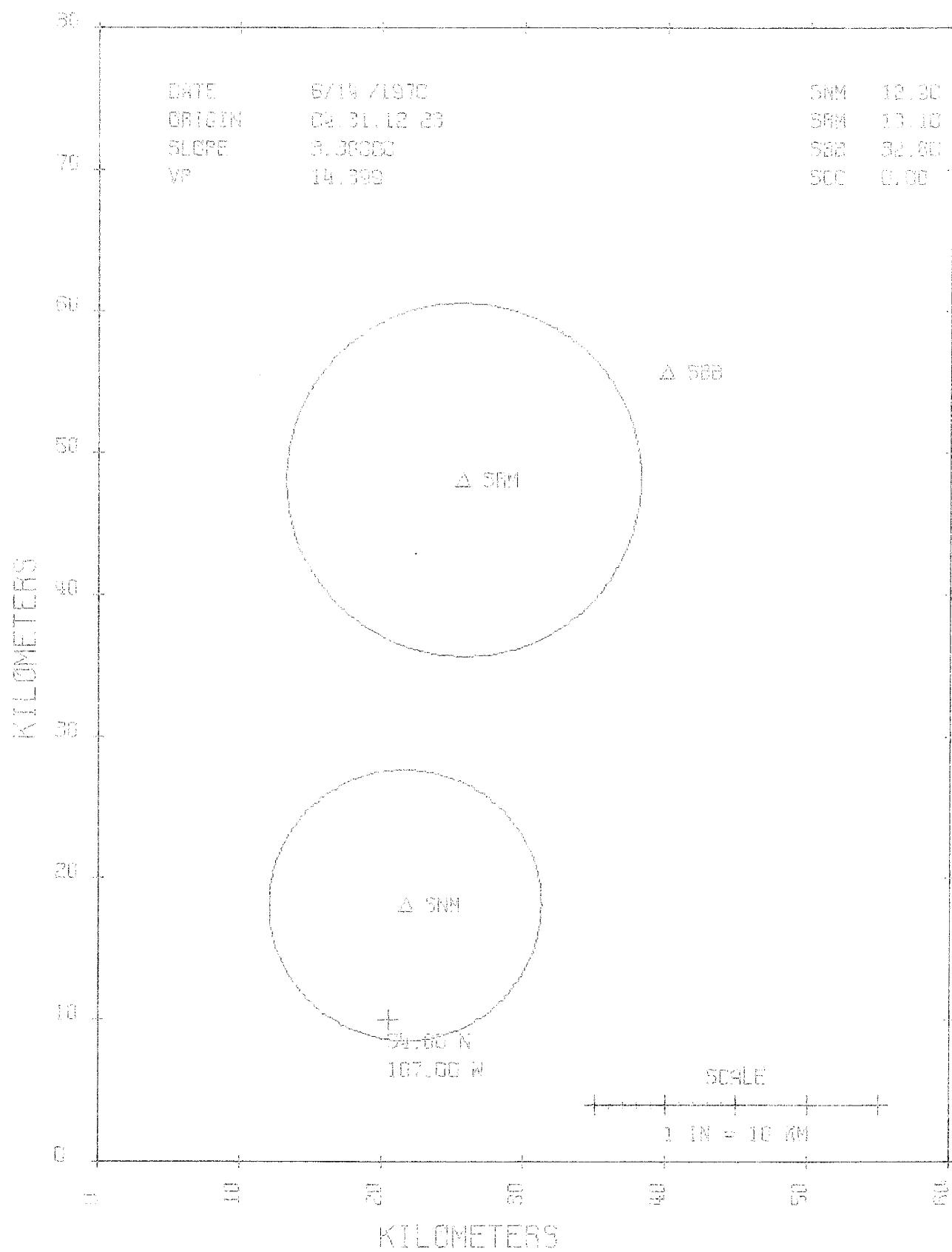


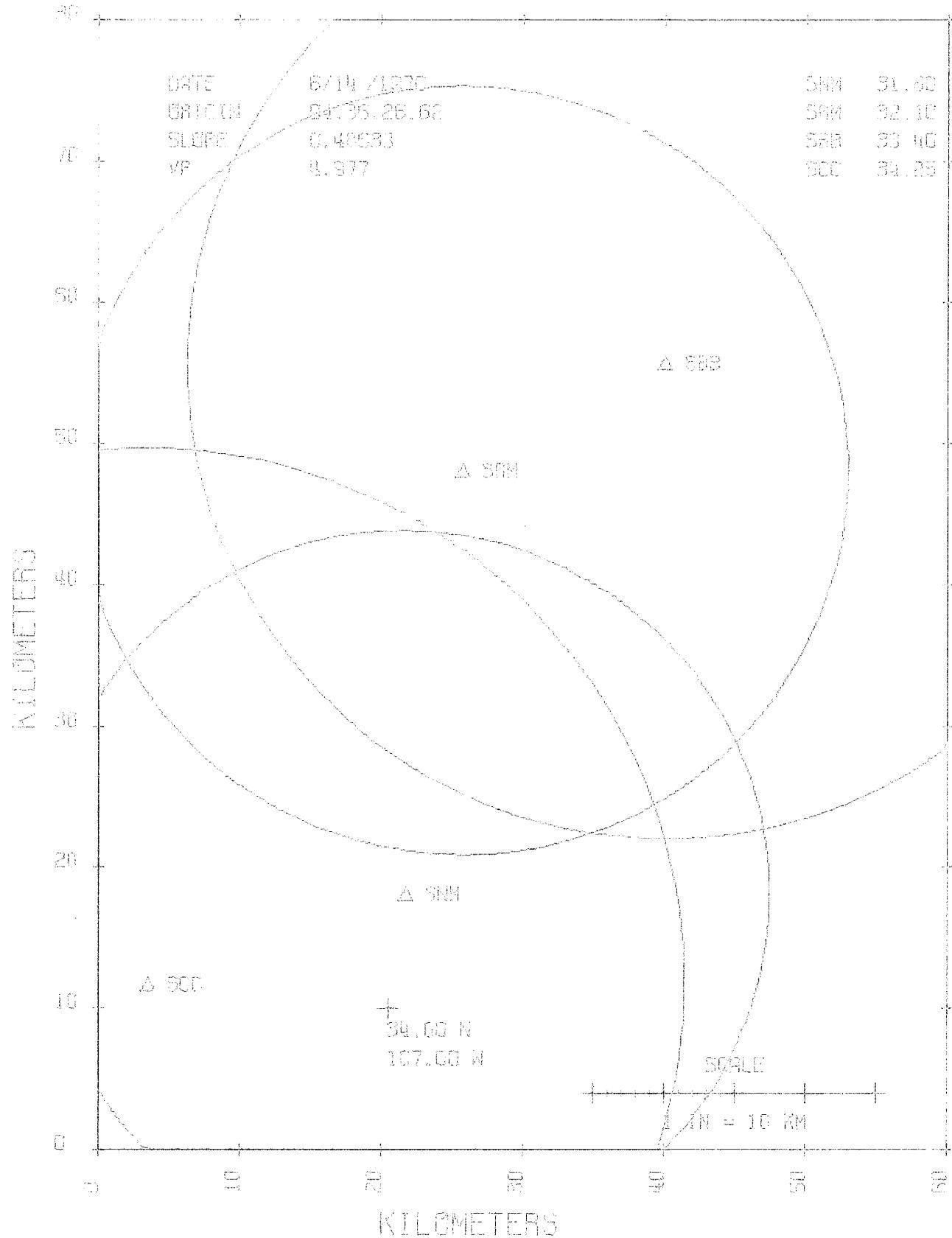


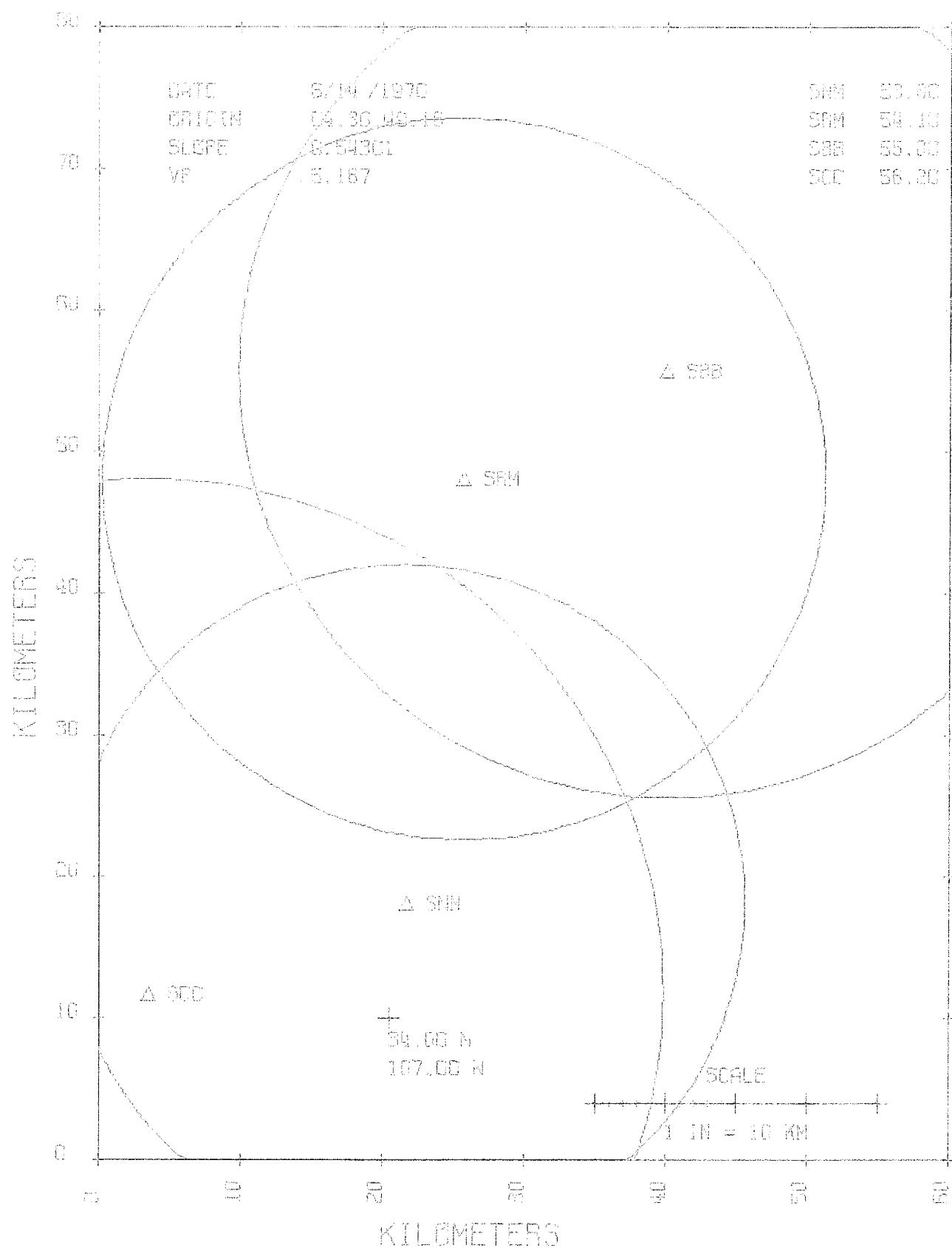


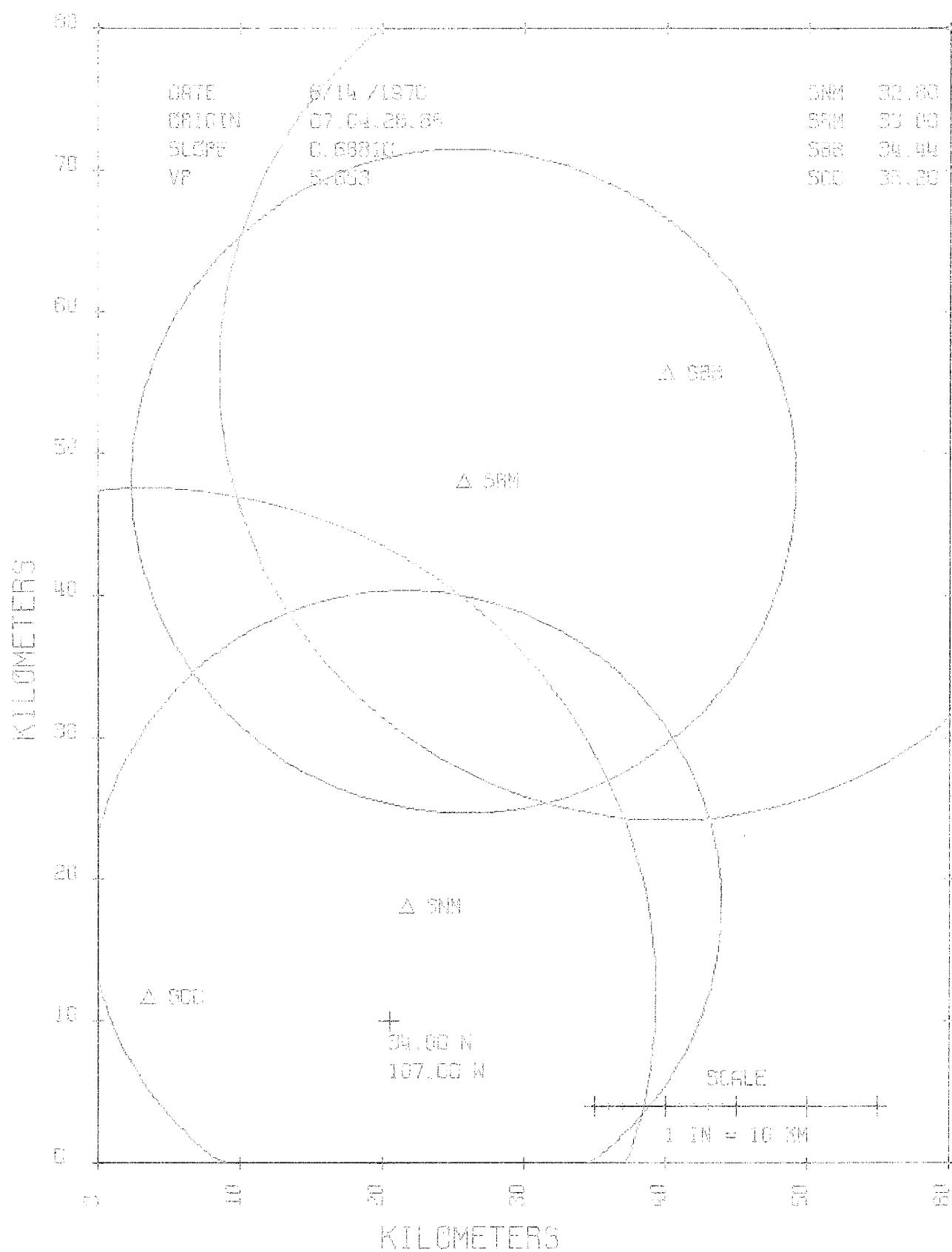


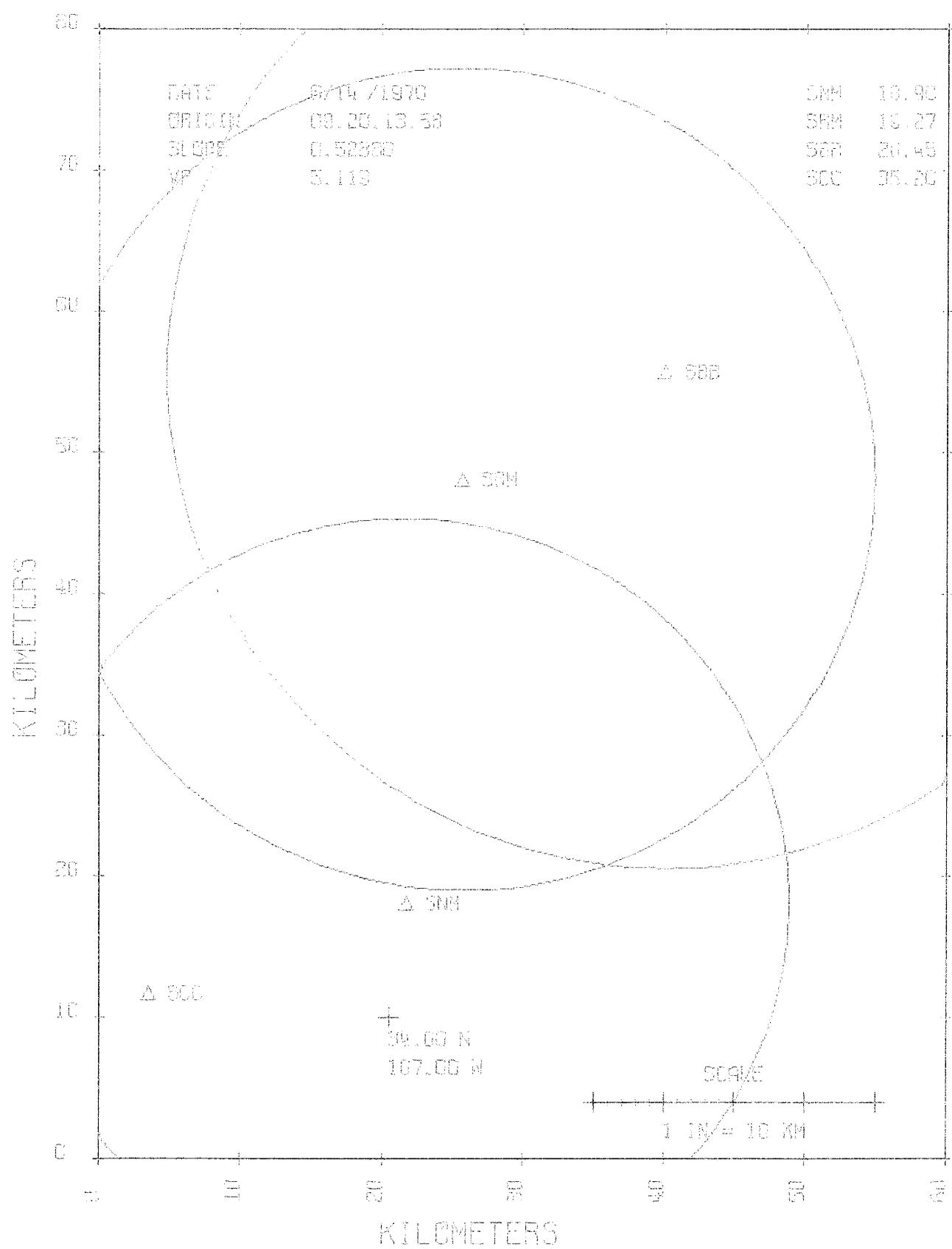


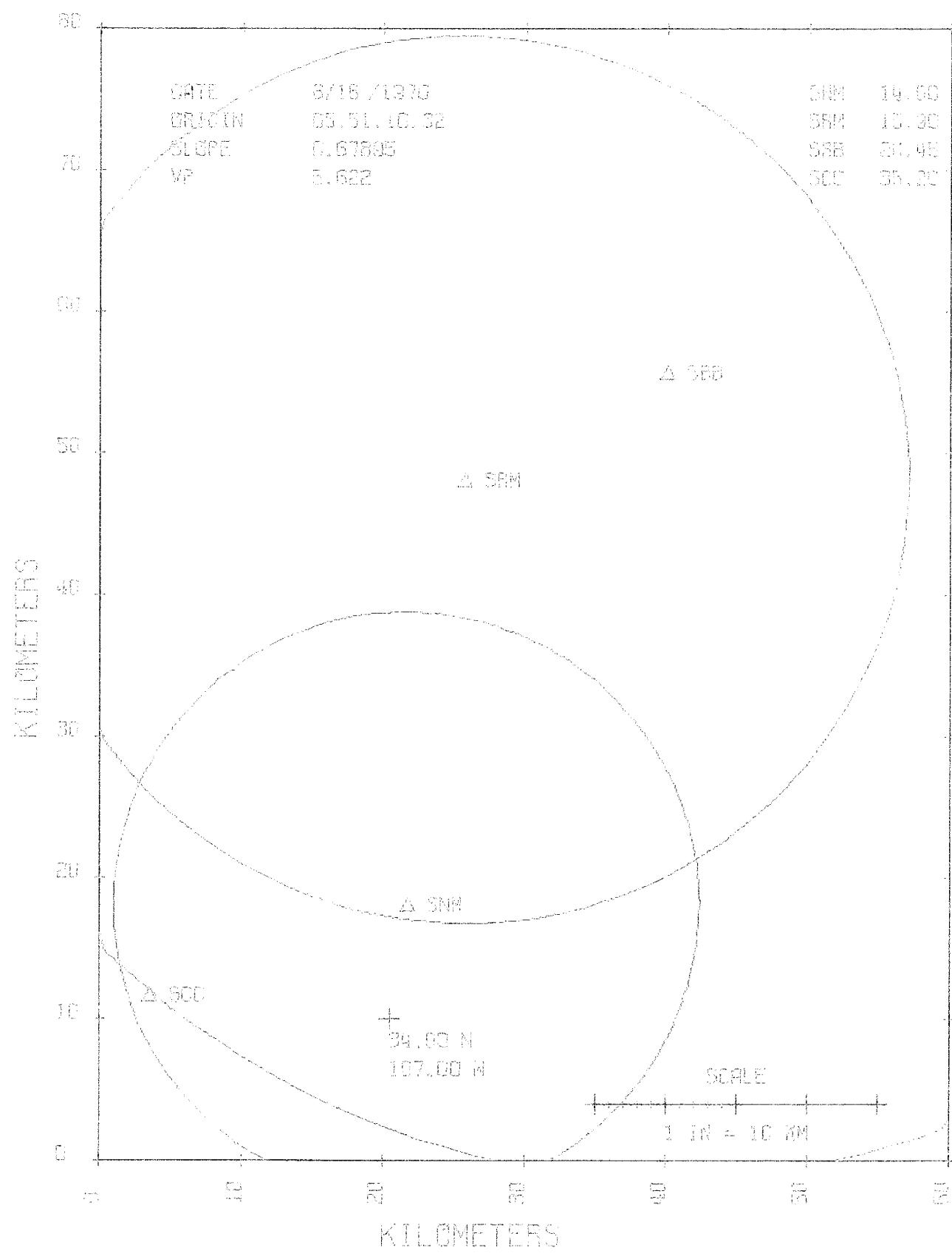


