

DISCRIMINATION AMONG DEPOSITIONAL ENVIRONMENTS BASED ON ELEMENT
ABUNDANCE IN UPPER CRETACEOUS ROCKS OF SOUTHERN ALBERTA

A Dissertation

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ABSTRACT

The major elements Si, Al, Fe, Mg, Ca, Na, K, Ti and Mn, and the trace elements Ba, Co, Cu, Ga, Li, Mo, Pb, Rb, S, Sr, Zn, Zr, V and Ni were studied in 776 samples from a single continuous core of Upper Cretaceous, dominantly argillaceous, rocks in Southern Alberta. The approximate amount of carbon plus free water was also determined. The environment of deposition (continental, brackish or marine) was known for one hundred and eight of the samples on the basis of fossil evidence. These 108 samples were used to formulate discriminant-functions which identify the environment of deposition of a sample based on its element abundances.

A two step, pairwise approach was used to separate the three environments. In the first step, marine samples were isolated from a composite continental-brackish group. In the second step, the composite group was separated into continental and brackish groups. Of the 24 elements determined, Ti, Mn, Ba, Co, Cu, Ga, Li, Sr, Zn, Zr, V and volatiles were found to be useful discriminators for the marine vs. continental brackish groups. For the continental vs. brackish groups the elements Mg, Na, K, Ti, Mn, Ba, Co, Cu, Ga, Li, Rb, Sr, Zr, Zn, V and volatiles were found to be the most useful environmental discriminators.

The formulated discriminant-functions permit complete separation of the continental, brackish and marine environments. The functions were used to classify the remaining core samples, which permitted the local depositional history of the Upper Cretaceous to be interpreted.

CHAPTER I: INTRODUCTION

GENERAL STATEMENT

Over the past few years there has been increasing interest in the study of the distribution of elements in sedimentary rocks from different environments of deposition. The literature suggests that different environments may well be characterized by different concentrations of major and trace elements. However, there is little agreement on which elements are relatively concentrated in marine deposits compared to continental or brackish environments. In fact, in most cases the brackish water environment has been ignored in geochemical facies analyses.

Methods of study have also been variable. Some workers have approached the problem from a theoretical standpoint, others have studied modern sediments, while still others have studied ancient sediments. Sampling methods are also quite diversified. Some have used outcrop samples, others have used core samples, while others have used a combination of outcrop and core samples. Many different sampling plans are used. They may be areally extensive or very restrictive. No set approach to the problem has been established.

Very few studies have used statistical techniques to measure the significance of their results or to construct a classification tool. Most conclusions are based purely on observation and comparison without statistical testing. The need is apparent, for a model which is statistically valid for the environmental classification of sediments based on element concentrations.

PURPOSE AND SCOPE OF THE INVESTIGATION

Geologists assume that sediments from different depositional environments can be characterized by different mineralogical assemblages. Therefore, the abundances of certain elements or associations of elements, should reflect their mode of deposition. It should then be possible to apply discriminant-functions for identifying continental, brackish and marine environments of deposition, based on elemental abundances in sediments. In order to use discriminant analysis, however, a standard must be established. The availability of a complete core for which lithologic, biostratigraphic and paleoecologic studies have been completed, for a portion of the core, provides an unusual opportunity to test this hypothesis.

One thousand nine hundred and forty feet of continuous core (from the 600 to 2540 foot depth), from the Canadian Pacific Oil and Gas EV Strathmore Well (Fig. 1) in southern Alberta, 30 miles east of Calgary (Lsd. 7, Sec. 12, Tp, 25, R. 25, W. 4 Mer.) are used in this study. The sediments in the core are dominantly argillaceous and are Late Cretaceous in age. A detailed paleoecologic study by Wall et al. (1971) and a lithologic description by Havard (1971), provide an environmental classification (ranging from continental through brackish to marine) for a 410 foot section of this core (from the 1350 to 1760 foot depth).

In this study, 776 samples, from known depths in the core are analyzed for the abundance of nine major (Si, Al, Fe, Mg, Ca, Na, K, Ti and Mn), fourteen trace (Ba, Co, Cu, Ga, Li, Mo, Pb, Rb, S, Sr, Zn, Ar, V and Ni) elements and volatiles (C plus H₂O). The environment of deposition, for one hundred and eight of these samples, is known on the basis of the work of Wall et al. (1971) and Havard (1971).

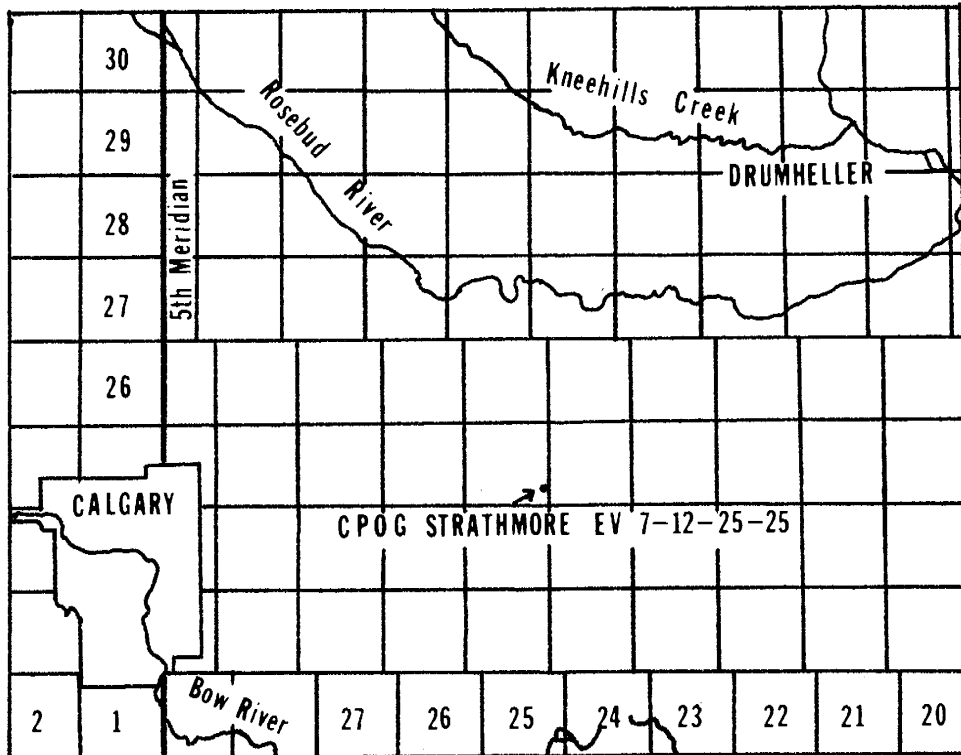


Fig. 1. Location of well CPOG Strathmore EV 7-12-25-25W4 (from Havard, 1971).

The purpose of this study is two-fold. First, to develop discriminant-functions based on the element abundances, using the 108 samples from known depositional environments. Second, to apply the formulated discriminant-functions to classify the environment of deposition of the remaining 668 samples. From these data, the Late Cretaceous depositional history of southern Alberta is interpreted.

PREVIOUS WORK

Element abundances and factors affecting element abundances in sediments and sedimentary rocks have been the subject of many investigations. Shaw (1954a,b, 1956) analyzed for 11 major oxides and 12 trace elements in pelitic rocks. Others who dealt with the abundance of elements and their mode of occurrence in sediments, include Horstman (1957) on the distribution of Li, Rb and Cs in igneous and sedimentary rocks, Greensmith (1958) on chemical data from some Upper Carboniferous shales in Great Britain and Mohr (1959) who studied the high Mn shales of the Halech dome, North Wales.

Research into geochemical facies analysis began with the work of Bishof (1847-1851) who first attempted to recognize sediments of different origin by geochemical means. Most of the data published before 1945 was, however, of questionable value for the recognition of depositional environments due to imprecise analytical techniques. After the development of modern geochemical techniques, many articles were published on geochemical facies analysis. Table 1 lists a few of the more important articles.

From Table 1 it is apparent that there is little agreement as to the usefulness of specific elements as environmental discriminators. Only a few of the elements have been studied by more than three workers. In many cases their results differ. This is not surprising, because geochemical facies analysis involves numerous variables which affect the mineralogic and, therefore, elemental composition of sediments. For example; sedimentation rates, grain size distributions, biologic influence, climatic influence, paleontologic control and sufficient sample size to make a study statistically valid.

Table 1

ELEMENT AND RELATIVE ABUNDANCE IN MARINE VS. CONTINENTAL DEPOSITS

Author (See Below)	No. of Samples	Major Elements											Trace Elements																									
		Al	Fe	Mg	Ca	Na	K	Ti	Mn	Li	Be	B	F	V	Cr	Ni	Cu	Zn	Ca	As	Se	Rb	Sr	Zr	Mo	Sn	Ba	Pb	Nd	Th								
1.	-																																					
2.	35				H																H	L	H															
3.	113	L	H	H	H																					L												
4.	60																				H																	
5.	75																				H																	
6.	-																																					
7.	374				L	H		H	H				L	L	L									L														
8.	54				L			H	H					H	H	H			L				L	H														
9.	-													L	L	L																						
10.	-																																					
11.	240																																					
12.	90													H	H	H	L																					
13.	66													H	H	H	H																					
14.	15,264																																					
15.	107													H	H	H	H	H	L	H	H			L	H													
16.	-													H	H	H	H																					
17.	45	L	L	L	H	H																																

H = High
L = Low

Table 1 (continued)

1. Ataman, G., (1964), Clay, based on theoretical geochemical considerations.
2. Campbell, F.A., and Lerbekmo, J.F., (1963), 35 outcrop samples all shales.
3. Campbell, F.A., and Williams, G.D., (1965), 113 core samples, all shales.
4. Degens, E.T., Williams, E.G., and Keith, M.L., (1957), 33 outcrop samples, Ni, V, Pb, Zn, Cu, Sn determined on organic material, sampled over a wide area.
5. Degens, E.T., Williams, E.G., and Keith, M.L., (1958), 75 outcrop samples, 7 shale samples, 20 limestone samples and 20 clay samples.
6. Goldschmidt, V.M., (1937), Based on theoretical geochemical considerations.
7. Katchenkov, S.M., (1952), 374 outcrop and core samples, anhydrites, dolomites, carbonates, terrigenous rocks and limestones.
8. Katchenkov, S.M., (1960, 12 recent marine muds, 19 continental clays, 23 marine clays, only 0.001 mm fraction studies, outcrop and recent samples.
9. Keith, M.L., and Degens, E.T., (1959), Literature review.
10. Landergren, S., (1944), sediments, iron ores.

Table 1 continued

11. Litvin, S.V., (1962), 240 outcrop samples, 78 sandstones, 43 siltstones, 32 argillites, 32 clays, 19 limestones, 14 marls, 22 argillaceous limestones, samples over a wide area.
12. Macpherson, H.G., (1958), 91 outcrop samples, graywackes, argillites and low-grade schists.
13. Potter, P.E., Shimp, N.F. and Witters, J., (1963), Argillaceous sediments, 14 modern marine, 19 modern fresh water, 20 ancient marine, 13 ancient fresh-water, sampled over wide area.
14. Ronov, A.B., and Ermishkina, A.S., (1959), 15,264 cuttings, 6381 sands and silts, 8883 clays.
15. Tourtelot, H.A., (1964) 107 outcrop samples: 8 noncarbonaceous, nonmarine claystones, 14 carbonaceous, nonmarine shales, 32 nearshore marine shales and claystones, 53 marine shales and claystones, sampled over wide area.
16. Van Houten, F.B., (1965), outcrop samples, arkose, mudstone, siltstone, shale, sampled over wide area.
17. Weber, J.N., and Williams, E.G., (1965), 45 siderite nodules, outcrop samples, 24 fresh-water, 12 brackish, 9 marine.

Many different approaches to geochemical facies analysis have been attempted. In most cases numerous rock types have been studied (Table 1). This only adds to the confusion. A more realistic approach is used by some of the workers (Degens et al., 1957, Potter et al., 1963, Weber and Williams, 1965). In these studies, sampling was limited to argillaceous sediments or specific rock types and a definite approach to sampling was used. Degens et al. (1957) and Weber and Williams (1965) use plans in which the number of outside variables is limited. In both cases, ancient sediments from one source area, within a single basin, with a variety of repetitive environments of deposition were studied. Potter et al. (1963) used a sampling plan which included as many variables as possible. Recent sediments from known environments of deposition were used as standards. Factors such as source area, climate, geologic age and sample locations, were allowed to vary to the greatest degree possible. Both plans have merit, and all three of the studies arrive at significant results.

Degens et al. (1957) conclude that continental and marine shales can be separated using B, Ga, and Rb. From their work they found B and Rb to be concentrated in marine samples, while Ga is concentrated in continental samples. They construct a triangular diagram Fig. 2 based on the relationship between the three elements. Using the diagram they show that continental and marine samples can be classified on the basis of the three trace elements (B, Rb and Ga). Only three of the marine samples overlap into the fresh water group, and one fresh-water sample falls into the marine group. No method for separating brackish water samples was established.

Potter et al. (1963) studied the abundance of B, Co, Cr, Cu, Ga, Ni, Pb, V and Zn in argillaceous sediments. In their study, they use the

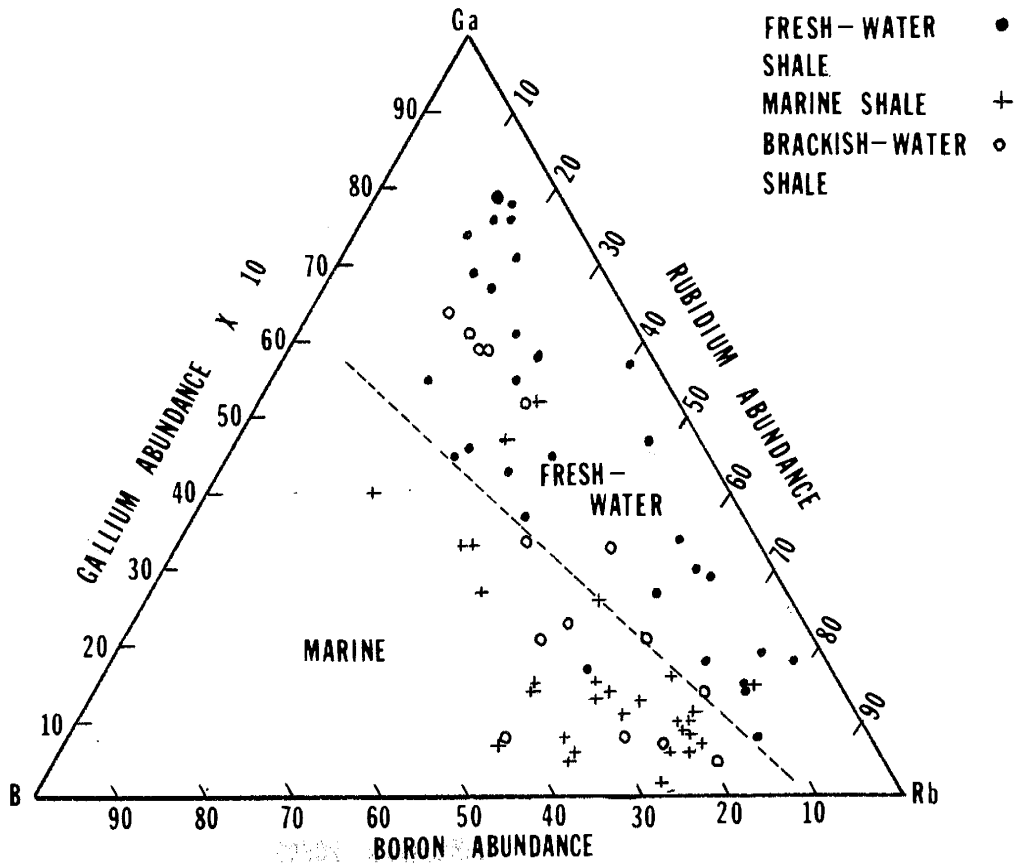


Figure 2. Triangular Diagram Showing Abundance of Gallium, Rubidium and Boron (from Degens et al., 1957).

sample plan previously mentioned. They found B, Cr, Cu, Ga, Ni, and V to be concentrated in marine sediments. Two schemes for the classification of sediments were used. First they used graphical methods and secondly they tried discriminant analysis. In both instances, their conclusions were similar. Figures 3 and 4 give their graphical results. After performing a number of statistical tests for significance and elimination of variables, they concluded that a discriminant-function based on two variables (B and V) can be used to classify unknown samples. The function used is $X = 5.3415 X_1 + 5.6928 X_7$ where X_1 is the logarithm of the boron concentration and X_7 is the logarithm of the vanadium concentration. Using this function, 85% of the ancient samples were correctly classified. By using the graphical method, 88% of the samples were correctly classified. No attempt was made to classify brackish-water samples.

Weber and Williams (1965) used the same sample plan as Degens et al. (1957) but instead of using whole rock analysis they studied only siderite nodules. In their study the environments of deposition were established by paleontologic evidence. Three categories were used; fresh-water, brackish and marine. A three group discriminant-function was used. In this study major oxides and trace element concentrations were considered. They conclude that based on a six variable (SiO_2 , Al_2O_3 , MgO , CaO , Ba, and V) discriminant-function, marine and fresh-water environments can be effectively separated, but that a brackish-water group could not be distinguished. The final functions used for classification or method were not given.

Considering geochemical facies analysis, and by studying Table 1, some elements do appear to be of some use. Boron and rubidium for example, both seem to be accepted as useful discriminators. There are

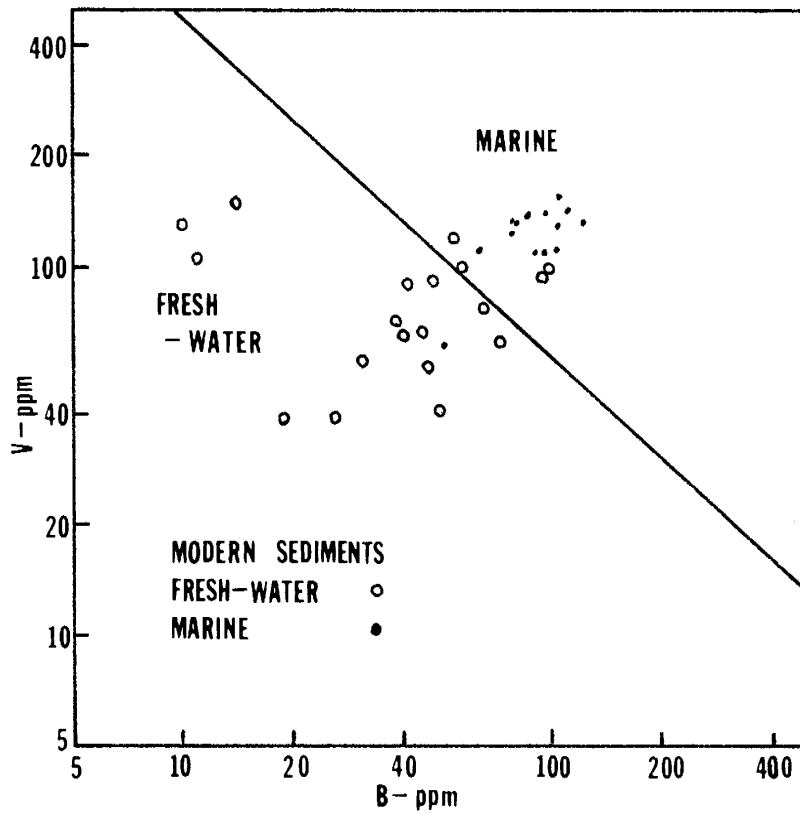


Figure 3. Plot of B and V concentrations in 33 modern sediments and estimated line of separation between marine and fresh-water fields (from Potter et al. 1963).

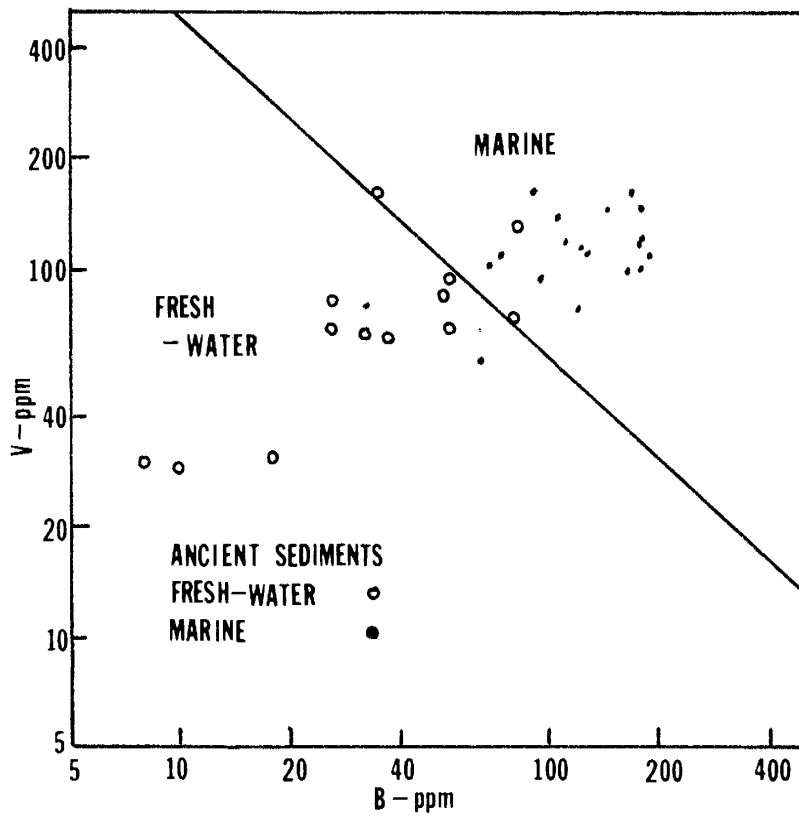


Figure 4. Plot of B and V concentrations in 33 ancient sediments and estimated line of separation between marine and fresh-water fields (from Potter et al., 1963).

also other elements which may prove useful, such as V, Cr, Ni and Cu. Their relative concentration appears to be higher in marine environments compared to continental environments. There is also some agreement that Ga is concentrated in continental sediments. An approach using a specific sampling plan utilizing most of the elements listed in Table 1 and others, appears to be a most promising way to handle geochemical facies analysis.

GENERAL GEOLOGY

Geologic Setting

During Cretaceous time a broad seaway extended northward from the Gulf of Mexico to the Arctic along the eastern side of the Cordilleran region, covering most of the area of the Eastern Ranges and Plateaus and overlapping the Interior Lowlands. As the Cordillera on the west developed in later Mesozoic time, a series of clastic wedges were laid down in this seaway. The growth of the Rocky Mountains provided a source for the terrigenous and volcanic debris which was shed eastward into the epicontinental sea.

The continental buildup of sediments along the margins of the seas resulted in thick accumulations of alternating continental and marine deposits (Williams and Burk, 1964). During the Late Cretaceous, the plains area of western Alberta was always at or near sea level. Transgressions and regressions of the epicontinental sea were frequent. Westward transgressions were due to regional subsidence and/or a low rate of supply of detritus from the west. Regressions to the east were caused by regional emergence and/or a high rate of supply of detritus from the west.

Environments of deposition over the area were highly variable. Continental deposits, largely fluvial and associated floodplain deposits, produced a broad lowlying coastal plain. At times, swamp conditions, where coals developed, were prevalent. Eastward prograding deltas produced a sinuous coastline. Brackish-water deposits accumulated in estuaries, bays, lagoons and swamps. Fine grained detritus deposited in the epicontinental sea formed shales and the rate of shale deposition was generally high enough to prevent the formation of carbonates.

CORE STRATIGRAPHY

The following is a brief description of the stratigraphic units sampled for this study. A correlation chart for the very Late Cretaceous and Paleocene is given in Figure 5.

Belly River Group

Dawson (1883) first introduced the name Belly River Series into the literature. All beds between the underlying Alberta Formation and the overlying Bearpaw Formation (outcropping along the Belly and Bow rivers in southern Alberta), were included in the series. Dawson (1883) believed that the beds were non-marine, and predominantly sandstones. Dowling (1917) redefined the series to include shales of the Pakowki Formation, as well as the sandy formations above and below them. Williams and Dyer (1930) restricted the term to include only the beds overlying the Pakowki Formation and underlying the Bearpaw Formation. Following their usage, the Foremost Formation and "Pale" beds of Dowling (1917) were included in the series. The Belly River Series was formally raised to group status by Russell and Landes (1940), and subdivided into the Foremost and Oldman Formation (previously "Pale" beds). The Belly River Group is correlative with the Judith River Formation, in the western United States.

Foremost Formation 2165' - 2540'

Before the deposition of the Foremost Formation, beds of the marine Pakowki Formation (Clagget Formation) were deposited by the Clagget sea. Foremost time began with the gradual recession of the sea. The oscillatory nature of the withdrawal is shown by the presence of coals, brackish-water molluscs and beach sands (Powers, 1931; Hale and Addison, 1931; Russell and Landes, 1940).

Figure 5. Correlation of the uppermost Cretaceous and Paleocene formations of the southern Alberta Plains and central Foothills.

UPPER CRETACEOUS			PALEOCENE	
WESTERN UNITED STATES	FORT UNION	PASKAPOO FORMATION	ENTRANCE CONG.	
			PORCUPINE HILLS FM	
			UPPER PART WILLOW CR. FM	
			LOWER PART WILLOW CREEK FORMATION	
LANCE	BEARPAW	BRAZEAU FORMATION	ST. MARY RIVER FORMATION	
			HORSESHOE CANYON FACIES	
PIERRE	JUDITH RIVER	ALBERTA GROUP	BATTLE FM	
			WHITEMUD FM	
CLAGGET EAGLE	CLAGGET EAGLE	ALBERTA GROUP	WILLOW CREEK FACIES	
			ST. MARY RIVER FACIES	
MONTANA GROUP			EDMONTON GROUP	
BELL RIVER GROUP			PASKAPOO FORMATION	
BLOOD RESERVE FM			PASKAPOO FORMATION	
BEARPAW FM			PASKAPOO FORMATION	
OLDMAN FORMATION			PASKAPOO FORMATION	
FOREMOST FORMATION			PASKAPOO FORMATION	
PAKOWKI FM			PASKAPOO FORMATION	
MILK RIVER RM			PASKAPOO FORMATION	
PAKOWKI FM			PASKAPOO FORMATION	
MILK RIVER RM			PASKAPOO FORMATION	
LEA PARK FORMATION			PASKAPOO FORMATION	
PAKOWKI FM			PASKAPOO FORMATION	

The formation was named by Dowling (1917) and is equivalent to Dawson's (1883) lower portion of the Belly River series. The Foremost Formation is incomplete in the Strathmore core (Havard, 1971), where it attains a thickness of 375 feet. The top of the formation is chosen as the highest occurrence of carbonaceous shale and coal within the Belly River Group (Havard, 1971).

According to Powers (1931) and Russell and Landes (1940) the formation consists chiefly of brackish-water and lagoonal deposits. A general description of the unit is difficult because the lithology varies greatly from place to place. The section contains dark grey and brown shales, silty shales, and subordinate amounts of grey, buff or tawny brown sandstones. Russell and Landes (1940) believe that the diagnostic feature of the formation is the presence of numerous beds of brackish-water molluscs and coal seams.

Oldman Formation 1732' - 2165'

With the subsequent regression of the sea to the east, beds of the dominantly continental Oldman Formation were deposited. Erratic conditions of deposition, however, persisted as shown by the alternations of shale and sandstone. During Late Oldman time the land was well drained so that organic matter was oxidized rather than carbonized (Hale and Addison, 1931).

The Oldman Formation was formally named by Russell and Landes (1940). The thickness of the formation within the cored interval is 433 feet (Havard, 1971) and is overlain by the Bearpaw Formation. Lithologically, the beds consist of brown, grey and green sandstones, siltstones, mudstones and shales. Some coals and coaly shales are also present in the section.

According to Powers (1931) and Russell and Landes (1940), the formation consists mainly of continental deposits. However, Wall et al. (1971)

recognize, by the presence of brackish-water microflora and microfauna, that the uppermost 20 feet of the Oldman Formation marks the initial transgressive phase of the Bearpaw sea.

Bearpaw Formation 1640' - 1732'

At the beginning of the Bearpaw time, a major transgression of the Bearpaw sea occurred. Powers (1931), Hake and Addison (1931) and Williams and Burk (1964) suggest that this transgression is related to subsidence within the basin. The Bearpaw shale records remarkably uniform marine deposition during a considerable time.

This formation was named by Stanton and Hatcher (1905) for the dark-grey shale occurring along the margins of the Bearpaw Mountains, in Montana. The formation is also present in central and southern Alberta and southwestern Saskatchewan, where it is overlain by the Edmonton Group (Shepherd and Hills, 1970). To the west, the formation wedges out, whereas the Edmonton Group thickens, and in combination with the Belly River Group, is defined as the Brazeau Formation.

In the Strathmore core, Havard (1971) recognized 92 feet of the Bearpaw Formation, composed of grey-brown to grey shale with interstratified thin beds of sandstones, siltstones, mudstones and abundant ironstone. Link and Childerhose (1931), Shepherd and Hills (1970) and Wall et al. (1971) classify the formation as being mainly marine.

"Transition Zone" 1362' - 1640'

Shepherd and Hills (1970) and Wall et al. (1971) informally recognize a "transition zone" between the marine Bearpaw and continental Horseshoe Canyon Formation. The interval consists of light to dark grey to brown sandstones, siltstones, mudstones and shales; locally containing coal and coaly shales. On the basis of foraminiferal and megaspore

evidence, Wall et al. (1971) believe that this zone represents a mainly brackish-water environment, although it also contains some continental and marine units.

Edmonton Group

Tyrrell (1887) designated a lithologically variable unit, located in the North Saskatchewan River Valley in the vicinity of Edmonton, the Edmonton Formation. This unit was formally redefined by Irish (1970) as the Edmonton Group. The group consists of all nonmarine strata (Irish, 1970) overlying the Bearpaw Formation, and overlain by the Paskapoo Formation. In descending order, the group consists of:

Battle Formation

Whitemud Formation

Horseshoe Canyon Formation

The Horseshoe Canyon Formation is the only formation of this group which was cored.

Horseshoe Canyon Formation 600' - 1362'

Horseshoe Canyon time is marked by an increase in tectonic activity in the Cordillera (Irish, 1970). Laramide Mountain building was at a maximum at this time (Irish, 1970). Erosion of the mountains to the west resulted in vast quantities of sediment being transported into the Bearpaw sea. Considerable volcanic activity is also shown by the abundance of bentonitic material in most beds of the Horseshoe Canyon Formation. The increased supply of sediments into the basin, with probable regional uplift (Irish, 1970), caused the final withdrawal of the Bearpaw sea. This marked the end of marine conditions in western Canada.

The Horseshoe Canyon Formation (Irish, 1970) is comprised of strata overlying the Bearpaw Formation and underlying the Whitemud Formation. The "transition zone" recognized by Shepheard and Hills (1970) and Wall et al. (1971) is placed within the lowest strata of the Horseshoe Canyon Formation by both Irish (1970) and Havard (1971). The formation consists of deltaic and fluvial deposits (Irish, 1970), of interstratified, fresh and brackish-water sandstones, mudstones and shales. Typically the beds consist of light grey and greenish-grey, grey and white weathering, fine grained, bentonitic, feldspathic, sandstones; silty, grey, green and brown bentonitic shales; beds of carbonaceous shale and coal seams. Beds of hard, brown weathering, calcareous sandstones, thin nodular beds of red to brown weathering ironstone; thin beds of bentonite; and concretions are found less commonly in this portion of the section.

CHAPTER II: SAMPLE ANALYSIS

GENERAL ANALYTICAL METHODS

Introduction

Analysis of 776 argillaceous rocks was performed by a combination of X-ray fluorescence, neutron activation, atomic absorption and ashing. Twenty four element concentrations were determined on each sample. The major elements, determined were: Si, Al, Fe, Mg, Ca, Na, K, Ti and Mn. Fourteen trace elements: Ba, Co, Cu, Ga, Li, Mo, Pb, Rb, S, Sr, Zn, Ar, V and Ni were also determined. The amount of carbon plus free water was estimated during the ashing procedure.

Explanation of Statistical Terms

This section presents definitions of the statistical terms used in describing the results of analytical procedures.

Mean (\bar{X}): the summation of a set of results (X_1, X_2, \dots, X_n) divided by the number of observations.

$$\bar{X} = \frac{1}{n} \sum_{i=1}^n X_i$$

Maximum (MAX.): the maximum observed value in a set of results.

Minimum (Min.): the minimum observed value in a set of results.

Range: the difference between the maximum and minimum observed values.

Standard Deviation (S): the root-mean-square deviation of a set of observations from their mean. For a finite number (n) of measurements with a mean \bar{X} the standard deviation is:

$$S = \sqrt{\frac{\sum_{i=1}^n (X_i - \bar{X})^2}{n - 1}} .$$

Upper Bound (U.B.): The upper bound is defined as the mean for a set of observations plus the standard deviation divided by two.

$$\text{U.B.} = \bar{X} + S/2$$

Lower Bound (L.B.): The lower bound is defined as the mean for a set of observations minus the standard deviation divided by two.

$$\text{L.B.} = \bar{X} - S/2$$

Coefficient of Variation (C.V.): The coefficient of variation is defined as the standard deviation expressed as a percentage of the mean.

$$\text{C.V.} = S/\bar{X} \cdot 100\%$$

Precision: Precision is defined as the closeness of agreement among replicate results obtained under a definite set of conditions.

Accuracy: Accuracy can be defined as the nearness of the mean (\bar{X}) of a number (n) of results to the "true" result.

X-ray Fluorescence Analysis

Before analysis, the samples were prepared using the method described by Leake et al. (1969). A Philips 8-position vacuum spectograph equipped with a simultaneous teletype was used to obtain the X-ray fluorescence data. The X-ray fluorescence methods described by Condie (1967a,b) were used for the analysis of the major elements: Si, Al, Fe, Ca, K, Ti, Mn and the trace elements: Cu, Ga, Mo, Pb, Rb, S, Sr, Zn and Zr. The major and trace element calibration curves were constructed using U.S. Geological

Survey standard rocks: W-1, BCR-1, AGV-1, GSP-1, and PCC-1. Instrumental parameters are listed in Table 2.

The precision of the X-ray analysis is given in Tables 3, 4, 5 and 6. The major oxide values are given in percent, while the trace element values are given in part per million. Fifteen separate replicate pellets from four different samples were used in the check of precision.

The results for the test of accuracy are given in Table 7. The accuracy was determined by treating BL 3571, the analyzed amphibolite, Leake et al. (1969), as an unknown. The analyses were then compared with the known values. The test results indicate that the method is highly accurate for most elements, and adequate for the remaining elements.

Appendix 1 contains the results of the X-ray analysis on the 776 argillaceous rocks. All values are reported in parts per million, to facilitate statistical handling of the data. In order to obtain the percent oxide contained in the sample, the following conversion must be made.

$$\text{Oxide Percent} = \text{ppm} (.0001) \times \frac{\text{Formula Weight Oxide}}{\text{Atomic Weight of Element}}$$

For example:

sample no.1 contains 298630 ppm Si

formula weight oxide (SiO₂) = 60.09

atomic weight of element (Si) = 28.09

$$\text{Oxide Percent} = 29860 (.0001) \times \frac{60.09}{28.09}$$

$$= 63.88\%$$

Table 2

X-RAY FLUORESCENCE INSTRUMENTAL PARAMETERS

ELEMENT	PEAK	TARGET	CRYSTAL	DETECTOR	GAS	COLLIMATOR	PATH	KV	MA	FT ¹
Si	K α	Cr	EDDT	FPC	P-10	Coarse	VAC	45	25	10
Al	K α	Cr	EDDT	FPC	P-10	Coarse	VAC	45	25	10
Fe	K α	W	LiF (200)	SCIN	----	Fine	AIR	50	35	10
Ca	K β	Cr	EDDT	FPC	P-10	Coarse	VAC	45	25	10
K	K α	Cr	EDDT	FPC	P-10	Coarse	VAC	45	25	10
Ti	K α	W	LiF (200)	SCIN	----	Coarse	VAC	50	37	20
Mn	K α	Mo	LiF (200)	SCIN	----	Coarse	AIR	50	38	10
Cu	K α	Mo	LiF (200)	SCIN ²	----	Coarse	AIR	50	37	20
Ga	K α	Mo	LiF (220)	SCIN ²	----	Coarse	AIR	45	35	20
Mo	K α	W	LiF (220)	SCIN	----	Coarse	AIR	45	35	10
Pb	L α	W	LiF (200)	SCIN	----	Coarse	AIR	50	35	20
Rb	K α	Mo	LiF (200)	SCIN	----	Coarse	AIR	45	35	10
S	K α	Cr	QTZ	FPC	P-10	Coarse	VAC	50	25	10
Sr	K α	Mo	LiF (200)	SCIN	----	Coarse	AIR	45	35	10
Zn	K α	Mo	LiF (200)	SCIN	----	Coarse	AIR	45	35	10
Zr	K α	Zr	LiF (220)	SCIN	----	Coarse	AIR	50	35	10

¹ FT = Fixed Time in Seconds. Each sample was counted seven times, for the number of seconds indicated.

² 0.0005" Ti Filter used

Table 3

X-RAY FLUORESCENCE
INSTRUMENTAL PRECISION

SAMPLE NO. 212

OXIDE OR ELEMENT	\bar{X}	MAX.	MIN.	RANGE	L.B.	U.B.	S.	C.V. %	NO. OF ANALYSIS
SiO ₂	61.28	62.60	59.79	2.81	60.89	61.76	0.96	1.56	9
Al ₂ O ₃	16.13	16.86	15.61	1.25	15.90	16.36	0.45	2.77	12
Fe ₂ O ₃	5.00	5.33	4.86	0.47	4.91	5.08	0.17	3.34	12
CaO	2.26	2.50	2.11	0.39	2.21	2.32	0.10	4.60	12
K ₂ O	2.33	2.64	2.06	0.58	2.25	2.41	0.17	7.09	13
TiO ₂	0.510	.519	.499	.02	0.506	0.514	0.01	1.42	10
MnO	0.107	.101	.117	0.016	0.104	0.11	0.01	4.83	10
Cu	21.	25.	13.	12.	19.	22.	3.48	16.87	13
Ga	24.	31.	20.	11.	22.	26.	3.33	13.95	12
Mo	.59	1.95	0.	1.95	.29	.90	0.64	108.4	13
Pb	17.	25.	11.	14.	15.	19.	4.33	25.39	15
Rb	52.	57.	47.	10.	51.	54.	3.33	6.38	12
S	98.	133.	71.	62.	90.	106.	17.7	18.0	15
Sr	215.	221.	201.	20.	212.	217.	5.15	2.40	15
Zn	59.	64.	49.	15.	56.	62.	5.07	8.57	10
Zr	130.	136.	124.	12.	128.	131.	3.89	3.00	13

Table 4

X-RAY FLUORESCENCE
INSTRUMENTAL PRECISION

SAMPLE NO. 386

OXIDE OR ELEMENT	\bar{X}	MAX.	MIN.	RANGE	L.B.	U.B.	S.	C.V. %	NO. OF ANALYSIS
SiO ₂	61.18	61.66	60.48	1.18	60.99	61.38	0.37	0.61	12
Al ₂ O ₃	15.99	16.68	15.51	1.17	15.79	16.19	0.37	2.31	11
Fe ₂ O ₃	2.52	2.58	2.45	0.13	2.49	2.55	0.05	2.05	13
CaO	1.35	1.39	1.33	0.06	1.34	1.36	0.02	1.57	12
K ₂ O	0.75	.80	.72	0.08	0.74	0.77	0.03	3.58	10
TiO ₂	0.486	.506	.468	.038	0.481	0.492	0.01	2.30	15
MnO	0.058	.060	.056	.004	0.057	0.058	0.00	1.94	15
Cu	14	18.	12.	6.	13	15	2.04	14.39	11
Ga	19	22.	17.	5.	18	20	1.53	8.11	12
Mo	.51	1.26	0.	1.26	.28	.74	.51	100.4	15
Pb	9	15.	2.	13.	7	10	3.68	42.79	15
Rb	19	25.	14.	11.	17	20	3.56	19.12	14
S	84	117.	52.	65.	76	93	19.06	22.64	15
Sr	227	253.	214.	39.	223	232	9.25	4.07	14
Zn	49	55.	40.	15.	46	52	4.96	10.17	10
Zr	119	127.	111.	15.	116	121	4.47	3.77	14

Table 5

X-RAY FLUORESCENCE
INSTRUMENTAL PRECISION

SAMPLE NO. 392

OXIDE OR ELEMENT	\bar{X}	MAX.	MIN.	RANGE	L.B.	U.B.	S.	C.V. %	NO. OF ANALYSIS
SiO ₂	60.91	61.62	60.11	1.51	60.62	61.2	0.50	0.83	10
Al ₂ O ₃	14.91	15.38	14.49	0.89	14.73	15.08	0.34	2.29	12
Fe ₂ O ₃	7.13	7.25	7.02	0.23	7.08	7.17	0.08	1.18	12
CaO	1.56	1.60	1.55	0.05	1.55	1.57	0.01	0.82	12
K ₂ O	1.42	1.47	1.38	0.09	1.41	1.44	0.03	1.87	11
TiO ₂	0.803	.823	.779	.054	0.798	0.809	0.01	1.50	15
MnO	0.12	.123	.118	.005	0.119	0.121	0.00	1.11	14
Cu	33.	42.	26.	13.	31.	35.	4.32	13.17	14
Ga	24.	29.	20.	9.	22.	26.	3.56	14.90	11
Mo	.80	2.049	.015	2.034	.54	1.05	0.80	69.80	15
Pb	20.	27.	13.	14.	19.	22.	9.92	15.54	15
Rb	87.	99.	80.	19.	83.	91.	6.92	7.95	11
S	502.	559.	430.	129.	477.	528.	41.78	8.32	9
Zn	93.	99.	84.	15.	90.	95.	5.05	5.45	11
Zr	149.	160.	138.	22.	146.	152.	5.98	4.02	14

Table 6

X-RAY FLUORESCENCE
INSTRUMENTAL PRECISION

SAMPLE NO. 810

OXIDE OR ELEMENT	\bar{X}	MAX.	MIN.	RANGE	L.B.	U.B.	S.	C.V. %	NO. OF ANALYSIS
SiO ₂	57.09	58.31	56.15	2.16	56.75	57.43	0.65	1.14	12
Al ₂ O ₃	15.57	15.98	15.38	0.60	14.46	15.68	0.20	1.27	11
Fe ₂ O ₃	8.01	8.15	7.92	0.23	7.97	8.05	0.08	0.97	13
CaO	1.71	1.75	1.69	0.06	1.70	1.72	0.02	1.04	12
K ₂ O	1.24	1.29	1.18	0.11	1.22	1.26	0.03	2.62	11
TiO ₂	0.839	.858	.816	.042	0.833	0.845	0.01	1.60	15
MnO	0.097	.100	.093	.007	0.096	0.097	0.00	2.00	15
Cu	31	35.	23.	12.	29	34	3.50	11.14	9
Ga	22	26.	18.	8.	21	23	2.45	11.13	12
Mo	.17	.41	0	.41	.05	.28	.17	104.0	8
Pb	13	19.	7.	12.	11	14	2.92	23.33	15
Rb	42	51.	36.	15.	40	44	4.70	11.17	14
S	80	96.	67.	29.	75	85	8.90	11.16	10
Sr	302	308	294.	14.	300	304	4.52	1.49	15
Zn	91	99.	84.	15.	89	94	4.75	5.20	12
Zr	135	143.	130.	13.	133	138	4.68	3.46	13

X-RAY FLUORESCENCE
INSTRUMENTAL ACCURACY

SAMPLE NO. BL 3571

OXIDE OR ELEMENT	ACCEPTED VALUE	OBSERVED VALUE	MAX.	MIN.	RANGE	L.B.	U.B.	S	C.V. %	NO. OF ANALYSIS
SiO ₂	47.23	47.45	47.534	47.368	.166	47.43	47.47	0.04	0.09	14
Al ₂ O ₃	14.71	11.80	11.808	11.742	.066	11.79	11.81	0.02	0.15	14
Fe ₂ O ₃	11.19	10.686	10.688	10.686	.002	10.685	10.687	0.00	0.01	14
CaO	8.40	9.53	9.601	9.501	0.10	9.52	9.54	0.02	0.25	14
K ₂ O	0.96	0.973	0.973	0.973	0.000	.973	.973	0.00	0.00	14
TiO ₂	0.54	0.685	0.685	0.684	0.001	.684	.685	0.00	0.00	14
MnO	0.178	0.143	0.143	0.143	0.000	.143	.143	0.00	0.00	14
Cu	85.7	63.6	64.1	63.0	1.10	63.5	63.7	0.24	0.38	14
Ga	13.0	17.53	17.7	17.4	0.30	17.49	17.57	0.09	0.52	14
Pb	5.9	7.11	7.2	6.9	0.30	7.05	7.16	0.12	1.70	14
Rb	20.4	28.	31.	25.	6.	27.	28.	1.49	5.38	14
S	137.7	238.	248.	232.	16.	236.	240.	4.08	1.71	14
Sr	267.4	496.	496.	495.	1.	495.	496.	0.51	0.10	14
Zn	85.1	76.31	76.7	75.6	1.10	76.18	76.45	0.29	0.37	14
Zr	62.3	100.46	100.8	100.3	0.50	100.49	100.63	0.14	0.14	14

Table 8

NEUTRON ACTIVATION INSTRUMENTAL ACCURACY

SAMPLE NO. G-2

Na ₂ O	4.10	4.10	4.258	3.9	.358	3.92	4.27	0.15	3.62
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Neutron Activation Analysis

Sodium was the only element determined by neutron activation analysis. The sample preparation and analytic method used is described in Condie and Lo (1971). Analyses were performed on a Canberra 4,096 channel gamma ray spectrometer, with a Li drifted Ge detector system. A fixed time mode was used for counting. Instrument parameters are given in Table 9.

The results of the test of precision for the neutron activation analysis are given in Table 11. In this case replicates of standards G-2 and BCR-1 were used as a check.

The accuracy of the neutron activation data is given in Table 8. The accuracy was determined by treating U.S. Geological Survey G-2 as an unknown. The test results indicate that the method is highly accurate for sodium.

Appendix 1 contains the Na analysis. All values are reported in parts per million. To convert to oxide percent the same method previously described is used.

Ashing

The approximate amount of free water plus carbon is obtained from the ashing procedure. The difference in weight of the sample, before and after ashing, is attributed to loss of carbon and free water. The weight loss was divided by the initial total weight and multiplied by 100% to calculate the approximate percentage of free water plus carbon. Results are given in Appendix 1. All values are listed in parts per million, that is, the percentage values were converted to ppm. The precision of the ashing technique was determined by using five replicate samples. The results of the test are given in Table 12. No tests of accuracy were made for the ashing techniques.

Table 9

NEUTRON ACTIVATION ANALYTICAL PARAMETERS

ELEMENT	IRRADIATION FLUX	LENGTH OF IRRADIATION (MIN)	COOLING PERIOD (DAYS)	PEAK (KEV)	COUNTING TIME (SEC)
Na	1×10^{14} n/cm ²	3.33	0.5	1369	6.0×10^2

Table 10

ATOMIC ABSORPTION INSTRUMENTAL PARAMETERS

ELEMENT	WAVE- LENGTH (nm)	CATHOD CURRENT (MA)	RANGE	SLIT (mm)	FUEL	OXIDANT
Mg	285.2	20	UV	4	C ₂ H ₂	Air
Ba	553.6	20	Vis	2	C ₂ H ₂	N ₂ O
Co	240.7	30	UV	3	C ₂ H ₂	Air
Li	670.8	20	Vis	4	C ₂ H ₂	Air
V	318	30	UV	4	C ₂ H ₂	Air
Ni	232	25	UV	3	C ₂ H ₂	Air

Table 11

NEUTRON ACTIVATION INSTRUMENTAL PRECISION

SAMPLE NO. G-2

OXIDE	\bar{X}	MAX.	MIN.	RANGE	L.B.	U.B.	S	C.V. %	NO. OF ANALYSIS
Na ₂ O	4.13	4.24	4.04	0.20	4.08	4.18	0.08	1.90	9

SAMPLE NO. BCR-1

Na ₂ O	2.99	3.28	2.86	0.32	2.88	3.10	0.16	5.49	8
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Table 12

PRECISION TEST FOR ASHING

SAMPLE NO. 202

C & H ₂ O	7.67	7.98	7.38	0.60	7.46	7.87	0.22	2.81	5
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SAMPLE NO. 441

C & H ₂ O	8.09	8.6	7.89	0.71	7.82	8.37	0.29	3.58	5
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SAMPLE NO. 533

C & H ₂ O	4.63	4.79	4.5	.29	4.52	4.75	0.12	2.54	5
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SAMPLE NO. 827

C & H ₂ O	4.36	4.54	4.19	0.35	4.23	4.50	0.15	3.37	5
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Atomic Absorption Analysis

The concentrations of Mg, Ba, Co, Li, V and Ni were determined by Atomic Absorption Analysis. The technique used for sample preparation and analysis were adapted from the Atomic Absorption Newsletter, as well as from information in Angino and Billings (1967).

The results of the tests for the precision of the atomic absorption analysis are given in Tables 13 and 14. Four replicates of eight different samples were used in the test.

Appendix 1 lists the results obtained from atomic absorption analysis for Mg, Ga, Co, Li, V and Ni. The values are reported in parts per million. The method used under X-ray fluorescence can be used to convert these values to oxide percent.

Table 13

ATOMIC ABSORPTION INSTRUMENTAL PRECISION

SAMPLE NO. 243

ELEMENT	\bar{X}	MAX.	MIN.	RANGE	L.B.	U.B.	S	C.V. %	NO. OF ANALYSIS
Mg	.431	.446	.418	.028	.417	.445	0.01	2.67	4
Ba	830.	860.	800.	60.	800.	860.	25.82	3.11	4
Ni	89.	94.	84.	10.	83.	94.	4.43	5.01	4
Co	45.	46.	44.	2.	44.	46.	1.15	2.57	4
V	160.	160.	160.	0.	160.	160.	0.00	0.00	4
Li	12.	11.	12.	1.	11.	12.	.5	4.26	4

SAMPLE NO. 404

Mg	1.15	1.136	1.052	.084	1.03	1.27	0.10	8.88	4
Ba	640.	740.	580.	160.	556.	724.	71.18	11.12	4
Ni	109.	112.	106.	6.	106.	112.	2.58	2.37	4
Co	41.	44.	36.	8.	37.	45.	3.42	8.43	4
V	255.	260.	240.	20.	243.	267.	10.0	3.92	4
Li	23.	22.	24.	2.	21.	24.	1.00	4.44	4

SAMPLE NO. 586

Mg	.785	.872	.718	.154	.707	.862	0.07	8.37	4
Ba	640.	680.	580.	100.	589.	691.	43.20	6.75	4
Ni	157.	168.	140.	28.	141.	172.	13.10	8.37	4
Co	94.	96.	90.	6.	91.	97.	2.83	3.01	4
V	115.	120.	100.	20.	103.	127.	10.0	8.70	4
Li	16.	17.	16.	1.	16.	17.	0.50	3.08	4

SAMPLE NO. 202

Mg	.728	.774	.692	.082	.687	.768	0.03	4.69	4
Ba	600.	620.	580.	40.	581.	619.	16.33	2.72	4
Ni	40.	36.	46.	10.	34.	45.	4.43	11.23	4
Co	54.	56.	52.	4.	51.	56.	1.91	3.58	4
V	115.	120.	100.	20.	103.	127.	10.0	8.70	4
Li	16.	17.	16.	1.	16.	17.	0.50	3.08	4

Table 14

ATOMIC ABSORPTION INSTRUMENTAL PRECISION (CONT.)

SAMPLE NO. 441

ELEMENT

Mg	.982	1.026	.958	.068	.946	1.017	0.03	3.08	4
Ba	560.	580.	540.	40.	541.	579.	16.33	2.91	4
Ni	64.	62.	66.	4.	61.	66.	1.91	3.02	4
Co	58.	58.	58.	0.	58.	58.	0.00	0.00	4
V	170.	180.	160.	20.	156.	184.	11.55	6.79	4
Li	27.	28.	27.	1.	27.	28.	0.50	1.83	4

SAMPLE NO. 533

Mg	0.93	1.386	.708	.878	.559	1.30	0.93	33.86	4
Ba	745.	860.	620.	240.	611.	879.	113.58	15.24	4
Ni	54.	56.	50.	6.	51.	57.	2.83	5.24	4
Co	51.	54.	48.	6.	47.	54.	3.00	5.94	4
V	105.	120.	100.	20.	93.	117.	10.00	9.52	4
Li	15.	15.	14.	1.	14.	15.	0.50	3.39	4

SAMPLE NO. 827

Mg	.698	.714	.678	.036	.680	.715	0.02	2.15	4
Ba	490.	500.	480.	20.	476.	504.	11.55	2.36	4
Ni	34.	36.	32.	4.	32.	36.	1.63	4.80	4
Co	42.	42.	42.	0.	42.	42.	0.00	0.00	4
V	175.	180.	160.	20.	163.	187.	10.00	5.71	4
Li	10.	10.	9.	1.	9.	10.	0.50	5.13	4

SAMPLE NO. 838

Mg	1.43	1.680	1.224	.456	1.20	1.65	0.19	13.26	4
Ba	780.	840.	740.	100.	722.	838.	48.99	6.28	4
Ni	69.	72.	64.	8.	65.	73.	3.42	4.99	4
Co	45.	50.	40.	10.	39.	51.	4.76	10.58	4
V	245.	260.	240.	20.	233.	257.	10.00	4.08	4
Li	17.	17.	16.	1.	16.	17.	0.50	2.99	4

CHAPTER III: DATA ANALYSIS

DISCRIMINANT-FUNCTION ANALYSIS

Introduction

Many problems in geology are concerned with classification. One approach to handling such problems is the "best" linear function of the form:

$$Y = C + a_1 X_1 + a_2 X_2 + \dots + a_i X_n$$

C = constant

a_i = discriminant coefficient for variable i

X_n = element concentrations

which can be used to separate categories of individuals. Rao (1952) and Anderson (1958) give good accounts of the theory behind the method. Miller and Kahn (1962), Klovan and Billings (1967) and Krumbein and Graybill (1965) summarize some geologic applications of discriminant-functions.

Qualitative Example

Before entering into the specific problem involved, a brief explanation of the method is in order. Consider a study by Campbell and Lerbekmo (1963), in which the concentrations of a number of major oxide and trace elements were determined. Their study involved shales from the marine Wapiabi Formation (I in Fig. 6a,b, and c) and the continental Belly River Group (II in Fig. 6a b and c). The frequency distributions of CaO and Sr concentrations (Campbell and Lerbekmo, 1963, p. 22, Fig. 7, and p. 224, Fig. 8) are considered in the example. Both the oxide and the element concentrations appear to be normally distributed. On

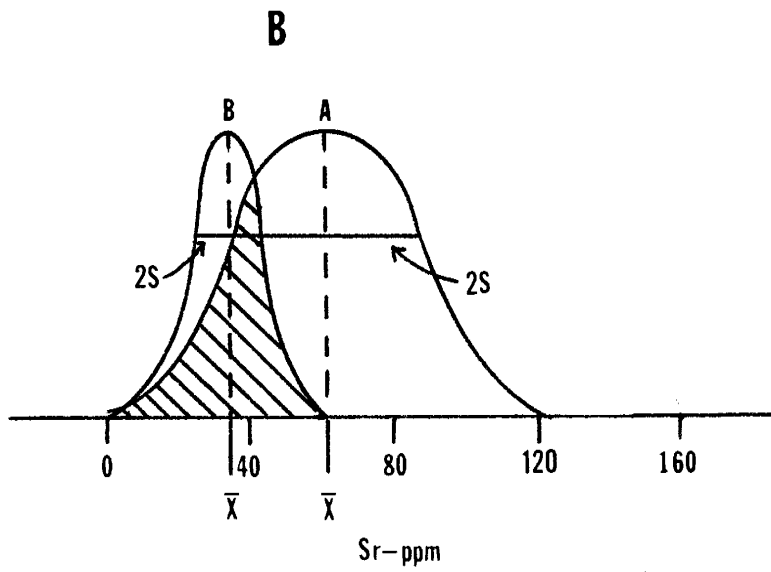
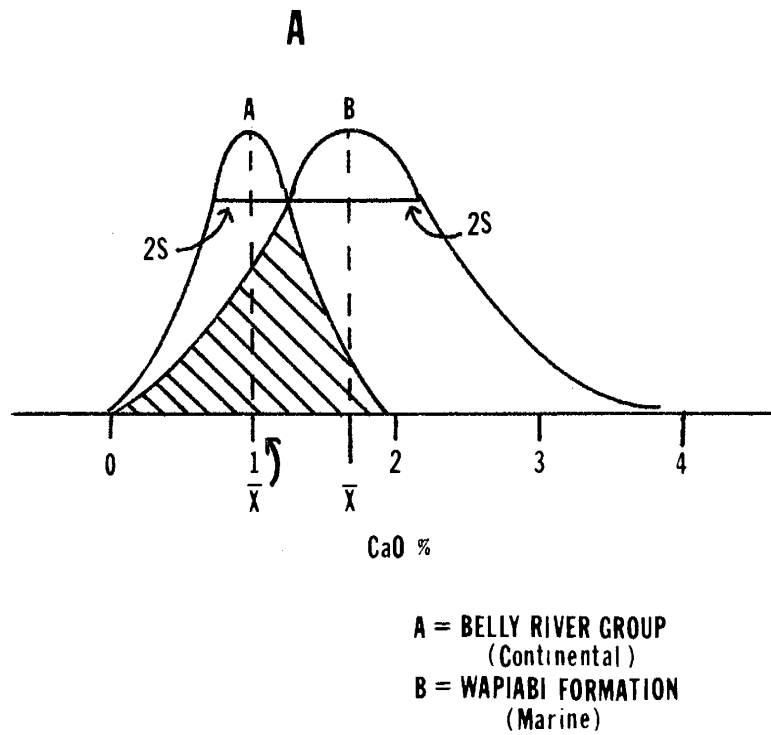


Figure 6. A: Frequency distribution of CaO %
B: Frequency distribution of Sr ppm.