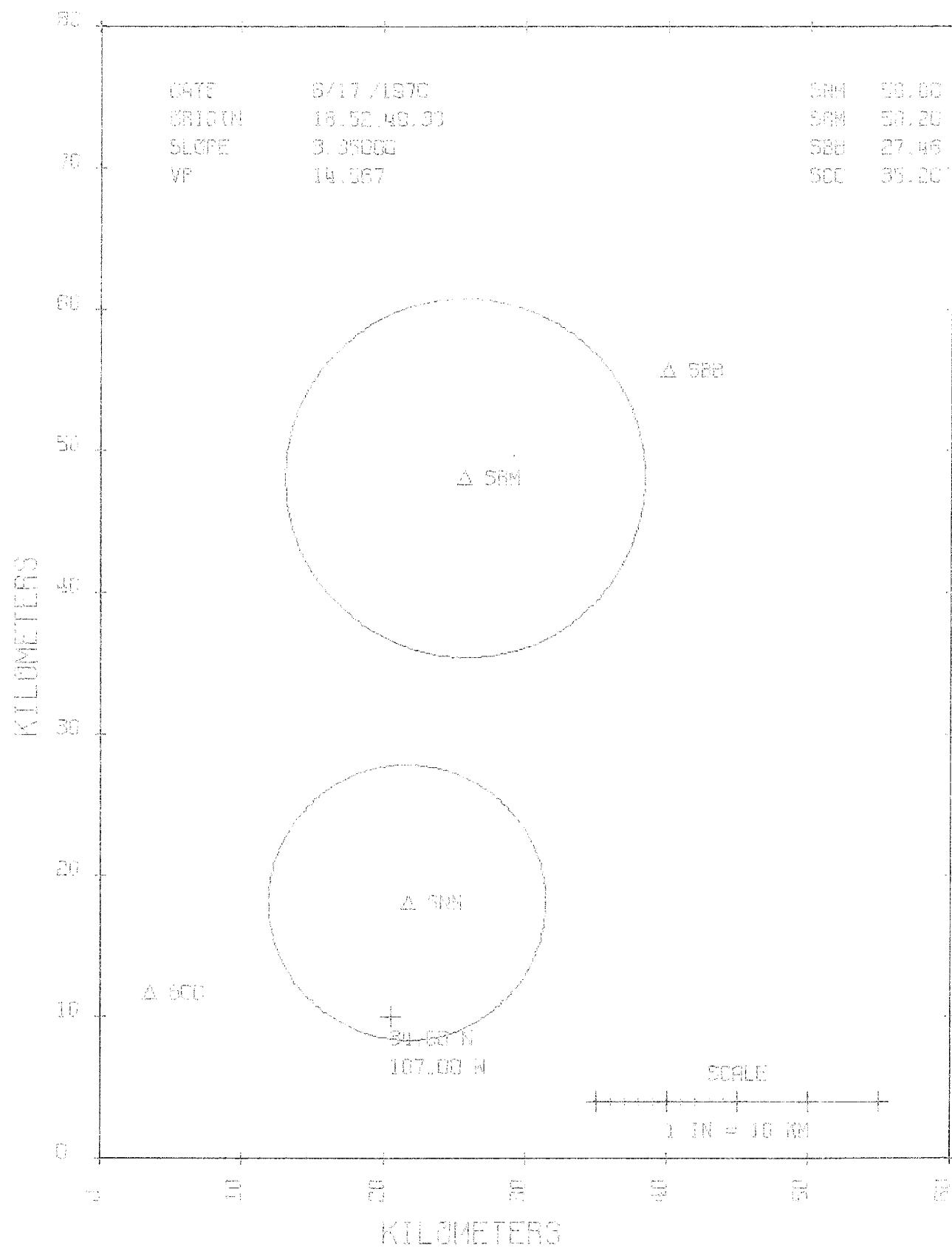


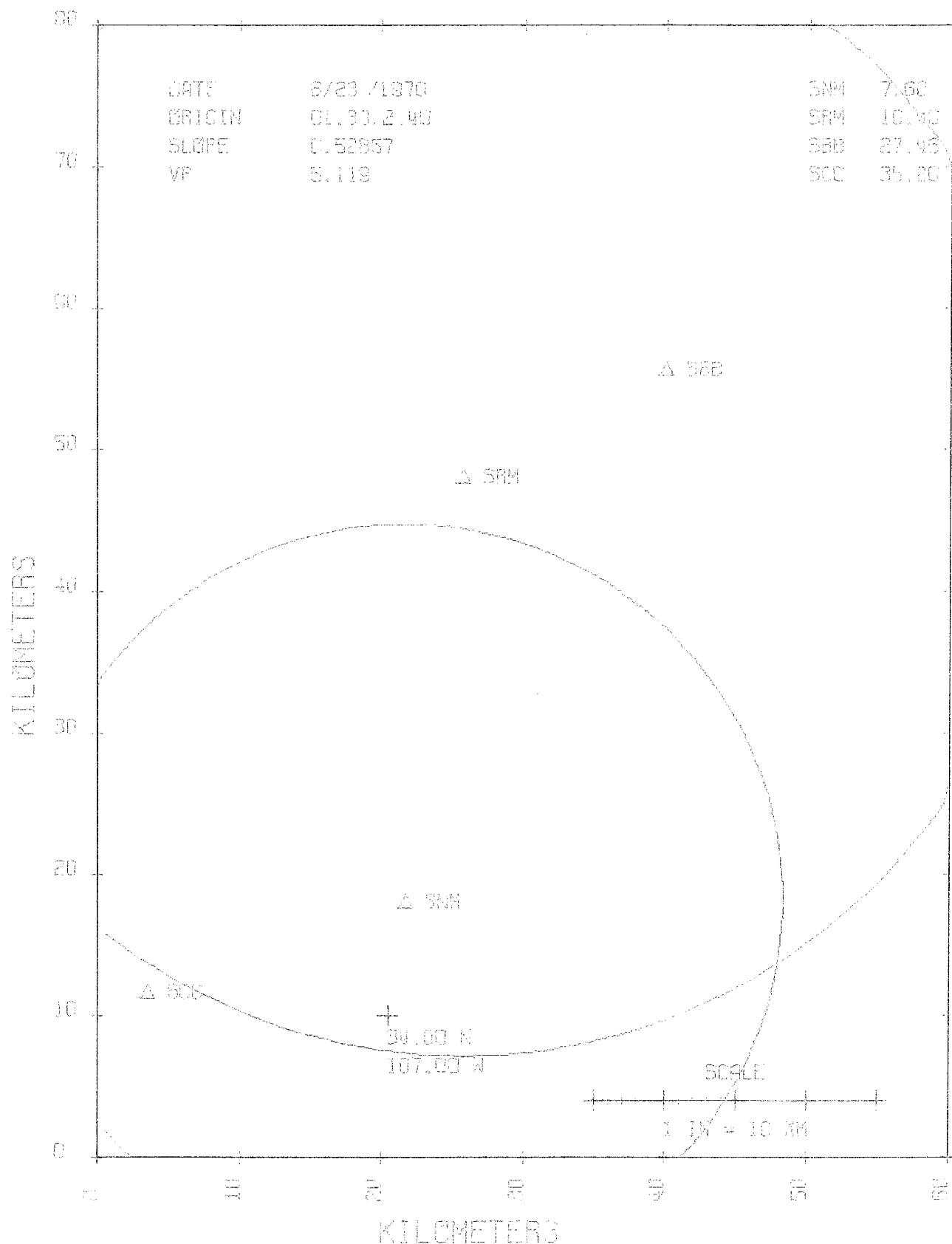


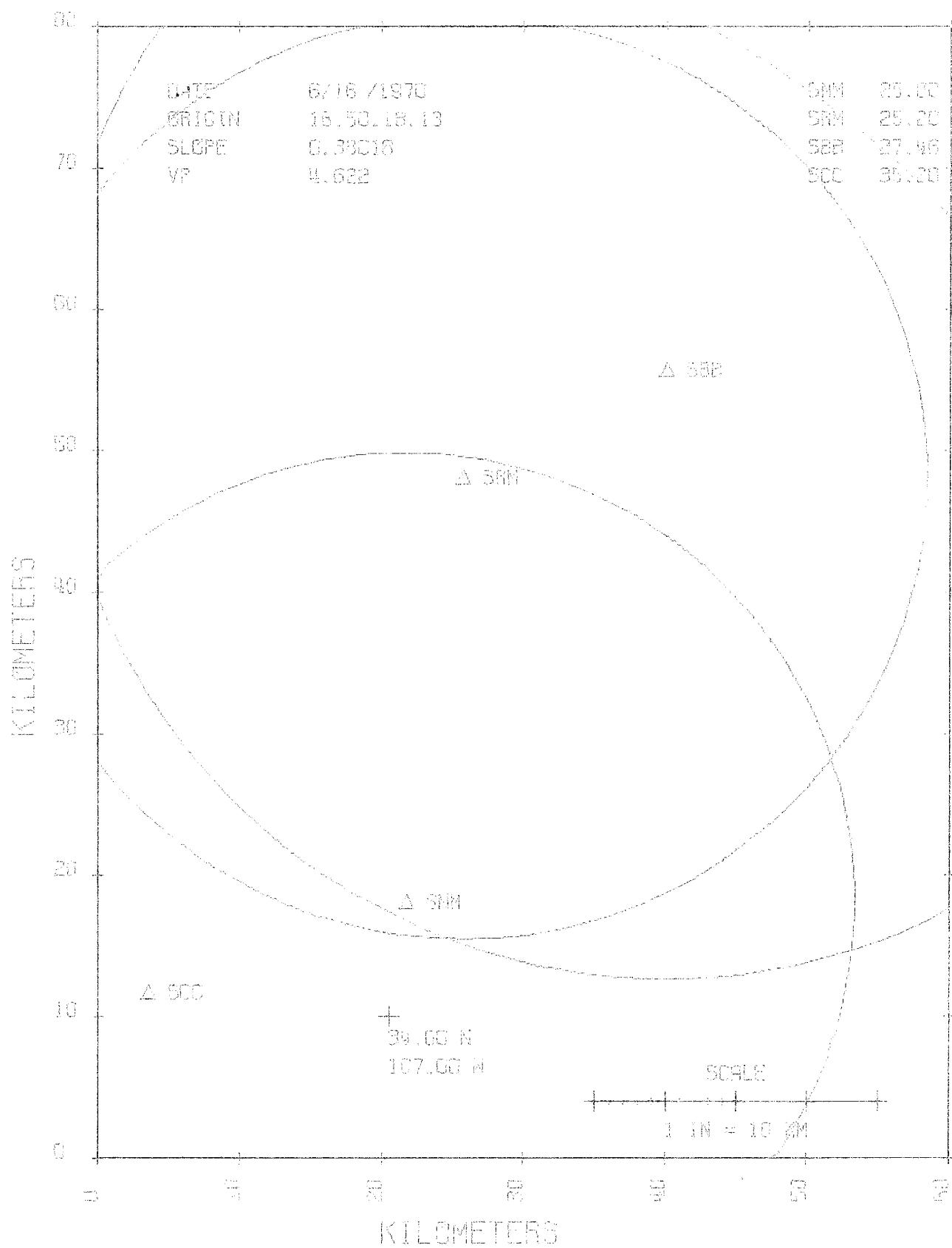


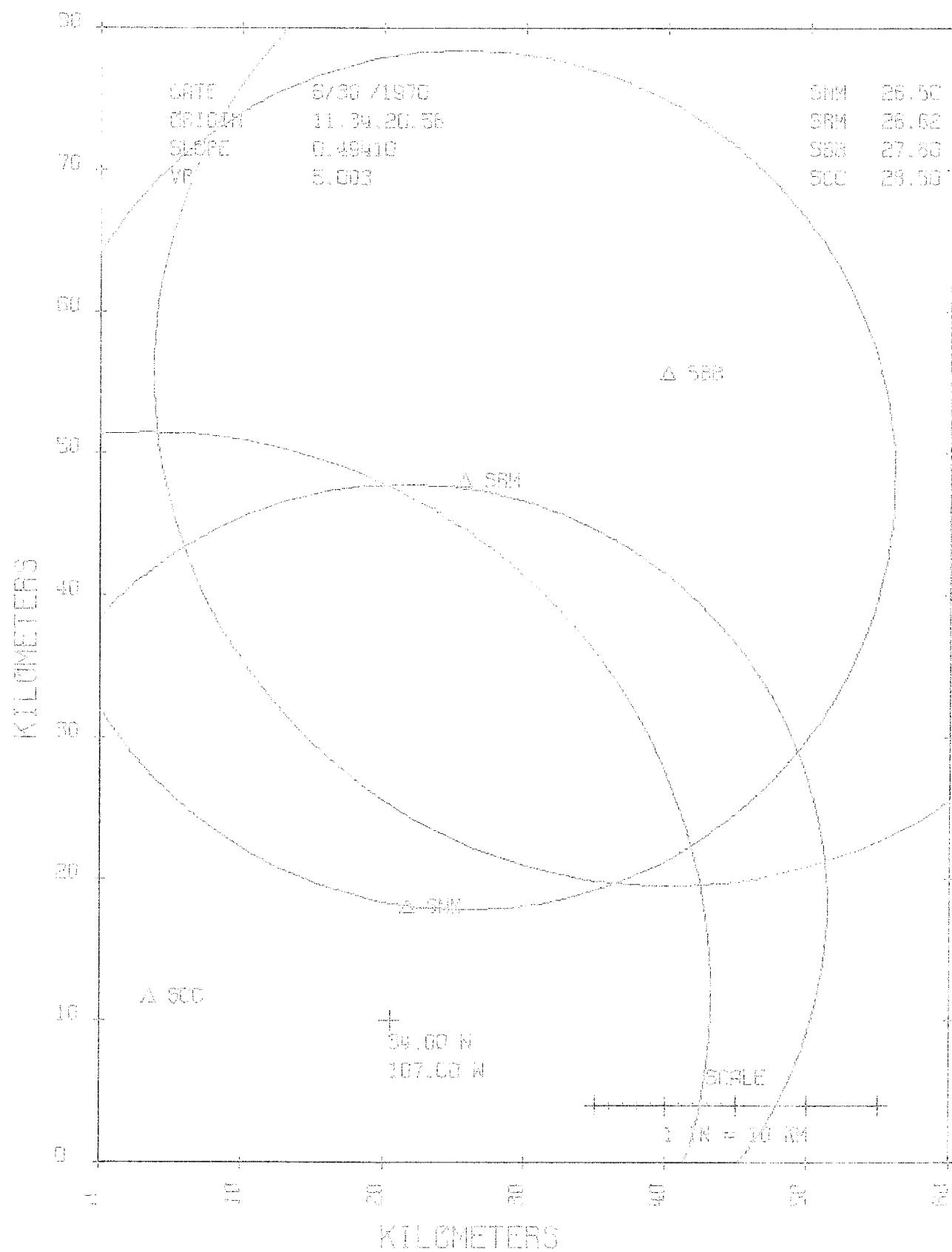


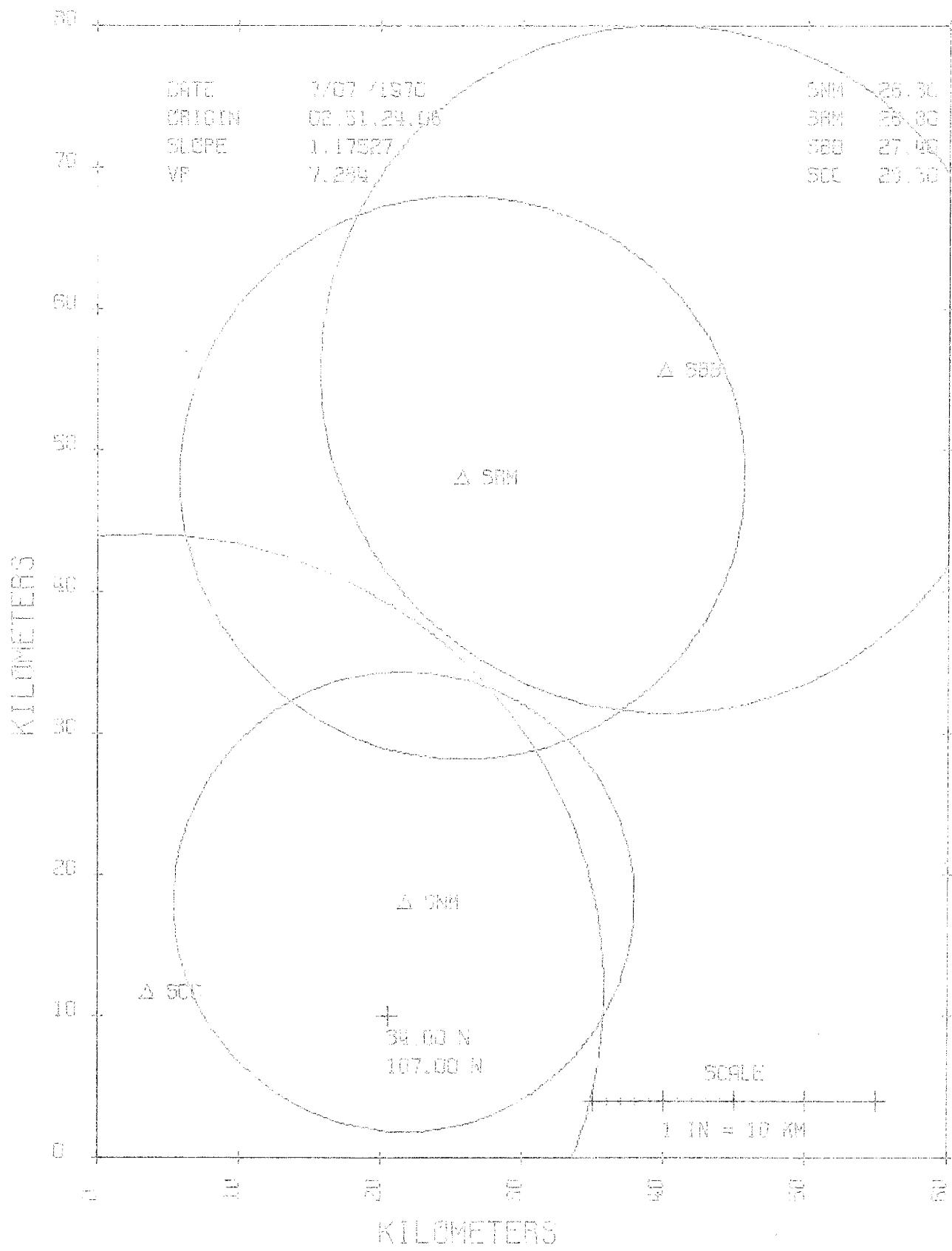


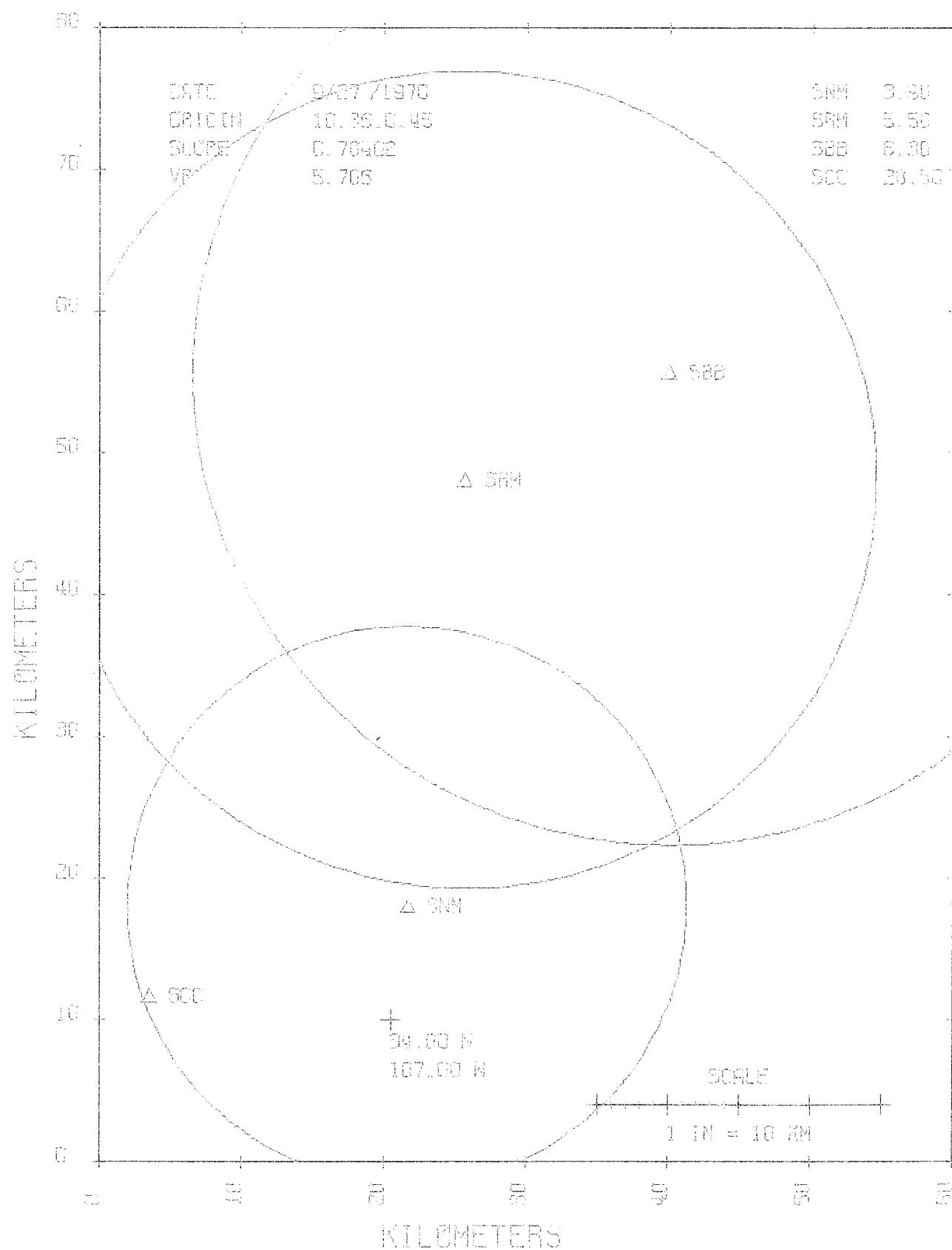


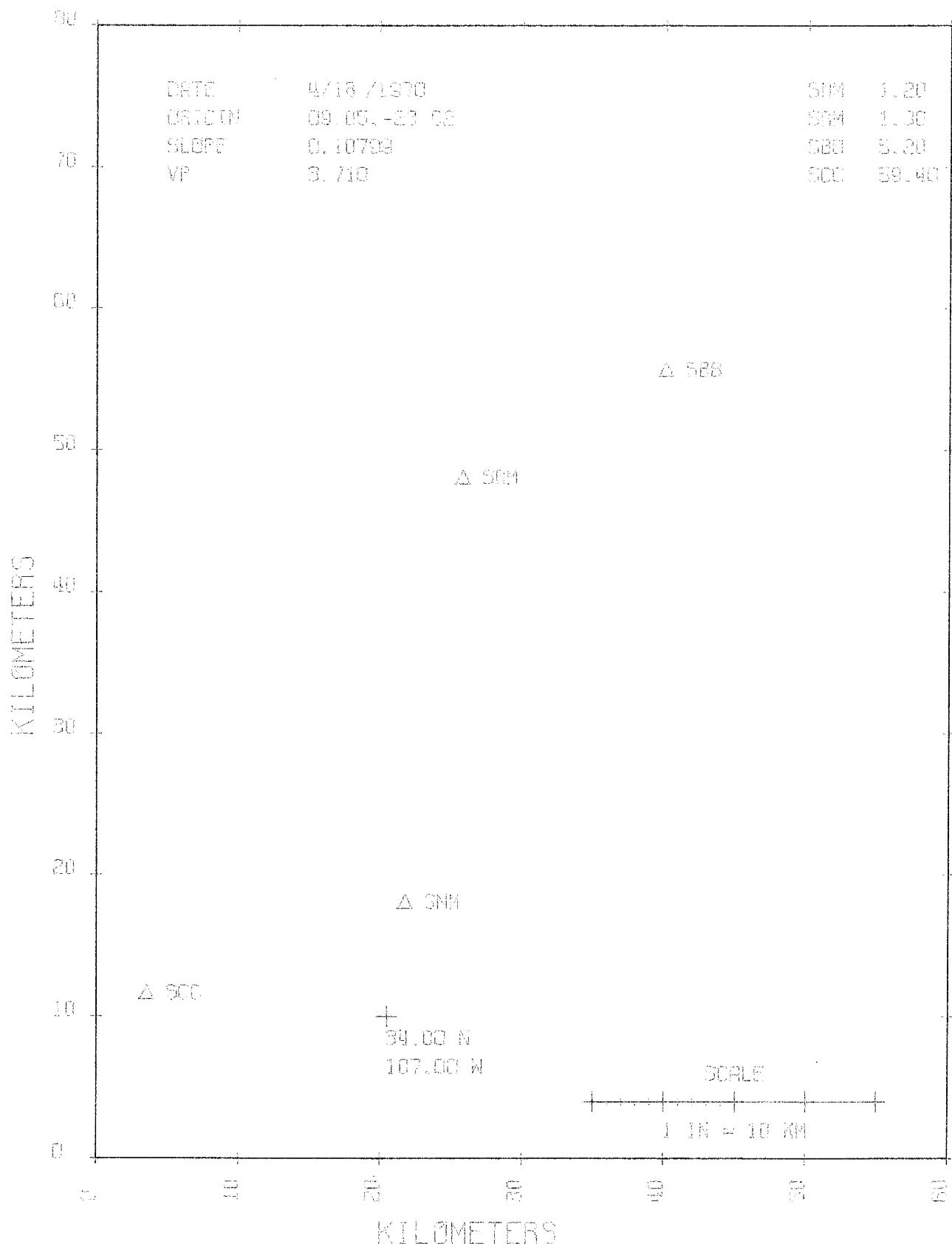