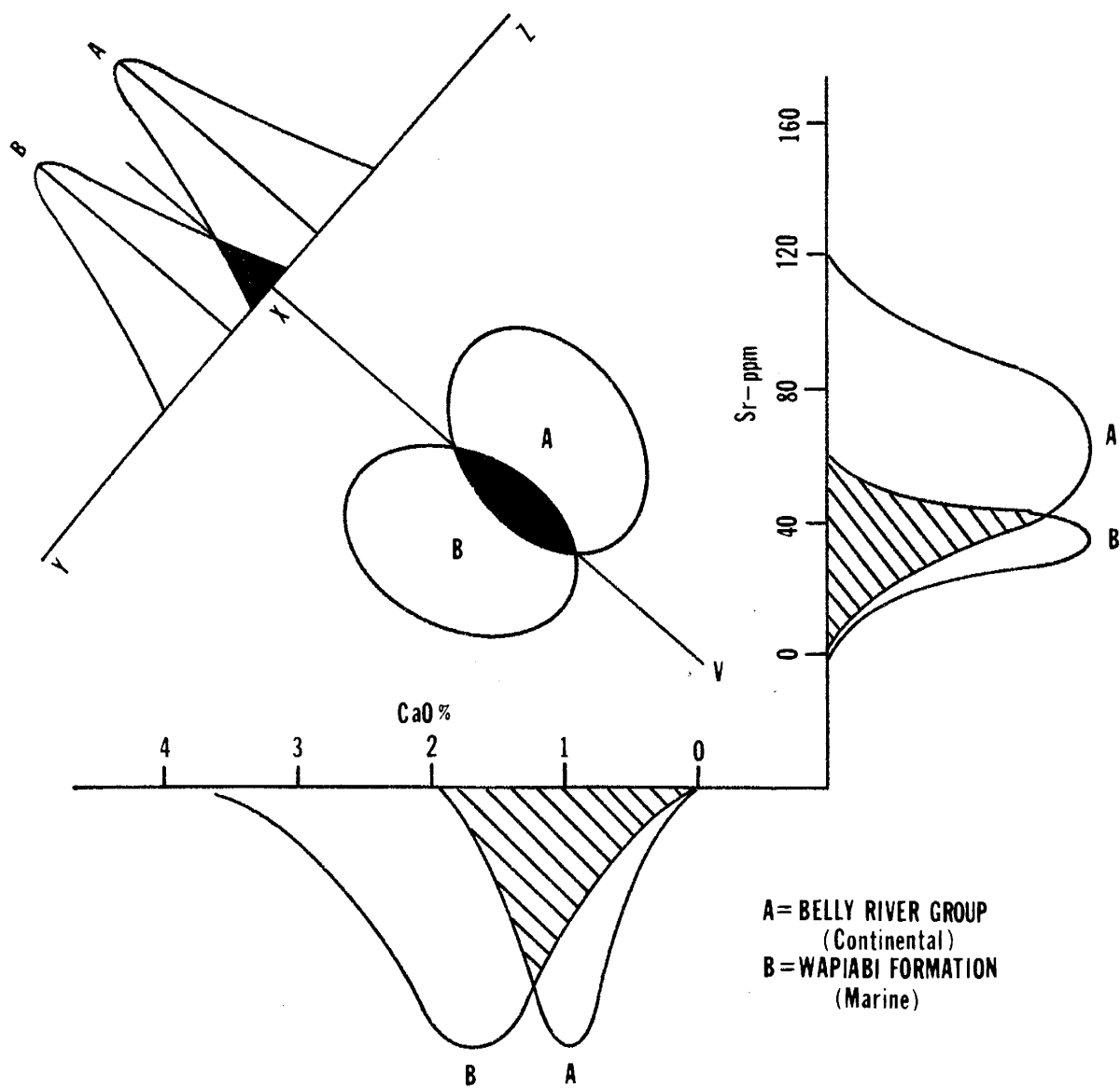


Figure 7. Bivariate plate with frequency contours and location of discriminant-functions.

examination of the frequency distributions (Fig. 6a and b), note that CaO appears to be more abundant, and Sr less abundant, in marine shales compared to continental shales. But considerable overlap exists between the frequency distribution of the concentrations in both cases. A classification scheme based on the abundance of a single oxide or element into one environment or another is tenuous at best.

If the oxide and element concentrations are assumed to be normally distributed, a series of ellipses within each group (Fig. 7) can be drawn. The ellipses represent contour values for the density of the items enclosed within them. A line can now be drawn through the intersection of the ellipses which have equal contour values (Line VX, Fig. 7). The two groups have now in fact, been separated in the "best" possible way. A second line (Line YXZ, Fig. 7) can be drawn perpendicular to VX. If all the points on the graph are projected on this line, they will show less overlap than along any other line on the graph. The line YXZ, does in fact represent two discriminant-functions of the form:

$$Y_1 = C_1 + a_{11} x_1 + a_{12} x_2$$

$$Y_2 = C_2 + a_{21} x_1 + a_{22} x_2$$

C = constant

a_{ij} = discriminant coefficient for variable j, in function i

x_1 = Sr concentration

x_2 = CaO concentrations.

That portion of the line YXZ (Fig. 7) between Z and X is represented by Y_1 , and Y_2 represents that segment of the line between Y and X.

The two functions Y_1 and Y_2 could now be used to classify an individual sample into the marine and continental groups, based on the two variables Sr and CaO. By substituting in sample values for Sr (x_1) and CaO (x_2), and evaluating the equations, the resulting values could be compared. If $Y_1 > Y_2$, the sample would be classified as marine. However, if $Y_2 > Y_1$, the sample would be classified as continental.

In this example, only two variables from two different populations were considered in order to facilitate visualization of the method. The example could be expanded to include more variables from the population, because the solution for the discriminant-function is similar in n-dimensional space as in two-dimensional space.

The Assumption of Normality

In trace and major element studies, the discriminant-function has the disadvantage of being a parametric technique. Thus, for the purpose of testing, it is assumed that the elements have a normal distribution. Much has been written in recent years, concerning this question. The main issue is whether elements are normally distributed, or if they have a special distribution function, and what its exact form is. Ahrens (1954), Miller and Goldberg (1955), Tennat and White (1959), and Vistelius (1960) use empirical data to test the form of the distribution. Their data suggests some elements, such as Na, might be normally distributed, but other elements, such as Cu, may be lognormally distributed. Shaw (1961) developed theoretical distributions, and concluded that no single distribution suited all elements.

Most workers agree that a normal distribution is appropriate for the major elements, but there is less agreement for trace elements.

Potter et al. (1963) found that in applying their original trace element data, and logarithmically transformed data to discriminant analysis, there was no major difference in the results.

When considering the problem of element distribution, one should make a distinction between the two concepts of normality that enter here. First, there is the question of how elements are distributed areally. However this question is distinct from the one which asks about the normality of observed measurements in a particular locality or, put another way, the normality of the data being used in the discriminant analysis. In the case in question, element concentrations are calculated using the mean value from a number of independent observations (for example using X-ray analysis, the concentration of an element is calculated from seven separate nonsequential observations on a sample).

The assumption that the variables are normally distributed can be justified by use of the central limit theorem. The theorem can be stated as follows: (Larson, 1968, p. 187). X_1, X_2, X_3, \dots is a sequence of independent identically distributed, random variables, each with mean μ and variance σ^2 . Define the sequence of random variables Z_1, Z_2, Z, \dots by

$$Z_n = \frac{\bar{X}_n - \mu}{\sigma/\sqrt{n}} \quad n = 1, 2, 3, \dots$$

Where

$$\bar{X}_n = \frac{1}{n} \sum_{i=1}^n X_i.$$

Then, for all real t ,

$$\lim_{n \rightarrow \infty} F_{Z_n}(t) = N_Z(t)$$

where N_Z is the standard normal distribution function.

Referring to the theorem, then $X_1, X_2, X_3, \dots, X_n$ (concentration of an element) are independent because:

$$P(X_1 = a_1, X_2 = a_2, \dots, X_n = a_n) = P(X_1 = a_1) P(X_2 = a_2) \dots P(X_n = a_n)$$

for all values of (a_1, a_2, \dots, a_n) . The concentration is then calculated

$$\bar{X}_n = \frac{1}{n} \sum_{i=1}^n x_i$$

where n equals the number of observations on a sample for the element in question. Even if the observations are taken sequentially, and are therefore correlated, the central limit theorem can be used to justify a normal approximation. Therefore, for a large sample size, use of the normal distribution is justified. A similar result can be used to justify a multivariate normal distribution.

Test of Significance

Under the assumptions that the original measurements have a multivariate normal distribution within the populations from which the samples were drawn, and that the variance-covariance matrices are equal for the populations, there are a number of tests which can be performed. The Mahalanobis D^2 statistics can be used to test if there is a significant difference between the mean discriminant-function scores. The D^2 statistics is defined as:

$$D^2 = d' C^{-1} d$$

$$d' = d = \text{vector of mean differences}$$

$$C^{-1} = \text{inverse of the within-groups variance-covariance matrix.}$$

Under the above assumptions, the D^2 statistic is related to the F distribution by:

$$F = \frac{n_1 n_2 (n_1 + n_2 - p - 1)}{p(n_1 + n_2)(n_1 + n_2 - 2)} D^2$$

Where

n_1 and n_2 = sample sizes

p = number of variables

The F statistic can be read from probability tables for $F(p, n_1 + n_2 - p - 1)$ degrees of freedom, to test whether there is a significant difference between the two groups. If the calculated value is greater than the tabulated F value, a significant difference exists.

Elimination of Inefficient Variables

In practice, the elimination of unneeded variables is very desirable. The goal of the study is to be able to classify individuals based on the smallest number of effective variables. The presence of ineffective variables not only increases the amount of analytical work, but also weakens the power of discriminant-functions.

The D^2 statistic can also be used to test whether certain variables can be eliminated from the discriminant-functions, without any significant loss in the power of the functions. The test statistic used, Rao (1952) is:

$$F = \frac{n_1 + n_2 - 1}{p - q} \cdot \frac{n_1 n_2 (D_p^2 - D_q^2)}{(n_1 + n_2)(n_1 + n_2 - 2) + n_1 n_2 D_q^2}$$

where

n_1 and n_2 = sample size

p = original number of variables

q = number of variables after elimination

$D_p^2 = d' C^{-1} d$ for original groups

$D_q^2 = d' C^{-1} d$ for groups after elimination.

The F statistic can then be read from probability tables for $F(p - q, n_1 + n_2 - p - 1)$ degrees of freedom. If the calculated value is less than the tabulated F value, no loss in the power of the discriminant-functions results from the elimination of variables.

Another method of selecting which variables to eliminate is based on the size of the coefficient of variation which gives some idea of the ease and precision with which elements can be analyzed. The coefficients of the discriminant-functions do not show the relative importance of the variables, and hence are not directly useful in making this choice.

Use of Discriminant-Functions

The form of the discriminant-functions used in this study is:

$$Y = C + a_1 X_2 + a_1 X_2 + \dots + a \cdot X_n .$$

A function of this form is calculated for each group. When using this method of analysis to separate two groups, the cutting point X (Fig. 7), can be found by:

$$\text{Cutting Point} = C_1 - C_2$$

C_1 and C_2 = constants.

To classify an unknown sample, into one of the two groups, compute:

$$\bar{Y}_{1n} = C_1 + a_{11} X_1 + a_{12} X_2 + \dots + a_{1n} X_n$$

and

$$\bar{Y}_{2n} = C_2 + a_{21} X_1 + a_{22} X_2 + \dots + a_{2n} X_n$$

for the sample. The $X_1, X_2, X_3, \dots, X_n$ are the observed values of the element concentrations on the unknown sample and C_1 and C_2 are constants. The sample is classified as belonging to population one if \bar{Y}_n is closer to \bar{Y}_{1n} , and from population two if the reverse is true.

That is:

$$V = \bar{Y}_n - \frac{(\bar{Y}_{1n} - \bar{Y}_{2n})}{2}$$

is computed and the sample is classified as belonging to group one if $V > 0$, and to group two if $V \leq 0$. Anderson (1958) shows that as $n_1 \rightarrow \infty$, and $n_2 \rightarrow \infty$, the distribution of V tends to be normal $(\alpha/2, \alpha)$ or $(-\alpha/2, \alpha)$ depending on whether the sample belongs to group one or two, and the difference, V , may be estimated by:

$$D^2 = d' C^{-1} d = \bar{Y}_{1n} - \bar{Y}_{2n} .$$

Therefore, for large n_1 and n_2 , the approximate probability of misclassifying a sample can be calculated by:

$$1 - F_Z(D/2) \quad (\text{Where } F_Z(D/2) \text{ indicates the normal distribution function at } D/2)$$

In order to classify a formation as belonging to group one or two, the following procedure can be used (Anderson, 1958):

$$\bar{Y}_{sn} = \sum_{i=1}^n a_i \bar{Y}_{si}$$

and

$$\bar{V} = \bar{Y}_{sn} - \frac{(\bar{Y}_{1n} + Y_{2n})}{2}$$

where \bar{Y}_{si} is the average of the Y_i 's of the samples. The formation is classified as belonging to group one, if $\bar{V} > 0$, and group two if $\bar{V} \leq 0$.

APPLICATION TO THE PROBLEM

Basis for Discriminant-Model

Wall et al. (1971) studied the paleoecology of the 57 samples from the Strathmore core, between 1350 ft. to 1760 ft. On the basis of foraminiferal and megaspore evidence, they classify portions of this section of the core as being either continental, brackish or marine. In formulating the discriminant model, those samples of the core for which the depositional environment is known, based on the following paleoecological evidence, were used as standards.

Continental:	20 samples (Table 20)	
Evidence:	Abundant megaspores and lack of formaminifera.	
Megaspores:	<u>Azolla spp.</u>	<u>Azolla conspicua</u>
	<u>Molaspora</u>	<u>Azollopsis</u>
	<u>Balmeisporites</u>	<u>Erlansonisporites</u>
	<u>Minerisporites</u>	<u>Bacutriletes</u>
	<u>Spermatites-Costatheca types</u>	
Brackish:	63 samples (Table 21)	
Evidence:	Exclusively agglutinated foraminiferal fauna and a reduced megaspore population.	

Foraminifera:	<u>Miliammina</u>
	<u>Trochammina</u>
	<u>Verneuilinoides</u>
Marine:	25 samples (Table 22)
Evidence:	Varied foraminiferal fauna, with the agglutinated element superior in both species diversity and total population. Reduction in the total megaspore numbers with complete disappearance at maximum transgression.

A total of 108 samples fulfilled these criteria and were used to set the model. A two-step approach was used to facilitate statistical testing. In the first step, the groups marine vs. continental-brackish were separated. Then in the second step, the composite group (continental-brackish) was separated into a continental group and a brackish group. Therefore, the final model consists of the groups: continental, brackish and marine. A three-way discriminant analysis was also tried, but the pairwise approach proved to be more effective. The discriminant analysis was carried out on an IBM 360/40 computer, using the program described in System/360 Scientific Subroutine Package (1968).

Discrimination Between Samples of Known Depositional Environment

Marine vs. Continental-Brackish Using All Variables

In applying discriminant-function analysis, it is assumed that there is a common covariance matrix for the groups of data, and that the means of the elements within the groups vary. To obtain the common covariance matrix, the covariance matrices of the groups were pooled.

All 24 variables were used, initially, to classify (the classifications are given in appendix 2) the samples into established groups (Marine vs.

Continental-Brackish). The discriminant-functions obtained (using all 24 variables) are given in Table 24. The constant is given first, followed by the discriminant coefficients. To use the functions for classification, the values of X_1, X_2, \dots, X_n (element concentrations) are substituted into the equations and solved. Based on the calculated value, the known sample is then classified as being either marine or continental-brackish origin.

A test of the significance of the functions was then performed using the D^2 value given in Table 15. The results of the test, given in Table 16, indicate that at the .999 significance level, the two populations can be separated using all 24 variables.

Tables 17, 18 and 19 give the depth and classification of the samples used as standards, based on paleontological evidence. The tables also give the sample classifications based on the discriminant-functions. Using the classification model, only 9.25% of the samples were misclassified.

Continental vs. Brackish Using All Variables

Once it was established that it was possible to separate the Marine vs. Continental-Brackish groups, a second step was taken. The group Continental-Brackish was divided into a continental group and a brackish group. The discriminant-functions obtained (using all 24 variables) are given in Table 20 and the classifications are given in Appendix 3.

The D^2 value (Table 20) was then used to test the significance of the functions. Results of the test are given in Table 16. The test indicates that at the .999 significance level, the two groups can be separated using all 24 variables.

The depth and classification of the samples used as standards is given in Table 17 and 18. Only 2.4% of the samples were misclassified using this model.

Table 15
DISCRIMINANT-FUNCTION 24 VARIABLES

ELEMENT CONCENTRATION	GROUP CONTINENTAL-BRACKISH		GROUP MARINE	
	Y_1		Y_2	
	$C_1 = 672.12109375$		$C_2 = 655.823486328$	
	COEFFICIENTS		COEFFICIENTS	
$X_1 = \text{Si}$	a_{11}	.002302214	a_{21}	.002271105
$X_2 = \text{Al}$	a_{12}	.003894767	a_{22}	.003866632
$X_3 = \text{Fe}$	a_{13}	.001746652	a_{23}	.001748435
$X_4 = \text{Mg}$	a_{14}	-.00099485	a_{23}	.000912193
$X_5 = \text{Ca}$	a_{15}	.003474343	a_{25}	.00343548
$X_6 = \text{Na}$	a_{16}	-.000355249	a_{26}	-.000346826
$X_7 = \text{K}$	a_{17}	.001326057	a_{27}	.00116819
$X_8 = \text{Ti}$	a_{18}	.009732164	a_{28}	.009451542
$X_9 = \text{Mn}$	a_{19}	.031533159	a_{29}	.034335159
$X_{10} = \text{Ba}$	a_{110}	-.001753531	a_{210}	-.006129816
$X_{11} = \text{Co}$	a_{111}	.228197813	a_{211}	-.117014527
$X_{12} = \text{Cu}$	a_{112}	.696543355	a_{212}	-.83538568

Table 15 (CONT.)

DISCRIMINANT-FUNCTION 24 VARIABLES

ELEMENT CONCENTRATION	GROUP		GROUP	
	CONTINENTAL-BRACKISH		MARINE	
	Y		Y	
	COEFFICIENTS		COEFFICIENTS	
X ₁₃ = Ga	a ₁₁₃	-2.655446053	a ₂₁₃	-2.722186089
X ₁₄ = Li	a ₁₁₄	-2.243256569	a ₂₁₄	2.798372269
X ₁₅ = Mo	a ₁₁₅	-.197466195	a ₂₁₅	.4448874
X ₁₆ = Pb	a ₁₁₆	.588289559	a ₂₁₆	.584162354
X ₁₇ = Rb	a ₁₁₇	-.154583931	a ₂₁₇	-.155018508
X ₁₈ = S	a ₁₁₈	-.002759227	a ₂₁₈	-.00339602
X ₁₉ = Sr	a ₁₁₉	.705316424	a ₂₁₉	.667390287
X ₂₀ = C and H ₂ O	a ₁₂₀	.000884702	a ₂₂₀	.000819143
X ₂₁ = Zn	a ₁₂₁	-.01688176	a ₂₂₁	-.004104771
X ₂₂ = Zr	a ₁₂₂	.041593067	a ₂₂₂	.058920398
X ₂₃ = V	a ₁₂₃	.20898813	a ₂₂₃	.213495553
X ₂₄ = Ni	a ₁₂₄	0.052475989	a ₂₂₄	-.056538284

$$D^2 = 148.7272$$

Table 16

TEST OF SIGNIFICANCE OF DISCRIMINANT-FUNCTIONS

GROUP	NO. OF VARIABLES	D ²	COMPUTED F	TABULATED F
Continental- Brackish vs. Marine	24	148.7272	93.22	F(24,83) = 2.58
Continental vs. Brackish	24	233.2939	104.37	F(24,58) = 2.72
Continental- Brackish vs. Marine	12	122.7419	176.12	F(12,83) = 3.20
Continental vs. Brackish	16	161.3536	124.74	F(16,58) = 3.06

Table 17

Samples used as Standards
Number of Samples: 20

Environment: Continental (Wall, et al. 1971)

Sample No.	Depth	Classification from Model
374	1351' - 1352.5'	Continental
375	1352.5'- 1355'	Continental
376	1355' - 1360'	Continental
378	1360.2'- 1364'	Continental
379	1364' - 1368'	Continental
381	1370' - 1371.7'	Continental
382	1371.7'- 1372.7'	Continental
383	1372.7'- 1376'	Continental
387	1386' - 1386.5'	Continental
388	1386.5'- 1392.5'	Continental
389	1392.5'- 1393.5'	Continental
390	1393.5'- 1398.5'	Continental
391	1398.5'- 1402'	Continental
393	1410' - 1412'	Continental
394	1412' - 1418'	Continental
395	1418' - 1425'	Continental
396	1425' - 1430.5'	Continental
397	1430.5'- 1437'	Continental
412	1492' - 1496.5'	Continental
413	1496.5'- 1499'	Continental

Table 18

Samples used as Standards
 Number of samples: 63

Environment: Brackish (Wall, et al. 1971)

Sample No.	Depth	Classification from Model
402	1456.5' - 1461.5'	Brackish
403	1461.5' - 1466.5'	Continental
404	1466.5' - 1471.5'	Brackish
405	1471.5' - 1477.5'	Brackish
406	1477.5' - 1483'	Brackish
407	1483' - 1483.5'	Brackish
408	1483.5' - 1489'	Brackish
409	1489' - 1491.5'	Brackish
410	1491.5' - 1492'	Brackish
411	1492' - 1496.5'	Brackish
414	1505.5' - 1506'	Brackish
415	1506' - 1511'	Brackish
416	1511' - 1514'	Brackish
417	1514' - 1515'	Brackish
418	1515' - 1519'	Brackish
420	1520' - 1529'	Brackish
421	1529' - 1536'	Brackish
422	1536' - 1537.5'	Brackish
423	1537.5' - 1539.5'	Brackish
424	1539.5' - 1540'	Brackish
425	1540' - 1545.5'	Brackish
426	1545.5' - 1551'	Brackish
427	1551' - 1553'	Brackish
428	1553' - 1555'	Brackish
429	1555' - 1560'	Brackish
430	1560' - 1562.5'	Brackish
431	1562.5' - 1563'	Brackish
433	1564' - 1566'	Brackish
434	1566' - 1569'	Brackish
435	1569' - 1570.5'	Brackish
436	1570.5' - 1571'	Brackish
437	1571' - 1572.5'	Brackish
439	1572.5' - 1573.5'	Brackish

Table 18 (CONT.)

Environment: Brackish (Wall, et al. 1971)

Sample No.	Depth	Classification from Model
444	1595' - 1597.5'	Brackish
445	1597.5' - 1600.5'	Brackish
447	1601' - 1601.2'	Brackish
448	1601.2' - 1605'	Brackish
449	1605' - 1608.5'	Brackish
451	1611.5' - 1613'	Brackish
452	1613' - 1614'	Brackish
454	1614.2' - 1614.5'	Brackish
456	1617.5' - 1617.6'	Brackish
458	1622.5' - 1623'	Continental
459	1623' - 1624'	Brackish
462	1625.7' - 1628'	Brackish
464	1631' - 1633.5'	Brackish
465	1633.5' - 1638.5'	Brackish
466	1638.5' - 1640'	Brackish
485	1702' - 1705'	Brackish
486	1705' - 1707'	Brackish
487	1707' - 1711'	Brackish
488	1711' - 1715.5'	Brackish
490	1716' - 1721'	Brackish
491	1721' - 1725.5'	Brackish
492	1725.5' - 1728'	Brackish
493	1728' - 1730'	Brackish
494	1730' - 1735'	Brackish
495	1735' - 1736'	Brackish
496	1736' - 1736.2'	Brackish
497	1736.2' - 1739.5'	Brackish
498	1739.5' - 1743'	Brackish
499	1743' - 1750.5'	Brackish
500	1750.5' - 1751.5'	Brackish

Table 19

Samples used as Standards
 Number of Samples: 25

Environment: Marine (Wall, et al. 1971)

Sample No.	Depth	Classification from Model
398	1437' - 1441.5'	Continental
399	1441.5' - 1442'	Marine
400	1442' - 1450'	Marine
401	1450' - 1456'	Marine
440	1577.5' - 1582'	Marine
441	1582' - 1585.5'	Brackish
442	1585.5' - 1590.5'	Marine
443	1590.5' - 1595'	Marine
468	1641' - 1647'	Marine
469	1647' - 1652'	Marine
470	1652' - 1657'	Marine
471	1657' - 1662'	Marine
472	1662' - 1666'	Marine
473	1666' - 1668'	Continental
474	1668' - 1672'	Marine
475	1672' - 1677'	Marine
476	1677' - 1683'	Marine
477	1683' - 1684'	Marine
478	1684' - 1688'	Marine
479	1688' - 1689'	Marine
480	1689' - 1693'	Marine
481	1693' - 1694'	Marine
482	1694' - 1697'	Marine
483	1697' - 1698'	Marine
484	1698' - 1702'	Marine

Table 20
DISCRIMINANT-FUNCTION 24 VARIABLES

ELEMENT CONCENTRATION	GROUP CONTINENTAL		GROUP BRACKISH	
	Y_1		Y_2	
	$C_1 = -663.8369140625$		$C_2 = -642.0764160156$	
	COEFFICIENTS		COEFFICIENTS	
$X_1 = \text{Si}$	a_{11}	.001965966	a_{21}	.00190019
$X_2 = \text{Al}$	a_{12}	.005069651	a_{22}	.00497276
$X_3 = \text{Fe}$	a_{13}	.00623142	a_{23}	.000759674
$X_4 = \text{Mg}$	a_{14}	-.000061675	a_{24}	-.000585826
$X_5 = \text{Ca}$	a_{15}	.003445059	a_{25}	.003435484
$X_6 = \text{Na}$	a_{16}	-.000779842	a_{26}	-.000576482
$X_7 = \text{K}$	a_{17}	-.000536586	a_{27}	.000025592
$X_8 = \text{Ti}$	a_{18}	.011025891	a_{28}	.010647856
$X_9 = \text{Mn}$	a_{19}	.065531731	a_{29}	.065516114
$X_{10} = \text{Ba}$	a_{110}	.023381993	a_{210}	.024494164
$X_{11} = \text{Co}$	a_{111}	-1.435041428	a_{211}	-1.177947998
$X_{12} = \text{Cu}$	a_{112}	-.745163262	a_{212}	-.711669028

Table 20 (CONT.)
DISCRIMINANT-FUNCTION 24 VARIABLES

ELEMENT CONCENTRATION	GROUP CONTINENTAL Y_1		GROUP BRACKISH Y_2	
	COEFFICIENTS		COEFFICIENTS	
X ₂₁₃ = Ga	a ₁₁₃	-2.457188606	a ₂₁₃	-2.512981878
X ₂₁₄ = Li	a ₁₁₄	4.810051918	a ₂₁₄	4.54336319
X ₂₁₅ = Mo	a ₁₁₅	-.248349905	a ₂₁₅	.307203293
X ₂₁₆ = Pb	a ₁₁₆	.515569746	a ₂₁₆	.489494443
X ₂₁₇ = Rb	a ₁₁₇	-.103220463	a ₂₁₇	-.10794884
X ₂₁₈ = X	a ₁₁₈	-.004675575	a ₂₁₈	-.003040926
X ₂₁₉ = Sr	a ₁₁₉	.558767855	a ₂₁₉	.578331649
X ₂₂₀ = C and H ₂ O	a ₁₂₀	.000838356	a ₂₂₀	.000766255
X ₂₂₁ = Zn	a ₁₂₁	.031175487	a ₂₂₁	.00687395
X ₂₂₂ = Zr	a ₁₂₂	.107873261	a ₂₂₂	.111444116
X ₂₂₃ = V	a ₁₂₃	.228050411	a ₂₂₃	.181617081
X ₂₂₄ = Ni	a ₁₂₄	-.00958246	a ₂₂₄	.012258112

$$D^2 = 233.2939$$

Marine vs. Continental - Brackish Using 12 Variables

The environments marine, brackish and continental can be effectively separated using discriminant-functions based on all the variables. The function used, however, may not be the most efficient. This is because some of the variables do not add to the discriminatory power of the functions. The most efficient functions would contain the smallest number of meaningful variables.

One basis (Potter, et al. 1963) for selecting a smaller number of variables is the ease and precision (size of coefficient of variation) with which the elements can be analyzed. Variables with high coefficients of variation tend to obscure the information contributed by those of low variability. Table 21 gives the coefficients of variation for the elements analyzed. The first elements eliminated were those with a coefficient of variation greater than 60%. In the second elimination variables with coefficients of variation greater than 50% were eliminated. In addition, Si and Al were also eliminated because of the abundance and variety of alumino-silicates in all three environments. Thus sixteen variables were left after the first elimination, and twelve were left after the second elimination.

Table 22 shows that 12.96% of the samples were misclassified using twelve variables. The variables used are given in Table 21.

An F test was used to test the significance of the functions. The results of the test are given in Table 16. The results indicate that the marine vs. continental-brackish groups can be effectively discriminated by using twelve variables at the .999 significance level.

Another F test was performed to determine whether the twelve variable functions are as effective as the functions based on all the variables.

Table 21

Coefficients of Variation for Analyzed Elements

ORIGINAL VARIABLES	C.V. %	SIXTEEN VARIABLES USED	TWELVE VARIABLES USED
Si	9.76		
Al	12.63		
Fe	60.33		
Mg	50.07	Mg	
Ca	91.42		
Na	57.03	Na	
K	52.19	K	
Ti	20.76	Ti	Ti
Mn	47.97	Mn	Mn
Ba	33.46	Ba	Ba
Co	30.00	Co	Co
Cu	35.48	Cu	Cu
Ga	26.08	Ga	Ga
Li	35.71	Li	Li
Mo	123.52		
Pb	100.00		
Rb	58.65	Rb	
S	160.36		
Sr	28.27	Sr	Sr
C and H ₂ O	48.70	C and H ₂ O	C and H ₂ O
Zn	35.16	Zn	Zn
Zr	18.43	Zr	Zr
V	40.35	V	V
Ni	69.53		

Table 22
Percent of Samples Using Discriminant-Functions

ENVIRONMENT	NO. OF VARIABLES	PERCENT MISCLASSIFIED
CONTINENTAL BRACKISH	24	9.25
VS.		
MARINE		
CONTINENTAL	24	2.40
VS.		
BRACKISH		
CONTINENTAL	16	7.22
VS.		
BRACKISH		
CONTINENTAL BRACKISH	12	12.96
VS.		
MARINE		
CONTINENTAL	12	10.84
VS.		
BRACKISH		

Results of the test are given in Table 23. Since the F test is not significant, the new discriminant-functions for the marine vs. continental-brackish group are as good as the original functions based on twenty four variables. The functions using twelve variables are given in Table 24 and the classifications are given in Appendix 4.

Continental vs. Brackish Using 16 Variables

The same procedures for the elimination of variables was used in this case, as in the previous section. Table 22 shows that 7.22% of the samples used as standards were misclassified using sixteen variables. Table 21 lists the variables used.

A test of significance was first used to test whether the environments continental vs. brackish could be separated using sixteen variables. Table 16 lists the results of the test. Since the results are not significant at the .999 level, it can be concluded that the new functions are as good as the original functions based on twenty four variables.