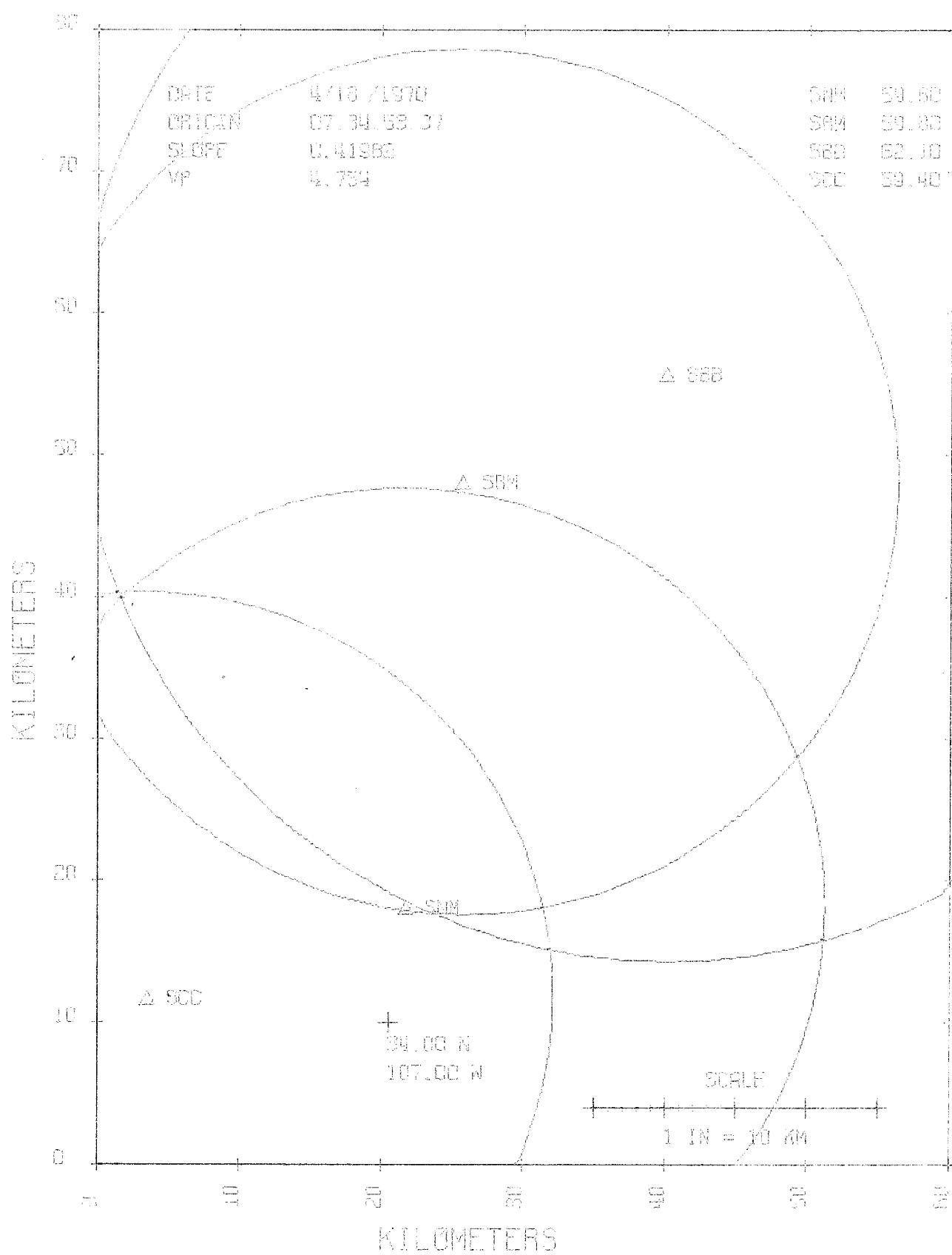


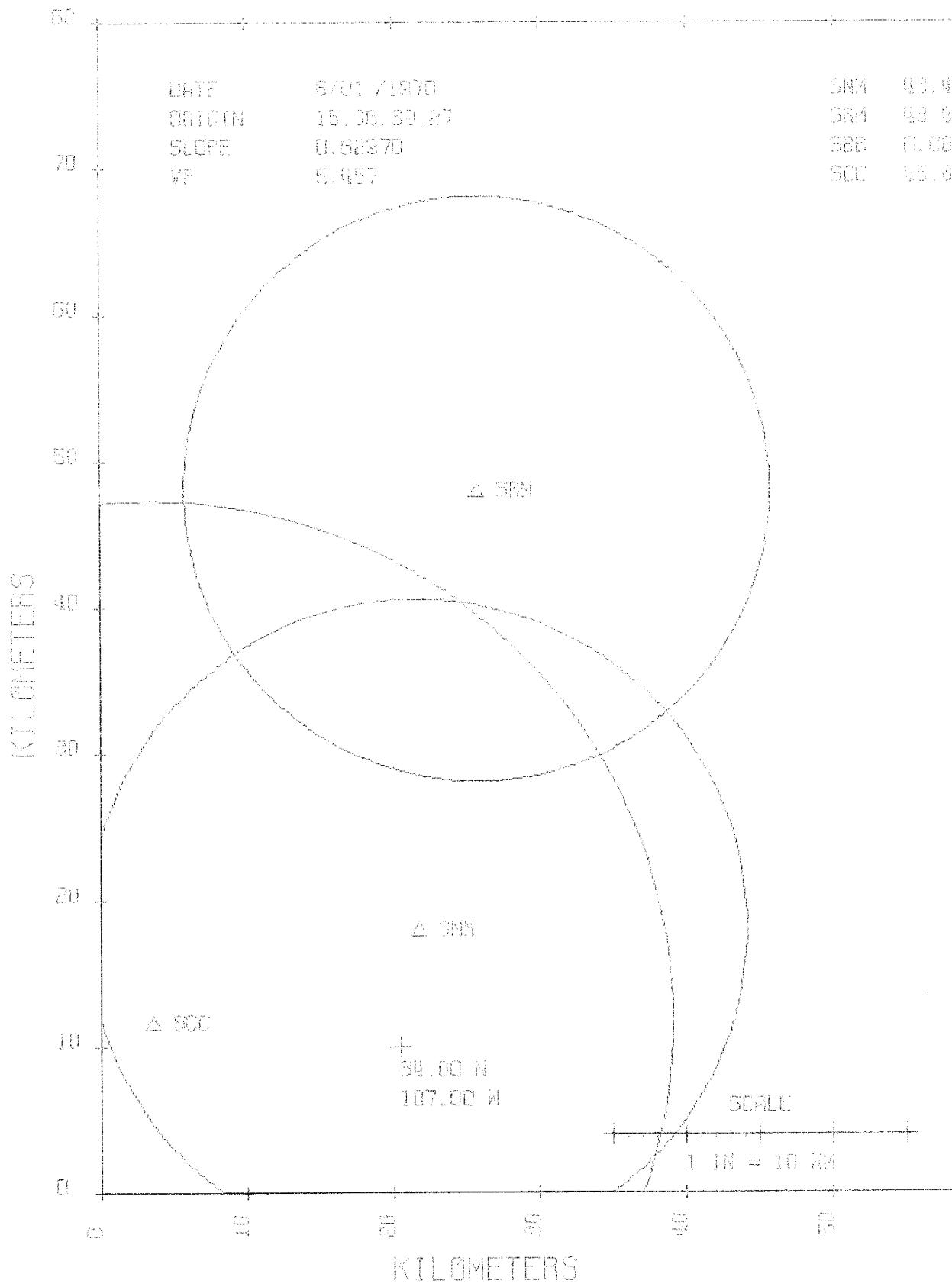


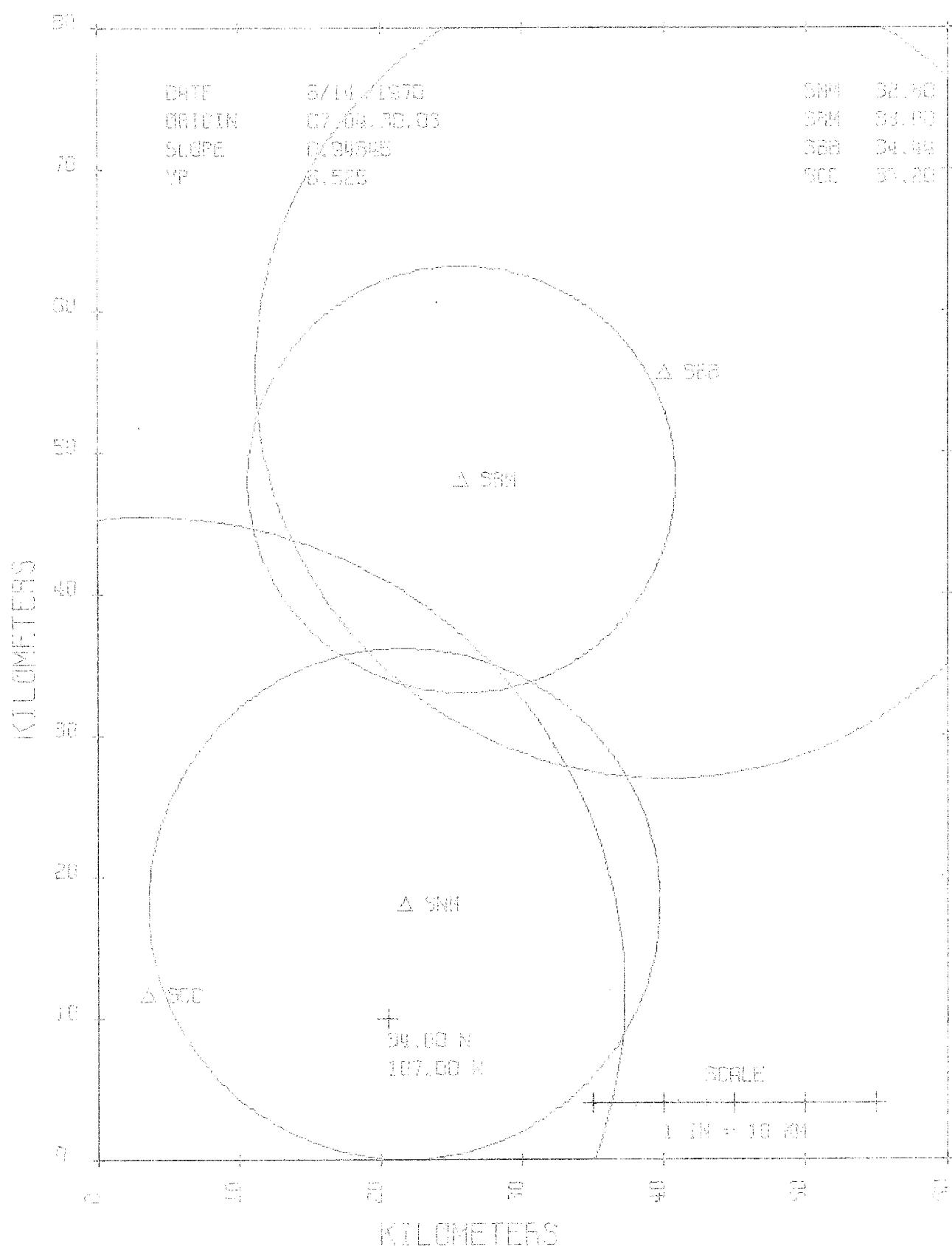


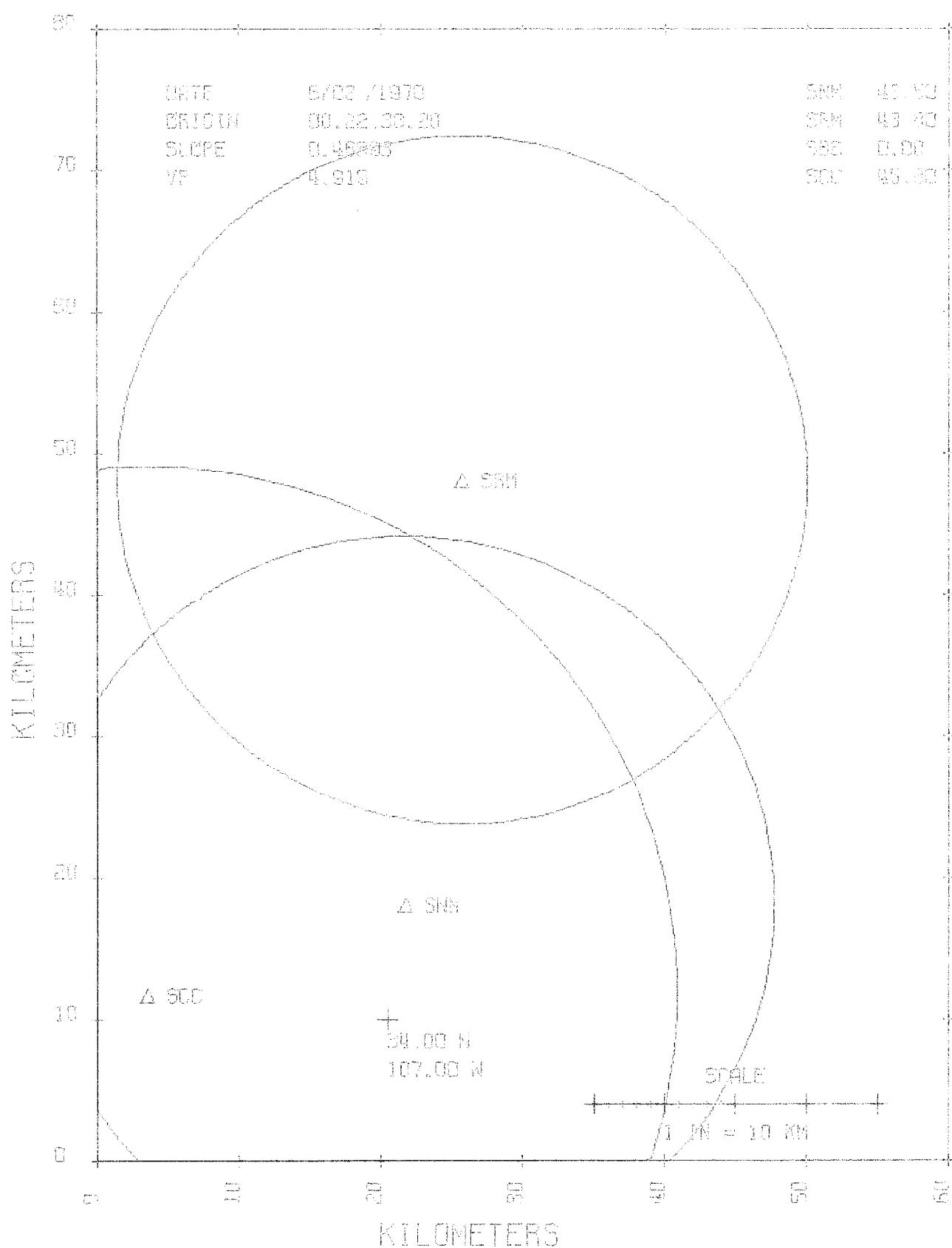


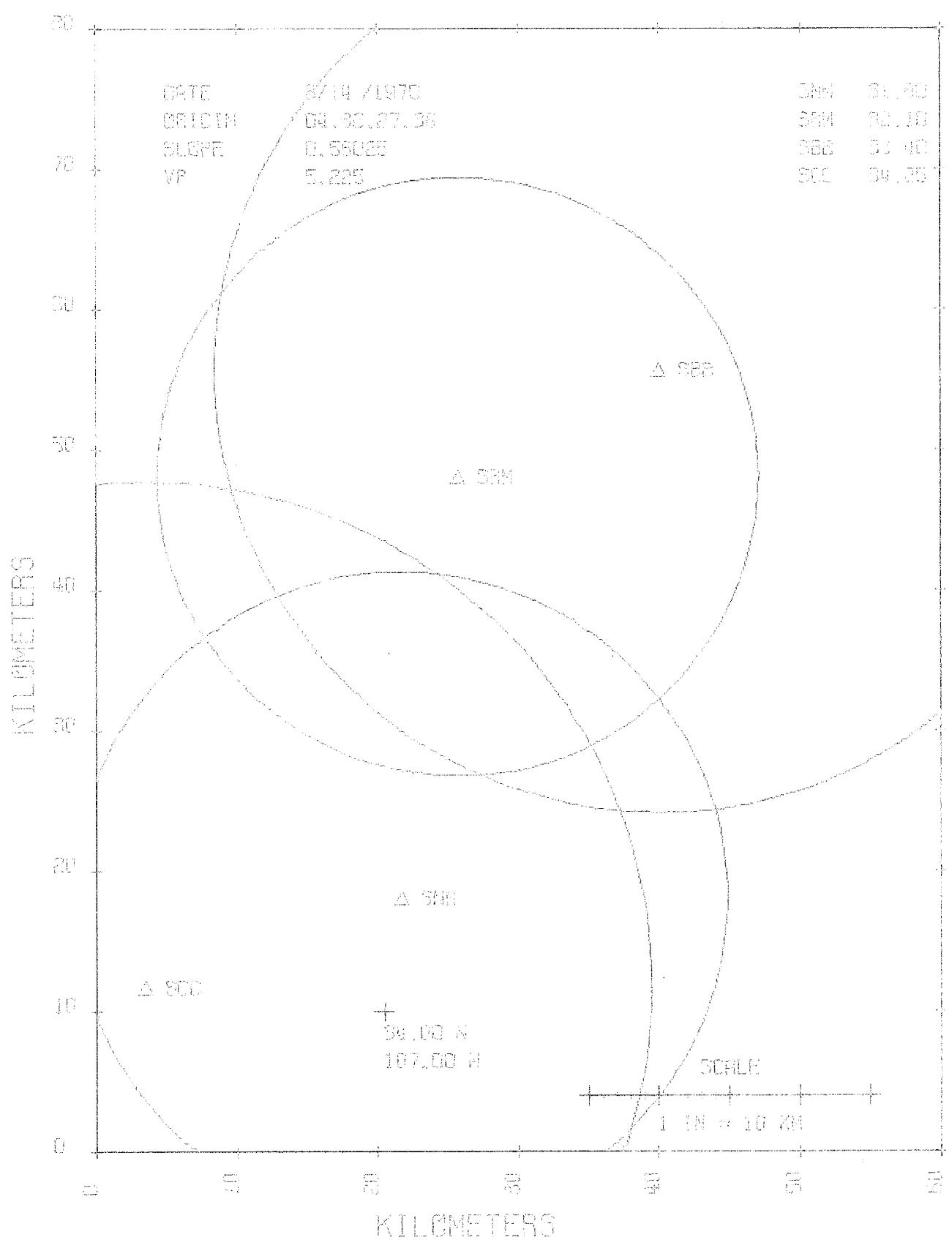


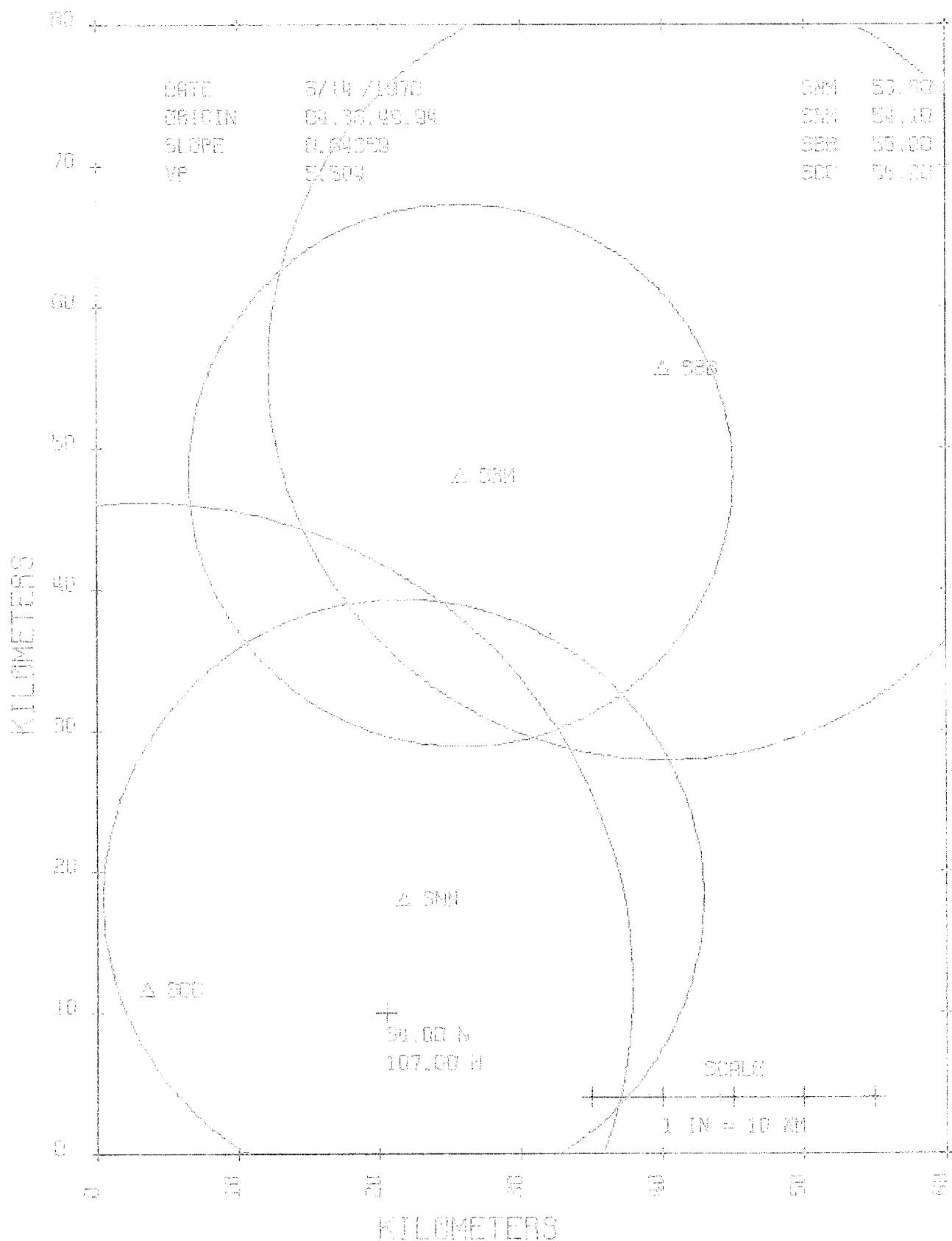