A second F test was also used to determine whether the sixteen variable functions were as effective as the twenty four variable functions. Table 23 lists the results of the test. From the table, note that the calculated F value is less than the tabulated F value. Therefore, the functions containing sixteen variables are as effective for separating the groups continental vs. brackish as the functions containing twenty four variables. The functions used for discriminating between the continental and brackish groups based on sixteen variables are given in Table 25 and the classifications are given in Appendix 5.

A further attempt at the elimination of variables was tried. The results of the F test at the .999 significance level, however, failed.

Test 23

Tests of significance for best discriminant-functions

Group	No. of Variables	Computed F	D ²	Tabulated F
Continental- Brackish vs. Marine	24		148.7272	
Continental vs. Brackish	24		233.2939	
Continental- Brackish vs. Marine	12	1.40	122.7419	F(12,83) = 3.20
Continental vs. Brackish	16	3.13	161.3536	F(8,58) = 3.90

Table 24

DISCRIMINANT-FUNCTION 12 VARIABLES

ELEMENT CONCENTRATION	GROUP		GROUP	
	CONTINENTAL-BRACKISH		MARINE	
	Y_1		Y_2	
	$C_1 = -66.758499146$		$C_2 = -64.052871704$	
	COEFFICIENTS		COEFFICIENTS	
X ₈ = Ti	a ₁₈	.005764309	a ₂₈	.005346049
X ₉ = Mn	a ₁₉	.014571335	a ₂₉	.018260937
X ₁₀ = Ba	a ₁₁₀	.02095557	a ₂₁₀	.017059784
X ₁₁ = Co	a ₁₁₁	.082721114	a ₂₁₁	.164994419
X ₁₂ = Cu	a ₁₁₂	-.028128639	a ₂₁₂	-.164303243
X ₁₃ = Ga	a ₁₁₃	-.03834337	a ₂₁₃	-.140111923
X ₁₄ = Li	a ₁₁₄	1.050294876	a ₂₁₄	1.512454033
X ₁₉ = Sr	a ₁₁₉	.216511965	a ₂₁₉	.199439049
X ₂₀ = C and H ₂ O	a ₁₂₀	.000167535	a ₂₂₀	.000122587
X ₂₁ = Zn	a ₁₂₁	-.130207002	a ₂₂₁	-.119072437
X ₂₂ = Zr	a ₁₂₂	.104708612	a ₂₂₂	.101185918
X ₂₃ = V	a ₁₂₃	.023740549	a ₂₂₃	.027622953

$$D^2 = 122.7419$$

Table 25
DISCRIMINANT-FUNCTION 16 VARIABLES

ELEMENT CONCENTRATIONS	GROUP CONTINENTAL		GROUP BRACKISH	
	Y ₁		Y ₂	
	C ₁ = -73.719589233		C ₂ = -79.568618774	
	COEFFICIENTS		COEFFICIENTS	
X ₄ = Mg	a ₁₄	.000157554	a ₂₄	-.000245353
X ₆ = Na	a ₁₆	-.00003794	a ₂₆	.000070451
X ₆ = K	a ₁₇	.000390766	a ₂₇	.000716941
X ₈ = Ti	a ₁₈	.0070289	a ₂₈	.006231286
X ₉ = Mn	a ₁₉	.003115894	a ₂₉	.011671495
X ₁₀ = Ba	a ₁₁₀	.026661061	a ₂₁₀	.027534287
X ₁₁ = Co	a ₁₁₁	-.282367647	a ₂₁₁	-.028423373
X ₁₂ = Cu	a ₁₁₂	.03970325	a ₂₁₂	.043120325
X ₁₃ = Ga	a ₁₁₃	-.197733819	a ₂₁₃	.400927782
X ₁₄ = Li	a ₁₁₄	1.965940475	a ₂₁₄	1.719291687
X ₁₇ = Rb	a ₁₁₇	.041430663	a ₂₁₇	.043033693
X ₁₉ = Sr	a ₁₁₉	.329023361	a ₂₁₉	.351169348
X ₂₀ = C and H ₂ O	a ₁₂₀	.000189272	a ₂₂₀	.000167543
X ₂₁ = Zn	a ₁₂₁	-.213716447	a ₂₂₁	-.190811217
X ₂₂ = Zr	a ₁₂₂	.029654499	a ₂₂₂	.041280117
X ₂₃ = V	a ₁₂₃	.022531826	a ₂₂₃	-.014962699

$$D^2 = 161.3536$$

This indicates that the sixteen variable functions for the group continental vs. brackish and the twelve variable functions for the group continental-brackish vs. marine are the most efficient functions to use for the purpose of classification.

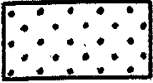

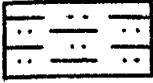
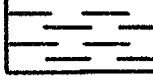

Further Elimination of Variables Based on Percent of Misclassification

When classifying unknown samples, the "best" results are obtained using the functions containing sixteen variables for the groups continental vs. brackish, and the functions containing twelve variables for the groups marine vs. continental-brackish. However, in an attempt to further eliminate variables, a test was formulated which considered only the percentage of misclassified samples. Table 22 gives the result of the test. Using twelve variables based on 108 samples; 12.96% of the samples are misclassified for the groups marine vs. continental-brackish. For the groups continental vs. brackish, using twelve variables based on 83 samples; 10.84% of the samples are misclassified. Even though the functions based on twelve variables are valid, they are not statistically significant at the .999 level. They could be used as a quick check for classifying unknown samples. The variables used are: Ti, Mn, Ba, Cu, Ga, Li, Sr, C plus H₂O, Zn, Zr and V.

Comparison of Paleoecologic Classification with Discriminant-Function

Figure 8 is an adaptation of the work from Wall et al. (1971) and Havard (1971). This figure checks the model against the curve for environments based on Wall's work, and the stratigraphic column based on Havard's work. The column to the right on Figure 8 includes samples used to formulate the discriminant-function plus 22 samples for which the paleoecologic evidence is not clear. Comparison of their work with the classification scheme based on discriminant-functions, shows that there

LEGEND
STRATHMORE EV 7-12-25-25
ROCK TYPES

	Sandstone		Siltstone
	Mudstone		Shale
	Coal, coaly		

ACCESSORIES










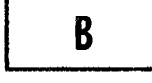



	Calcareous		Carbonaceous
	Sideritic		Sandstone pebbles
	Siderite nodules		Cross-bedding
	Shale pebbles		Fossils
	Mudstone pebbles		Bentonitic
	Siltstone pebbles		Convolute bedding
	Worm burrows		

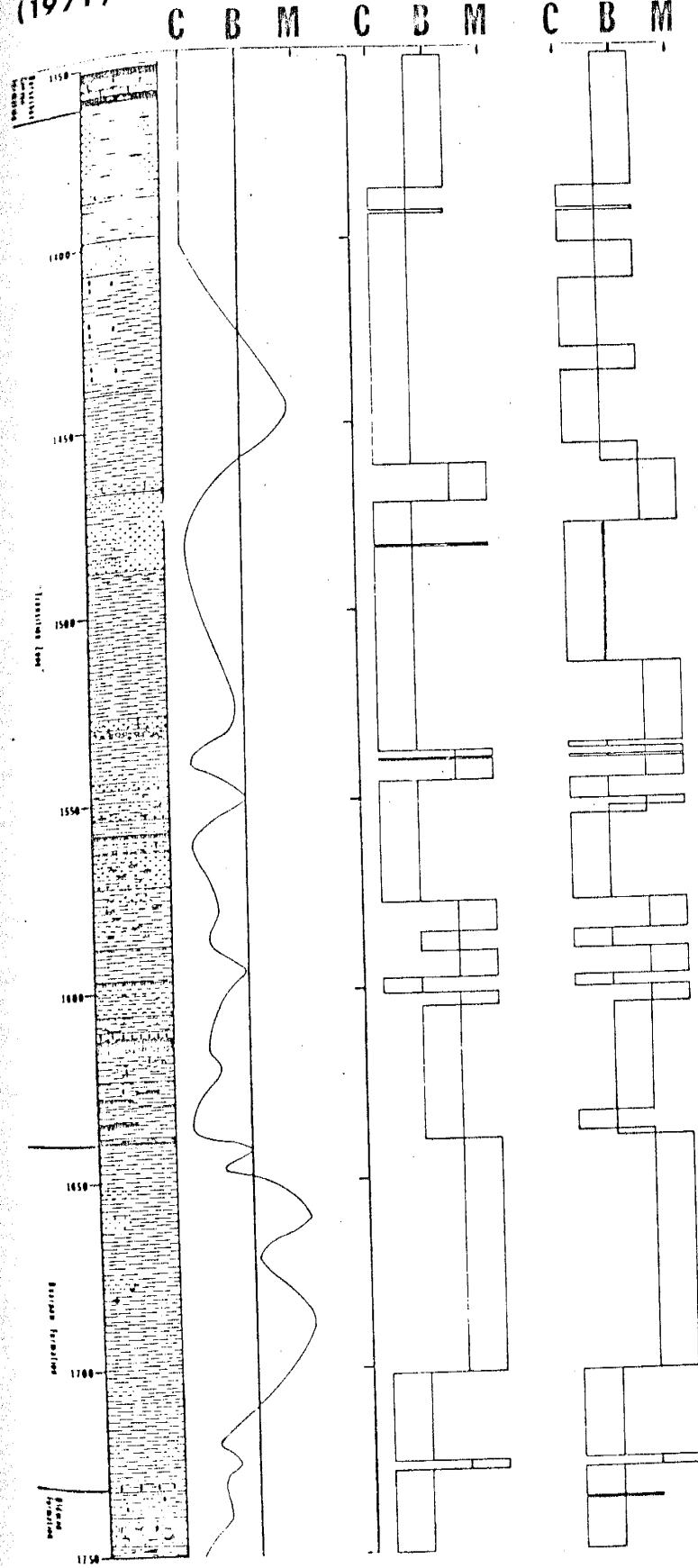
Fig. 8. Legend, CPOG Strathmore EV7-25-25W4 and comparison of paleoecologic classification with discriminant-function.

Havard
(1971)

Wall et al.
(1971)

24
Variables

12 & 16
Variables



C = Continental
B = Brackish
M = Marine

Fig. 8 (CONT.)

is good correspondence. The only significant conflict noted is for the interval between 1425' to 1460' (Fig. 8). Wall et al. (1971) classify this interval as marine, but in this study the interval is mainly continental. With reference to Figure 8 based on the discriminant-functions, a definite marine interval is noted from 1462' to 1478'. This interval is probably correlative to the above interval. This conflict in interpretation between both studies is probably caused by either a misclassification of the samples by Wall et al. (1971) or this worker, or incorrect depths for the samples. Other problems of interpretation between this work and the work of Wall et al. (1971) could be caused by sample size. In Wall's paper 57 samples were studied, while in this work 130 samples were used for the same interval. From this figure, and statistical tests of the model, it is apparent that we can use the formulated discriminant-functions to classify the unknown portions of the core.

Discrimination Between Samples of Unknown Depositional Environment

As mentioned previously, 1940 ft. of the core were studied. The discriminant-functions were developed using selected samples from that portion of the core studied by Wall et al. (1971). Therefore, as far as environment of deposition is concerned, 1530 ft. of core can be considered as unknown.

In classifying the unknown portion of the core, a pairwise approach was still followed. First, the groups marine vs. continental-brackish were separated. Then in a second step, all samples classified as belonging to the continental-brackish group were separated into the groups continental or brackish.

The most efficient functions were used, that is, the twelve variable functions are used for the groups marine vs. continental-brackish, and the sixteen variable functions are used for the continental vs. brackish groups. The results are given in Appendix 6 and 7. Figure 9 is constructed using these classification functions and the core description given in Havard (1971). An interpretation of the depositional history for the Upper Cretaceous is given in the following chapter.

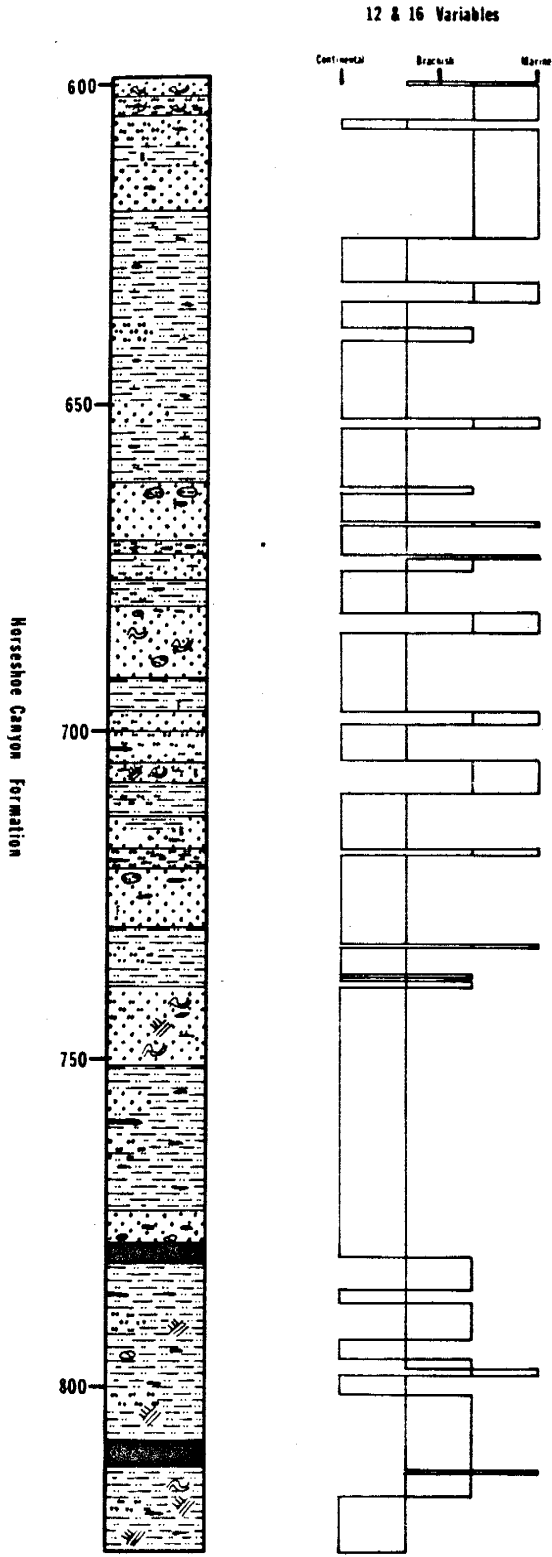


Fig. 9. Discrimination between samples of unknown depositional environment.

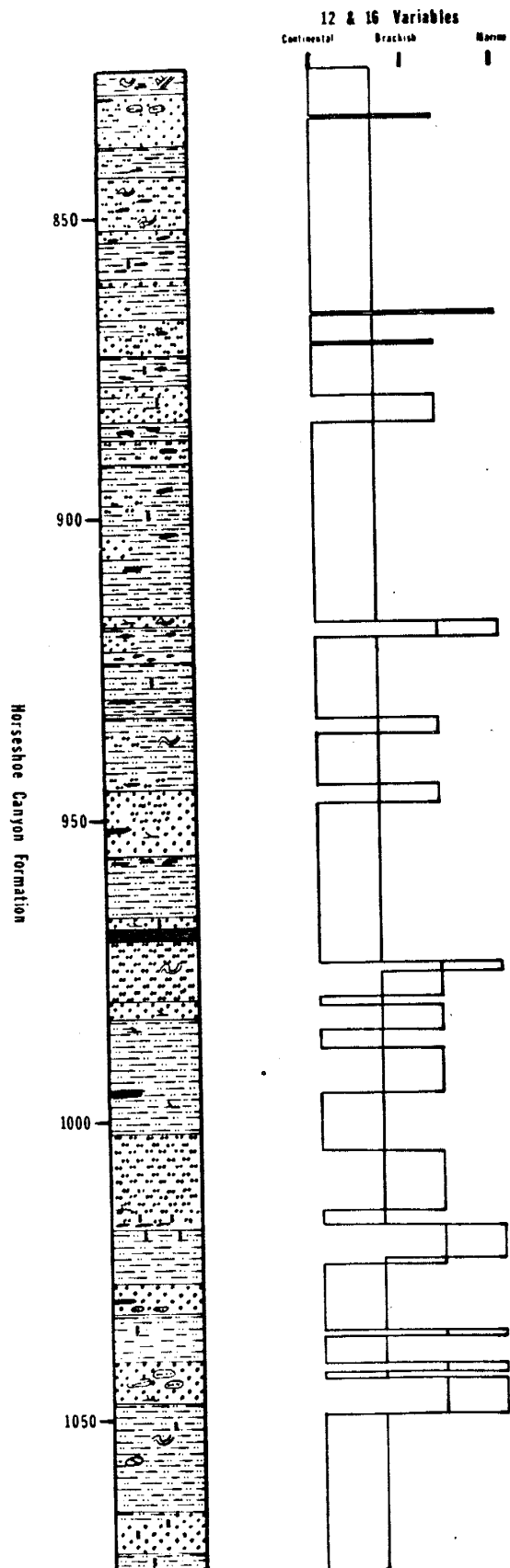


Figure 9 (CONT.)

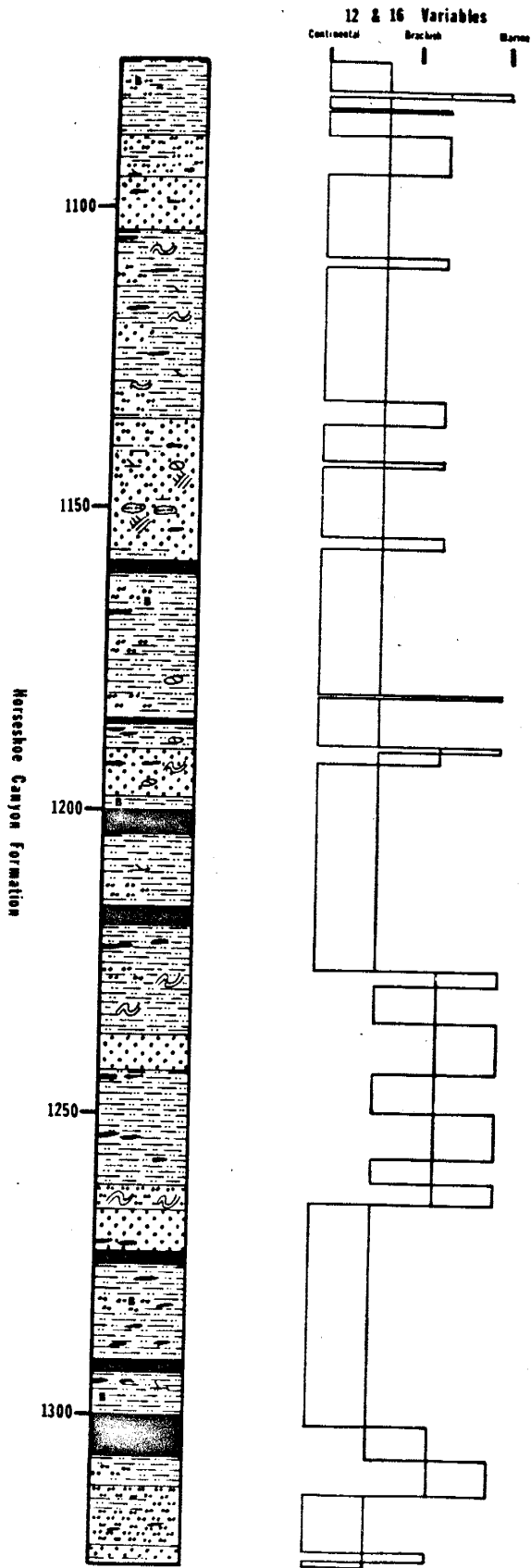


Figure 9 (CONT.)

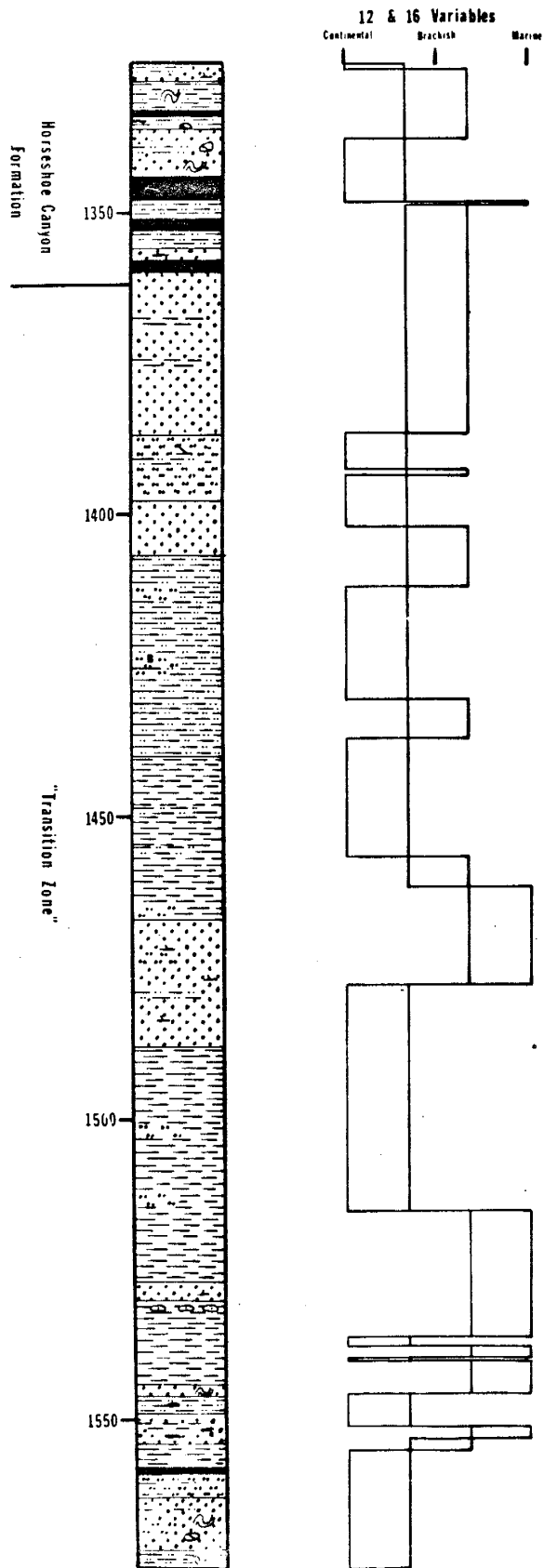


Figure 9 (CONT.)

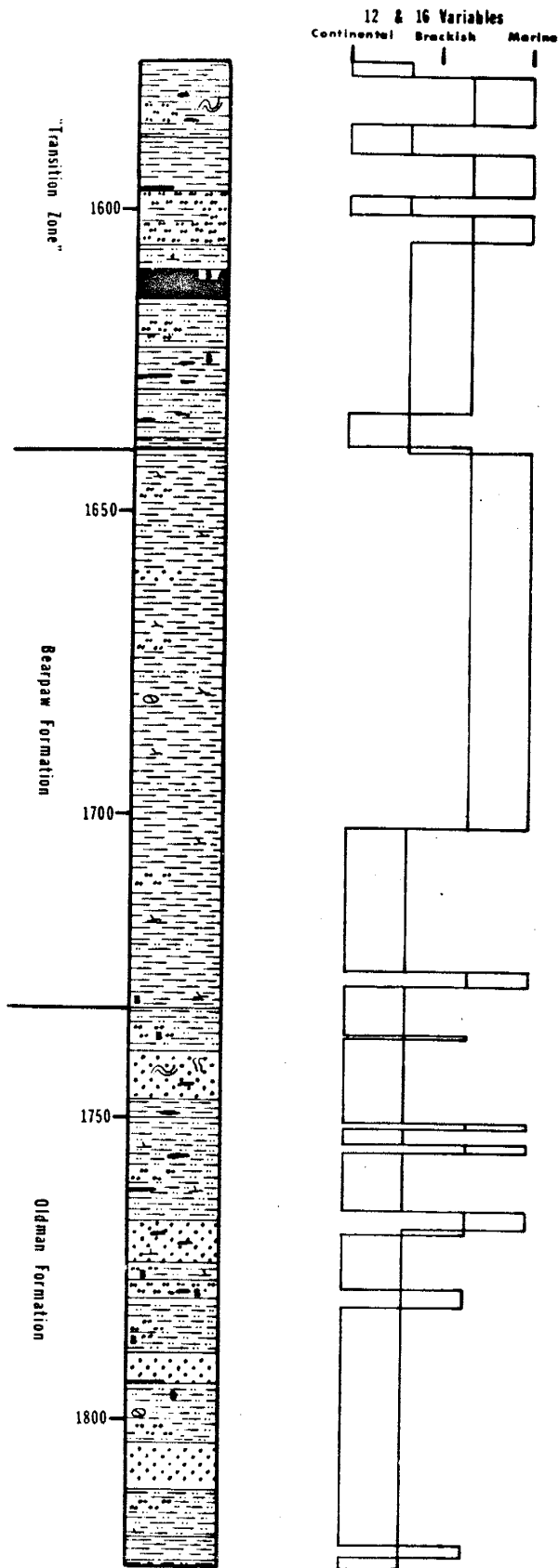


Figure 9 (CONT.)

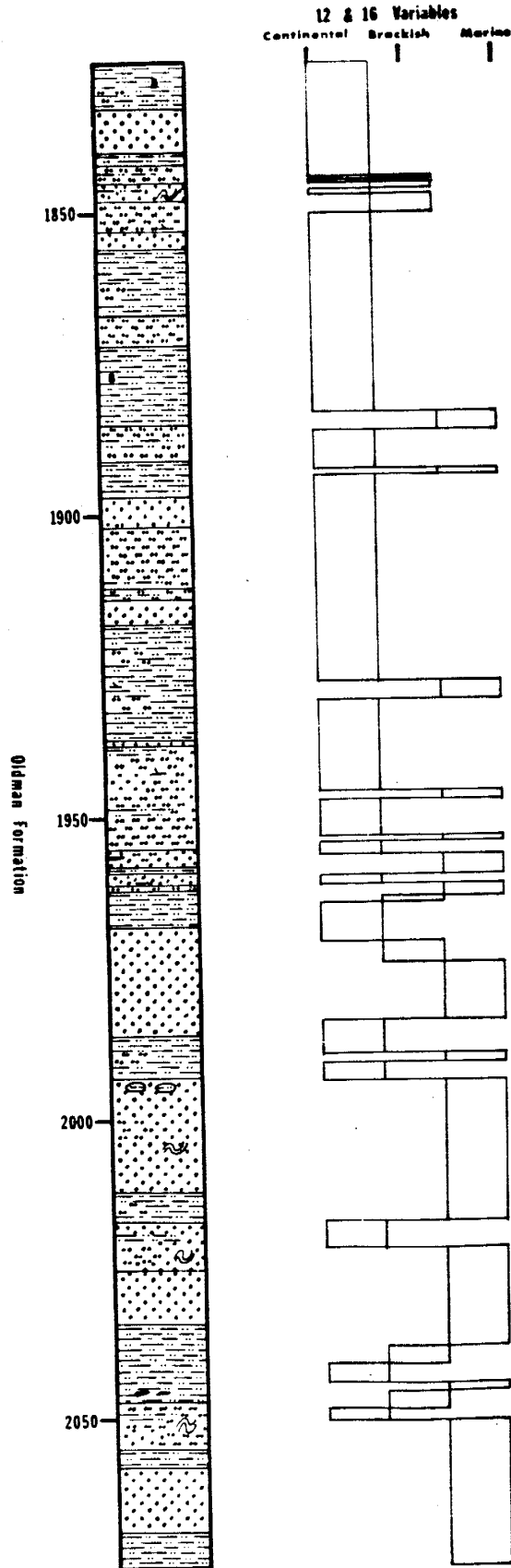


Figure 9 (CONT.)

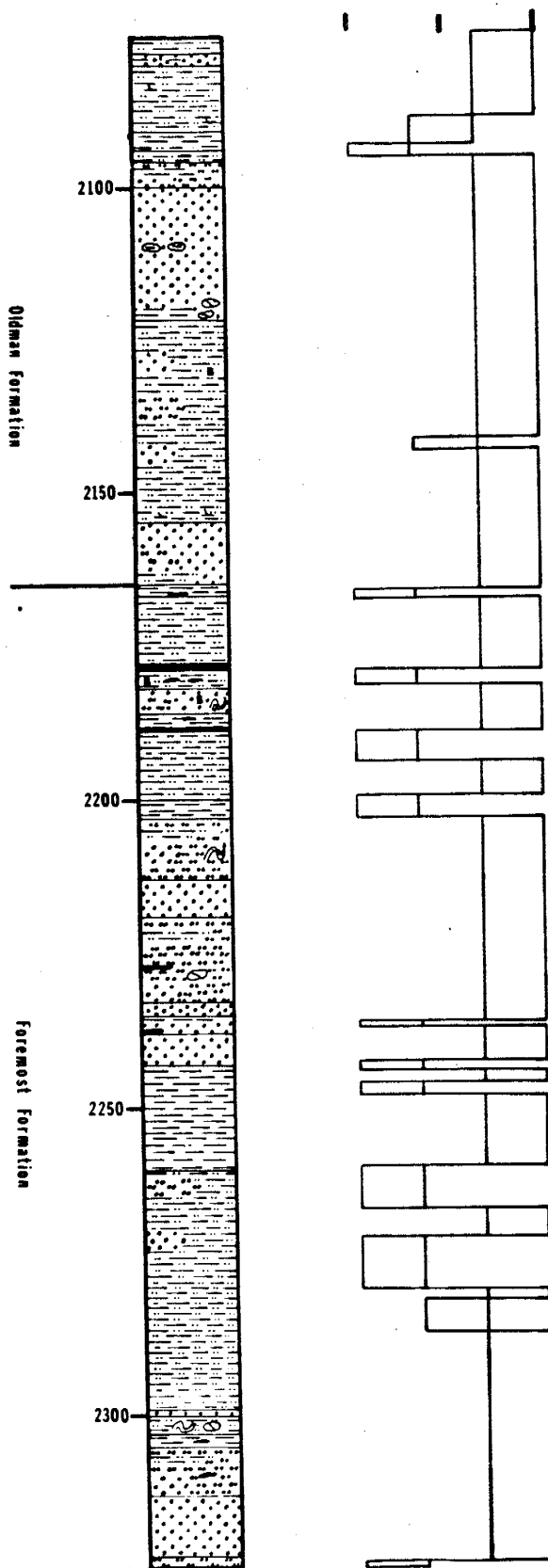


Figure 9 (CONT.)

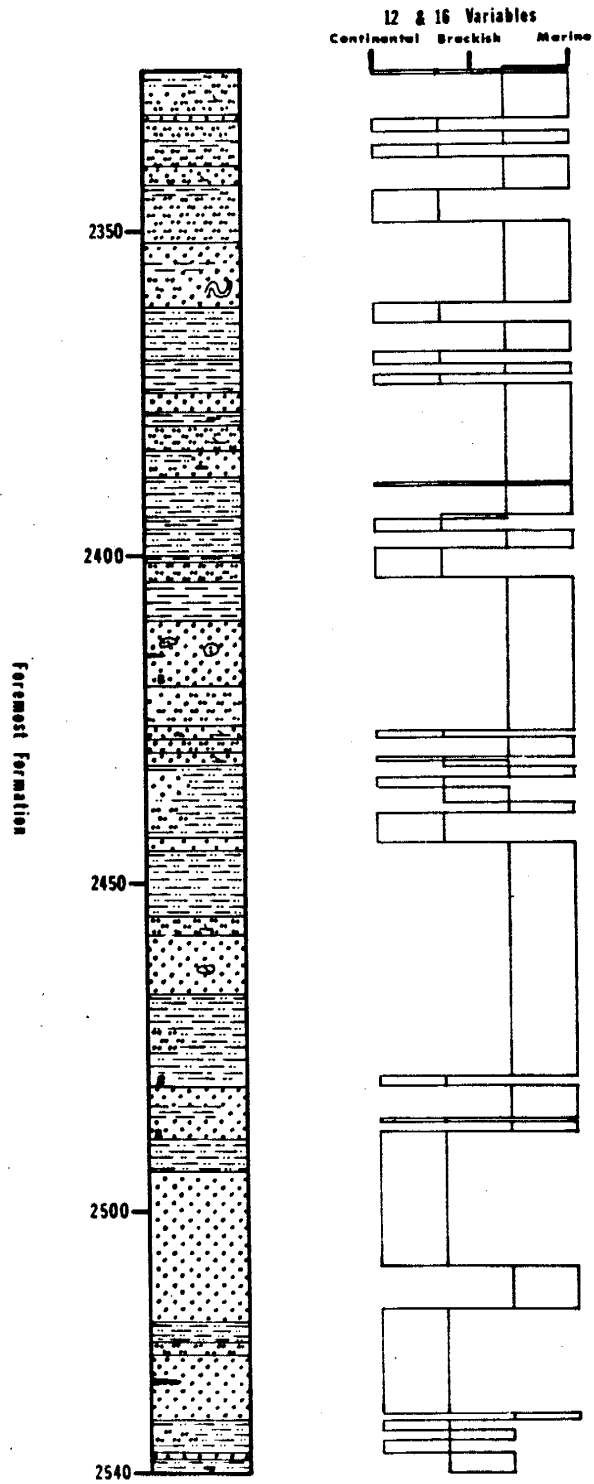


Figure 9 (CONT.)

CHAPTER IV: SUMMARY AND CONCLUSIONS

DEPOSITIONAL HISTORY OF THE LATE CRETACEOUS IN SOUTHERN ALBERTA

Introduction

The interpretation of the depositional history for the Late Cretaceous in southern Alberta is described in the following paragraphs. This interpretation is based on the published lithologic log (Havard, 1971) of the core, plus the classifications obtained through use of the formulated discriminant-functions and from the many papers which have been published on the area (Wall, et al. 1971; Havard, 1971; Williams and Burk, 1964; Powers, 1931; Russell and Landes, 1940; Hake and Addison, 1931; Shepherd and Hills, 1970; and Irish, 1970). Figure 5 gives a correlation chart for the Late Cretaceous and Paleocene in the area.

Foremost Time

Foremost time in the study area reflects the beginning of the gradual regression of the Claggett sea. The oscillatory nature of the process is shown in Figure 9. The depositional history during Foremost time can be broadly subdivided into two intervals. Many minor transgressions and regressions are recorded in the lower interval (2325' to 2540'). Within this interval both continental and marine deposits are of equal importance, with brackish elements almost lacking. Bentonites are common, probably reflecting a volcanic source to the west. No important coals occur in this interval, but coaly stringers are fairly common.

The upper interval (2165' to 2325') is dominantly marine, indicating a transgression of the Claggett sea. This sequence is composed mainly of

siltstones, mudstones and shales with minor sandstones, bentonites and coals. Environments of deposition were more stable than within the previous interval.

The terrain during Foremost time was probably very flat, poorly drained and covered by vegetation. The drainage systems covering the coastal plain were unable to carry any coarse sediments. The coastline at this time was probably very sinuous and consisted of shallow bays and estuaries, resulting in the simultaneous deposition of continental and marine deposits over adjacent areas. The average chemical composition of the Foremost Formation is given in Table 26.

Oldman Time

The depositional history during Oldman time can be broadly subdivided into three intervals. Marine deposition remained important during the lower interval (2165' to 2045'). The sequence is still mainly siltstones, mudstones and shales with minor sandstones. During deposition of this interval, the terrain was probably quite similar to that of late Foremost time. Deposition from a source to the west, over a broad coastal plain, into shallow embayments was prevalent. Very little coarse material was deposited.

A middle interval (1925' to 2045') marks regression of the Claggett sea. Marine deposition is still predominant, but both continental and brackish elements are more common. Within this section, sandstones become more prevalent. At this time the coastal plain was probably being uplifted above sea level causing the Claggett sea to retreat to the east. This situation created a more efficient drainage system which allowed coarser material to be deposited. Most of the organic matter being deposited at this time was being oxidized, and very little carbonaceous matter was preserved.

Table 26

Average Element Abundances (in ppm) for
Foremost Formation 2165' - 2540'

No. of Samples = 159

Element	\bar{X}	S	C.V. %
Si	252170	40715	16.14
Al	87322	8739	10.00
Fe	52332	11019	21.05
Mg	10934	5303	48.5
Ca	12356	14496	117.31
Na	15635	3223	20.61
K	10934	2425	22.17
Ti	5816	764	13.13
Mn	1491	9154	613.95
Ba	569	144	25.3
Co	54	13	24.03
Cu	41	14	34.14
Ga	21	8	38.09
Li	19	5	26.31
Mo	1	1	100.00
Pb	17	12	70.58
Rb	56	31	55.35
S	134	85	63.43
Sr	258	100	38.75
C and H ₂ O	50236	18393	36.61
Zn	91	29	31.86
Zr	180	45	25.0
V	181	44	24.3
Ni	63	18	28.57

An upper interval (1734' to 1925') can be characterized as being continental with minor marine and brackish units. This interval marks complete withdrawal of the Claggett sea. Sediments deposited in this interval record a time when once again the drainage system became sluggish, and mainly deposited mud and silt. Very few sands were deposited. Coal swamp conditions, however, were not established at this time as shown by the lack of carbonaceous material in this portion of the column.

The average element concentrations for the Oldman Formation are given in Table 27.

Bearpaw Time

The depositional history during Bearpaw time can be subdivided into three intervals. Continental conditions, similar to late Oldman time, persisted through the lower interval (1704' to 1734'). Shales and mudstones are most prevalent. A marked change, however, is noted for the middle interval (1650' to 1704'). At this time a major transgression of the Bearpaw sea occurred. Stable marine conditions persisted for this time. A major regression then occurred, as shown by the presence of a coal bed at 1640'. During the upper interval (1640' to 1650') brackish conditions of deposition were most prevalent, with minor continental elements.

Deposition for all of Bearpaw time can be characterized as being mainly marine, with continental and brackish deposits of secondary importance. This major incursion of marine waters, could possibly have been caused by subsidence within the basin. Near the end of Bearpaw time, however, the area was near sea level. Coal swamp conditions were established, and brackish water lagoons were common.

Table 27

Average Element Abundances (values in ppm) for
Oldman Formation 1732'-2165'

No. of Samples = 181

Element	\bar{X}	S	C.V. %
Si	295924	23545	7.95
Al	82502	10338	12.53
Fe	39763	15836	39.82
Mg	11896	7506	63.09
Ca	14490	15665	108.10
Na	13643	3862	28.30
K	14599	7107	48.68
Ti	4761	1057	22.20
Mn	735	996	135.51
Ba	602	178	29.56
Co	42	14	33.33
Cu	32	14	43.75
Ga	20	7	35.00
Li	14	7	50.00
Mo	1	1	100.00
Pb	13	7	53.84
Rb	89	45	50.56
S	206	264	128.15
Sr	194	65	33.50
C and H ₂ O	50493	26770	53.01
Zn	70	29	41.42
Zr	194	54	27.83
V	101	49	48.51
Ni	107	61	57.00

Drainage over the area was sluggish, not unlike modern deltas such as the Mississippi Delta. The average element concentrations for the Bearpaw Formation are given in Table 28.

"Transition Zone" Time

The entire "zone" (1364' to 1615') can be characterized as being mainly continental but containing important marine and brackish units. A lower interval (1615' to 1404') within the "zone" is composed principally of siltstones, mudstones and shales, with two prominent coal beds. This section marks the initiation of the regression of the Bearpaw sea. A low energy flow regime was dominant. This is recorded by the prevalence of silts and muds being deposited. The climate was humid and the area was well vegetated allowing coal swamp conditions to be established. An upper interval (1404' to 1364') within the "zone" marks a change in depositional environment. More sands were deposited, indicating an increase in the transporting power of the streams draining the area. At this time, the sediments were probably being deposited on a broad coastal plain and in brackish water lagoons. The average chemical composition of the "transition zone" is given in Table 29.

Horseshoe Canyon Time

Deposition during Horseshoe Canyon time, Figure 9, was highly variable between continental, brackish and marine. The continental element, however, is most important. A period of deltaic sedimentation seems most appropriate to account for the great diversity of sediment types being deposited. The material varies from sandstones to shales over short intervals. Coals and organic matter are common. Many of the sands are crossbedded. Contorted and convolute bedding is also very common within the section.

Table 28

Average Element Abundances (values in ppm) for
Bearpaw Formation 1640'-1732'

No. of Samples = 25

Element	\bar{X}	S	C.V. %
Si	271692	36987	13.61
Al	83318	12988	15.98
Fe	68197	52887	77.55
Mg	13385	5844	43.66
Ca	13408	11511	85.85
Na	9072	3693	40.7
K	21242	8280	38.97
Ti	5098	898	17.61
Mn	1038	604	58.18
Ba	695	213	30.64
Co	51	13	25.49
Cu	33	6	18.18
Ga	24	6	25.00
Li	17	4	23.52
Mo	1	1	100.00
Pb	23	5	21.73
Rb	145	52	35.86
S	794	416	52.39
Sr	152	51	33.55
C and H ₂ O	69188	23574	34.07
Zn	105	36	34.28
Zr	131	26	19.84
V	170	62	36.47
Ni	188	155	82.44

Table 29

Average Element Abundances (values in ppm)
 "Transition Zone" 1362'-1640'

No. of Samples = 72

Element	\bar{X}	S	C.V. %
Si	273824	22841	8.34
Al	81390	9604	11.79
Fe	44954	16130	35.88
Mg	12905	6315	48.93
Ca	17000	15709	92.4
Na	14197	8243	58.06
K	15994	8657	54.12
Ti	4727	997	21.09
Mn	767	267	34.81
Ba	795	261	32.83
Co	37	10	27.02
Cu	31	12	38.7
Ga	22	6	27.27
Li	13	5	38.46
Mo	1	1	100.00
Pb	23	27	117.39
Rb	90	53	58.88
S	762	1530	200.78
Sr	202	49	24.25
C and H ₂ O	77338	37731	48.78
Zn	88	30	34.09
Zr	143	24	16.78
V	179	65	36.31
Ni	105	38	36.19

It is suggested that as Laramide mountain building reached a peak to the west, the influx of sediments and bentonitic material increased. Large deltas formed, and enroached on the Bearpaw sea. Many different depositional environments are recorded, from coal swamp, beach, brackish-water lagoon to fluvial, similar to the rapid facies changes in the Mississippi Delta today. A humid climate prevailed. Very temporary swamps formed locally, on the subaerial inter-distributary areas of the deltas. In these areas, vegetation accumulated to form coals. As the deltas prograded they forced the Bearpaw sea to retreat to the east. Minor incursions of the Bearpaw sea still occurred, however, up until the end of Horseshoe Canyon time. The average element concentration for the Horseshoe Canyon Formation is given in Table 30.

UTILITY OF GEOCHEMICAL FACIES ANALYSIS

This study has shown that a statistical approach to geochemical facies analysis is most appropriate. The method is an important tool which can be used by most geologists. Many problems in geology are applicable to this approach. In this case, it was used to classify sediments and to interpret the depositional history. It could, however, also be used for correlating fossil-free sediments, tracing oil to source rock, tracing ore forming fluids, and to determine parent material of metamorphic rocks, to name a few functions. The need for concise techniques, which give statistically significant answers, is apparent.

Table 30

Average Element Abundances (values in ppm) for
Horseshoe Canyon Formation 599'-1362'

No. of Samples = 399

Element	\bar{X}	S	C.V. %
Si	293262	25681	8.75
Al	82614	7203	8.71
Fe	37847	17979	47.5
Mg	8819	5734	65.01
Ca	12452	12469	100.13
Na	16166	4251	26.29
K	15073	8036	53.31
Ti	4513	2409	53.37
Mn	1503	14781	983.43
Ba	911	296	32.49
Co	35	13	37.14
Cu	28	16	57.14
Ga	23	8	34.78
Li	15	12	80.00
Mo	1	2	200.00
Pb	13	8	61.53
Rb	80	49	61.25
S	180	138	76.66
Sr	214	62	28.97
C and H ₂ O	66909	32505	48.58
Zn	74	23	31.08
Zr	143	24	16.78
V	139	52	37.41
Ni	127	62	48.81

CONCLUSIONS

Major and trace elements were studied in ancient argillaceous sediments to determine their importance for discriminating between continental, brackish and marine environments of deposition.

In order to provide as concise a test as possible, samples from known environments of deposition were used to formulate discriminant-functions. These samples are from one basin of deposition where source area, tectonic conditions, climate and sedimentation rates were similar.

The following was determined:

1. Ancient continental, brackish and marine sediments, can be distinguished on the basis of major and trace element concentrations.
2. The group marine vs. composite group continental-brackish, can be separated using a discriminant-function containing the variable Ti, Mn, Ba, Co, Cu, Ga, Li, Sr, C plus H₂O, Zn, Zr and V.
3. The composite group continental-brackish can be separated using a discriminant-function based on the variables Mg, Na, K, Ti, Mn, Ba, Co, Cu, Ga, Li, Rb, Sr, C plus H₂O, Zn, Zr and V.
4. The depositional history for the Upper Cretaceous in southern Alberta can be interpreted by applying discriminant analysis to the element concentration data for the classification of samples of unknown environment.

5. It is shown that the model as implied by Wall et al. (1971) of gradual transitions between continental and marine deposits, passing through a brackish stage is probably inappropriate. Brackish water deposits are relatively rare during a regression or transgression of an epicontinental sea. This is due to the rapid rates to transgression or regression over a broad, flat, coastal plane at or near sea level.
6. While transgressions and regressions are harmonic in nature, over short intervals rapid rates are noted.

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Appendix 1
Elements Concentrations

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -1 599.5	0.0	ST- 2 600.0	0.0	ST -3 600.0	-602.0	ST -4 602.0	-603.2
SI	298630.		295630.		295260.		290090.	
AL	83900.		83850.		81960.		81420.	
FE	32750.		37180.		33780.		41840.	
MG	5980.		6240.		5580.		6520.	
CA	10370.		9860.		10480.		10100.	
NA	17300.		18600.		20100.		17800.	
K	14510.		17640.		18920.		22260.	
TI	3660.		4200.		3770.		4090.	
MN	120.		160.		150.		250.	
BA	980.		660.		700.		540.	
CO	24.		26.		36.		38.	
CU	24.		25.		23.		23.	
GA	24.		23.		22.		22.	
LI	22.		24.		24.		24.	
MO	1.		1.		1.		1.	
PB	7.		8.		21.		9.	
RB	47.		59.		58.		81.	
S	105.		134.		173.		205.	
SR	284.		276.		297.		294.	
CGH20	32600.		39800.		29500.		28900.	
ZN	82.		98.		75.		80.	
ZR	162.		166.		144.		157.	
V	140.		160.		140.		180.	
NI	90.		94.		126.		148.	