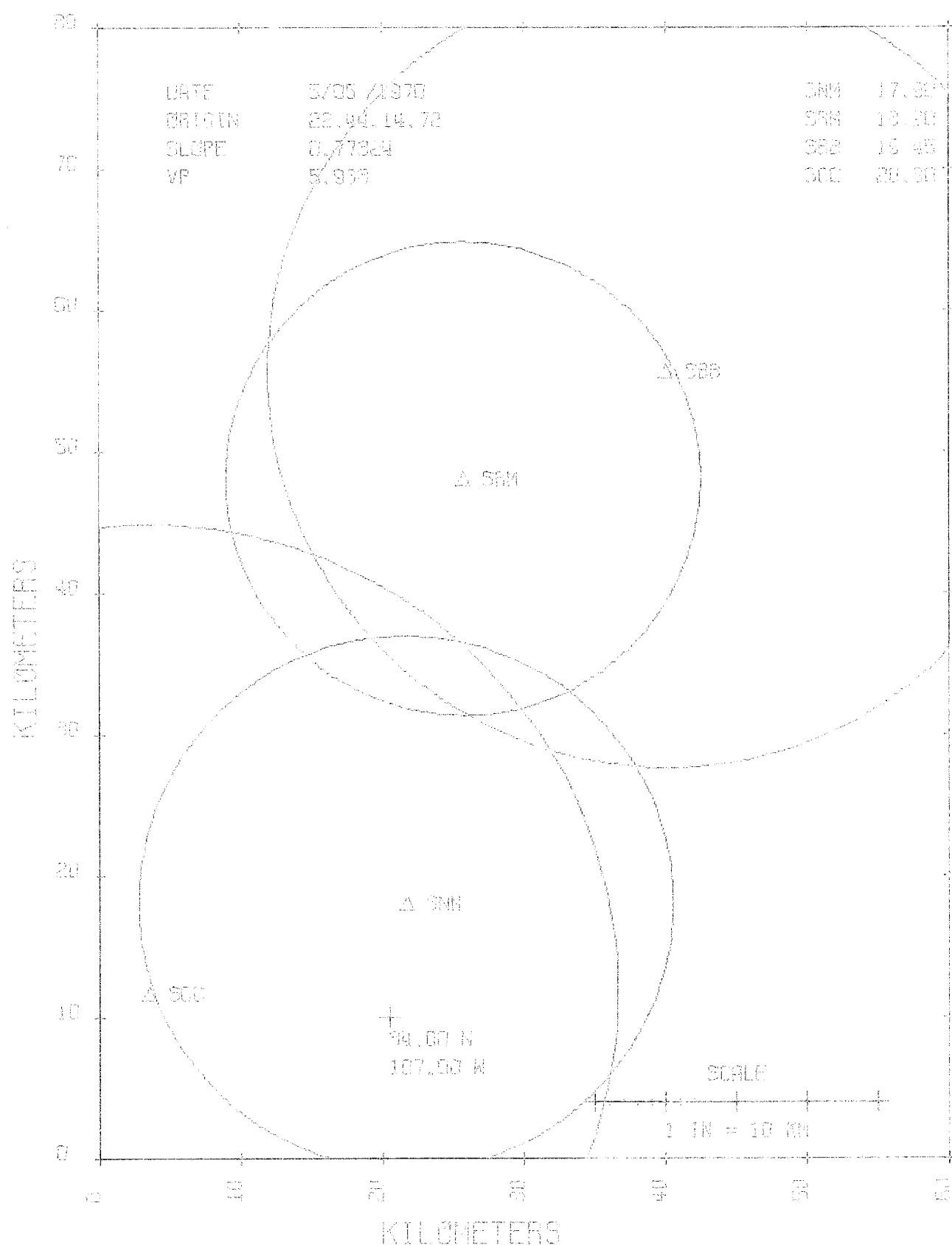


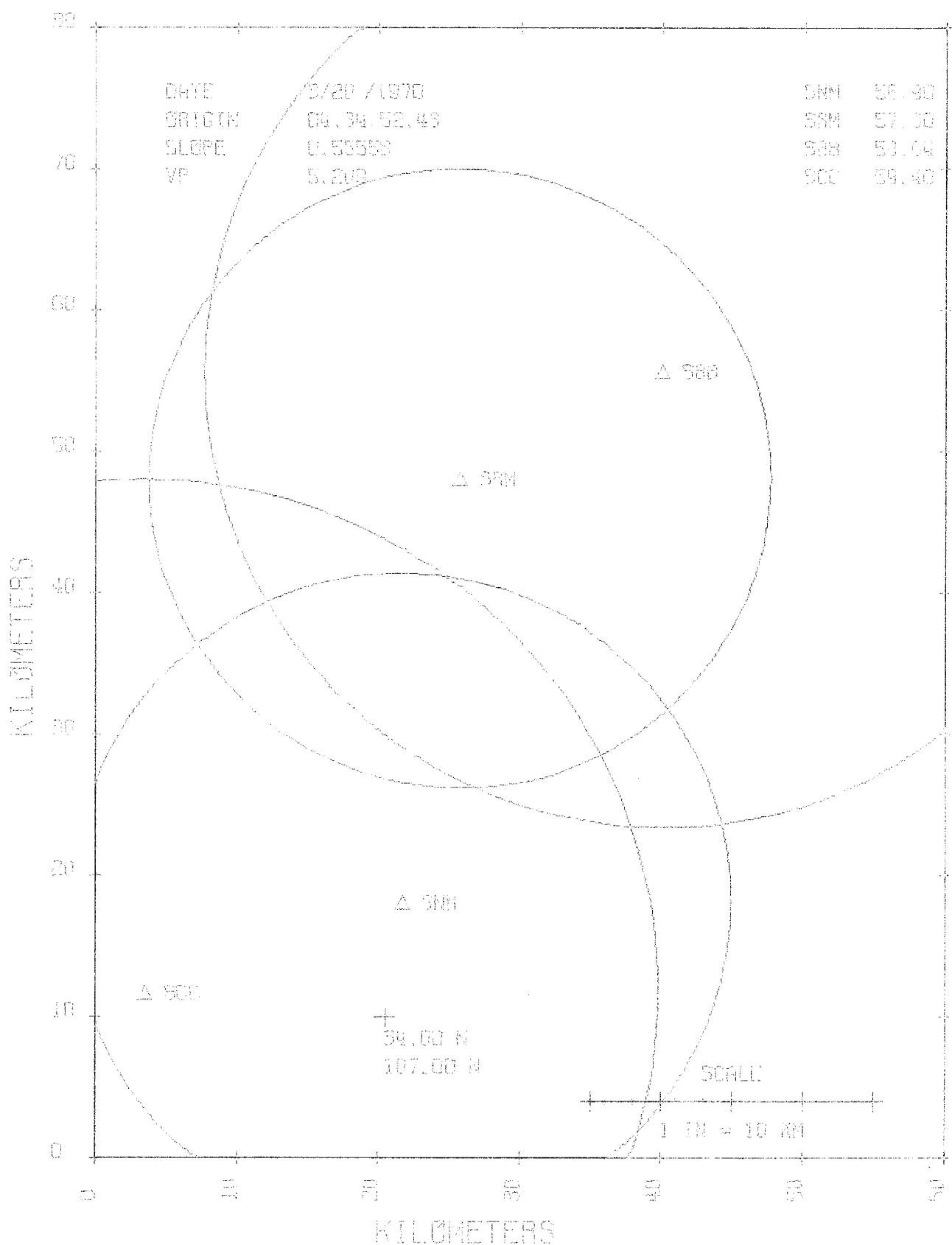


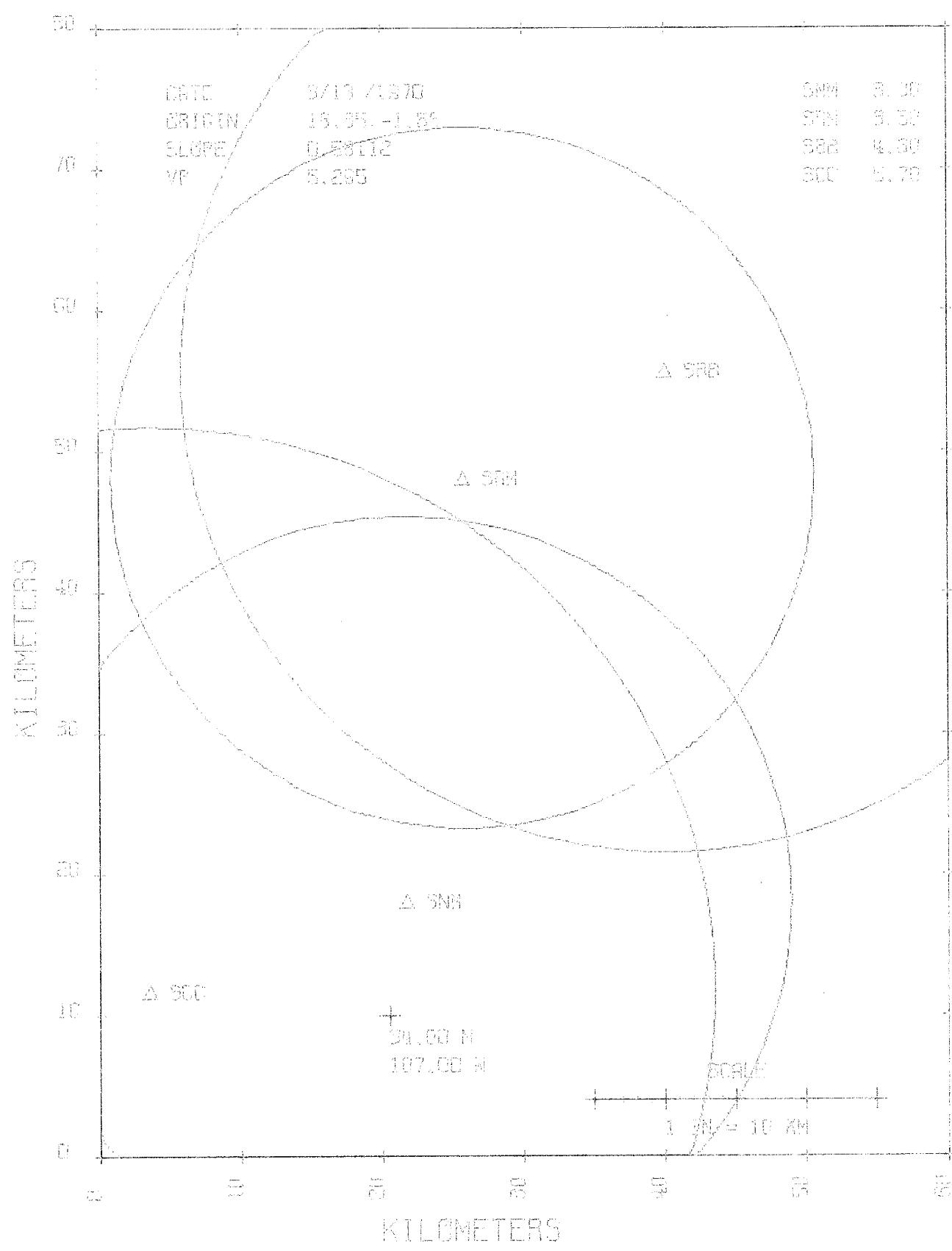


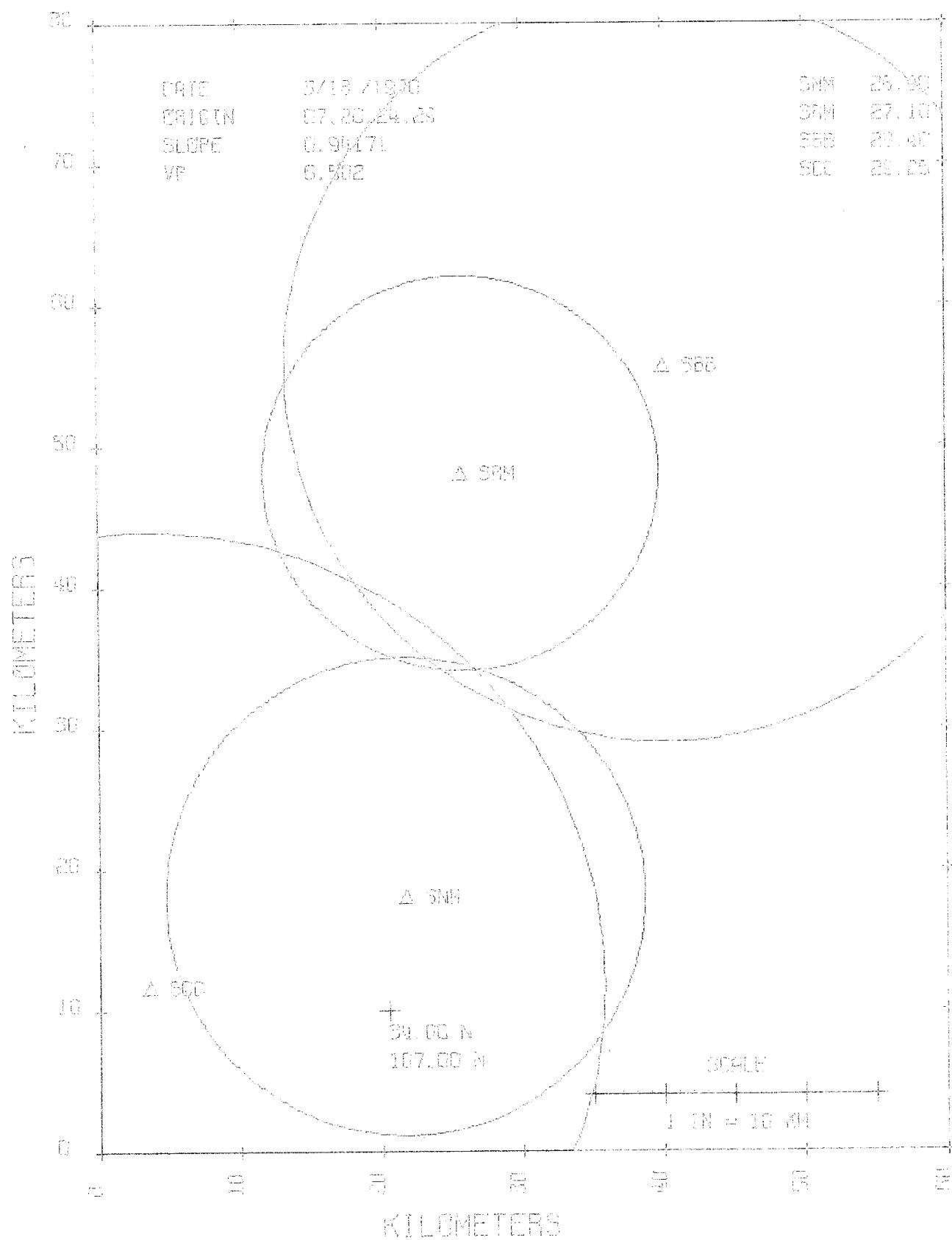


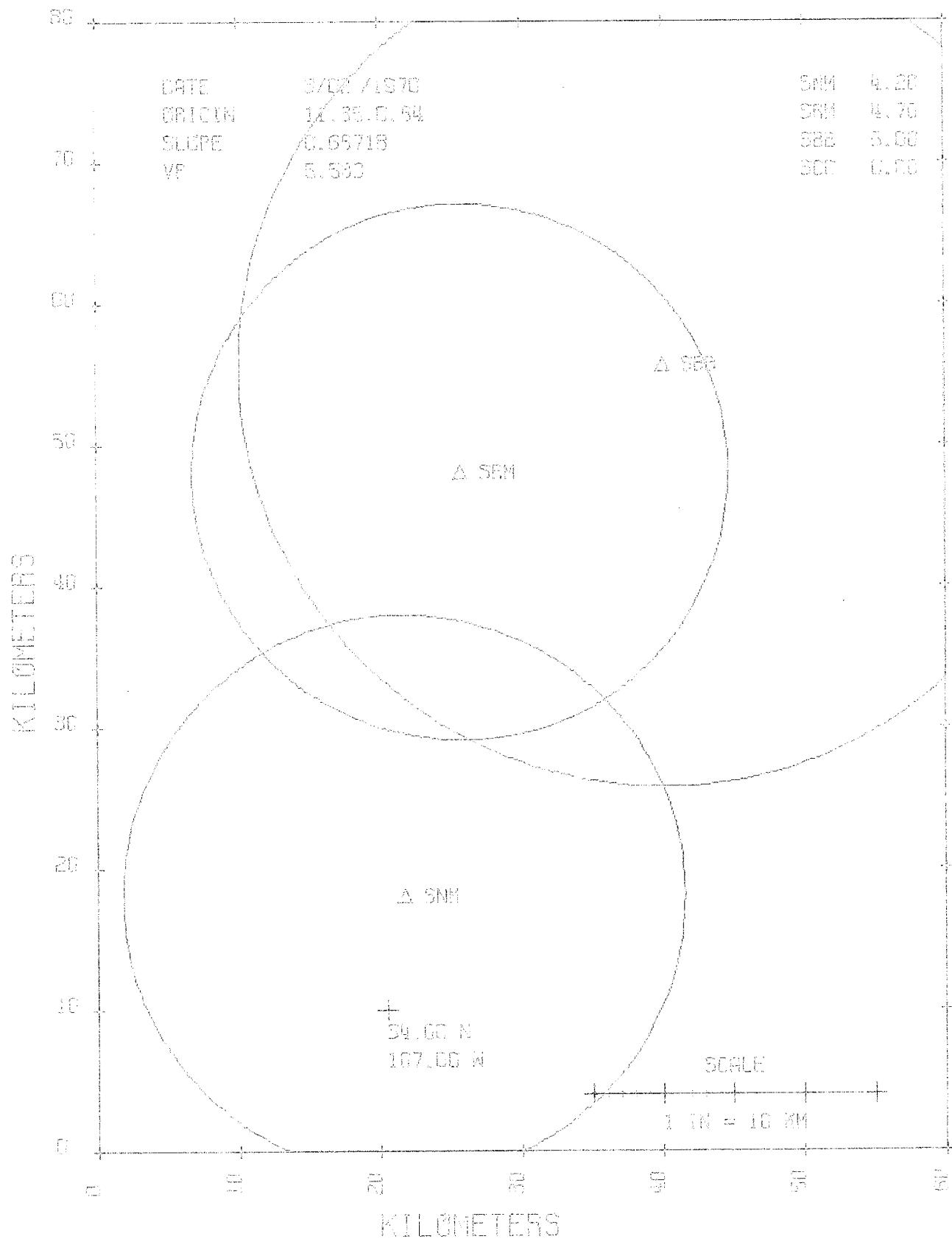


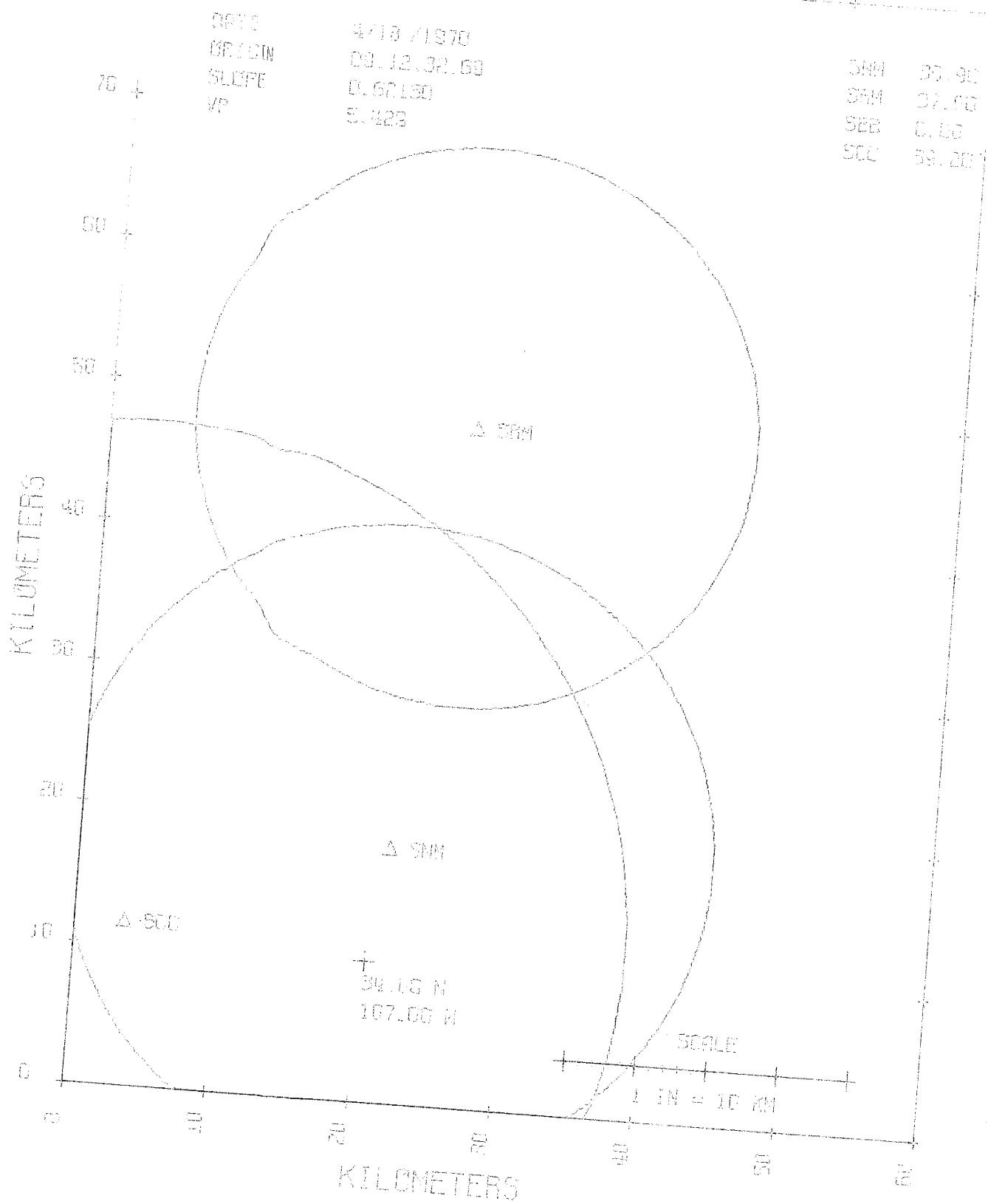


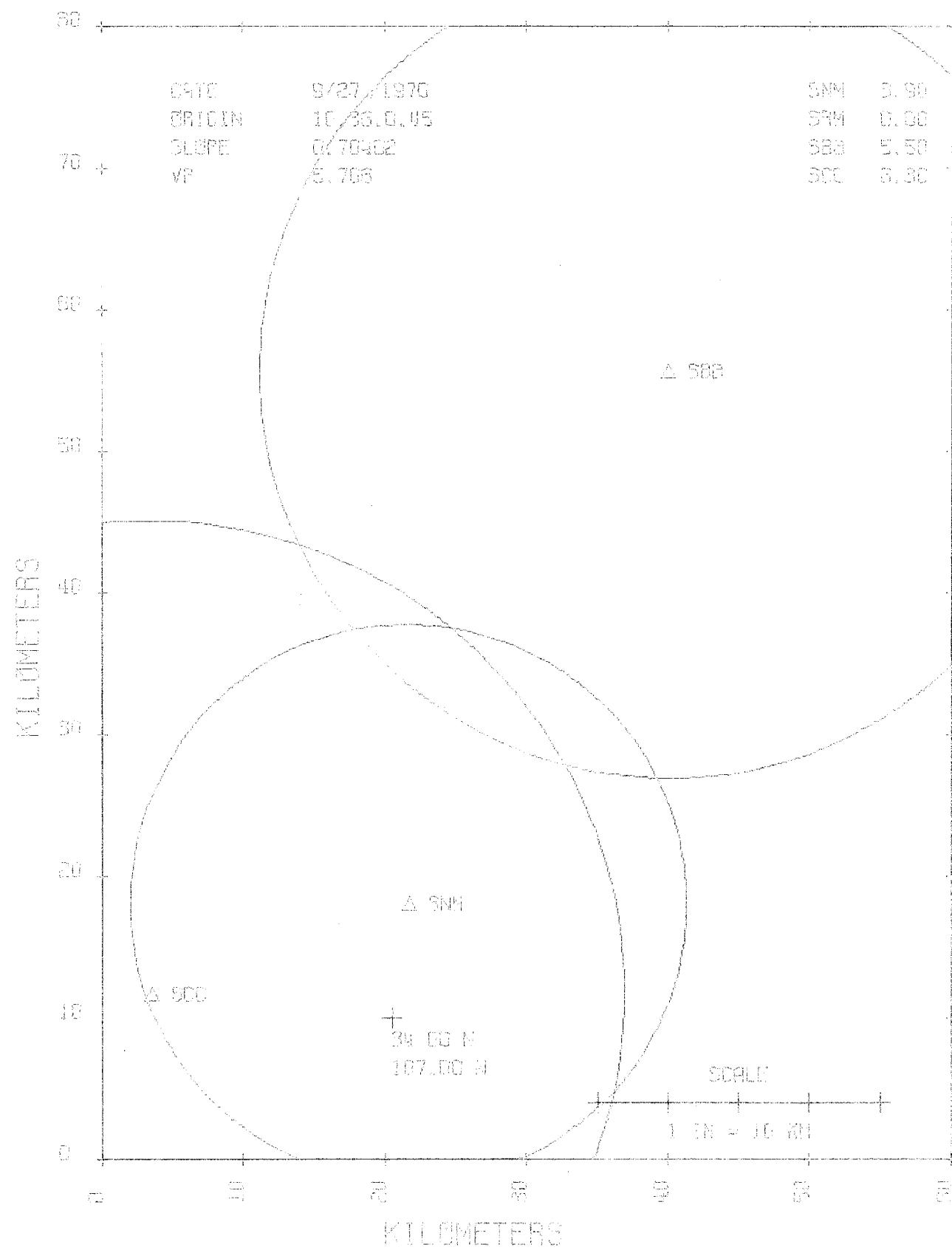


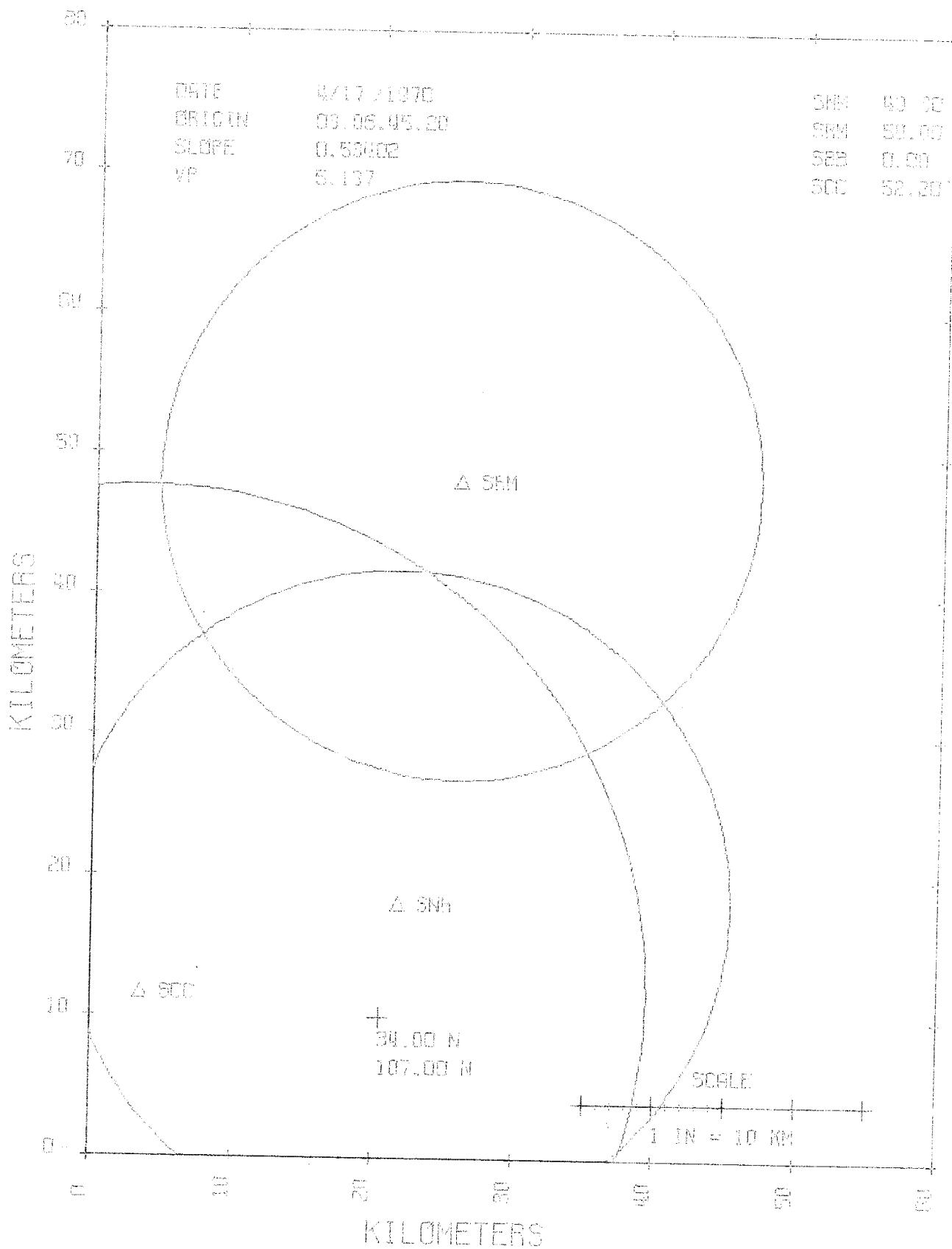


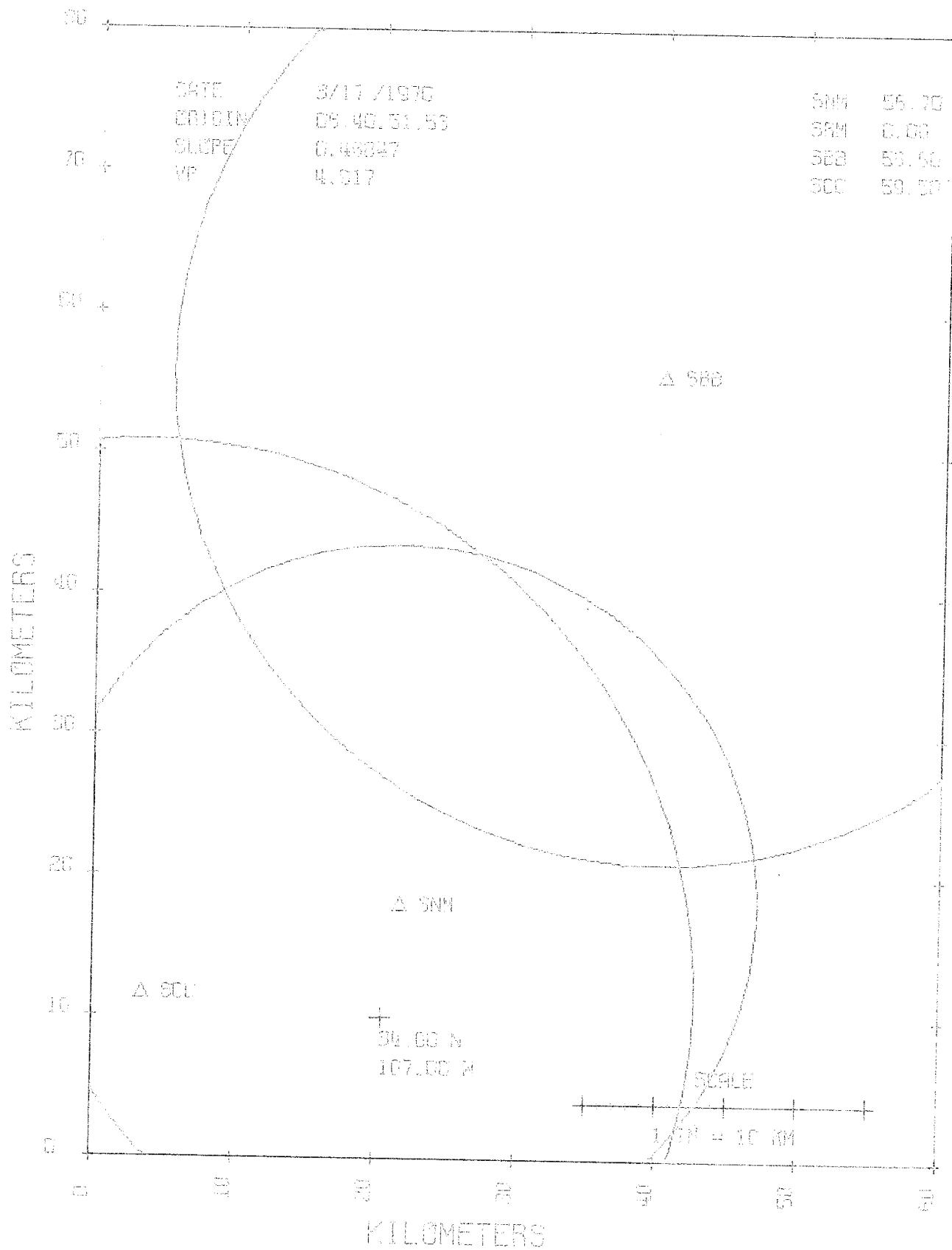










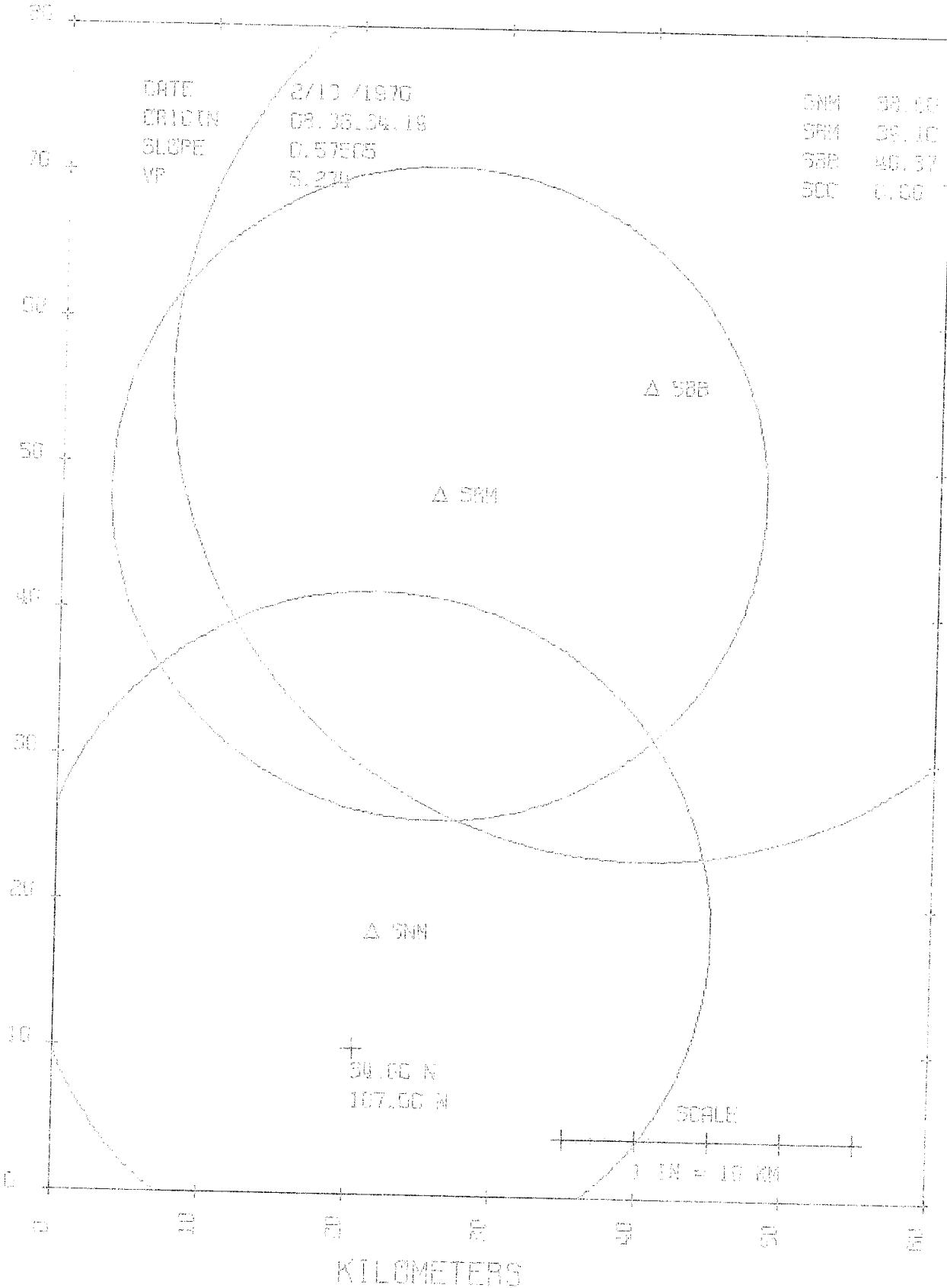


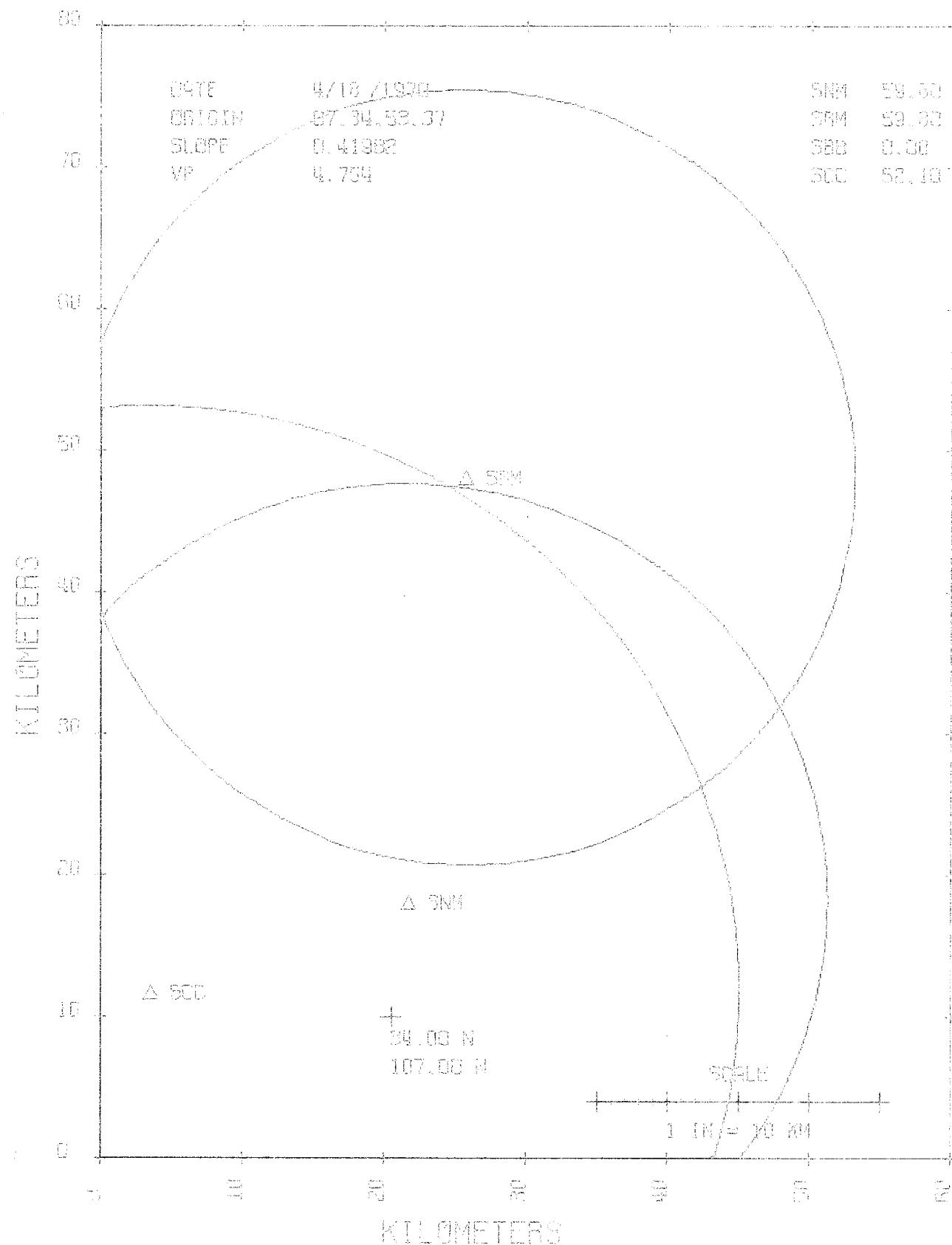
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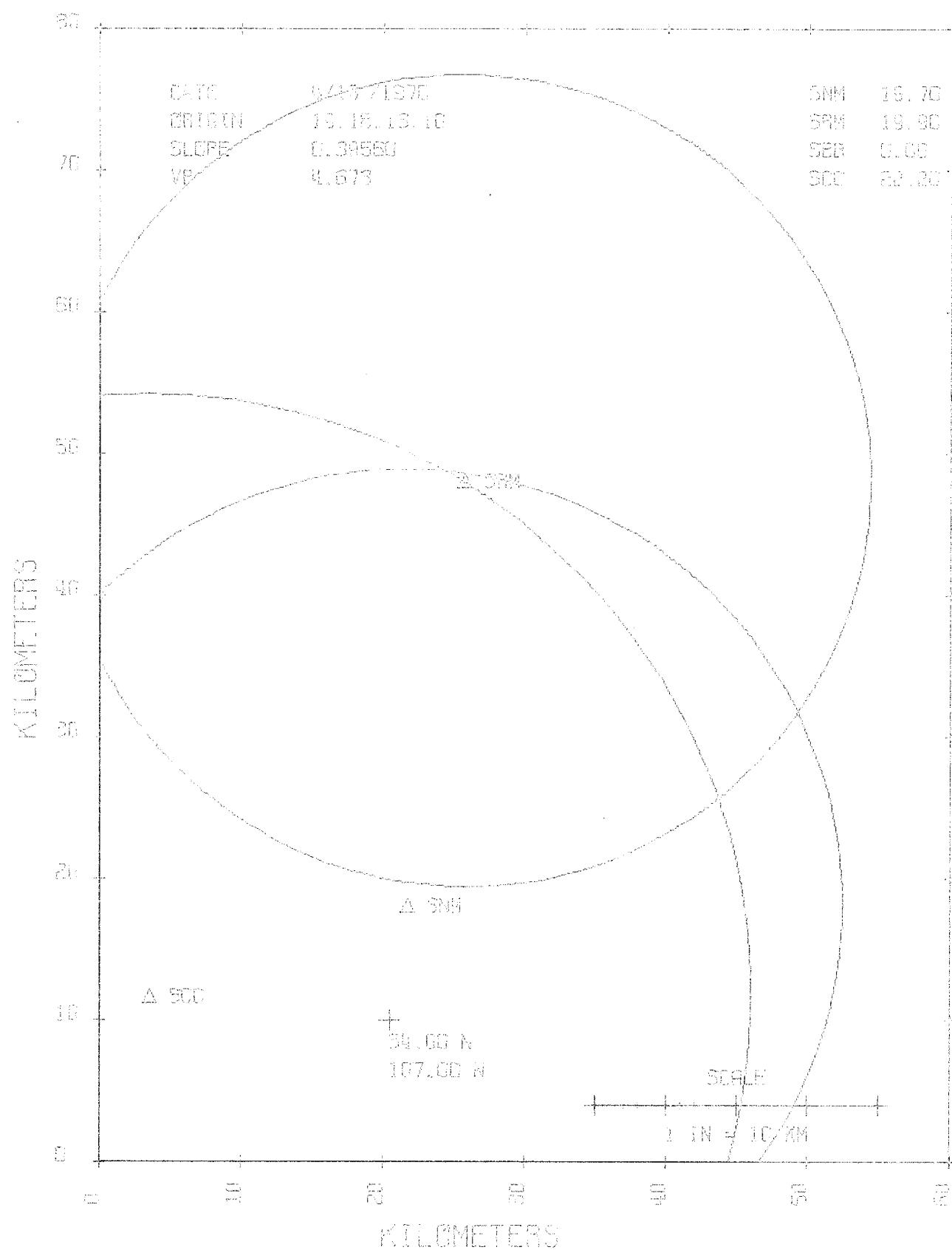