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -5 603.2 -603.4	ST -6 603.4 -605.7	ST -7 605.7 -607.2	ST -9 607.4 -611.5
SI	290320.	293500.	299490.	294700.
AL	82550.	82810.	84850.	71880.
FE	46110.	46450.	26390.	31750.
MG	8020.	7240.	4280.	6060.
CA	9380.	9270.	11440.	28010.
NA	15400.	17900.	16700.	18400.
K	20890.	20180.	16220.	17650.
TI	4120.	4100.	3220.	3660.
MN	340.	270.	200.	1040.
BA	540.	660.	680.	840.
CO	42.	40.	30.	35.
CU	31.	32.	23.	22.
GA	27.	24.	35.	23.
LI	24.	28.	22.	24.
MO	1.	0.	1.	0.
PB	8.	6.	23.	14.
RB	81.	78.	58.	53.
S	201.	159.	190.	193.
SR	249.	261.	431.	307.
CaH2O	38300.	36700.	28300.	32400.
ZN	99.	87.	73.	61.
ZR	149.	160.	218.	174.
V	220.	180.	120.	180.
NI	180.	170.	134.	202.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -10 611.5 -612.0	ST -11 612.0 -616.3	ST -12 616.3 -618.0	ST -13 618.0 -622.0
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SI	236480.	293390.	297630.	298780.
AL	84450.	82870.	82230.	76560.
FE	49490.	33650.	42970.	27030.
MG	9640.	6440.	7220.	5280.
CA	14120.	22960.	9880.	12260.
NA	16700.	19800.	16400.	16500.
K	18670.	17500.	22210.	17810.
TI	3980.	3610.	4000.	3290.
MN	1050.	1140.	420.	300.
BA	720.	840.	440.	480.
CO	58.	40.	36.	32.
CU	29.	25.	36.	21.
GA	21.	26.	25.	20.
LI	24.	24.	36.	28.
MO	1.	1.	0.	1.
PB	9.	9.	12.	9.
RB	48.	49.	83.	43.
S	232.	112.	308.	145.
SR	217.	296.	272.	290.
CEH2O	56900.	28900.	40800.	27800.
ZN	63.	64.	80.	50.
ZP	116.	157.	161.	180.
V	160.	180.	180.	100.
NI	264.	198.	208.	162.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -14 622.0 -623.0	ST -15 623.0 -624.0	ST -16 624.0 -631.0	ST -17 631.0 -632.3
SI	294720.	307780.	298480.	250330.
AL	82810.	78360.	78890.	63520.
FE	43340.	36800.	43080.	101860.
MG	6160.	4720.	7180.	9120.
CA	9160.	9950.	10460.	41950.
NA	17600.	15200.	5400.	12400.
K	20870.	19490.	20160.	10670.
TI	4150.	3720.	3870.	3030.
MN	210.	520.	440.	6020.
BA	400.	440.	600.	400.
CO	34.	30.	12.	22.
CU	37.	29.	31.	32.
GA	30.	22.	21.	24.
LI	30.	28.	22.	28.
MO	2.	1.	0.	1.
PB	13.	11.	9.	9.
RB	98.	68.	87.	54.
S	416.	360.	72.	228.
SR	301.	290.	278.	208.
CEH20	48300.	39400.	25600.	93600.
ZN	67.	60.	80.	64.
ZR	167.	158.	158.	115.
V	200.	120.	100.	180.
NI	198.	182.	222.	368.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -18 632.3 -633.8	ST -19 633.8 -635.0	ST -20 635.0 -638.0	ST -21 638.0 -640.0
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SI	281090.	281970.	281460.	306450.
AL	74560.	69700.	86110.	81800.
FE	26500.	52760.	36280.	39090.
MG	6020.	9420.	7260.	7208.
CA	36470.	12720.	13560.	9680.
NA	20000.	16900.	20600.	18600.
K	9430.	9890.	7930.	12240.
TI	2760.	3320.	3070.	3620.
MN	2240.	1080.	1000.	80.
BA	980.	640.	720.	440.
CO	30.	32.	30.	22.
CU	19.	28.	22.	23.
GA	19.	30.	28.	27.
LI	30.	13.	11.	11.
MO	1.	1.	1.	1.
PB	11.	9.	9.	9.
RB	25.	58.	36.	80.
S	158.	87.	177.	181.
SR	360.	288.	337.	285.
CGH20	32000.	45800.	41500.	36100.
ZN	42.	86.	69.	62.
ZR	157.	156.	155.	171.
V	120.	180.	180.	180.
NI	168.	174.	174.	182.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -22 640.0 -644.5	ST -23 644.5 -645.0	ST -24 645.0 -648.0	ST -25 645.0 -650.5
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SI	304940.	301410.	289430.	288730.
AL	89540.	82970.	82970.	83850.
FE	35670.	35420.	46270.	44660.
MG	4900.	5580.	7260.	7900.
CA	9770.	10600.	9800.	10300.
NA	16700.	15800.	19000.	16900.
K	15870.	17130.	18850.	24300.
TI	3650.	3540.	3950.	4140.
MN	170.	130.	220.	270.
BA	720.	720.	800.	780.
CO	32.	26.	28.	32.
CU	30.	25.	34.	48.
GA	26.	26.	32.	22.
LI	12.	11.	11.	13.
MO	1.	5.	1.	1.
PB	10.	23.	15.	10.
RB	74.	65.	100.	97.
S	490.	281.	175.	233.
SR	284.	310.	297.	275.
CGH2O	42000.	36700.	37100.	38800.
ZN	72.	69.	85.	90.
ZR	168.	166.	172.	158.
V	180.	180.	220.	220.
NI	180.	188.	216.	200.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -26 650.5 -652.0	ST -27 652.0 -653.5	ST -28 653.5 -657.0	ST -29 657.0 -658.0
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SI	284090.	241300.	191750.	281670.
AL	84250.	65620.	82070.	83900.
FE	50900.	56830.	41980.	34960.
MG	9000.	8280.	5420.	5360.
CA	11730.	86160.	8950.	12100.
NA	17800.	13200.	18100.	21600.
K	23380.	14770.	18190.	13310.
TI	3940.	2750.	3960.	2960.
MN	1190.	3470.	220.	1030.
BA	760.	720.	760.	800.
CO	48.	24.	16.	32.
CU	48.	37.	39.	30.
GA	22.	18.	20.	19.
LI	13.	9.	11.	11.
MO	2.	1.	2.	1.
PB	13.	7.	9.	29.
RB	83.	63.	91.	40.
S	241.	266.	187.	189.
SR	275.	234.	389.	324.
CEH2O	49300.	54400.	49500.	46300.
ZN	96.	66.	88.	57.
ZR	155.	127.	156.	133.
V	200.	140.	160.	120.
NI	280.	250.	206.	190.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -30 658.0 -660.5	ST -31 660.5 -661.0	ST -32 661.0 -662.0	ST -33 662.0 -662.5
SI	283710.	285090.	299200.	296590.
AL	79410.	77590.	86110.	80370.
FE	32690.	27030.	37390.	28360.
MG	4300.	3760.	5400.	3800.
CA	10210.	18450.	10920.	17940.
NA	20600.	21500.	17100.	21500.
K	14300.	8820.	10820.	7040.
TI	3580.	2890.	3440.	3470.
MN	30.	600.	450.	630.
BA	720.	1260.	940.	1300.
CO	26.	18.	18.	24.
CU	24.	19.	29.	18.
GA	17.	28.	32.	23.
LI	11.	9.	11.	11.
MO	2.	1.	0.	2.
PB	18.	15.	11.	14.
RB	65.	24.	49.	12.
S	277.	246.	102.	157.
SR	291.	397.	315.	389.
C&H2O	45100.	32200.	39700.	33500.
ZN	56.	64.	69.	59.
ZR	164.	200.	169.	268.
V	140.	100.	129.	160.
NI	172.	86.	50.	122.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -34 662.5 -663.5	ST -35 663.5 -667.5	ST -36 667.5 -667.7	ST -37 667.7 -667.9
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SI	281990.	275920.	288080.	228600.
AL	89270.	79230.	80820.	65320.
FE	47110.	29250.	41250.	116960.
MG	7340.	4440.	5220.	6860.
CA	11190.	17550.	17620.	17330.
NA	17100.	20400.	16700.	9900.
K	6120.	6220.	8370.	4350.
TI	3390.	2810.	3620.	2010.
MN	540.	670.	690.	3130.
BA	620.	1440.	800.	880.
CO	26.	22.	28.	20.
CU	26.	15.	26.	22.
GA	31.	27.	32.	25.
LI	21.	13.	12.	16.
MO	2.	1.	1.	0.
PB	14.	13.	12.	18.
RB	28.	4.	42.	10.
S	149.	145.	137.	44.
SR	318.	425.	322.	232.
CaH2O	60700.	36400.	49100.	133200.
ZN	60.	51.	83.	71.
ZR	223.	221.	196.	142.
V	180.	90.	180.	120.
NI	162.	128.	158.	320.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -38 667.9 -668.1	ST -39 668.1 -673.0	ST -40 673.0 -673.5	ST -41 673.5 -674.5
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SI	294810.	278660.	284700.	289780.
AL	81960.	75450.	82440.	82970.
FE	38540.	41500.	43540.	33720.
MG	5120.	6140.	6000.	5620.
CA	9360.	33330.	11540.	10180.
NA	33900.	19500.	18100.	20700.
K	13820.	12260.	16830.	18210.
TI	3790.	3430.	3960.	3910.
MN	460.	1530.	690.	490.
BA	940.	1240.	920.	660.
CO	18.	22.	34.	16.
CU	26.	26.	24.	23.
GA	25.	24.	26.	26.
LI	15.	17.	22.	19.
MO	0.	1.	0.	1.
PB	15.	18.	40.	22.
RB	66.	43.	64.	54.
S	127.	166.	504.	166.
SR	297.	319.	288.	293.
CaH2O	35700.	40200.	53500.	39300.
ZN	82.	67.	88.	80.
ZR	150.	167.	179.	153.
V	160.	120.	140.	200.
NI	136.	136.	132.	86.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -42 674.5 -675.5	ST -43 675.5 -677.0	ST -44 677.0 -679.0	ST -45 679.0 -679.5
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SI	290910.	291850.	279540.	288260.
AL	85630.	84850.	83700.	81910.
FE	38820.	36380.	47940.	36440.
MG	7540.	3860.	7360.	6420.
CA	3830.	9180.	8150.	11270.
NA	16900.	18800.	18300.	18300.
K	22010.	18310.	22300.	17030.
TI	4330.	4120.	4370.	4120.
MN	460.	530.	550.	530.
BA	780.	1020.	768.	840.
CO	18.	22.	24.	18.
CU	35.	25.	35.	28.
GA	29.	23.	25.	20.
LI	20.	19.	21.	21.
MO	0.	1.	2.	1.
PB	13.	7.	10.	5.
RB	71.	55.	93.	56.
S	177.	123.	149.	95.
SR	260.	264.	233.	262.
CH2O	41000.	36000.	51600.	41000.
ZN	100.	72.	107.	83.
ZR	156.	154.	160.	152.
V	180.	140.	200.	140.
NI	113.	136.	184.	120.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -46 679.5 -682.0	ST -47 682.0 -685.0	ST -48 685.0 -685.2	ST -49 685.2 -693.0
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SI	284430.	274760.	191630.	289850.
AL	82970.	79290.	45530.	79750.
FE	44010.	48620.	161890.	32070.
MG	9280.	9740.	7820.	5180.
CA	10670.	14880.	31360.	18510.
NA	17000.	17600.	9800.	19800.
K	18360.	17130.	6980.	19670.
TI	4220.	3790.	2430.	3240.
MN	660.	1000.	6240.	890.
BA	1000.	780.	1000.	860.
CO	18.	24.	14.	16.
CU	29.	23.	25.	19.
GA	23.	27.	15.	21.
LI	17.	20.	24.	13.
MO	1.	1.	1.	1.
PB	9.	10.	12.	18.
RB	74.	52.	20.	49.
S	253.	160.	156.	101.
SR	247.	257.	122.	237.
CGH20	43200.	53000.	171500.	28700.
ZN	88.	82.	36.	47.
ZR	164.	171.	105.	140.
V	160.	140.	360.	100.
NI	126.	86.	200.	86.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -50 693.0 -697.0	ST -51 697.0 -699.0	ST -52 699.0 -700.5	ST -53 700.5 -702.0
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SI	286820.	296550.	291140.	287230.
AL	84750.	60090.	83640.	82120.
FE	42820.	31010.	39510.	41750.
MG	5840.	6360.	7160.	7580.
CA	25160.	18570.	9100.	9810.
NA	15800.	16200.	14700.	15300.
K	25910.	24460.	27750.	16920.
TI	3890.	3730.	4080.	4110.
MN	590.	750.	520.	500.
BA	760.	540.	520.	520.
CO	16.	34.	68.	36.
CU	34.	20.	30.	35.
GA	25.	24.	25.	25.
LI	14.	106.	12.	12.
MO	0.	0.	1.	0.
PB	5.	9.	9.	3.
RB	102.	68.	88.	71.
S	213.	121.	332.	92.
SR	360.	281.	254.	256.
C&H2O	42100.	35400.	46000.	47000.
ZN	87.	68.	87.	77.
ZR	180.	149.	158.	157.
V	160.	300.	140.	140.
NI	94.	98.	116.	232.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -54 702.0 -703.0	ST -55 703.0 -704.5	ST -56 704.5 -705.5	ST -57 705.5 -709.0
SI	277080.	302370.	265850.	271830.
AL	81040.	81370.	72420.	75120.
FE	36340.	34190.	92320.	29840.
MG	8040.	4120.	7340.	4260.
CA	13210.	9580.	21620.	49380.
NA	19800.	13000.	15500.	20000.
K	10980.	15160.	10950.	11720.
TI	3720.	3710.	2940.	3130.
MN	700.	440.	2170.	1130.
BA	400.	440.	380.	400.
CO	46.	32.	36.	36.
CU	28.	30.	28.	19.
GA	26.	18.	11.	17.
LI	12.	10.	9.	10.
MO	0.	2.	1.	3.
PB	6.	17.	20.	26.
RB	42.	64.	51.	33.
S	176.	105.	288.	82.
SR	286.	290.	283.	342.
CaH2O	47700.	46500.	57000.	25800.
ZN	94.	66.	45.	61.
ZR	148.	178.	170.	152.
V	140.	180.	180.	180.
NI	136.	112.	242.	152.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -58 709.0 -709.5	ST -59 709.5 -710.5	ST -60 710.5 -711.0	ST -61 711.0 -712.0
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SI	294900.	304430.	296640.	293120.
AL	79750.	83750.	79690.	79120.
FE	69750.	38850.	37060.	39550.
MG	6220.	4360.	4720.	4840.
CA	10430.	8810.	9160.	9270.
NA	13900.	18500.	19900.	17900.
K	15970.	16450.	13860.	14040.
TI	3800.	3950.	3780.	4750.
MN	1380.	440.	450.	450.
BA	480.	480.	500.	440.
CO	46.	50.	34.	38.
CU	32.	33.	25.	24.
GA	21.	17.	17.	16.
LI	10.	9.	9.	8.
MO	2.	2.	2.	2.
PB	39.	14.	29.	9.
PB	88.	31.	69.	80.
S	181.	250.	155.	143.
SR	269.	274.	289.	292.
CEH2O	48600.	46500.	48700.	46600.
ZN	70.	85.	75.	76.
ZR	174.	171.	165.	167.
V	220.	140.	140.	140.
NI	214.	148.	96.	110.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -62 712.0 -713.0	ST -63 713.0 -713.5	ST -64 713.5 -718.0	ST -65 718.0 -719.2
SI	293650.	296160.	299500.	298210.
AL	85970.	82810.	82280.	78710.
FE	39800.	43320.	31580.	45340.
MG	3760.	5480.	4960.	5460.
CA	9830.	9370.	15690.	10740.
NA	19600.	18400.	11000.	13100.
K	12620.	15380.	10560.	6220.
TI	4330.	4510.	4290.	3810.
MN	460.	470.	610.	490.
BA	460.	480.	560.	420.
CO	30.	34.	36.	42.
CU	24.	27.	18.	14.
GA	13.	19.	19.	21.
LI	11.	10.	12.	19.
MO	9.	3.	1.	2.
PB	8.	9.	5.	6.
RB	60.	77.	33.	29.
S	59.	211.	155.	231.
SR	304.	295.	340.	258.
CH2O	50100.	48100.	40000.	111000.
ZN	79.	75.	65.	53.
ZR	154.	147.	157.	151.
V	200.	220.	160.	120.
NI	124.	156.	146.	170.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -66 713.2 -719.4	ST -69 721.0 -730.0	ST -70 730.0 -732.0	ST -71 732.0 -732.6
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SI	251090.	292940.	302820.	295140.
AL	84950.	80480.	82920.	80710.
FE	66450.	26840.	41050.	55990.
MG	7080.	2960.	6040.	8520.
CA	14250.	16630.	8570.	11660.
NA	13100.	20630.	18400.	17200.
K	3040.	14020.	24010.	19060.
TI	3340.	4590.	5070.	4750.
MN	490.	720.	650.	1100.
BA	380.	540.	520.	860.
CO	24.	38.	36.	24.
CU	6.	12.	23.	19.
GA	23.	20.	22.	25.
LI	16.	9.	9.	9.
MO	2.	2.	1.	1.
PB	10.	5.	13.	13.
RB	0.	38.	112.	81.
S	56.	102.	116.	170.
SP	369.	285.	258.	270.
CGH2O	101300.	31000.	48600.	60600.
ZN	60.	61.	68.	84.
ZR	202.	152.	152.	158.
V	40.	140.	200.	140.
NI	196.	168.	188.	138.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -72 732.6 -733.2	ST -73 733.2 -734.5	ST -74 734.5 -735.0	ST -75 735.0 -737.2
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SI	174370.	303780.	302119.	302510.
AL	36050.	89280.	85090.	85120.
FE	41120.	23990.	36120.	40990.
MG	7160.	5040.	6020.	8640.
CA	84690.	10010.	8960.	6210.
NA	19240.	21300.	13060.	17400.
K	9980.	18060.	22870.	19040.
TI	1720.	4330.	4870.	5200.
MN	1220.	570.	450.	520.
BA	680.	740.	720.	1540.
CO	34.	27.	24.	28.
CU	0.	11.	18.	44.
GA	16.	17.	21.	24.
LI	13.	11.	10.	20.
MO	0.	1.	0.	0.
PB	13.	17.	13.	13.
PP	36.	47.	93.	87.
S	185.	195.	132.	192.
SR	217.	291.	276.	257.
COH2O	51200.	39200.	48500.	57900.
ZN	37.	56.	74.	77.
ZR	113.	148.	167.	156.
V	140.	120.	140.	120.
NI	150.	134.	142.	170.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -76 737.2 -737.6	ST -77 737.5 -738.0	ST -78 738.0 -739.2	ST -79 739.2 -743.0
SI	300195.	297870.	269610.	302880.
AL	79410.	81760.	91380.	79070.
FE	36340.	45650.	41920.	21760.
MG	6360.	7480.	11440.	5560.
CA	9250.	8140.	9830.	25750.
NA	18100.	14300.	17100.	20900.
K	11710.	13760.	4080.	11330.
TI	45500.	6150.	3640.	4110.
MN	430.	450.	420.	710.
BA	900.	860.	580.	1040.
CO	33.	38.	30.	30.
CU	22.	39.	11.	16.
GA	19.	22.	24.	21.
LI	10.	12.	15.	12.
MO	0.	1.	1.	1.
PB	12.	7.	13.	8.
RB	54.	86.	8.	24.
S	146.	60.	87.	149.
SR	284.	247.	259.	297.
C&H2O	51000.	62100.	104600.	32000.
ZN	95.	62.	39.	51.
ZR	152.	169.	174.	150.
V	120.	180.	60.	100.
NI	166.	188.	164.	142.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -80 743.0 -744.3	ST -81 744.3 -746.5	ST -82 746.5 -747.4	ST -83 747.4 -750.8
SI	301360.	302580.	300290.	298850.
AL	82260.	81230.	81670.	85850.
FE	35010.	26150.	34830.	32890.
MG	6420.	5460.	6280.	4760.
CA	8780.	10970.	9680.	11670.
NA	20100.	22500.	16800.	19100.
K	14950.	9370.	13200.	10520.
TI	5020.	3770.	4640.	3770.
MN	500.	530.	540.	610.
BA	940.	840.	620.	480.
CO	28.	18.	22.	28.
CU	27.	12.	14.	17.
GA	19.	15.	20.	17.
LI	12.	10.	9.	10.
MO	1.	1.	1.	1.
PB	10.	10.	9.	12.
RB	67.	36.	569.	40.
S	76.	90.	104.	171.
SR	275.	301.	289.	310.
C&H2O	57900.	45200.	49500.	48800.
ZN	50.	46.	61.	59.
ZR	165.	160.	169.	158.
V	140.	80.	100.	160.
NI	148.	124.	170.	128.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -84 750.8 -752.5	ST -85 752.5 -754.0	ST -86 754.0 -755.2	ST -87 755.2 -757.5
SI	292330.	283180.	292670.	296550.
AL	82220.	82930.	84910.	80440.
FE	45340.	43630.	35360.	31390.
MG	6340.	7160.	7020.	5940.
CA	8170.	7860.	8280.	9270.
NA	12360.	13250.	17000.	17200.
K	14770.	14690.	12300.	14590.
TI	4850.	4810.	4670.	4440.
MN	460.	460.	430.	430.
BA	320.	660.	800.	920.
CO	24.	26.	22.	18.
CU	23.	37.	30.	32.
GA	19.	24.	21.	20.
LI	10.	12.	10.	10.
MO	0.	1.	0.	0.
PB	10.	10.	8.	15.
RB	99.	94.	54.	65.
S	112.	374.	125.	113.
SR	247.	232.	262.	292.
C&H2O	61500.	70800.	57000.	45200.
ZN	97.	113.	64.	64.
ZR	152.	143.	160.	156.
V	160.	140.	120.	140.
NI	156.	168.	164.	138.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -88 757.5 -758.3	ST -90 759.2 -763.8	ST -91 763.8 -765.8	ST -92 765.8 -770.3
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ST	300870.	306940.	302490.	295810.
AL	89450.	85830.	84010.	82390.
FE	36840.	35420.	39510.	42770.
MG	8580.	5260.	6160.	5640.
CA	8950.	8220.	7840.	8040.
NA	17200.	16400.	15900.	14100.
K	23770.	20630.	19860.	19880.
TI	4050.	4860.	5020.	5330.
MN	460.	440.	440.	490.
BA	920.	760.	960.	820.
CO	22.	24.	28.	50.
CU	22.	38.	21.	263.
GA	26.	25.	22.	27.
LI	13.	10.	12.	11.
MO	1.	1.	0.	0.
PR	17.	13.	12.	11.
PB	128.	100.	115.	111.
S	298.	138.	196.	243.
SR	280.	268.	247.	235.
CGH2O	49600.	64400.	52900.	45300.
ZN	84.	110.	82.	91.
ZR	152.	148.	148.	153.
V	160.	140.	200.	180.
NI	190.	138.	166.	270.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -93 770.1 -770.8	ST -94 770.8 -775.5	ST -95 775.5 -780.0	ST -97 782.3 -782.9
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SI	288420.	293000.	267840.	287590.
AL	89880.	86870.	79470.	85890.
FE	43990.	37470.	57500.	36970.
MG	9680.	9460.	5700.	5720.
CA	14050.	8250.	24210.	6810.
NA	15500.	15400.	20700.	6800.
K	18460.	25950.	17880.	5980.
TI	5110.	5360.	4580.	6370.
MN	850.	600.	1300.	410.
BA	820.	900.	960.	620.
CO	28.	34.	38.	16.
CU	41.	46.	33.	29.
GA	24.	20.	19.	26.
LI	11.	13.	12.	16.
MO	0.	0.	0.	0.
PB	15.	7.	17.	2.
RB	70.	97.	61.	70.
S	166.	162.	169.	130.
SR	270.	226.	247.	134.
C&H2O	47700.	51100.	51750.	107000.
ZN	94.	103.	80.	44.
ZR	157.	147.	134.	121.
V	160.	200.	180.	180.
NI	140.	174.	186.	164.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST -99 782.9 -784.8	ST -99 784.8 -785.3	ST-100 785.3 -786.5	ST-101 786.5 -787.2
SI	285570.	289160.	290650.	292010.
AL	84540.	85950.	84060.	83640.
FE	38620.	31260.	41320.	38060.
MG	5540.	5120.	7080.	7800.
CA	6320.	6890.	6450.	6620.
NA	10800.	12460.	12800.	15200.
K	12860.	18300.	21050.	21430.
TI	5410.	5340.	5410.	5650.
MN	400.	410.	430.	430.
BA	700.	680.	860.	740.
CO	32.	26.	40.	32.
CU	35.	43.	42.	39.
GA	12.	19.	4.	28.
LI	14.	15.	16.	17.
MO	0.	0.	0.	1.
PB	4.	7.	8.	13.
RB	102.	86.	116.	113.
S	87.	434.	211.	181.
SR	157.	151.	179.	160.
CO&H2O	74900.	133200.	60100.	75500.
ZN	78.	80.	96.	172.
ZR	123.	144.	140.	144.
V	130.	260.	200.	180.
NI	178.	158.	184.	168.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-102 787.2 -791.2	ST-103 791.2 -791.5	ST-104 791.5 -792.0	ST-105 792.0 -792.5
SI	301760.	267350.	323490.	303100.
AL	97640.	86980.	85800.	85020.
FE	36040.	41250.	32110.	44970.
MG	13520.	11020.	20420.	16880.
CA	7200.	7230.	5960.	6490.
NA	12900.	12350.	11600.	11600.
K	13080.	10980.	20810.	19320.
TI	5570.	5100.	5140.	5140.
MN	420.	430.	420.	430.
BA	900.	1180.	1500.	1420.
CO	30.	50.	46.	38.
CU	33.	29.	33.	34.
GA	26.	27.	24.	25.
LI	15.	22.	20.	18.
MO	1.	1.	2.	1.
PB	11.	25.	17.	32.
RB	104.	67.	94.	187.
S	152.	755.	213.	201.
SR	207.	152.	145.	174.
C&H2O	72000.	153600.	56100.	63300.
ZN	80.	74.	71.	78.
ZR	150.	155.	141.	142.
V	200.	180.	200.	200.
NI	160.	190.	200.	198.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-107		ST-108		ST-109		ST-110	
	794.0	-794.5	794.5	-795.5	795.5	-796.0	796.0	-797.0
SI	300710.		306650.		300220.		292760.	
AL	83900.		84170.		88670.		82550.	
FE	34270.		26950.		34900.		35810.	
MG	22740.		13180.		13980.		12500.	
CA	7410.		10920.		7860.		8740.	
NA	23500.		10200.		13000.		19300.	
K	17530.		11920.		15470.		12660.	
TI	5470.		4740.		5300.		4980.	
MN	450.		450.		460.		480.	
BA	1440.		1180.		1200.		1200.	
CO	46.		44.		36.		26.	
CU	42.		23.		34.		20.	
GA	24.		20.		22.		24.	
LI	15.		18.		20.		17.	
MO	1.		0.		1.		1.	
PB	14.		21.		15.		13.	
FB	83.		51.		83.		74.	
S	320.		165.		245.		193.	
SR	206.		254.		213.		245.	
COH2O	52900.		79400.		71200.		69600.	
ZN	123.		38.		106.		89.	
ZR	145.		147.		250.		157.	
V	180.		140.		140.		120.	
NI	170.		168.		174.		162.	

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-111 797.0 -798.0	ST-112 798.0 -799.0	ST-113 799.0 -801.0	ST-114 801.0 -801.5
SI	297510.	291110.	291650.	297160.
AL	86060.	87780.	82930.	73620.
FE	39550.	38160.	46170.	37860.
MG	9420.	15660.	19040.	11360.
CA	8500.	135060.	6880.	7500.
NA	11900.	17500.	14400.	13500.
K	11110.	7000.	8270.	12340.
TI	4400.	3870.	3980.	4485.
MN	2790.	470.	810.	520.
BA	1120.	1620.	1400.	1080.
CO	34.	26.	32.	28.
CU	38.	22.	26.	40.
GA	28.	28.	25.	20.
LI	15.	12.	15.	18.
MO	0.	1.	0.	1.
PB	20.	18.	15.	11.
RB	89.	32.	49.	82.
S	199.	196.	240.	364.
SR	238.	291.	225.	168.
C&H2O	73100.	61200.	71200.	104700.
ZN	93.	79.	72.	94.
ZR	157.	165.	151.	115.
V	80.	60.	60.	120.
NI	294.	264.	280.	264.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-115 801.5 - 805.5	ST-116 805.5 - 806.0	ST-117 806.0 - 807.5	ST-118 807.5 - 809.0
SI	316100.	315390.	320830.	304840.
AL	86160.	74970.	84960.	79130.
FE	41110.	30370.	29530.	32280.
MG	10860.	23520.	14620.	16860.
CA	8250.	7520.	8370.	8330.
NA	18450.	18700.	23100.	16700.
K	4280.	5480.	4310.	4700.
TI	3090.	3700.	2830.	3540.
MN	780.	580.	520.	580.
BA	1920.	1660.	2320.	1620.
CO	12.	24.	16.	12.
CU	19.	22.	18.	23.
GA	27.	23.	22.	23.
LI	15.	17.	15.	19.
MO	2.	4.	1.	2.
PB	11.	12.	11.	6.
RB	22.	26.	13.	13.
S	40.	128.	83.	88.
SR	195.	147.	193.	134.
CaH2O	84800.	76600.	75500.	77900.
ZN	56.	63.	60.	53.
ZR	200.	162.	187.	168.
V	40.	60.	20.	40.
NI	254.	262.	232.	166.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-119 809.0 -810.2	ST-120 810.2 -810.5	ST-122 812.5 -813.0	ST-124 814.2 -816.7
SI	599240.	306800.	287859.	302000.
AL	75420.	79810.	89400.	84860.
FE	33440.	27610.	50070.	33340.
MG	10380.	9360.	13300.	5700.
CA	7140.	7950.	9260.	6730.
NA	15450.	19500.	16900.	14700.
K	5950.	4540.	3530.	14080.
TI	3810.	2940.	3250.	5080.
MN	470.	450.	800.	420.
BA	800.	1100.	740.	1060.
CO	18.	14.	24.	24.
CU	29.	12.	16.	32.
GA	25.	21.	27.	23.
LI	15.	13.	27.	10.
MO	1.	1.	2.	0.
PB	6.	5.	7.	6.
RB	56.	22.	0.	103.
S	75.	78.	60.	160.
SR	159.	217.	203.	182.
C&H2O	87000.	55400.	92100.	73200.
ZN	53.	65.	63.	70.
ZR	157.	155.	200.	137.
V	100.	80.	40.	180.
NI	78.	90.	122.	114.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-125 816.7 -817.7	ST-126 817.7 -820.0	ST-127 820.0 -821.5	ST-128 821.5 -823.0
SI	311876.	311810.	290690.	284650.
AL	94440.	84960.	79930.	81280.
FE	37800.	42500.	33640.	54710.
MG	6360.	8260.	5940.	8560.
CA	6370.	6620.	18560.	11100.
NA	17400.	17500.	15200.	13900.
K	22840.	24930.	24320.	25490.
TI	5170.	5310.	4200.	4910.
MN	420.	420.	730.	990.
BA	1100.	1200.	1400.	1300.
CO	58.	36.	34.	38.
CU	38.	35.	30.	46.
GA	23.	26.	20.	24.
LI	13.	18.	10.	15.
MO	0.	1.	0.	2.
PR	9.	21.	14.	13.
RB	149.	150.	77.	105.
S	218.	179.	232.	343.
SR	184.	222.	257.	219.
C&H2O	52400.	54730.	43200.	68200.
ZN	107.	74.	94.	116.
ZR	146.	148.	142.	145.
V	205.	180.	168.	160.
NI	204.	142.	132.	170.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-129 823.0 -825.0	ST-130 825.0 -826.0	ST-131 826.0 -827.0	ST-132 827.0 -829.5
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SJ	310620.	307210.	306070.	278100.
AL	23820.	85070.	82150.	79810.
FE	39470.	35860.	36530.	70700.
MG	9420.	6900.	6680.	8460.
CA	6900.	7370.	9400.	11010.
NA	17400.	17800.	20400.	17500.
K	19020.	21030.	14080.	16700.
TI	5260.	5240.	4700.	4940.
MN	420.	430.	790.	1400.
BA	1300.	1160.	1100.	900.
CO	26.	40.	40.	38.
CU	34.	36.	25.	43.
GA	24.	22.	21.	27.
LI	12.	14.	13.	14.
MO	2.	2.	3.	1.
PR	12.	8.	7.	14.
RB	137.	116.	54.	95.
S	186.	221.	229.	226.
SR	203.	229.	276.	238.
CH2O	71900.	55300.	53170.	86700.
ZN	137.	127.	62.	131.
ZR	154.	155.	164.	172.
V	140.	140.	140.	100.
NI	172.	130.	134.	136.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-133 829.5 - 832.0	ST-134 833.0 - 832.5	ST-135 832.5 - 833.0	ST-136 833.0 - 833.2
SI	328150.	297160.	284900.	308110.
AL	77910.	80950.	97500.	77550.
FF	31560.	22420.	29470.	56130.
MG	6960.	7160.	9200.	10540.
CA	14670.	8410.	16250.	10450.
NA	19930.	25400.	23100.	15000.
K	12810.	11210.	5060.	10820.
TI	4670.	5470.	3940.	4950.
MN	850.	480.	590.	1210.
BA	940.	880.	710.	820.
CO	26.	40.	34.	32.
CU	21.	26.	23.	47.
GA	22.	27.	27.	26.
LI	10.	14.	11.	14.
MO	3.	0.	0.	0.
PB	14.	15.	10.	11.
RB	41.	85.	13.	65.
S	153.	205.	111.	134.
SR	258.	212.	304.	205.
CaH2O	40250.	39800.	76700.	71000.
ZN	67.	71.	91.	90.
ZR	124.	170.	153.	155.
V	60.	160.	60.	140.
NI	124.	120.	180.	170.

HOFSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-137 833.2 - 833.5	ST-138 833.5 - 834.0	ST-139 834.0 - 838.0	ST-140 838.0 - 838.5
SI	269590.	309110.	297290.	287550.
AL	94200.	86520.	84600.	85230.
FE	34900.	27390.	35960.	52810.
MG	13920.	14440.	9500.	11540.
CA	13130.	10120.	14070.	9410.
NA	20200.	18100.	22900.	13500.
K	3420.	11080.	11400.	15300.
TI	3520.	4760.	4440.	5230.
MN	450.	500.	720.	950.
BA	460.	1180.	980.	1040.
CO	34.	42.	78.	40.
CU	23.	31.	22.	38.
GA	25.	22.	22.	21.
LI	11.	13.	10.	13.
MO	0.	5.	16.	1.
PB	7.	15.	12.	11.
RB	0.	56.	47.	97.
S	35.	139.	94.	143.
SR	256.	226.	259.	212.
CGH2O	94400.	85200.	47000.	78700.
ZN	8.	22.	63.	74.
ZR	159.	142.	138.	158.
V	40.	142.	80.	200.
NI	108.	142.	118.	108.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-141 839.5 -840.0	ST-142 840.0 -841.0	ST-143 841.0 -844.2	ST-144 844.2 -845.5
SI	302670.	299280.	296800.	294010.
AL	92070.	84330.	84650.	84170.
FE	22670.	41300.	34000.	45450.
MG	7900.	11520.	9160.	14620.
CA	15200.	12660.	20590.	17080.
NA	13700.	14700.	18400.	16900.
K	13510.	16610.	17960.	20070.
TI	4660.	5950.	4560.	5190.
MN	520.	820.	800.	970.
BA	1000.	960.	1120.	1180.
CO	30.	38.	36.	40.
CU	21.	32.	15.	44.
GA	17.	23.	19.	25.
LI	10.	13.	8.	12.
MO	0.	0.	0.	0.
PB	13.	12.	27.	13.
RB	38.	79.	55.	83.
S	105.	150.	154.	189.
SR	271.	214.	231.	220.
COH2O	44800.	65700.	40500.	66700.
ZN	70.	59.	73.	103.
ZR	164.	151.	135.	155.
V	160.	220.	160.	240.
NI	76.	140.	170.	146.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-145 845.5 -846.0	ST-146 846.0 -848.0	ST-147 848.0 -849.0	ST-148 849.0 -850.5
SI	291100.	308870.	302260.	307660.
AL	90210.	88910.	84810.	85070.
FE	40570.	38370.	41400.	23750.
MG	11720.	7000.	7240.	14680.
CA	11110.	6760.	6990.	10760.
NA	14100.	13000.	17100.	19800.
K	14250.	19660.	22080.	18650.
TI	5330.	5310.	5060.	4330.
MN	680.	420.	430.	500.
BA	960.	960.	980.	1560.
CO	44.	40.	26.	24.
CU	36.	38.	46.	22.
GA	20.	20.	25.	17.
LI	13.	12.	13.	10.
MO	0.	0.	1.	1.
PB	8.	26.	26.	17.
RE	83.	137.	126.	60.
S	192.	251.	208.	350.
SR	217.	173.	197.	257.
C&H2O	65400.	63400.	47800.	34700.
ZN	101.	58.	67.	68.
ZR	141.	138.	142.	138.
V	200.	200.	200.	140.
NI	170.	180.	134.	114.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-149	ST-150	ST-151	ST-152
	850.5 - 856.0	854.0 - 857.0	857.0 - 858.5	858.5 - 859.0
SI	312460.	295600.	299950.	300600.
AL	89110.	87420.	81840.	85590.
FE	29320.	28990.	46920.	13510.
MG	15280.	8640.	9680.	18920.
CA	12900.	13920.	9500.	8840.
NA	19300.	14600.	15000.	23100.
K	20100.	19490.	18980.	23790.
TI	5030.	4770.	4750.	3610.
MN	620.	780.	1100.	430.
BA	1400.	960.	1160.	1960.
CO	30.	26.	26.	32.
CU	33.	43.	36.	13.
GA	21.	24.	26.	16.
LI	11.	13.	11.	8.
MO	1.	0.	0.	0.
PB	13.	17.	21.	21.
RB	72.	44.	136.	75.
S	162.	169.	219.	202.
SR	241.	241.	192.	244.
CaH20	50700.	55500.	66000.	46000.
ZN	75.	83.	92.	54.
ZR	150.	146.	154.	115.
V	180.	160.	120.	80.
NI	142.	140.	120.	84.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-153 859.0 -859.5	ST-154 859.5 -860.5	ST-156 860.7 -865.5	ST-158 866.0 -866.2
ST	234350.	303920.	252490.	192610.
AL	35430.	27230.	72490.	45830.
FE	36620.	31240.	62590.	165380.
MG	11940.	7500.	15660.	52600.
CA	7060.	6780.	68490.	23090.
NA	10400.	27300.	15800.	4700.
K	20220.	25060.	12760.	8750.
TI	4630.	5020.	2940.	3230.
MN	650.	510.	1440.	6410.
BA	1150.	1120.	1520.	1720.
CO	30.	34.	26.	50.
CU	20.	32.	24.	42.
GA	23.	20.	21.	14.
LI	15.	15.	12.	16.
MO	2.	1.	1.	0.
PB	33.	17.	15.	12.
PB	111.	126.	54.	53.
S	348.	325.	274.	986.
SR	136.	157.	263.	75.
CGH20	93600.	77800.	74500.	208700.
ZN	30.	85.	71.	39.
ZP	149.	116.	116.	95.
V	140.	140.	160.	160.
NI	142.	140.	100.	550.