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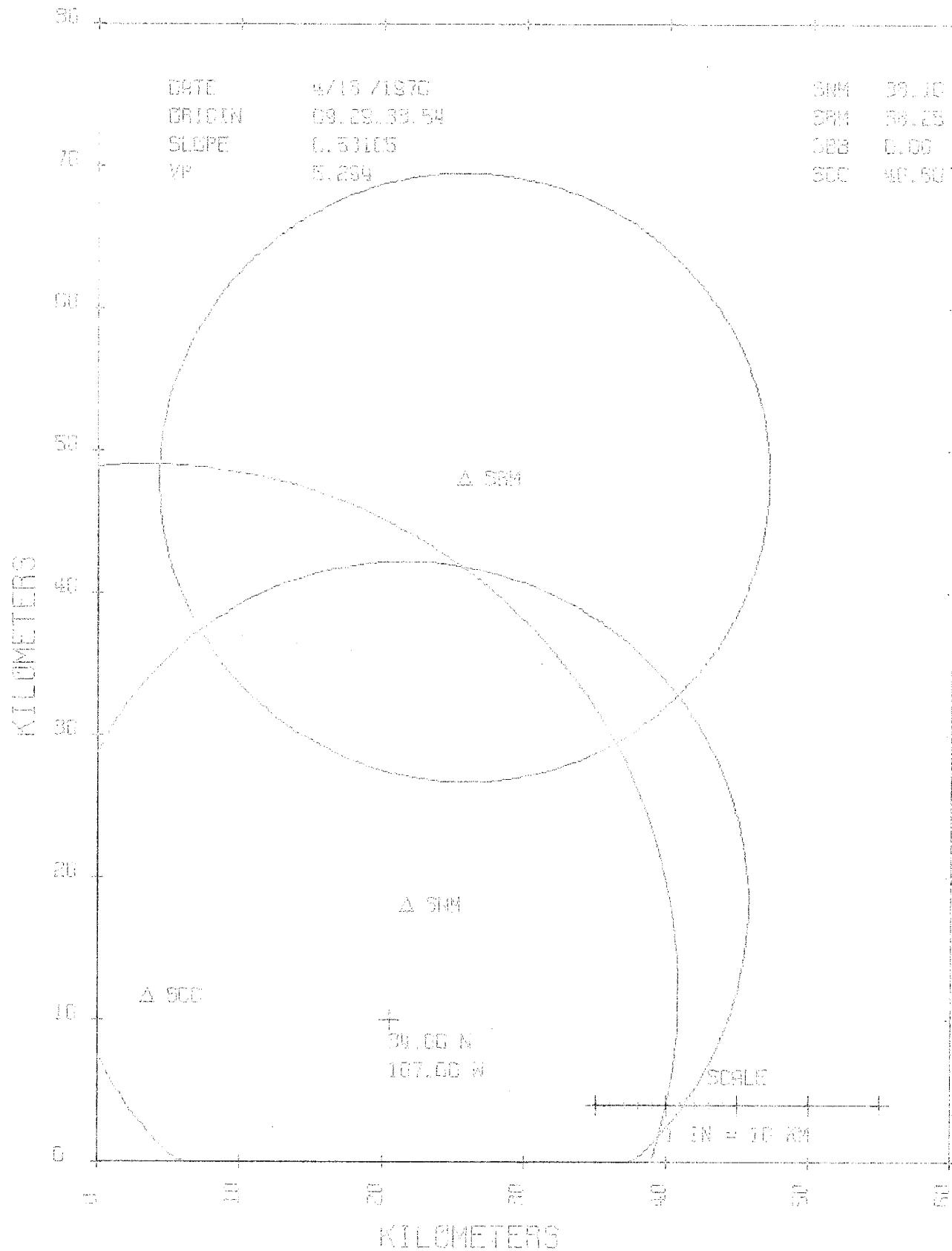
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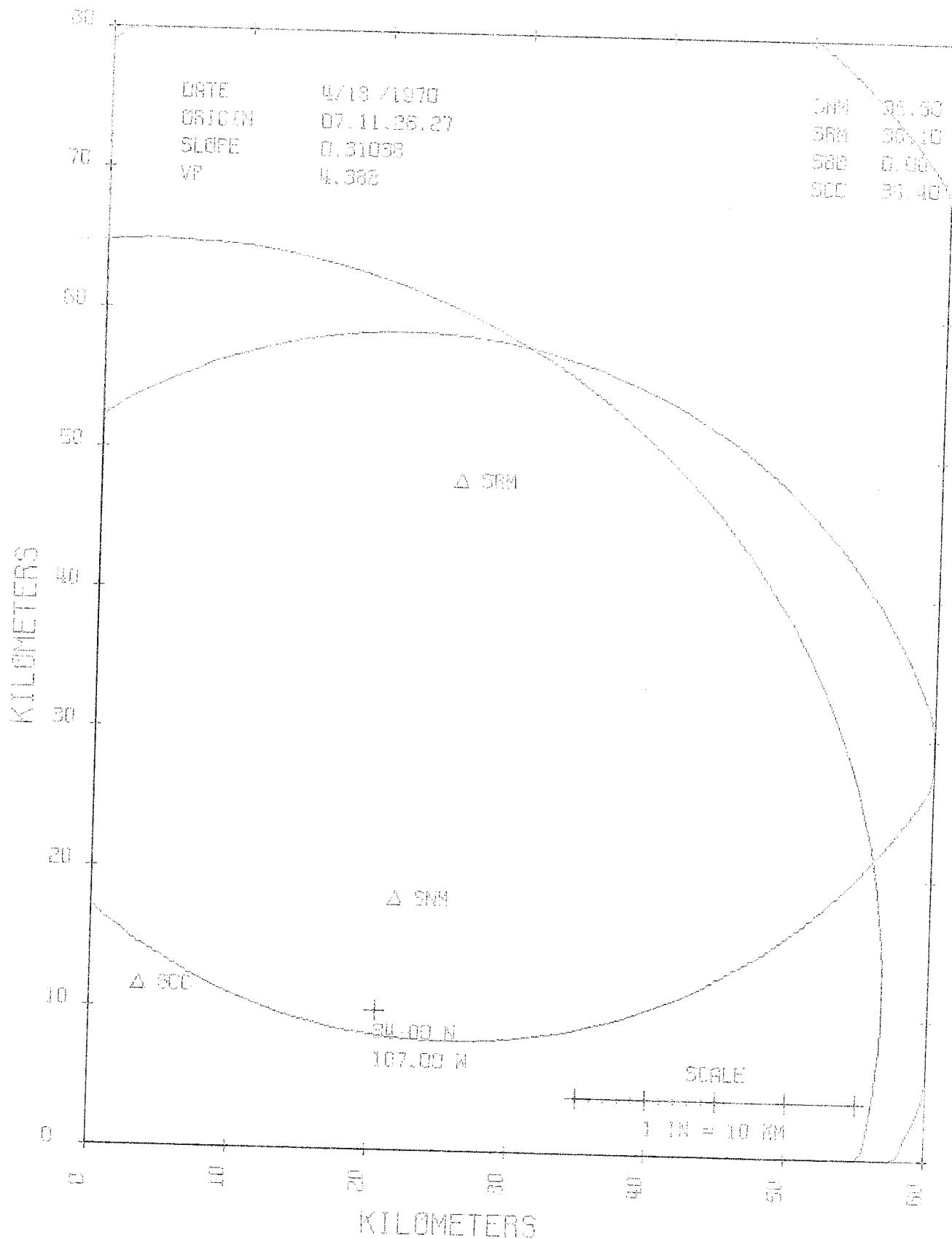
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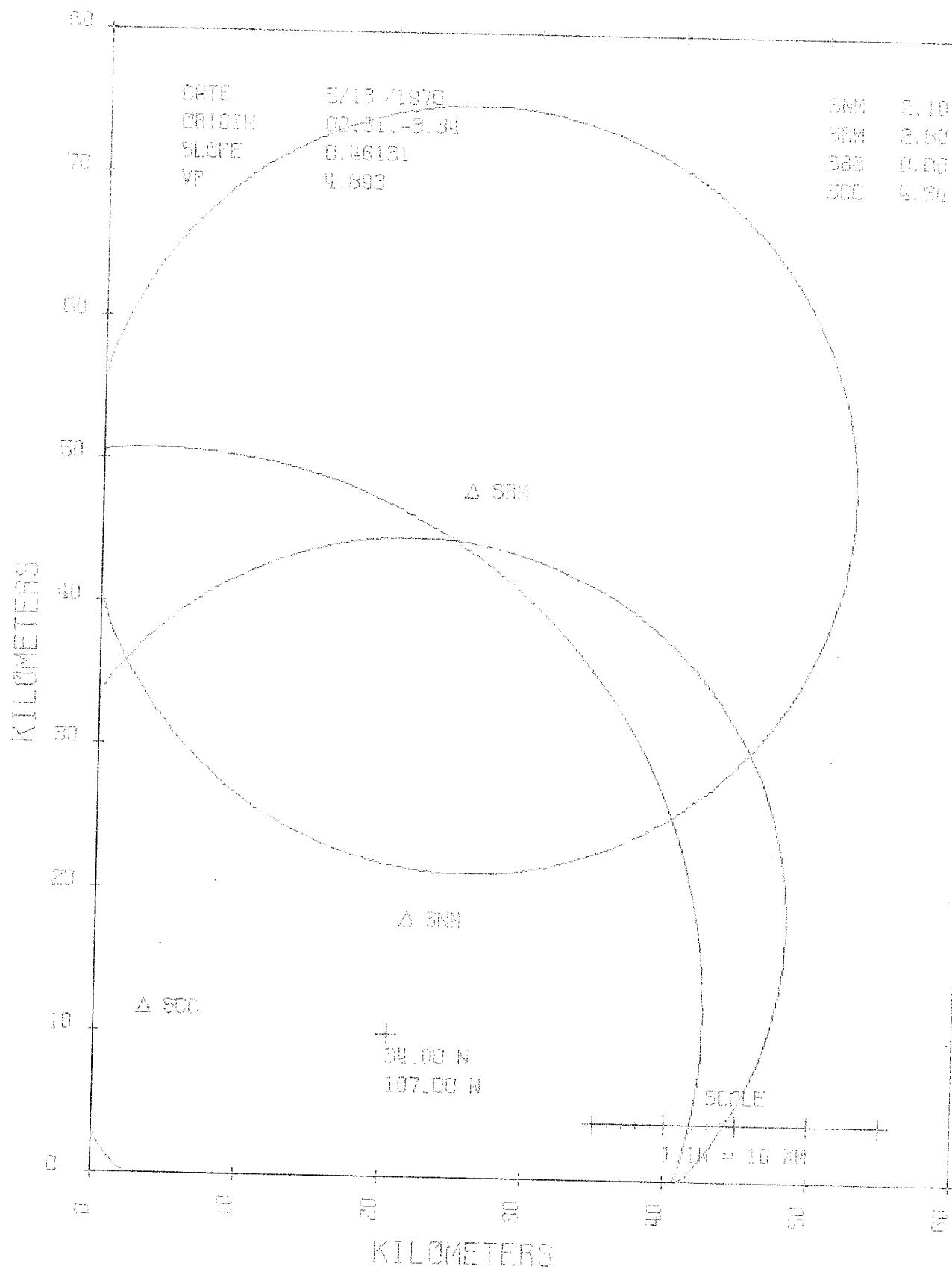


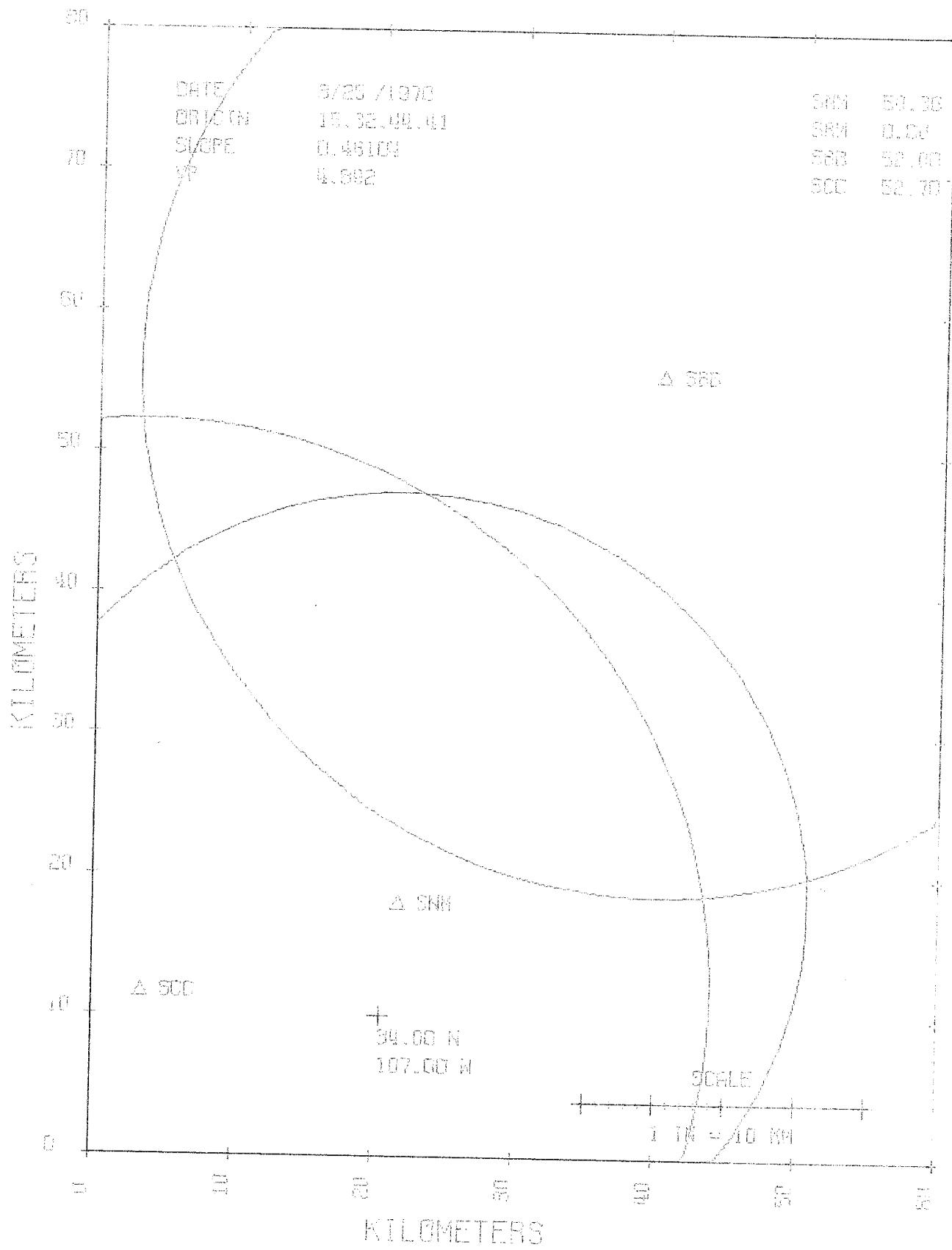


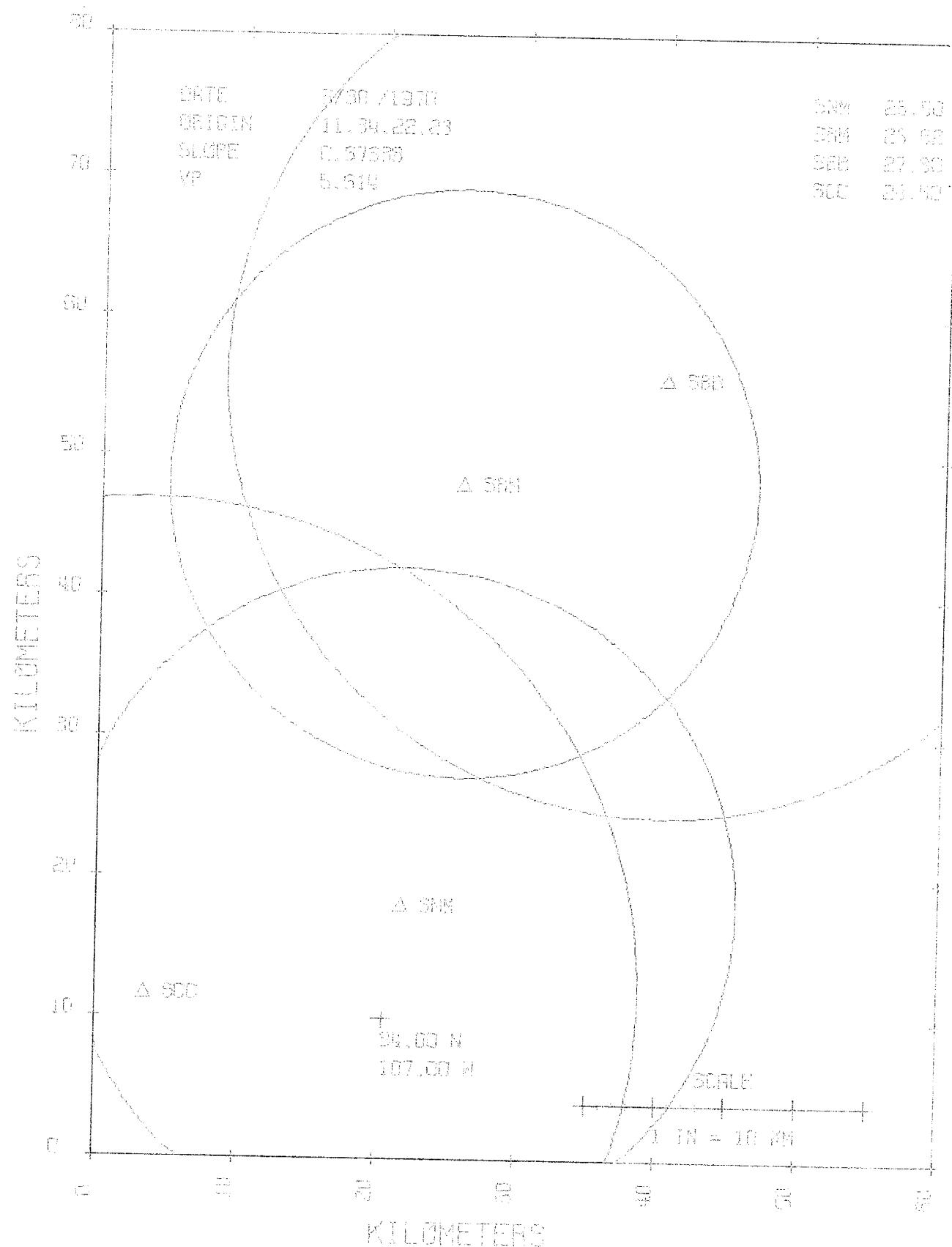


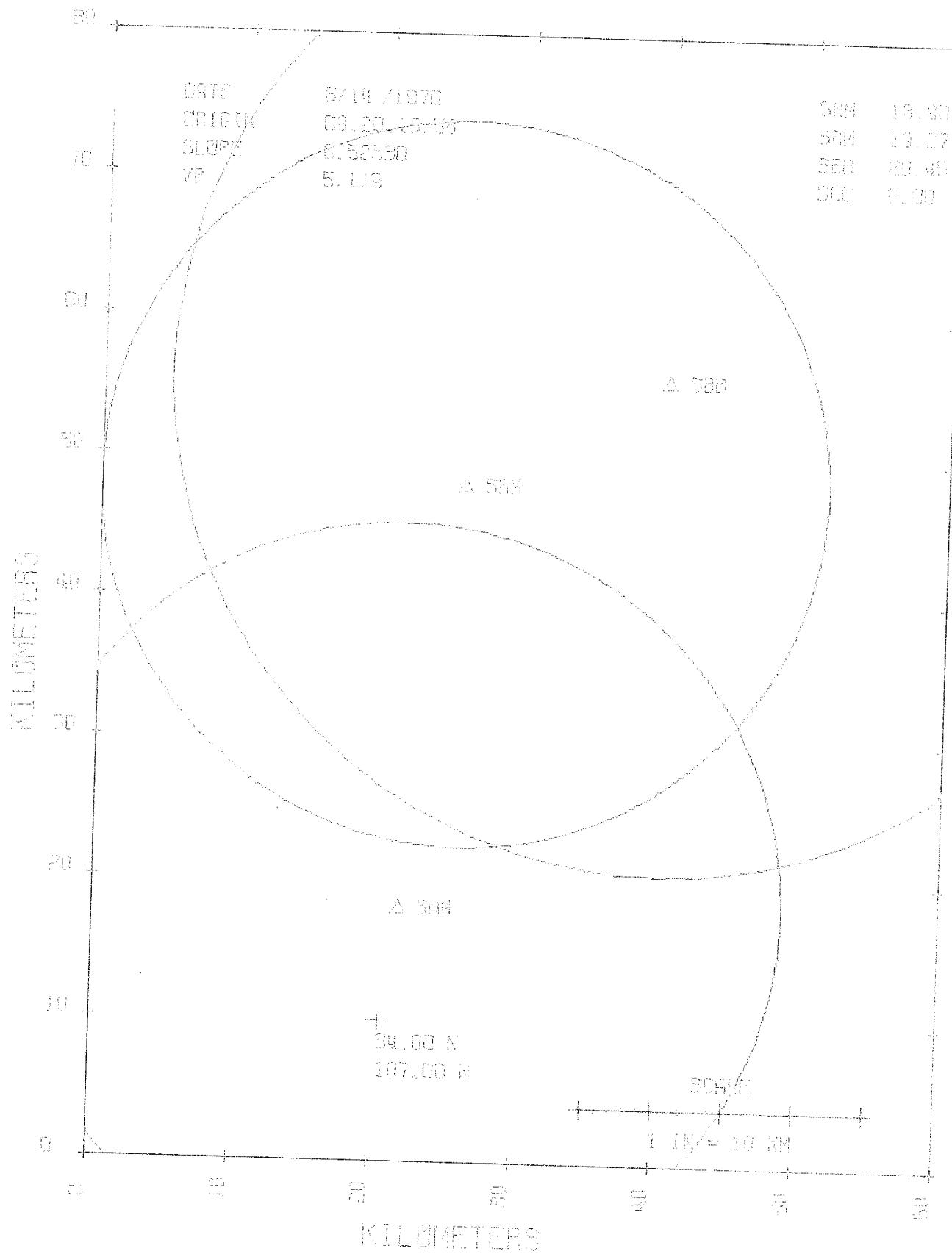


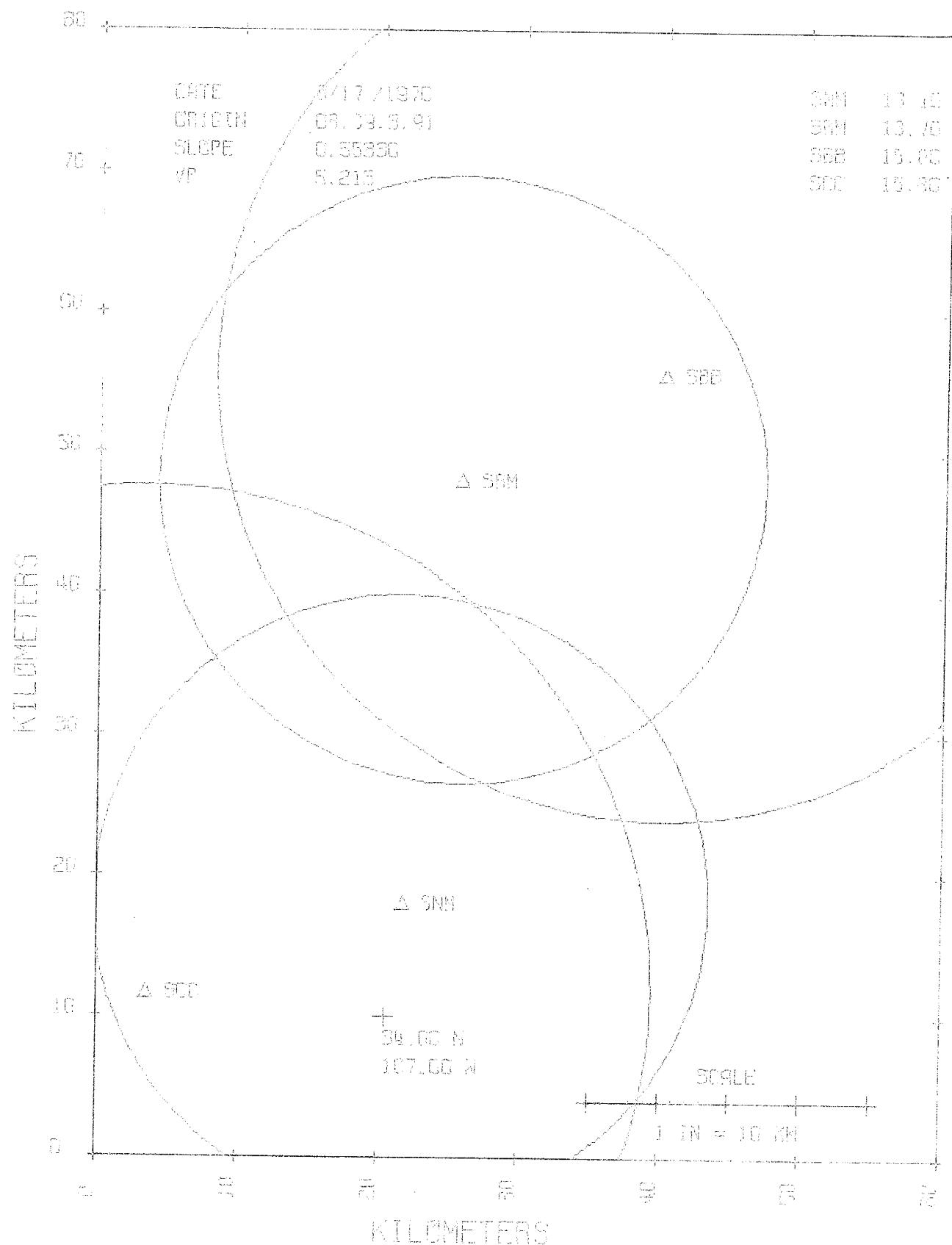


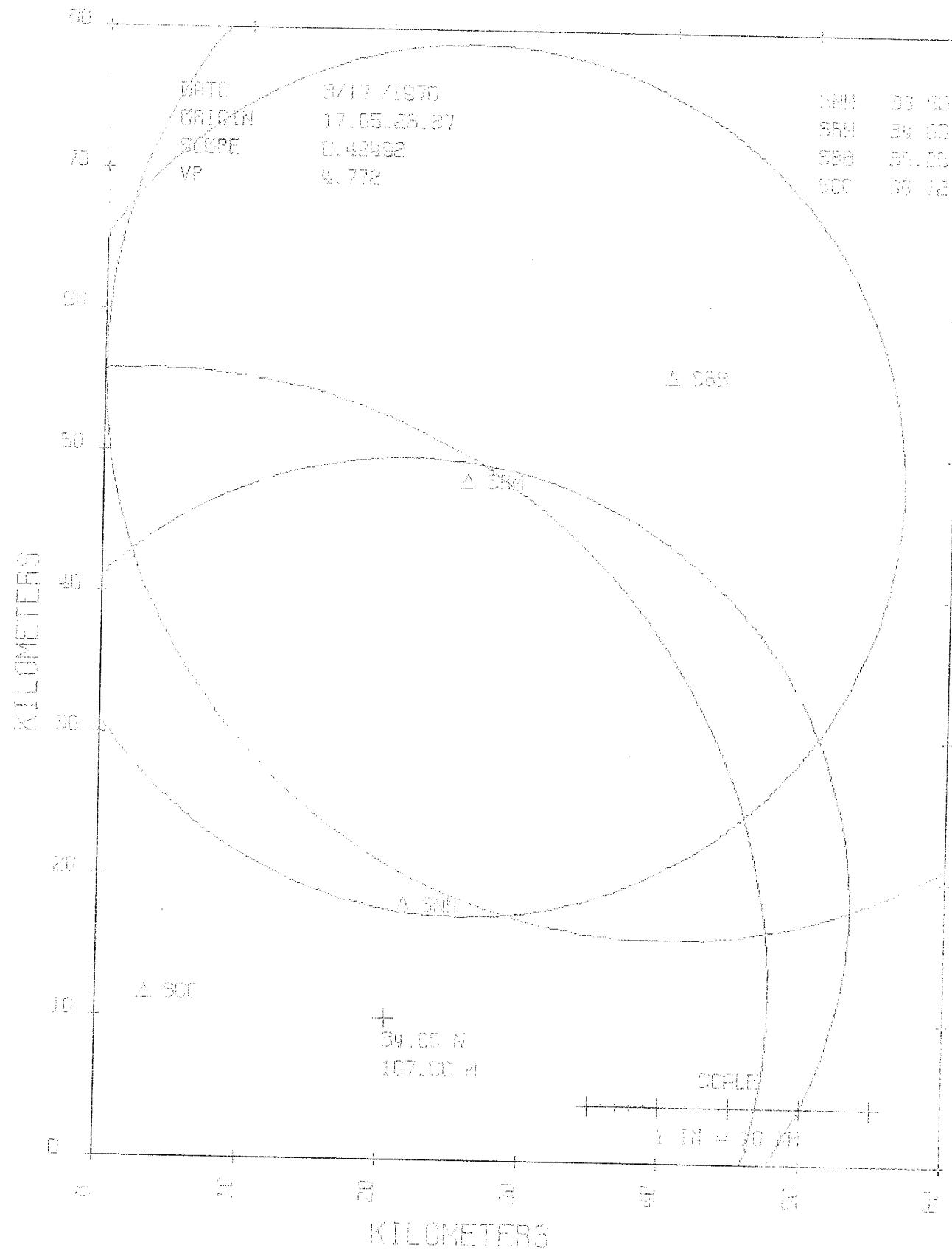


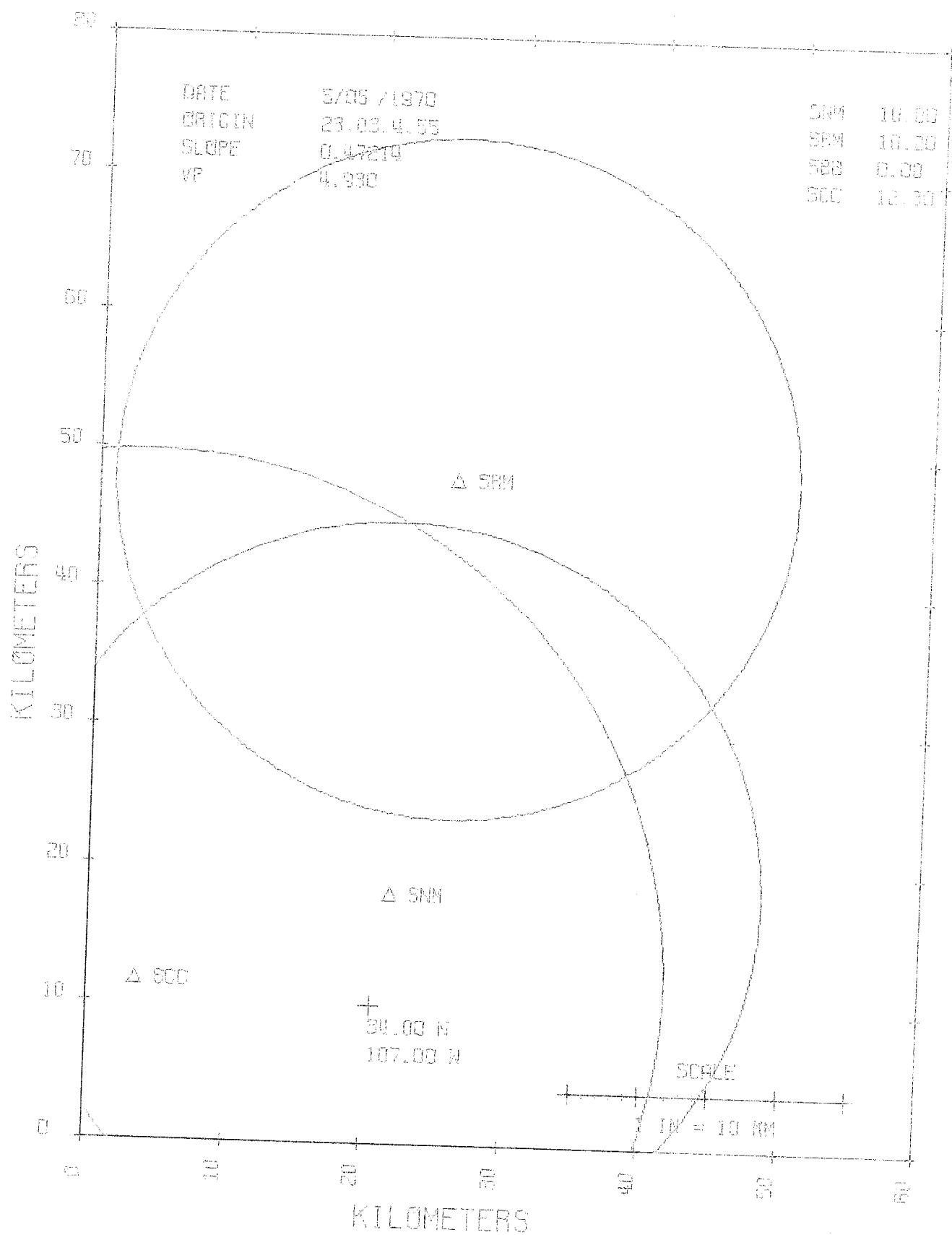


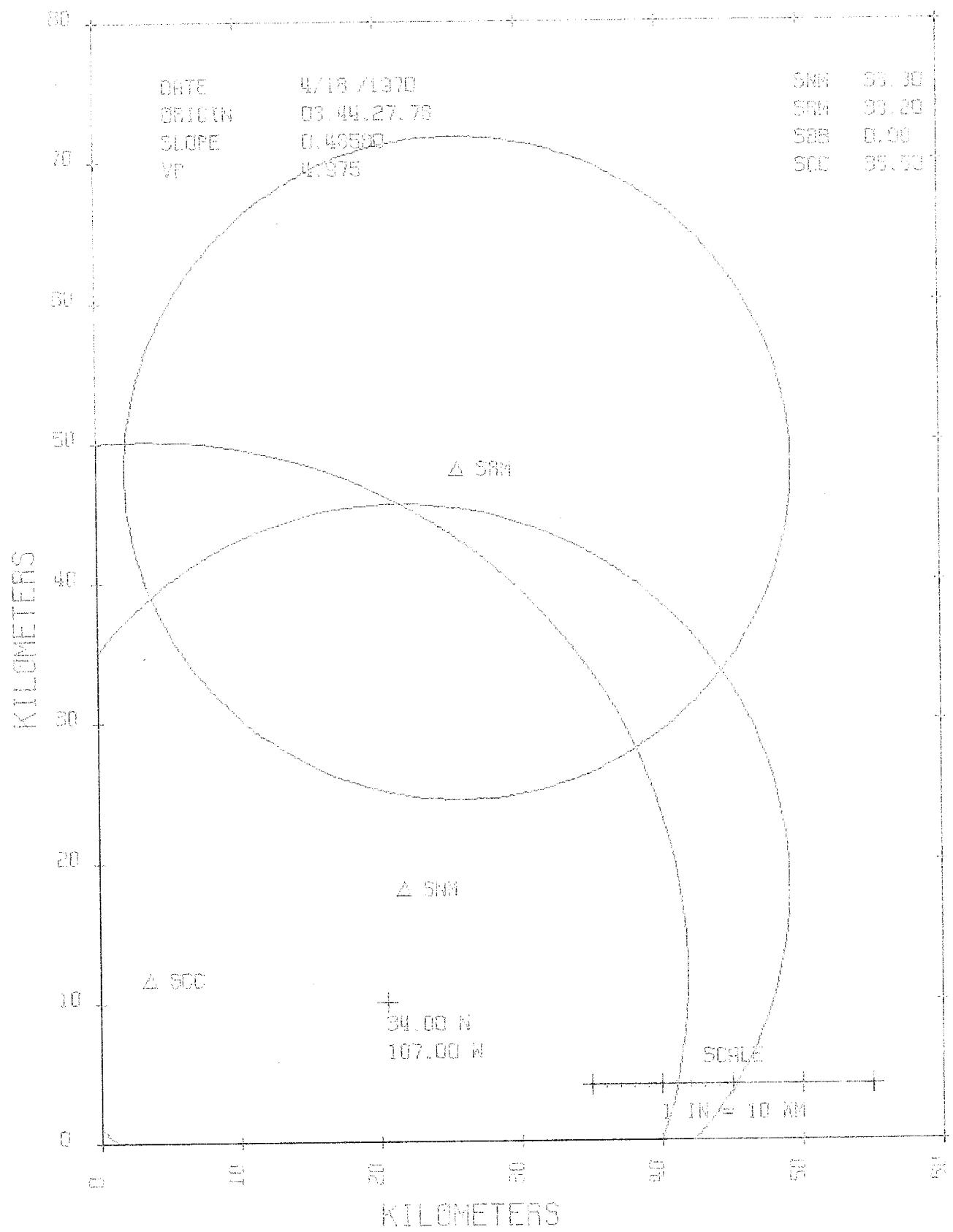












| CLASS I EVENTS | | | | CLASS II EVENTS | | | |
|----------------|-------|-----------|-------|-----------------|-------|-----------|-------|
| Date | Time | Magnitude | log A | Date | Time | Magnitude | log A |
| 1969 | | C.T.I | LRSM | 1970 | | C.T.I | LRSM |
| June 14 | 02:35 | -0.3 | 0.60 | May 5 | 22:44 | 0.14 | 1.21 |
| June 27 | 09:35 | -0.1 | 0.78 | May 5 | 22:44 | 0.21 | 1.34 |
| July 7 | 08:58 | -0.74 | 0.60 | May 5 | 23:03 | -0.32 | 0.78 |
| July 7 | 09:03 | -0.14 | 0.85 | May 11 | 08:07 | 0.15 | 1.00 |
| July 7 | 11:25 | -0.43 | 0.60 | May 13 | 02:31 | Sat. | 1.0 |
| July 12 | 04:05 | 0.2 | 1.00 | June 1 | 12:23 | -0.16 | 0.70 |
| July 18 | 04:07 | 0.6 | 0.50 | June 1 | 15:36 | 0.03 | 0.78 |
| July 18 | 11:39 | -0.1 | 0.78 | June 1 | 22:17 | Sat. | 0.65 |
| July 18 | 02:34 | 0.05 | 0.78 | June 2 | 00:22 | -0.02 | 0.81 |
| July 19 | 05:50 | -0.23 | 0.78 | June 2 | 12:24 | -0.29 | 0.48 |
| July 30 | 10:47 | 0.2 | — | June 7 | 09:14 | -0.48 | 0.30 |
| Aug. 9 | 02:34 | -0.5 | 0.40 | June 14 | 04:31 | 0.28 | 0.30 |
| Aug. 15 | 04:41 | -0.35 | 0.65 | June 14 | 04:36 | 0.30 | 1.35 |
| Sept. 9 | 13:12 | 0.12 | 1.18 | June 14 | 04:36 | 0.28 | 1.53 |
| Sept. 9 | 15:10 | 0.18 | 0.88 | June 16 | 16:50 | 0.29 | 1.51 |
| Oct. 4 | 17:30 | 0.21 | 1.37 | June 17 | 18:52 | -0.02 | 0.84 |
| Oct. 31 | 03:06 | 0.0 | 0.69 | June 23 | 01:33 | 0.22 | — |
| Nov. 7, 1970 | 13:35 | 0.27 | — | June 30 | 11:34 | 0.21 | 1.32 |
| Nov. 11 | 20:40 | -0.35 | 0.00 | | | | |
| Dec. 12 | 05:17 | 0.05 | 0.78 | | | | |
| Dec. 13 | 08:36 | 0.30 | 1.18 | | | | |
| Dec. 2 | 11:35 | -0.72 | 0.85 | | | | |
| Dec. 17 | 06:40 | 0.13 | — | | | | |
| Dec. 17 | 08:37 | -0.13 | 0.84 | | | | |
| Dec. 17 | 17:05 | 0.36 | 1.43 | | | | |
| Dec. 18 | 07:20 | 0.11 | 1.02 | | | | |
| Dec. 18 | 16:35 | 0.03 | 1.02 | | | | |
| Dec. 22 | 04:34 | 0.18 | 1.15 | | | | |
| Dec. 25 | 15:31 | Sat. | 2.10 | | | | |
| Dec. 28 | 09:02 | -0.24 | 0.48 | | | | |
| Dec. 30 | 02:15 | -0.10 | 0.60 | | | | |
| Jan. 13 | 06:29 | -0.34 | 0.48 | | | | |
| Jan. 17 | 03:06 | 0.26 | 1.08 | | | | |
| Jan. 18 | 03:14 | 0.30 | 1.21 | | | | |
| Jan. 18 | 07:11 | -0.25 | 0.40 | | | | |
| Jan. 18 | 07:34 | -0.24 | 0.96 | | | | |
| Jan. 18 | 09:05 | -0.24 | 1.34 | | | | |
| Jan. 18 | 09:12 | 0.23 | 1.34 | | | | |
| Jan. 18 | 09:29 | -0.24 | 0.30 | | | | |
| Jan. 18 | 19:18 | 0.30 | 1.32 | | | | |

| SWM | N | Magitude | N | ΣN | Log A | SRM |
|------|------|----------|------|------------|-------|-----|
| 2.10 | 1.00 | 0.50 | 0.40 | 1.23 | 0.44 | 0.7 |
| | 1.00 | 0.60 | 0.20 | 1.05 | 0.39 | 0.8 |
| | 1.6 | 0.30 | 0.10 | 1.29 | 0.34 | 1.2 |
| | 1.6 | 0.00 | 0.00 | 1.34 | 0.29 | 1.0 |
| | 1.6 | -0.10 | 0.10 | 1.44 | 0.24 | 0.9 |
| | 1.6 | -0.20 | 0.20 | 1.53 | 0.21 | 0.8 |
| | 1.6 | -0.30 | 0.30 | 1.55 | 0.19 | 0.7 |
| | 1.6 | -0.40 | 0.40 | 1.55 | 0.17 | 0.6 |
| | 1.6 | -0.50 | 0.50 | 1.55 | 0.15 | 0.5 |
| | 1.6 | -0.60 | 0.60 | 1.58 | 0.13 | 0.4 |
| | 1.6 | -0.70 | 0.70 | 1.64 | 0.11 | 0.3 |
| | 1.6 | -0.80 | 0.80 | 1.77 | 0.09 | 0.2 |
| | 1.6 | -0.90 | 0.90 | 1.91 | 0.07 | 0.1 |
| | 1.6 | -1.00 | 1.00 | 2.11 | 0.05 | 0.0 |

Rock samples

Class I

2200 550 500 500 500 500 500 500 500 500 500 500 500 500 500

Pebbles

Pebbles

500 500 500 500 500 500 500 500 500 500 500 500 500 500 500

Pebbles

500 500 500 500 500 500 500 500 500 500 500 500 500 500 500

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Pebbles

Class I

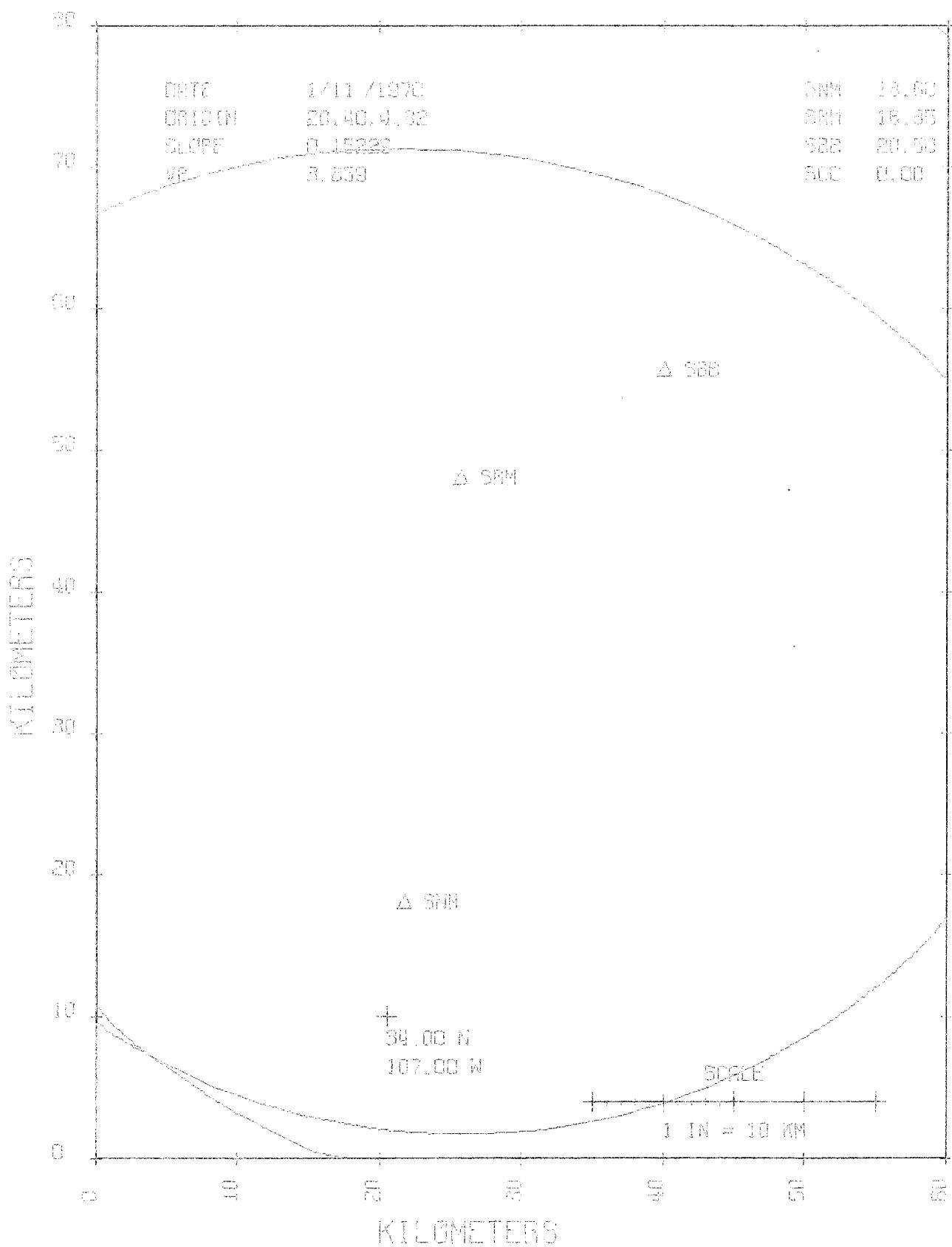
John G. Kelly

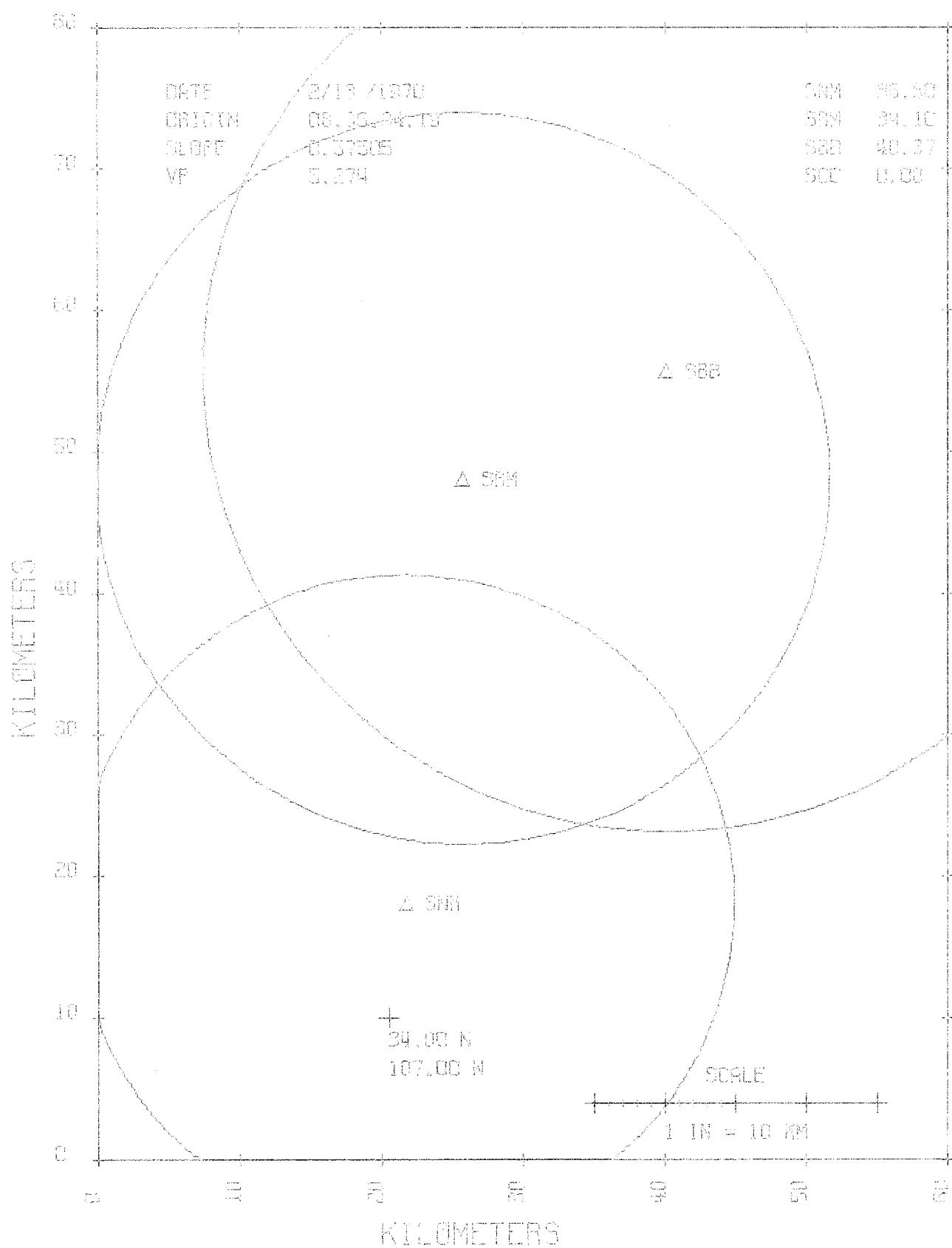
Post - office - box - No. 500 - 5th Street - San Francisco - Calif.

Times —
SUN-SAT SUN-SEC SUN-MON SUN-FRI

四百九

| Date | Sra | Sra | Sra | Sra | Sra | Sra | Sra |
|--------------|----------|---------|--------|--------|-------|------|------|
| 7/7 - 13:35 | 2.85 F | 3.16 P | | | 7.375 | 5.95 | |
| 7/11 - 20:40 | 2.125 P | 2.56 P | | | 4.75 | 5.95 | |
| 2/12 - 05:17 | 2.90 P | 1.78 F | 2.34 P | | 5.00 | 3.11 | 7.09 |
| 2/13 - 08:36 | 2.50 F | 2.815 F | 3.54 F | | 7.50 | 4.75 | |
| 3/2 - 14:35 | 2.25 P | 2.89 F | 3.53 P | | 6.75 | 4.66 | 6.94 |
| 3/11 - 06:40 | 2.325 F | 2.80 F | 3.61 F | 3.53 G | 7.00 | 4.13 | 7.36 |
| 3/19 - 08:39 | 2.25 F | 2.81 F | 3.36 P | 3.54 F | 7.00 | 4.17 | 7.44 |
| 3/19 - 19:05 | 2.25 F | 3.82 F | 3.33 F | 3.59 P | 7.00 | 4.89 | 7.33 |
| 7/18 - 07:20 | 2.25 G | 2.84 G | 3.84 P | 3.55 P | 7.125 | 4.83 | 7.53 |
| 3/18 - 16:35 | 2.375 F | 3.85 F | 3.64 F | 3.63 F | 7.35 | 5.39 | 7.87 |
| 3/20 - 04:34 | 2.4125 F | 2.80 F | 3.43 G | 3.59 G | 9.25 | 4.54 | 7.27 |
| 3/25 - 15:32 | 2.75 F | | 3.44 G | 3.84 G | 7.125 | 6.03 | 6.89 |
| 4/28 - 09:02 | 2.20 F | 2.82 F | 2.2 P | 4.00 | 4.77 | 6.44 | |
| 5/30 - 02:51 | 3.25 F | 1.96 P | 3.40 P | 7.25 | 4.25 | 6.68 | |
| 4/13 - 06:29 | 3.80 P | 1.94 P | | | 4.13 | | |

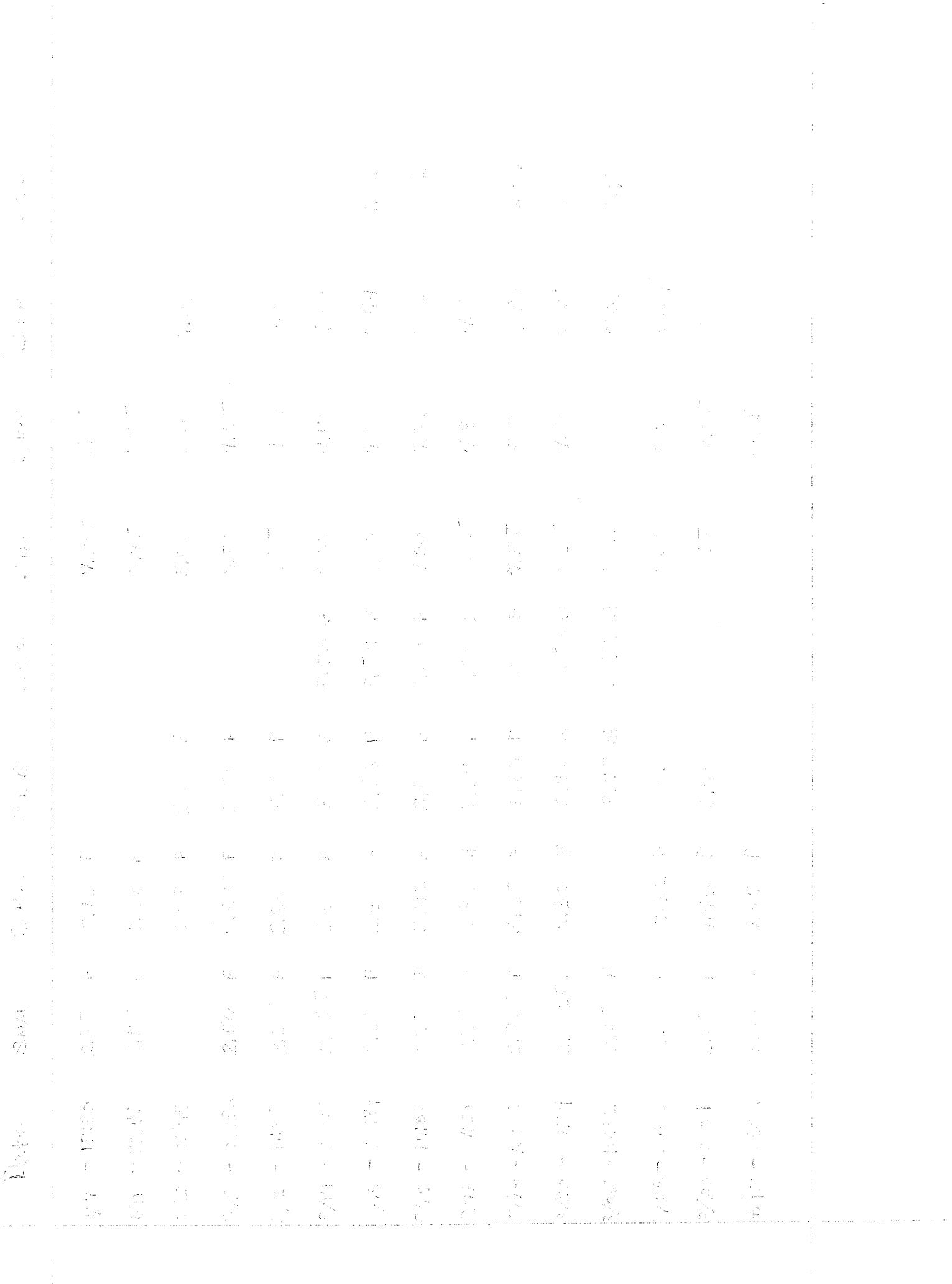




| Date | Time | Magnitude log A | | | Date | Time | Magnitude log A | | |
|------------|-------|-----------------|------|-------|---------|-------|-----------------|------|-------|
| | | C.T.I | LRSM | SRM | | | C.T.I | LRSM | SRM |
| 1969 | | | | | 1970 | | | | |
| June 14 | 02:35 | -0.3 | | 0.60 | May 5 | 22:44 | 0.14 | | 1.21 |
| June 27 | 09:35 | -0.1 | | 0.78 | May 5 | 22:44 | 0.21 | | 1.34 |
| July 7 | 08:58 | -0.74 | | 0.60 | May 5 | 23:03 | -0.32 | | 0.78 |
| July 7 | 09:03 | -0.14 | | 0.85 | May 11 | 08:07 | 0.15 | | 1.00 |
| July 7 | 11:25 | -0.43 | | 0.60 | May 13 | 02:31 | Sat 1.0 | | 1.73* |
| July 12 | 04:05 | 0.2 | | 1.00 | June 1 | 12:23 | -0.16 | | 0.70 |
| July 18 | 04:07 | 0.6 | 0.50 | 1.65 | June 1 | 15:36 | 0.03 | | 0.78 |
| July 18 | 11:39 | -0.1 | | 0.78 | June 1 | 22:17 | Sat. 0.65 | 1.45 | |
| July 18 | 02:34 | 0.05 | | 0.78 | June 2 | 00:22 | -0.02 | | 0.81 |
| July 19 | 05:50 | -0.23 | | 0.78 | June 2 | 12:24 | -0.29 | | 0.48 |
| July 30 | 10:47 | 0.2 | | — | June 7 | 09:14 | -0.48 | | 0.30 |
| Aug. 9 | 02:34 | -0.5 | | 0.40 | June 14 | 04:31 | 0.28 | | 0.30 |
| Aug. 15 | 04:41 | -0.35 | | 0.65 | June 14 | 04:36 | 0.30 | | 1.35 |
| Aug. 9 | 13:12 | 0.12 | | 1.18 | June 14 | 04:36 | 0.28 | | 1.53 |
| Aug. 9 | 15:10 | 0.18 | | 0.88 | June 16 | 16:50 | 0.29 | | 1.51 |
| Aug. 4 | 17:30 | 0.21 | | 1.37 | June 17 | 18:52 | -0.02 | | 0.84 |
| Aug. 31 | 02:06 | 0.0 | | 0.69 | June 23 | 01:33 | 0.22 | | — |
| Aug. 7, 70 | 13:35 | 0.27 | | — | June 30 | 11:34 | 0.21 | | 1.32 |
| Aug. 11 | 20:40 | -0.35 | | 0.00 | | | | | |
| Aug. 12 | 05:17 | 0.05 | | 0.78 | | | | | |
| Aug. 13 | 08:35 | 0.30 | | 1.18 | | | | | |
| Aug. 2 | 11:35 | -0.72 | | 0.85 | | | | | |
| Aug. 17 | 06:40 | 0.13 | | — | | | | | |
| Aug. 17 | 08:37 | -0.13 | | 0.84 | | | | | |
| Aug. 17 | 17:05 | 0.36 | | 1.43* | | | | | |
| Aug. 18 | 07:20 | 0.11 | | 1.02 | | | | | |
| Aug. 18 | 16:35 | 0.03 | | 1.02 | | | | | |
| Aug. 20 | 04:34 | 0.18 | | 1.15 | | | | | |
| Aug. 25 | 15:31 | Sat 2.10 | | — | | | | | |
| Aug. 28 | 09:02 | -0.34 | | 0.48 | | | | | |
| Aug. 30 | 02:51 | -0.10 | | 0.60 | | | | | |
| Sept. 13 | 06:29 | -0.34 | | 0.48 | | | | | |
| Sept. 17 | 03:06 | 0.26 | | 1.08 | | | | | |
| Sept. 18 | 03:44 | 0.30 | | 1.21 | | | | | |
| Sept. 18 | 07:11 | -0.25 | | 0.40 | | | | | |
| Sept. 18 | 07:34 | -0.34 | | 0.96 | | | | | |
| Sept. 18 | 09:05 | -0.24 | | 1.34 | | | | | |
| Sept. 18 | 09:12 | 0.23 | | 1.34 | | | | | |
| Sept. 18 | 09:29 | -0.24 | | 0.30 | | | | | |
| Sept. 18 | 19:18 | 0.30 | | 1.32 | | | | | |

| Date | Sun | Srm | S13B | Sec | Srm | S12B | Sun | Srm | S12B | Sec |
|----------------|-------|-----|------|-----|------|------|-------|-----|------|-------|
| 4/1/9 - 03:06 | 2.25 | F | 2.79 | P | 3.72 | F | 2.25 | | 4.46 | 7.1 |
| 4/1/8 - 03:44 | 2.50 | F | 2.81 | P | 3.70 | F | 2.00 | | 4.55 | 7.14 |
| 4/1/8 - 04:11 | 3.00 | VP | 2.88 | P | 3.60 | P | 2.75 | | 4.87 | 7.06 |
| 4/1/8 - 07:34 | 2.575 | G | 2.74 | P | 3.66 | G | 2.25 | | 4.32 | 7.30 |
| 4/1/8 - 09:05 | 2.575 | G | 2.80 | F | 3.11 | DP | 2.19 | | 8.87 | |
| 4/1/8 - 07:12 | 2.50 | F | 2.80 | F | 4.04 | G | 2.25 | | 4.52 | 7.125 |
| 4/1/8 - 07:29 | 2.50 | P | 2.89 | P | 4.09 | F | 2.00 | | 7.07 | 7.17 |
| 4/1/8 - 17:02 | 2.50 | P | 2.81 | P | 3.59 | | 2.87 | | 4.79 | 7.05 |
| 5/1/5 - 22:44 | 2.30 | P | 2.89 | P | 3.62 | | 3.53 | F | 7.1 | 6.92 |
| 5/1/5 - 23:03 | 2.50 | P | 3.12 | F | 3.33 | | 2.25 | | 4.89 | |
| 5/1/11 - 03:07 | 2.75 | G | 3.10 | P | 3.72 | F | 3.62 | G | 7.00 | 7.05 |
| 5/1/13 - 02:31 | 2.45 | F | 2.92 | F | 3.66 | F | 2.875 | | 4.83 | 6.98 |
| 6/1 - 12:23 | 2.425 | G | 2.87 | P | | | | | 5.42 | |
| 6/1 - 15:36 | 2.50 | F | 2.83 | P | 4.10 | F | 2.50 | | 5.42 | 6.83 |

| Date | Min | Sec | S 2 M | S 3 M | S 4 M | S 5 M | S 6 M | S 7 M | S 8 M | S 9 M | S 10 M | S 11 M | S 12 M | S 13 M | S 14 M |
|--------------|-------|-----|-------|-------|-------|-------|-------|-------|-------|-------|--------|--------|--------|--------|--------|
| 6/1 - 22:07 | 2,375 | P | 2,64 | F | | 3,58 | F | 7,175 | | 5,375 | | | | 7,14 | |
| 6/2 - 00:22 | 2,45 | G | 2,69 | P | | 3,56 | G | 7,375 | | 4,5 | | | | 7,02 | |
| 6/2 - 12:24 | 2,375 | F | 2,86 | P | | 7,25 | | | | | | | | | |
| 6/4 - 09:14 | 2,125 | F | 2,82 | P | | 6,875 | | | | | | | | | |
| 6/14 - 04:23 | 2,475 | F | 3,04 | P | | 3,19 | G | 7,125 | | 4,61 | | | | 7,07 | |
| 6/14 - 04:31 | 2,20 | F | 2,86 | P | | 7,00 | | | | | | | | | |
| 6/14 - 04:36 | 2,375 | F | 2,80 | G | | 3,36 | G | 7,125 | | 5,39 | | | | 8,15 | ? |
| 6/14 - 04:36 | 2,350 | F | 2,85 | F | | 3,21 | G | 7,125 | | 5,41 | | | | 7,4 | |
| 6/14 - 07:01 | 2,375 | P | 3,11 | F | | 4,15 | G | 7,125 | | 5,53 | | | | 7,5 | |
| 6/14 - 09:20 | 2,625 | F | 3,26 | P | | 3,595 | G | 7,5 | | 5,7 | | | | 7,125 | |
| 6/16 - 05:51 | 2,50 | G | | | | 3,99 | G | | | 7,075 | | | | 7,27 | |
| 6/16 - 16:53 | 2,425 | G | 2,89 | G | | 3,53 | G | 7,125 | | 4,70 | | | | 7,33 | |
| 6/19 - 18:52 | 2,35 | F | 2,92 | F | | 7,00 | | | | | | | | | |
| 6/23 - 01:33 | 2,75 | F | 2,39 | P | | 4,23 | G | 7,15 | | 3,8 | | | | 6,74 | |
| 6/26 - 11:34 | 2,80 | F | 3,09 | G | | 3,46 | F | 3,80 | | 5,6 | | | | 7,26 | |
| 6/27 - 02:57 | 2,375 | P | 3,68 | F | | 3,71 | F | 7,00 | | 7,10 | | | | 7,25 | |
| 6/27 - 10:36 | 2,475 | G | 4,42 | G | | 4,21 | P | 7,25 | | 6,78 | | | | 7,24 | |



Comments: -

1. Time differences between most evident
in the first case & probably ^{the} same
for all.
2. Temperature & the physical condition of a bird
are probably dependent of character.
Physical condition of a bird is probably
the best criterion.
3. However extreme range can be seen in
the first case and probably more extreme
in the second, but not so extreme.
4. The range of variation of temperature
too great estimates. At first by 3
of individuals were used. Estimated range
of temperature was large, probably too large.
At first it was done from 10° to 15°
but later from 10° to 12°.

Very interesting

5. Estimating the range of temperature
from the first case.

Good point

5. Estimating the range of temperature
from the first case. Range should be
estimated from the first case.
Temperature of the environment is probably
the best criterion for the first case.