HOPESSHORE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-154 866.2 -873.0	ST-160 870.0 -871.0	ST-161 871.0 -871.3	ST-162 871.3 -872.5
SI	5045.80.	3271.60.	3237.60.	3166.10.
AL	952.10.	815.00.	525.80.	870.80.
FE	421.70.	324.40.	246.70.	404.80.
MG	118.60.	82.80.	178.20.	150.40.
CA	71.70.	59.80.	62.50.	65.70.
NA	155.00.	116.00.	149.00.	113.00.
K	175.30.	174.90.	137.40.	182.70.
TI	49.80.	49.30.	54.20.	50.70.
MN	8.50.	3.90.	3.80.	6.60.
BA	10.00.	15.40.	15.40.	14.40.
CO	24.	24.	30.	38.
CU	27.	23.	23.	21.
GA	19.	18.	18.	26.
LI	13.	11.	12.	13.
MO	1.	0.	1.	1.
PB	11.	30.	24.	17.
PP	14.9.	18.4.	10.6.	15.9.
S	21.9.	18.6.	36.3.	25.8.
SR	15.8.	14.0.	12.8.	15.6.
C&H2O	769.00.	477.00.	940.00.	654.00.
ZN	104.	115.	100.	81.
ZR	147.	151.	153.	151.
V	100.	160.	140.	180.
NI	98.	116.	96.	88.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-163 877.5 -876.5	ST-164 876.5 -879.2	ST-165 879.2 -880.0	ST-166 880.0 -882.8
SI	294100.	261930.	307660.	299630.
AL	78350.	71630.	82530.	87480.
FE	29630.	105780.	26730.	37130.
MG	13320.	13400.	13900.	9440.
CA	15390.	12940.	6460.	6440.
NA	16800.	11300.	29800.	15700.
K	19270.	11930.	19100.	11800.
TI	3720.	4310.	4950.	5250.
MN	790.	3250.	410.	440.
BA	1740.	1580.	1380.	1060.
CO	40.	38.	40.	40.
CU	22.	51.	26.	30.
GA	22.	24.	19.	25.
LI	8.	14.	11.	12.
MO	0.	0.	1.	1.
PB	29.	12.	11.	20.
RB	60.	77.	121.	144.
S	217.	163.	501.	115.
SR	212.	176.	115.	167.
C&H2O	43500.	129700.	59500.	57600.
ZN	53.	77.	72.	68.
ZR	143.	123.	119.	143.
V	170.	140.	120.	260.
NI	90.	378.	100.	126.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-167 882.3 - 894.5	ST-168 884.5 - 885.5	ST-169 885.5 - 887.0	ST-170 887.0 - 891.4
SI	283670.	301840.	301930.	308760.
AL	88520.	88590.	88030.	85070.
FE	38170.	35660.	31690.	28000.
MG	3220.	33960.	10920.	9920.
CA	6970.	7430.	8680.	8270.
NA	14900.	18700.	18600.	22600.
K	9870.	11060.	9140.	10550.
TI	5430.	4560.	4110.	4090.
MN	420.	420.	610.	420.
BA	1820.	1540.	1280.	1240.
CO	44.	42.	46.	42.
CU	11.	32.	27.	22.
GA	22.	22.	21.	14.
LI	15.	13.	10.	10.
MO	1.	1.	1.	2.
PB	3.	10.	4.	9.
RB	122.	104.	67.	56.
S	247.	175.	158.	242.
SR	164.	207.	234.	277.
COH ₂ O	105600.	68900.	69000.	37400.
ZN	95.	76.	77.	86.
ZR	140.	155.	144.	145.
V	120.	140.	220.	140.
NI	112.	102.	100.	94.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-171 891.4 - 892.5	ST-172 892.5 - 899.0	ST-173 904.0 - 905.2	ST-174 905.2 - 907.7
SI	303860.	299180.	310630.	296570.
AL	83640.	92150.	90820.	77080.
FE	39620.	31710.	27950.	58660.
MG	9250.	6640.	9320.	8500.
CA	8450.	7810.	9120.	10120.
NA	16700.	26800.	18700.	15900.
K	3230.	24570.	18720.	17080.
TI	4770.	5290.	4790.	5030.
MN	830.	440.	440.	1190.
BA	1000.	960.	960.	860.
CO	40.	42.	36.	40.
CU	36.	31.	27.	35.
GA	22.	22.	20.	22.
LI	13.	14.	11.	14.
MO	0.	1.	0.	1.
PB	3.	2.	5.	3.
RB	93.	122.	81.	102.
S	260.	182.	147.	187.
SR	205.	172.	211.	193.
CH20	58290.	48790.	50000.	63600.
ZN	80.	80.	87.	70.
ZR	141.	135.	142.	151.
V	160.	160.	140.	200.
NI	118.	98.	108.	154.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-175 967.7 - 909.5	ST-176 909.5 - 912.5	ST-177 912.5 - 917.5	ST-178 917.5 - 920.0
SI	393520.	309970.	299360.	317500.
AL	84750.	85900.	73870.	81280.
FE	31780.	27340.	47780.	33170.
MG	5860.	6940.	6040.	5060.
CA	3090.	10790.	9590.	6270.
NA	19100.	16600.	14700.	16700.
K	12620.	15060.	12550.	20780.
TI	4890.	4400.	4850.	4850.
MN	600.	670.	1010.	420.
BA	940.	1040.	960.	960.
CO	42.	40.	34.	124.
CU	20.	24.	28.	31.
GA	19.	27.	17.	23.
LI	15.	11.	12.	12.
MO	0.	1.	2.	1.
PB	5.	9.	3.	4.
RB	72.	66.	92.	125.
S	227.	154.	285.	306.
SR	197.	244.	189.	198.
COH2O	75400.	54900.	78800.	48600.
ZN	60.	76.	65.	73.
ZP	152.	154.	158.	156.
V	140.	140.	160.	180.
NI	112.	90.	112.	264.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-179		ST-180		ST-181		ST-182	
	920.9	921.5	921.5	924.8	924.8	929.6	929.6	933.0
SI	300360.		209690.		310630.		298490.	
AL	85950.		82280.		84440.		82280.	
FE	49470.		43730.		37290.		37410.	
MG	6520.		6440.		6340.		8140.	
CA	8910.		8140.		9280.		14940.	
NA	14900.		35600.		14800.		16100.	
K	13180.		17210.		11880.		9000.	
TI	5130.		5080.		4760.		4270.	
MN	970.		430.		480.		750.	
BA	960.		940.		1040.		1100.	
CO	44.		32.		34.		32.	
CU	48.		41.		34.		23.	
GA	28.		28.		23.		24.	
LI	14.		14.		12.		10.	
MO	2.		0.		2.		0.	
PB	14.		21.		8.		11.	
RB	121.		133.		91.		39.	
S	214.		158.		229.		123.	
SR	204.		201.		213.		262.	
C&H2O	63200.		52200.		64900.		66000.	
ZN	34.		96.		79.		57.	
ZR	154.		152.		152.		158.	
V	130.		160.		140.		120.	
NI	140.		66.		70.		84.	

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-183 922.0 -933.5	ST-184 933.5 -935.5	ST-185 935.5 -936.0	ST-186 936.0 -938.5
SI	294190.	309466.	307919.	318150.
AL	89720.	94750.	84380.	82500.
FE	59340.	30290.	26150.	31380.
MG	8120.	8000.	5760.	5840.
CA	12300.	8810.	8670.	10450.
NA	14900.	10700.	12400.	12900.
K	13950.	9180.	7560.	9300.
TI	5420.	4490.	4680.	4120.
MN	1230.	530.	410.	470.
BA	960.	900.	920.	760.
CO	40.	36.	34.	52.
CU	60.	24.	20.	20.
GA	27.	21.	17.	20.
LI	13.	11.	13.	15.
MO	1.	7.	1.	2.
PB	7.	8.	5.	12.
RB	90.	60.	57.	62.
S	256.	261.	303.	204.
SR	205.	181.	165.	245.
C&H2O	72400.	73600.	91200.	117700.
ZN	73.	48.	60.	73.
ZR	144.	136.	138.	155.
V	200.	140.	120.	200.
NI	120.	98.	90.	120.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-187 938.5 -939.0	ST-188 939.0 -944.5	ST-189 944.5 -945.7	ST-190 945.7 -947.5
SI	304720.	302660.	305150.	305890.
AL	79070.	93370.	86720.	85750.
FE	31420.	44220.	35640.	36210.
MG	6480.	8360.	6320.	7940.
CA	9160.	10350.	7930.	8080.
NA	22250.	16500.	16400.	16600.
K	3640.	14220.	9350.	9440.
TI	4410.	5060.	5040.	4810.
MN	460.	790.	490.	420.
BA	980.	980.	860.	1060.
CO	30.	40.	36.	38.
CU	22.	33.	19.	23.
GA	26.	30.	22.	23.
LI	12.	13.	13.	12.
MO	2.	0.	1.	1.
PB	11.	9.	7.	14.
PB	77.	104.	92.	81.
S	269.	172.	198.	148.
SR	198.	190.	161.	171.
C&H2O	72610.	66900.	83600.	73700.
ZN	60.	83.	74.	73.
ZR	136.	137.	126.	131.
V	140.	160.	140.	140.
NI	90.	124.	106.	112.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-191 947.5 -954.0	ST-192 959.0 -960.2	ST-193 969.2 -960.5	ST-197 970.0 -971.0
SI	29492.0	31864.0	30227.0	33734.0
AL	8559.0	8288.0	9837.0	8239.0
FE	5394.0	3461.0	3943.0	1314.0
MG	742.0	696.0	864.0	290.0
CA	1026.0	735.0	993.0	735.0
NA	3080.0	1310.0	1440.0	1590.0
K	946.0	1489.0	1268.0	4679.0
TI	432.0	514.0	487.0	486.0
MN	106.0	44.0	64.0	43.0
BA	86.0	90.0	100.0	108.0
CO	36.0	36.0	52.0	46.0
CU	26.0	35.0	22.0	18.0
GA	25.0	21.0	23.0	16.0
LI	11.0	13.0	14.0	9.0
MO	0.0	1.0	1.0	1.0
PB	8.0	17.0	9.0	12.0
RB	7.0	101.0	83.0	113.0
S	156.0	216.0	162.0	341.0
SR	216.0	161.0	201.0	137.0
CO&H2O	85100.0	57800.0	63200.0	63900.0
ZN	89.0	75.0	100.0	53.0
ZR	159.0	136.0	148.0	131.0
V	120.0	160.0	140.0	140.0
NI	136.0	102.0	142.0	82.0

HOPSESHOF CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-198 971.0 - 972.0	ST-199 972.8 - 973.5	ST-200 973.5 - 974.0	ST-201 974.0 - 975.0
SI	298710.	291830.	318070.	281930.
AL	86620.	83470.	78660.	80890.
FE	39320.	46540.	19920.	24370.
MG	7980.	18660.	5000.	9880.
CA	14140.	10430.	11560.	8360.
NA	17500.	16100.	18100.	12700.
K	18690.	13450.	10630.	6810.
TI	4160.	4260.	3430.	4980.
MN	690.	1190.	570.	420.
BA	1060.	1740.	980.	820.
CO	36.	42.	38.	36.
CU	10.	25.	13.	6.
GA	13.	27.	16.	14.
LI	10.	12.	9.	156.
MO	1.	2.	1.	6.
PB	26.	14.	17.	5.
RB	62.	30.	39.	30.
S	346.	160.	229.	452.
SR	226.	243.	241.	76.
CaH2O	34500.	63000.	49100.	205800.
ZN	62.	64.	64.	39.
ZR	122.	247.	110.	106.
V	80.	140.	60.	140.
NI	60.	86.	54.	66.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-202		ST-203		ST-204		ST-205	
	975.0	975.5	975.3	979.2	979.2	980.7	980.7	982.0

SI	306020.		319800.		313630.		314560.	
AL	88520.		79700.		87180.		81170.	
FE	30440.		31260.		42570.		33480.	
MG	9740.		8780.		10240.		12680.	
CA	7830.		8270.		9280.		8950.	
NA	11500.		16100.		16100.		30100.	
K	6260.		5950.		8850.		10130.	
TI	4500.		3850.		4410.		4420.	
MN	460.		450.		710.		430.	
BA	940.		680.		820.		920.	
CO	34.		26.		32.		28.	
CU	14.		19.		35.		34.	
GA	25.		19.		25.		25.	
LI	120.		11.		9.		11.	
MO	1.		0.		0.		2.	
PB	11.		9.		15.		5.	
RE	55.		59.		78.		88.	
S	47.		78.		99.		84.	
SR	147.		153.		209.		189.	
CGH2O	74200.		70100.		65800.		62900.	
ZN	34.		43.		81.		80.	
ZR	117.		125.		123.		123.	
V	180.		100.		140.		160.	
NI	102.		68.		118.		86.	

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-206 982.0 - 985.2	ST-207 985.2 - 988.0	ST-209 989.0 - 989.3	ST-211 989.5 - 995.5
SI	297340.	302080.	293870.	317100.
AL	80780.	77430.	80950.	88820.
FE	27150.	33630.	24350.	20320.
MG	9320.	7040.	17580.	13220.
CA	9630.	25030.	9830.	10030.
NA	16400.	14990.	13700.	17000.
K	7300.	7570.	2530.	6270.
TI	3930.	3590.	860.	3550.
MN	550.	900.	410.	430.
BA	340.	840.	560.	1100.
CO	18.	30.	16.	16.
CU	23.	28.	9.	16.
GA	22.	20.	20.	23.
LI	9.	14.	8.	10.
MO	0.	1.	0.	1.
PR	6.	0.	7.	14.
RB	49.	36.	0.	23.
S	70.	166.	57.	115.
SR	209.	234.	123.	228.
CGH2O	57100.	99500.	85900.	49100.
ZN	64.	58.	13.	52.
ZR	131.	128.	93.	136.
V	120.	160.	0.	80.
NI	70.	130.	70.	74.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-212 995.5-1001.5	ST-213 1001.5-1004.0	ST-214 1004.0-1005.0	ST-215 1007.5-1013.0
SI	303350.	299990.	250650.	315320.
AL	92880.	92670.	73560.	91800.
FE	24580.	27360.	84590.	38050.
MG	4820.	6620.	5740.	5900.
CA	6650.	6700.	45880.	7010.
NA	11200.	12100.	8200.	12200.
K	51680.	40030.	51580.	20110.
TI	5240.	5560.	3830.	5730.
MN	540.	420.	2590.	610.
BA	900.	780.	1180.	840.
CO	24.	36.	24.	26.
CU	36.	36.	29.	27.
GA	27.	29.	29.	30.
LI	13.	15.	8.	17.
MO	1.	1.	2.	1.
PB	1.	10.	17.	19.
RB	171.	175.	152.	156.
S	192.	252.	234.	122.
SR	118.	130.	143.	164.
COH2O	39500.	67300.	67500.	56400.
ZN	100.	79.	77.	108.
ZR	124.	141.	113.	146.
V	180.	300.	100.	180.
NI	97.	134.	216.	112.

HERSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-217 1013.0-1015.0	ST-218 1015.0-1017.5	ST-219 1017.5-1023.0	ST-220 1023.0-1024.0
SI	30200.	279810.	329200.	313210.
AL	90640.	85490.	86210.	85280.
FE	30660.	66280.	26640.	29360.
MG	9660.	5960.	7260.	4880.
CA	7160.	10650.	7000.	7910.
NA	9700.	13700.	13800.	13700.
K	17680.	20250.	7210.	6600.
TI	5780.	4760.	5230.	4500.
MN	410.	1460.	410.	420.
BA	980.	920.	860.	660.
CO	24.	26.	18.	24.
CU	34.	36.	17.	17.
GA	23.	21.	14.	15.
LI	21.	15.	18.	15.
MO	1.	2.	2.	1.
PB	6.	9.	11.	10.
PP	126.	115.	64.	48.
S	190.	987.	217.	312.
SR	132.	148.	116.	134.
C&H2O	89000.	110500.	61300.	95300.
ZN	110.	97.	28.	61.
ZR	131.	140.	133.	143.
V	200.	120.	100.	100.
NI	102.	152.	70.	76.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-221 1024.0-1030.0	ST-222 1030.0-1035.2	ST-223 1035.2-1036.0	ST-224 1036.0-1040.5
SI	317510.	317860.	311520.	306390.
AL	86000.	82990.	84280.	77080.
FE	24180.	21680.	26210.	20090.
MG	10840.	6900.	8940.	10600.
CA	10400.	12360.	9350.	16530.
NA	33300.	17900.	11600.	15700.
K	6550.	6680.	20420.	5010.
TI	3480.	3530.	4810.	2840.
MN	430.	550.	470.	500.
BA	1420.	1100.	800.	860.
CO	24.	34.	28.	32.
CU	20.	19.	18.	22.
GA	20.	17.	18.	17.
LI	12.	12.	15.	10.
MO	7.	1.	4.	2.
PB	17.	13.	6.	13.
RB	20.	27.	102.	20.
S	82.	168.	271.	78.
SR	237.	227.	150.	219.
COH2O	49400.	53590.	25200.	59700.
ZN	51.	68.	78.	64.
ZR	129.	132.	232.	126.
V	100.	100.	120.	40.
NI	68.	76.	94.	88.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-225 1040.5-1040.6	ST-226 1040.6-1041.4	ST-227 1041.4-1041.5	ST-228 1041.5-1042.0
SI	289880.	324390.	298640.	359760.
AL	89570.	69410.	75460.	61870.
FE	32510.	22230.	23380.	18830.
MG	5300.	7240.	7780.	4640.
CA	11470.	8480.	64970.	7130.
NA	15700.	9800.	12700.	8700.
K	2560.	5000.	3090.	4270.
TI	2310.	2370.	1180.	6290.
MN	460.	420.	1150.	400.
BA	1060.	730.	760.	620.
CO	36.	38.	12.	14.
CU	11.	10.	10.	12.
GA	13.	12.	21.	6.
LI	12.	16.	11.	18.
MO	2.	2.	1.	4.
PB	20.	10.	12.	7.
RB	10.	35.	0.	25.
S	63.	74.	82.	192.
SR	907.	120.	176.	83.
CH ₂ O	68700.	52100.	67300.	77800.
ZN	44.	41.	23.	15.
ZP	127.	92.	101.	77.
V	60.	80.	20.	40.
NI	66.	94.	72.	66.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-229 1042.0-1043.0	ST-230 1043.0-1049.0	ST-231 1049.0-1054.2	ST-232 1054.2-1055.2
SI	265470.	310720.	323430.	305550.
AL	64450.	85120.	82770.	87630.
FE	119060.	31440.	14420.	33990.
MG	16220.	5120.	7440.	4740.
CA	19750.	7480.	10440.	7970.
NA	11300.	13500.	14500.	29100.
K	2850.	12240.	34800.	16620.
TI	6610.	5640.	4020.	5460.
MN	1990.	420.	450.	420.
BA	1180.	660.	1520.	800.
CO	24.	34.	30.	36.
CU	18.	0.	15.	29.
GA	19.	20.	14.	23.
LI	14.	13.	10.	17.
MO	2.	0.	1.	1.
PB	21.	12.	19.	11.
RB	0.	110.	80.	120.
S	215.	142.	74.	132.
SR	173.	147.	176.	185.
CaH2O	96700.	66200.	26200.	56500.
ZN	40.	71.	62.	69.
ZR	119.	130.	123.	154.
V	40.	140.	80.	180.
NI	244.	86.	82.	94.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-233 1055.2-1061.5	ST-234 1061.0-1063.0	ST-235 1063.0-1064.0	ST-236 1064.0-1067.0
SI	310250.	311070.	309670.	324690.
AL	82320.	82170.	84860.	80330.
FE	36630.	31240.	34510.	11830.
MG	5840.	4620.	3860.	1660.
CA	9050.	8170.	7560.	23140.
NA	21300.	14400.	12900.	9000.
K	10280.	11540.	34240.	48980.
TI	4400.	4990.	4530.	3750.
MN	500.	400.	420.	550.
BA	840.	780.	1100.	1420.
CO	42.	36.	39.	46.
CU	24.	22.	23.	20.
GA	21.	21.	18.	18.
LI	13.	10.	16.	6.
MO	1.	0.	0.	1.
PB	12.	14.	8.	14.
RB	93.	113.	131.	163.
S	160.	73.	144.	208.
SR	212.	196.	185.	129.
C&H2O	71300.	50100.	25900.	21000.
ZN	78.	52.	65.	48.
ZR	152.	139.	139.	121.
V	140.	140.	120.	100.
NI	120.	102.	32.	62.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-227 1067.0-1070.5	ST-238 1070.5-1072.0	ST-239 1072.0-1073.0	ST-240 1073.0-1074.0
SI	298440.	313400.	307440.	311050.
AL	79070.	84750.	83470.	82330.
FE	64440.	32310.	33950.	29360.
MG	5700.	4680.	4440.	4340.
CA	8740.	7850.	8040.	8860.
NA	15600.	16200.	15800.	31300.
K	35950.	26760.	30290.	19810.
TI	4490.	4740.	5010.	4710.
MN	1090.	440.	470.	530.
BA	1000.	940.	940.	820.
CO	34.	48.	36.	32.
CU	35.	28.	37.	24.
GA	23.	21.	22.	20.
LI	10.	12.	13.	11.
MO	0.	0.	0.	1.
PB	0.	12.	9.	8.
RB	165.	154.	152.	104.
S	208.	444.	307.	117.
SR	175.	204.	198.	229.
CO&H2O	63200.	53200.	72700.	47400.
ZN	68.	106.	115.	68.
ZR	143.	142.	135.	139.
V	120.	140.	140.	120.
NI	116.	96.	96.	72.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-241 1074.0-1075.2	ST-242 1075.2-1078.5	ST-243 1078.5-1079.0	ST-244 1079.0-1080.2
SI	311080.	323700.	312820.	315870.
AL	85640.	85280.	80720.	81950.
FE	33690.	29930.	30470.	20130.
MG	4500.	4160.	3992.	4120.
CA	8520.	7565.	8240.	9850.
NA	17700.	22900.	14700.	18400.
K	22140.	18330.	24510.	13190.
TI	5050.	5150.	5160.	3820.
MN	640.	430.	430.	440.
BA	900.	890.	864.	940.
CO	38.	34.	40.	28.
CU	23.	34.	32.	25.
GA	16.	23.	22.	20.
LI	12.	11.	12.	9.
MO	0.	1.	1.	1.
PB	7.	9.	6.	10.
RB	71.	129.	149.	62.
S	115.	137.	276.	157.
SR	131.	184.	179.	241.
CGH2O	46900.	56900.	84400.	42900.
ZN	53.	68.	82.	57.
ZR	63.	144.	157.	144.
V	140.	140.	160.	80.
NI	84.	90.	82.	60.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-245 1080.2-1081.2	ST-246 1081.2-1082.5	ST-247 1082.5-1083.0	ST-248 1083.0-1083.5
SI	282890.	283460.	296260.	325620.
AL	79410.	79990.	83350.	85950.
FE	78710.	62900.	33150.	28770.
MG	5100.	10860.	13220.	4400.
CA	8930.	12460.	8090.	7770.
NA	11200.	17600.	15000.	15800.
K	18470.	11580.	10830.	11240.
TI	4660.	4440.	4940.	4610.
MN	3470.	1310.	420.	410.
BA	840.	840.	1220.	680.
CO	40.	34.	50.	34.
CU	50.	35.	21.	16.
GA	29.	26.	22.	24.
LI	14.	10.	13.	10.
MO	2.	1.	2.	0.
PB	11.	9.	31.	11.
RB	132.	73.	82.	89.
S	205.	182.	319.	64.
SR	184.	252.	177.	183.
COH ₂ O	204400.	78900.	95700.	56600.
ZN	65.	85.	115.	28.
ZR	151.	157.	167.	141.
V	180.	120.	120.	100.
NI	180.	144.	100.	70.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-249 1083.5-1085.5	ST-250 1085.5-1087.5	ST-251 1087.5-1093.5	ST-252 1093.5-1096.0
SI	316160.	316960.	306880.	326810.
AL	84440.	84170.	80500.	82550.
FE	29590.	34940.	22860.	31940.
MG	4380.	5280.	4760.	5760.
CA	8120.	8610.	14010.	8070.
NA	15700.	14700.	36300.	19200.
K	11940.	14710.	7680.	13000.
TI	4740.	4870.	3250.	4950.
MN	410.	430.	540.	410.
BA	760.	700.	840.	760.
CO	34.	38.	34.	58.
CU	6.	25.	8.	22.
GA	24.	21.	84.	24.
LI	12.	12.	9.	12.
MO	2.	1.	1.	0.
PB	7.	5.	16.	10.
RB	93.	109.	21.	130.
S	110.	127.	112.	191.
SR	186.	208.	275.	198.
CGH2O	69800.	56000.	29400.	56600.
ZN	54.	71.	48.	51.
ZR	156.	138.	132.	144.
V	120.	150.	80.	140.
NI	56.	54.	70.	118.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-253 1096.0-1097.0	ST-254 1097.0-1101.0	ST-255 1101.0-1104.0	ST-256 1104.0-1105.5
SI	313876.	301923.	312100.	320720.
AL	83310.	84540.	83150.	35380.
FE	33160.	37100.	35490.	30760.
MG	6420.	5220.	4160.	5140.
CA	9230.	8180.	8490.	8490.
NA	11000.	12600.	20300.	15500.
K	10110.	10010.	15700.	17000.
TJ	4860.	4720.	5080.	4920.
MN	420.	400.	410.	430.
BA	720.	700.	960.	900.
CO	52.	36.	30.	46.
CU	27.	25.	32.	34.
GA	23.	20.	18.	19.
LI	13.	11.	13.	17.
MO	1.	1.	0.	12.
PB	20.	10.	10.	15.
RB	82.	117.	125.	106.
S	291.	34.	73.	132.
SR	198.	198.	219.	206.
CaH2O	85600.	68100.	55500.	64700.
ZN	120.	61.	55.	82.
ZP	131.	135.	141.	145.
V	100.	120.	140.	120.
NI	96.	92.	76.	94.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-257 1105.5-1108.2	ST-258 1108.0-1109.5	ST-259 1109.5-1112.0	ST-260 1112.0-1112.7
SI	306650.	316570.	320110.	302490.
AL	34280.	86060.	82610.	87380.
FE	40720.	33690.	31620.	39770.
MG	5480.	4600.	4700.	5860.
CA	8480.	7400.	7510.	12650.
NA	15300.	12400.	15800.	17700.
K	15420.	11630.	12120.	8560.
TI	4390.	5270.	4850.	3510.
MN	420.	410.	400.	800.
BA	860.	720.	700.	920.
CO	34.	36.	32.	28.
CU	34.	25.	28.	12.
GA	70.	26.	22.	22.
LI	12.	14.	10.	9.
MO	0.	2.	1.	1.
PB	13.	15.	4.	11.
BB	24.	115.	124.	31.
S	71.	67.	26.	131.
SE	158.	166.	175.	294.
COH2O	63600.	69800.	61700.	48000.
ZN	95.	51.	44.	52.
ZR	143.	132.	126.	131.
V	140.	160.	140.	80.
NI	94.	104.	70.	76.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-261 1112.7-1115.0	ST-262 1115.0-1117.5	ST-263 1117.5-1123.0	ST-264 1123.0-1127.0
SI	343860.	203960.	295490.	303470.
AL	80950.	74970.	82060.	84010.
FE	25830.	84810.	21240.	27240.
MG	3420.	75600.	2600.	3340.
CA	8250.	11210.	56840.	24580.
NA	18500.	11800.	14100.	12200.
K	11720.	12340.	18690.	16120.
TI	4570.	4490.	3580.	4180.
MN	400.	1450.	660.	690.
BA	720.	1020.	1060.	900.
CO	26.	42.	26.	30.
CU	29.	44.	21.	20.
GA	19.	32.	24.	23.
LI	8.	11.	9.	9.
MO	1.	1.	1.	1.
PB	6.	4.	12.	12.
PP	91.	107.	60.	0.
S	81.	131.	43.	77.
SR	216.	215.	282.	284.
COH2O	44500.	72300.	25500.	30800.
ZN	48.	66.	62.	56.
ZR	140.	144.	102.	114.
V	80.	140.	80.	63.
NI	60.	150.	56.	62.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-265 1127.0-1130.0	ST-266 1130.0-1132.0	ST-267 1132.0-1135.0	ST-268 1135.0-1136.0
SI	313640.	307580.	307990.	320250.
AL	86260.	88370.	84860.	79760.
FE	34090.	29450.	31140.	26940.
MG	6000.	11200.	5720.	4340.
CA	9480.	12820.	8270.	7420.
NA	14400.	18500.	14100.	9900.
K	9010.	6450.	7590.	10230.
TI	4120.	3700.	4590.	5120.
MN	500.	650.	410.	410.
BA	560.	920.	620.	620.
CO	32.	24.	30.	30.
CU	25.	8.	23.	24.
GA	29.	23.	26.	21.
LI	10.	10.	13.	7.
MO	2.	2.	1.	2.
PR	7.	7.	9.	5.
RB	72.	28.	75.	90.
S	79.	119.	168.	305.
SR	215.	246.	161.	130.
(GH2)	82700.	82700.	88400.	100500.
ZN	72.	61.	71.	45.
ZK	140.	148.	125.	126.
V	120.	80.	120.	160.
NI	82.	86.	74.	72.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-269 1136.0-1137.5	ST-270 1137.5-1140.0	ST-271 1140.0-1141.0	ST-272 1141.0-1142.0
SI	317750.	300610.	310520.	300200.
AL	78430.	81280.	86700.	86700.
FE	22990.	18710.	29020.	20900.
MG	4240.	3620.	3940.	4060.
CA	7150.	6890.	7270.	7860.
NA	13200.	10100.	16000.	15600.
K	34220.	47750.	27140.	42230.
TI	4880.	4980.	4330.	4740.
MN	410.	400.	410.	420.
BA	800.	760.	760.	800.
CO	32.	30.	22.	32.
CU	34.	19.	21.	31.
GA	21.	20.	26.	26.
LI	14.	15.	11.	13.
MO	2.	1.	2.	1.
PB	16.	5.	32.	5.
BB	112.	69.	113.	106.
S	250.	443.	116.	211.
SR	145.	90.	173.	191.
CGHZO	63260.	142600.	39500.	49600.
ZN	117.	66.	30.	117.
ZR	130.	111.	140.	135.
V	100.	100.	80.	100.
NI	80.	60.	50.	64.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-273 1142.0-1143.0	ST-274 1143.0-1150.0	ST-275 1150.0-1151.0	ST-276 1151.0-1154.5
SI	306820.	302360.	297990.	301890.
AL	82920.	90120.	83450.	87700.
FE	15710.	26240.	18470.	25300.
MG	25620.	7290.	5700.	6400.
CA	9900.	8510.	10930.	9570.
NA	19900.	16900.	21500.	19800.
K	15320.	22440.	10400.	12990.
TI	3980.	4930.	4860.	4880.
MN	420.	430.	420.	430.
BA	1620.	780.	760.	720.
CD	26.	30.	26.	26.
CU	20.	37.	20.	45.
GA	21.	24.	22.	27.
LI	9.	12.	7.	10.
MO	1.	0.	1.	19.
PB	14.	7.	4.	12.
RB	50.	100.	45.	80.
S	70.	121.	88.	92.
SR	236.	196.	260.	224.
CO<H2O	26300.	57100.	35000.	50600.
ZN	48.	82.	64.	87.
ZR	51.	141.	150.	135.
V	80.	120.	100.	100.
NI	46.	64.	46.	52.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-277 1154.5-1156.5	ST-278 1156.5-1157.5	ST-279 1157.5-1160.0	ST-281 1165.0-1170.0
SI	294540.	289580.	263240.	311650.
AL	32920.	86610.	75620.	85310.
FE	47250.	46790.	106300.	20480.
MG	8040.	3990.	6680.	6780.
CA	7680.	38120.	12700.	12640.
NA	17900.	28090.	19700.	14300.
K	15270.	10660.	11490.	6660.
TI	4690.	4440.	4160.	3330.
MN	910.	650.	2230.	500.
BA	760.	940.	680.	1340.
CO	34.	24.	30.	32.
CU	38.	30.	45.	15.
GA	107.	73.	28.	21.
LI	12.	7.	12.	8.
MO	3.	0.	2.	0.
PB	9.	26.	8.	27.
RB	92.	32.	94.	15.
S	159.	104.	124.	61.
SR	196.	266.	171.	255.
CGH2O	63900.	31300.	129500.	40100.
ZN	79.	65.	70.	53.
ZR	144.	161.	137.	169.
V	120.	60.	140.	60.
NI	64.	68.	72.	46.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-282 1178.0-1178.5	ST-283 1175.5-1176.0	ST-284 1176.0-1179.0	ST-285 1179.0-1180.0
SI	291460.	281160.	293340.	288730.
AL	76690.	73290.	81980.	88940.
FE	41350.	24420.	24910.	26810.
MG	5840.	4300.	4540.	5540.
CA	13470.	76800.	13230.	7680.
NA	19000.	15800.	20100.	16400.
K	7320.	6820.	8490.	14510.
TI	2340.	3790.	2830.	4800.
MN	910.	1390.	660.	410.
BA	1400.	1000.	1180.	840.
CO	36.	32.	22.	44.
CU	18.	24.	13.	27.
GA	24.	23.	19.	15.
LI	8.	3.	8.	13.
MO	1.	0.	0.	0.
PB	23.	19.	10.	35.
RB	17.	24.	23.	93.
S	57.	71.	33.	119.
SR	269.	242.	253.	166.
CGH2O	47000.	52200.	26100.	37800.
ZN	43.	58.	47.	93.
ZR	125.	156.	140.	120.
V	60.	60.	40.	100.
NI	42.	42.	26.	50.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-286 1180.0-1180.5	ST-287 1180.5-1181.0	ST-288 1181.0-1182.0	ST-289 1182.0-1184.0
SI	273260.	277370.	297690.	287540.
AL	83980.	81440.	91010.	88100.
FE	25300.	27890.	30030.	30990.
MG	5540.	7360.	5260.	5940.
CA	8860.	7270.	7170.	7490.
NA	17900.	9300.	10700.	12300.
K	9310.	13020.	12960.	13390.
TI	4240.	5110.	5090.	4870.
MN	420.	410.	410.	420.
BA	940.	480.	860.	700.
CU	38.	64.	36.	46.
CO	27.	26.	31.	33.
GA	16.	14.	18.	20.
LI	10.	22.	14.	15.
MO	1.	2.	0.	1.
PB	13.	8.	8.	8.
RB	63.	92.	114.	111.
S	157.	397.	75.	143.
SR	214.	99.	153.	154.
CH2O	67500.	175800.	73100.	90500.
ZN	79.	37.	68.	77.
ZO	126.	107.	119.	126.
V	66.	160.	120.	120.
NI	42.	80.	46.	73.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-290 1179.0-1181.5	ST-294 1184.0-1188.0	ST-295 1188.0-1189.0	ST-296 1184.0-1189.5
SI	279240.	272630.	283310.	294010.
AL	80480.	85120.	86610.	87110.
FE	43500.	77400.	45710.	28810.
MG	11360.	20200.	6680.	13380.
CA	13760.	8130.	8330.	7330.
NA	13700.	12000.	17500.	14100.
K	5860.	10070.	11380.	9130.
TI	2170.	4640.	5000.	4840.
MN	850.	1420.	1140.	410.
BA	1260.	1660.	880.	1240.
CO	24.	62.	40.	52.
CU	20.	37.	38.	20.
GA	11.	32.	23.	22.
LI	9.	12.	10.	15.
MO	2.	1.	2.	1.
PB	11.	13.	8.	5.
RB	17.	140.	122.	105.
S	95.	117.	155.	97.
SR	252.	128.	179.	144.
CaH2O	49800.	68700.	61500.	71700.
ZN	77.	129.	122.	132.
ZR	123.	136.	152.	117.
V	40.	30.	60.	100.
NI	42.	102.	50.	46.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-297 1185.5-1189.0	ST-298 1189.0-1190.0	ST-299 1190.0-1192.0	ST-300 1192.0-1193.0
SI	299920.	277820.	274220.	279890.
AL	84650.	83060.	79820.	79150.
FE	32900.	55470.	42340.	51600.
MG	6140.	6980.	6420.	7920.
CA	7540.	8700.	11990.	9280.
NA	16500.	12400.	15600.	10700.
K	7370.	11475.	9200.	20840.
TI	4250.	4880.	3900.	5190.
MN	400.	1330.	1280.	1120.
BA	740.	300.	1000.	920.
CO	38.	54.	46.	63.
CU	10.	28.	29.	48.
GA	23.	29.	26.	27.
LI	11.	15.	10.	15.
MO	1.	1.	0.	0.
PB	9.	8.	16.	20.
BB	28.	127.	65.	107.
S	83.	115.	145.	328.
SR	169.	189.	239.	154.
CaH2O	57000.	89500.	83900.	119800.
ZN	61.	116.	68.	87.
ZP	136.	140.	145.	139.
V	60.	120.	60.	100.
NI	24.	52.	46.	76.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-301 1193.0-1198.0	ST-304 1200.5-1209.5	ST-306 1204.0-1207.5	ST-307 1207.5-1208.5
SI	298700.	276600.	305810.	278230.
AL	88860.	82620.	85730.	80780.
FE	28270.	46010.	16930.	25530.
MG	14940.	6840.	6340.	6600.
CA	7050.	13480.	9820.	8290.
NA	11700.	11000.	14100.	11500.
K	33860.	21200.	10650.	11790.
TI	5280.	5160.	4190.	4630.
MN	600.	900.	460.	590.
BA	920.	880.	920.	400.
CO	64.	50.	46.	64.
CU	46.	47.	21.	36.
GA	28.	24.	16.	18.
LI	17.	13.	9.	18.
MO	0.	0.	0.	1.
PB	9.	17.	22.	30.
RB	140.	116.	45.	53.
S	94.	151.	151.	310.
SR	132.	170.	185.	125.
CH ₂ O	54100.	82800.	59800.	151900.
ZN	78.	106.	54.	48.
ZR	116.	103.	110.	125.
V	120.	120.	40.	160.
NI	96.	70.	68.	88.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-308 1208.5-1211.0	ST-309 1211.0-1213.0	ST-310 1213.0-1214.0	ST-312 1217.0-1221.5
SI	273100.	296020.	259030.	270610.
AL	83590.	88410.	85730.	86840.
FE	49290.	34500.	52100.	34000.
MG	13480.	8640.	7600.	8360.
CA	19160.	8910.	8190.	6670.
NA	14100.	16900.	9700.	13500.
K	9850.	13770.	6770.	20630.
TI	3930.	4880.	4020.	5410.
MN	1280.	460.	500.	420.
BA	1020.	840.	640.	760.
CO	44.	43.	53.	38.
CU	28.	30.	20.	45.
GA	22.	17.	21.	21.
LI	8.	13.	18.	17.
MO	2.	1.	2.	0.
PB	19.	20.	83.	9.
RB	49.	73.	78.	62.
S	196.	226.	1697.	95.
SR	245.	189.	155.	132.
CaH2O	82400.	61700.	143400.	71700.
ZN	96.	86.	73.	72.
ZR	148.	127.	132.	123.
V	80.	100.	100.	160.
NI	78.	74.	100.	90.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-313 1221.5-1225.0	ST-314 1225.0-1226.0	ST-315 1226.0-1228.5	ST-317 1232.0-1234.5
SI	273880.	208350.	296090.	290320.
AL	82180.	94280.	88720.	81590.
FE	63150.	23210.	24100.	29450.
MG	11760.	16340.	7320.	6720.
CA	20810.	7480.	6650.	6700.
NA	13900.	16100.	12100.	11200.
K	15790.	22540.	31350.	10380.
TI	4480.	5000.	5620.	4800.
MN	1240.	480.	450.	460.
BA	820.	1260.	720.	640.
CO	38.	58.	58.	38.
CU	34.	30.	38.	31.
GA	22.	16.	23.	26.
LI	11.	12.	17.	15.
MO	2.	1.	2.	1.
PB	14.	12.	9.	5.
RB	74.	86.	124.	106.
S	100.	137.	126.	63.
SR	194.	159.	128.	138.
C&H2O	69100.	54000.	68800.	65400.
ZN	74.	96.	122.	80.
ZR	168.	127.	125.	111.
V	100.	100.	140.	120.
NI	78.	106.	108.	62.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-318 1234.5-1235.5	ST-319 1235.5-1238.0	ST-320 1238.0-1242.5	ST-321 1242.5-1242.8
SI	302430.	300280.	303430.	260710.
AL	82260.	78640.	76430.	94150.
FE	24970.	26470.	22350.	33910.
MG	9460.	9300.	15040.	15220.
CA	7340.	7550.	7340.	8720.
NA	14300.	14900.	13700.	18700.
K	5130.	4240.	5360.	3370.
TI	2690.	2110.	2400.	970.
MN	420.	410.	430.	420.
BA	660.	560.	780.	500.
CO	46.	34.	40.	42.
CU	11.	7.	10.	5.
GA	21.	19.	19.	31.
LI	11.	10.	12.	5.
MO	2.	1.	1.	1.
PB	13.	13.	10.	13.
RB	36.	21.	34.	0.
S	94.	55.	57.	33.
SR	132.	148.	127.	173.
CaH2O	89000.	66200.	70500.	106700.
ZN	90.	63.	58.	131.
ZR	124.	133.	114.	151.
V	48.	40.	60.	200.
NI	82.	70.	80.	93.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-322 1242.8-1244.5	ST-323 1244.5-1245.5	ST-324 1245.5-1247.5	ST-325 1247.5-1249.5
SI	303250.	293500.	286300.	289140.
AL	80230.	87380.	87060.	90250.
FE	28810.	32910.	29180.	35160.
MG	12780.	26440.	29420.	14220.
CA	7000.	7110.	7200.	7080.
NA	11500.	17100.	14400.	13200.
K	9570.	13740.	15480.	17630.
TI	5190.	5170.	5330.	5420.
MN	410.	410.	430.	500.
BA	1060.	1440.	1380.	1000.
CO	48.	58.	52.	40.
CU	32.	28.	34.	35.
GA	21.	23.	22.	22.
LI	16.	13.	16.	15.
MO	1.	1.	0.	1.
PB	2.	18.	8.	13.
RB	112.	121.	111.	145.
S	110.	92.	105.	63.
SR	138.	180.	173.	173.
COH2O	150000.	50300.	62900.	61200.
ZN	57.	47.	85.	85.
ZR	134.	133.	144.	147.
V	160.	180.	160.	180.
NI	66.	106.	120.	118.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-326 1249.5-1250.5	ST-327 1250.5-1257.0	ST-329 1257.5-1258.0	ST-331 1258.5-1261.0
SI	282990.	287530.	297110.	283720.
AL	89730.	86420.	84460.	84790.
FE	26510.	32860.	22190.	26660.
MG	9000.	10480.	11936.	6040.
CA	7340.	39380.	7050.	7010.
NA	13580.	11800.	15700.	13800.
K	18070.	32510.	12800.	12480.
TI	5520.	4100.	4810.	5230.
MN	510.	670.	410.	410.
BA	720.	1480.	1100.	720.
CO	52.	80.	34.	36.
CU	34.	15.	25.	29.
GA	25.	17.	18.	21.
LI	19.	24.	14.	15.
MO	1.	1.	1.	1.
PB	9.	29.	7.	8.
RB	116.	83.	65.	65.
S	144.	71.	105.	191.
SR	140.	164.	142.	132.
CSH2O	82000.	25300.	99400.	121000.
ZN	78.	63.	72.	46.
ZR	146.	130.	148.	135.
V	180.	120.	100.	140.
NI	125.	96.	88.	88.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-132 1261.0-1264.5	ST-353 1264.5-1265.5	ST-325 1266.5-1271.0	ST-336 1271.5-1276.5
SI	295810.	290500.	285870.	297060.
AL	85960.	85120.	87560.	88770.
FE	32680.	68450.	33060.	30550.
MG	3280.	10540.	5820.	8860.
CA	6710.	8060.	6780.	7610.
NA	13700.	9300.	18160.	15900.
K	21040.	36260.	24740.	20100.
TI	5360.	5410.	5420.	5360.
MN	420.	1290.	490.	440.
BA	740.	780.	680.	860.
CO	112.	46.	40.	38.
CU	35.	52.	37.	35.
GA	28.	30.	32.	25.
LI	17.	19.	15.	14.
MO	1.	1.	1.	0.
PB	26.	6.	15.	13.
KB	122.	151.	133.	117.
S	314.	282.	306.	75.
SR	159.	120.	156.	182.
CaH2O	69800.	120400.	62500.	53300.
ZN	151.	113.	72.	73.
ZK	135.	117.	136.	147.
V	140.	160.	140.	120.
NI	348.	198.	166.	110.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-327 1276.5-1281.0	ST-338 1281.0-1285.5	ST-340 1286.0-1286.5	ST-342 1286.7-1288.5
SI	285760.	277170.	276660.	286860.
AL	92910.	89340.	85730.	89250.
FE	31990.	24490.	34980.	26460.
MG	9280.	12700.	9580.	21040.
CA	10030.	16480.	6800.	7720.
NA	15700.	14100.	11800.	14800.
K	20840.	37110.	15260.	14590.
TI	5010.	4900.	5100.	5270.
MN	660.	640.	420.	430.
BA	780.	1240.	760.	1220.
CO	32.	26.	66.	64.
CU	23.	15.	32.	33.
GA	21.	20.	24.	20.
LI	9.	8.	17.	16.
MO	0.	0.	0.	1.
PB	17.	27.	11.	19.
RB	70.	82.	122.	69.
S	105.	52.	137.	158.
SR	186.	164.	133.	153.
CGH2O	50800.	35400.	109600.	97200.
ZN	73.	49.	59.	80.
ZP	154.	133.	98.	122.
V	80.	80.	160.	140.
NI	92.	86.	118.	148.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-343 1288.5-1294.0	ST-344 1288.5-1294.0	ST-345 1294.0-1296.0	ST-347 1298.0-1301.5
ST	290440.	282100.	279980.	270870.
AL	89340.	95960.	85170.	80890.
FE	38220.	33180.	36190.	70010.
MG	12540.	12000.	8800.	11380.
CA	7750.	7700.	7740.	9230.
NA	15500.	16300.	13900.	12200.
K	16560.	14370.	13000.	13260.
TI	5210.	5400.	4900.	5130.
MN	510.	460.	430.	1080.
BA	940.	880.	780.	740.
Cl	46.	50.	38.	42.
CU	23.	27.	26.	51.
GA	25.	24.	23.	31.
LI	16.	16.	13.	21.
MO	0.	1.	1.	2.
PB	11.	13.	12.	8.
RB	110.	110.	115.	112.
S	38.	121.	73.	149.
SR	176.	174.	184.	169.
COH ₂ O	55100.	69500.	62300.	120400.
ZN	91.	82.	68.	121.
ZR	124.	133.	139.	141.
V	140.	140.	140.	160.
NI	123.	94.	104.	112.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-348 1301.5-1305.0	ST-350 1305.5-1305.7	ST-351 1305.7-1306.5	ST-352 1306.5-1306.7
SI	271730.	282080.	267990.	251940.
AL	79800.	80180.	76960.	89770.
FE	30490.	33260.	32670.	33790.
MG	20200.	9840.	11520.	14580.
CA	7950.	7290.	7350.	9490.
NA	12000.	12500.	14400.	19500.
K	11580.	7290.	6710.	3540.
TI	5250.	3780.	3340.	1690.
MN	430.	410.	470.	400.
BA	1220.	720.	820.	620.
CO	60.	36.	38.	46.
CU	28.	17.	19.	10.
GA	75.	27.	20.	23.
LI	22.	13.	14.	9.
MO	1.	0.	0.	0.
PB	10.	9.	12.	24.
RB	63.	85.	77.	0.
S	278.	56.	61.	95.
SR	120.	140.	153.	174.
CH2O	102400.	104700.	106100.	124600.
ZN	55.	38.	46.	83.
ZR	105.	90.	104.	139.
V	140.	100.	100.	200.
NI	152.	76.	76.	86.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-353 1306.7-1307.2	ST-356 1310.5-1313.0	ST-357 1313.0-1314.0	ST-363 1320.0-1322.5
SI	284300.	272200.	269540.	275930.
AL	79150.	86330.	79770.	93830.
FE	35980.	39550.	45660.	27610.
MG	24760.	6100.	8100.	9860.
CA	6740.	7220.	9080.	7520.
NA	10300.	16900.	11800.	15800.
K	11390.	15260.	14100.	7380.
TI	4390.	4970.	5610.	4220.
MN	410.	550.	880.	420.
BA	1240.	880.	740.	660.
CO	60.	60.	54.	34.
CU	32.	39.	47.	23.
GA	15.	22.	17.	19.
LI	15.	19.	20.	11.
MO	1.	0.	1.	1.
PB	3.	21.	11.	14.
RR	141.	184.	88.	39.
S	222.	156.	265.	69.
SR	136.	175.	137.	181.
CaH2O	141800.	87200.	138300.	73500.
Zn	81.	120.	94.	76.
Zr	10.	15.	110.	160.
V	100.	160.	140.	60.
NI	110.	155.	132.	68.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-361 1322.5-1324.0	ST-362 1324.0-1326.0	ST-363 1326.0-1330.0	ST-364 1330.0-1337.5
SI	283120.	292300.	287250.	287190.
AL	89730.	91140.	87790.	85640.
FE	30120.	18100.	27150.	22150.
MG	6640.	7260.	11020.	11340.
CA	6730.	8440.	7030.	8570.
NA	11200.	18200.	10900.	18900.
K	15460.	15430.	21510.	12870.
TI	5110.	5100.	5650.	4670.
MN	430.	430.	460.	540.
BA	620.	900.	1000.	800.
CO	44.	42.	44.	38.
CU	36.	26.	30.	30.
GA	27.	19.	25.	23.
LI	17.	12.	18.	10.
MO	0.	1.	1.	0.
PR	11.	10.	14.	15.
PB	114.	61.	111.	64.
S	71.	76.	110.	93.
SR	155.	121.	160.	220.
CGH2O	70300.	54000.	72000.	62800.
ZN	134.	95.	105.	64.
ZR	133.	120.	136.	139.
V	223.	180.	280.	220.
NI	96.	107.	130.	132.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-365 1337.5-1337.7	ST-366 1337.7-1340.0	ST-367 1340.0-1341.5	ST-368 1341.5-1345.0
SI	238450.	286590.	269770.	271820.
AL	87740.	90200.	79050.	88280.
FE	26520.	17350.	99040.	23130.
MG	8700.	12460.	9320.	8260.
CA	7940.	11890.	11200.	24680.
NA	12400.	21300.	14200.	20100.
K	15380.	12380.	10060.	12210.
TI	5100.	4530.	4320.	4350.
MN	430.	510.	1700.	590.
BA	900.	960.	800.	960.
CO	40.	38.	36.	38.
CU	30.	15.	34.	20.
GA	20.	21.	27.	25.
LI	15.	8.	8.	6.
MO	1.	2.	3.	2.
PB	16.	18.	21.	16.
RB	84.	45.	67.	41.
S	157.	64.	289.	54.
SR	216.	256.	215.	193.
COH2O	67100.	68100.	117400.	43900.
ZN	77.	52.	59.	39.
ZR	146.	128.	147.	116.
V	200.	126.	180.	140.
NI	114.	84.	228.	46.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-369 1345.0-1346.0	ST-370 1346.0-1348.0	ST-371 1348.0-1348.5	ST-374 1351.0-1352.5
SI	289118.	291360.	168650.	282440.
AL	93590.	90250.	27730.	83550.
FE	25990.	28330.	15990.	27580.
MG	7260.	7580.	14460.	9160.
CA	8820.	9860.	57950.	7660.
NA	16400.	14000.	2220.	14600.
K	13590.	12260.	3470.	13810.
TI	5410.	5190.	1360.	5400.
MN	520.	730.	272550.	490.
BA	700.	660.	440.	560.
CO	68.	52.	22.	30.
CU	53.	39.	19.	30.
GA	27.	26.	5.	17.
LI	12.	10.	10.	14.
MO	2.	2.	0.	1.
PB	06.	15.	51.	5.
RB	83.	74.	2.	97.
S	210.	111.	423.	159.
SR	213.	226.	50.	165.
CaH2O	71000.	97400.	233200.	110700.
ZN	79.	86.	7.	66.
ZR	146.	135.	38.	136.
V	260.	200.	140.	300.
NI	108.	98.	296.	90.

HORSESHOE CANYON FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-375 1352.5-1355.0	ST-376 1355.0-1360.0	ST-378 1360.2-1364.0
SI	278930.	285000.	255910.
AL	38940.	93790.	78000.
FE	25760.	33600.	29550.
MG	10220.	8860.	7520.
CA	6980.	11710.	7700.
NA	14400.	19300.	12900.
K	19980.	13610.	10680.
TI	5550.	4850.	5400.
MN	450.	790.	420.
BA	640.	600.	560.
CO	28.	24.	30.
CU	40.	33.	20.
GA	19.	18.	10.
LI	71.	9.	16.
MO	2.	2.	9.
PB	15.	13.	13.
RB	110.	285.	61.
S	143.	107.	331.
SR	145.	219.	100.
C&H2O	58300.	69000.	245100.
ZN	92.	69.	56.
ZR	131.	141.	81.
V	300.	260.	300.
NI	92.	96.	120.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-379 1364.0-1368.0	ST-361 1370.0-1371.7	ST-382 1371.7-1372.7	ST-383 1372.7-1376.0
SI	279580.	270610.	265350.	286200.
AL	83790.	84550.	78480.	81140.
FE	47060.	33290.	66220.	33430.
MG	8800.	8700.	9360.	5920.
CA	9940.	8720.	9640.	19100.
NA	15400.	13900.	10700.	18400.
K	14800.	7590.	8430.	7740.
TI	5150.	4290.	4200.	3600.
MN	760.	510.	990.	680.
BA	560.	560.	520.	580.
CO	24.	29.	22.	18.
CU	49.	17.	29.	16.
GA	21.	18.	26.	19.
LI	15.	12.	12.	7.
MO	3.	2.	3.	2.
PB	10.	11.	10.	23.
RB	101.	60.	81.	23.
S	162.	156.	154.	117.
SR	195.	138.	195.	253.
COH2O	93800.	123900.	102900.	59200.
ZN	122.	76.	79.	58.
ZR	131.	125.	147.	115.
V	200.	220.	280.	160.
NI	108.	84.	86.	50.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-387 1386.0-1386.5	ST-388 1386.5-1392.5	ST-389 1392.5-1393.5	ST-390 1393.5-1398.5
SI	277840.	269090.	271840.	266950.
AL	87380.	73600.	92630.	77960.
FE	36470.	21000.	25300.	23990.
MG	9080.	4800.	15740.	8000.
CA	9290.	41610.	11090.	35400.
NA	16700.	12800.	20100.	18900.
K	12920.	10890.	5690.	7450.
TI	5980.	4530.	3140.	3680.
MN	590.	660.	520.	610.
BA	560.	700.	960.	680.
CO	38.	26.	30.	28.
CU	25.	11.	7.	17.
GA	19.	19.	25.	20.
LI	11.	7.	8.	7.
MO	3.	1.	1.	1.
PB	10.	10.	9.	10.
RB	72.	34.	34.	33.
S	131.	81.	51.	87.
SR	222.	234.	273.	271.
CaH2O	82300.	35300.	61300.	45500.
ZN	65.	41.	51.	49.
ZR	166.	172.	157.	143.
V	440.	160.	120.	140.
NI	92.	66.	38.	62.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-391 1398.5-1402.0	ST-393 1410.0-1412.0	ST-394 1412.0-1418.0	ST-395 1418.0-1425.0
SI	271210.	202080.	252470.	196280.
AL	82980.	77700.	73100.	54520.
FE	29330.	69050.	33600.	32100.
MG	7140.	10940.	9080.	7930.
CA	13650.	13020.	49810.	70420.
NA	17500.	15400.	17500.	6100.
K	30860.	11800.	7240.	5630.
TI	3920.	4600.	5660.	2680.
MN	600.	920.	730.	690.
BA	760.	580.	740.	520.
CO	20.	28.	26.	18.
CU	17.	24.	22.	22.
GA	20.	24.	19.	15.
LI	7.	10.	6.	4.
MO	2.	1.	3.	0.
PB	6.	21.	9.	7.
RB	48.	79.	22.	0.
S	66.	350.	77.	130.
SR	262.	298.	279.	293.
CGH2O	47800.	78200.	49000.	36200.
ZN	61.	75.	65.	50.
ZR	133.	161.	223.	130.
V	120.	220.	140.	140.
NI	50.	108.	72.	56.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-396 1425.0-1430.5	ST-397 1430.5-1437.0	ST-398 1437.0-1441.5	ST-399 1441.5-1442.0
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SI	267540.	274670.	269620.	256630.
AL	83500.	84690.	78840.	79510.
FE	42280.	46190.	46640.	61190.
MG	10680.	12740.	10640.	11240.
CA	13920.	13210.	13240.	29310.
NA	14700.	14500.	23000.	14500.
K	15190.	16760.	15840.	10860.
TI	5430.	5360.	5060.	3900.
MN	880.	870.	870.	950.
BA	560.	660.	700.	640.
CO	36.	40.	36.	30.
CU	50.	46.	47.	40.
GA	21.	43.	29.	23.
LI	13.	13.	13.	9.
NI	2.	0.	1.	1.
PB	20.	18.	9.	24.
RB	94.	94.	104.	67.
S	183.	220.	155.	290.
SR	271.	217.	225.	261.
CGH2O	74600.	79700.	77000.	62800.
ZN	95.	104.	109.	86.
ZR	154.	147.	141.	129.
V	222.	220.	200.	120.
NI	116.	130.	122.	120.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-400 1442.0-1450.0	ST-401 1450.0-1456.5	ST-402 1456.5-1461.5	ST-403 1461.5-1466.5
SI	261900.	267690.	270900.	277710.
AL	78740.	77800.	83840.	81190.
FE	59450.	55730.	53110.	49660.
MG	12000.	12300.	10660.	10720.
CA	15110.	14260.	11350.	9030.
NA	11700.	16100.	12900.	10700.
K	16540.	16240.	19720.	25760.
TI	5450.	5270.	5770.	5370.
MN	930.	840.	670.	590.
BA	680.	680.	560.	640.
CO	32.	30.	30.	30.
CU	42.	43.	42.	38.
GA	20.	23.	27.	23.
LI	13.	14.	16.	23.
MO	1.	0.	0.	0.
PB	14.	19.	20.	30.
RB	108.	97.	120.	156.
S	214.	340.	468.	948.
SR	225.	225.	194.	166.
CGH2O	73900.	69300.	68700.	64800.
ZN	104.	101.	105.	123.
ZR	142.	152.	144.	152.
V	200.	200.	220.	260.
NI	126.	110.	114.	90.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-404 1466.5-1471.5	ST-405 1471.5-1477.5	ST-406 1477.5-1483.0	ST-407 1483.0-1483.5
SI	274860.	273290.	288220.	177660.
AL	80480.	82960.	80940.	42470.
FE	51380.	55350.	21880.	51550.
MG	11150.	11300.	21120.	12440.
CA	8970.	8820.	58510.	72530.
NA	10400.	13900.	17500.	6300.
K	27420.	26690.	22980.	7250.
TI	5440.	5610.	4520.	6750.
MN	900.	990.	610.	960.
BA	640.	620.	1060.	580.
CO	37.	46.	40.	30.
CU	40.	46.	23.	25.
GA	30.	26.	18.	12.
LI	24.	20.	8.	11.
MO	0.	3.	1.	1.
PB	28.	25.	13.	32.
RB	177.	131.	58.	9.
S	384.	660.	90.	285.
SR	176.	190.	224.	301.
COH2O	62200.	68900.	28200.	42800.
ZN	110.	115.	71.	159.
ZR	145.	149.	151.	161.
V	248.	180.	100.	140.
NI	117.	146.	66.	132.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-406 1483.5-1489.0	ST-409 1489.0-1491.5	ST-410 1491.5-1492.0	ST-411 1492.0-1496.5
SI	290250.	302800.	242030.	266220.
AL	83740.	89590.	69920.	79720.
FE	28740.	26440.	92330.	42970.
MG	16240.	8460.	21120.	10400.
CA	29950.	11665.	31590.	32200.
NA	16400.	13450.	15600.	19100.
K	33560.	22650.	11300.	14520.
TI	4310.	4690.	4660.	4570.
MN	700.	550.	1350.	710.
PA	1100.	890.	780.	900.
CO	36.	34.	38.	34.
CU	32.	25.	45.	32.
GA	22.	20.	26.	23.
LI	9.	7.	8.	7.
MO	2.	0.	1.	1.
PB	12.	17.	1.	2.
BB	79.	62.	50.	59.
S	77.	182.	74.	29.
SR	229.	217.	277.	264.
CaH2O	50300.	54000.	80200.	45100.
ZN	70.	66.	190.	71.
ZR	119.	141.	156.	151.
V	100.	109.	160.	140.
NI	86.	76.	178.	88.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-412 1498.5-1499.0	ST-413 1499.0-1505.5	ST-414 1505.5-1506.0	ST-415 1506.0-1511.0
SI	281130.	273300.	224380.	266810.
AL	91290.	93160.	65540.	84310.
FE	38310.	51740.	72610.	48540.
MG	16940.	14340.	10780.	9200.
CA	13570.	11850.	73740.	9670.
NA	17300.	14900.	14900.	13200.
K	16730.	23740.	10550.	29320.
TI	5230.	5400.	3410.	5900.
MN	650.	870.	1030.	870.
BA	1200.	1320.	740.	640.
CO	33.	46.	24.	44.
CU	26.	39.	27.	49.
GA	19.	23.	21.	30.
LI	8.	13.	7.	17.
MO	2.	1.	9.	0.
PB	6.	5.	11.	6.
KB	71.	111.	38.	130.
S	65.	131.	205.	205.
SR	227.	190.	240.	180.
COH ₂ O	54700.	60800.	46500.	73400.
ZN	68.	89.	64.	100.
ZR	157.	147.	115.	157.
V	160.	180.	100.	200.
NI	96.	138.	134.	136.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-415 1511.0-1514.0	ST-417 1514.0-1515.0	ST-418 1515.0-1519.0	ST-420 1520.0-1529.0
SI	26435.	30260.	29522.	29307.
AL	8379.	7867.	8729.	9040.
FE	8444.	3111.	4338.	4102.
MG	960.	1118.	940.	816.
CA	961.	704.	1327.	735.
NA	1050.	910.	1030.	990.
K	3017.	3192.	3673.	3664.
TI	534.	438.	522.	566.
MN	103.	45.	69.	98.
BA	40.	112.	94.	78.
CO	10.	3.	6.	3.
CU	8.	1.	1.	3.
GA	1.	1.	1.	3.
LI	1.	1.	1.	2.
MO	1.	1.	1.	1.
PB	15.	39.	15.	30.
RB	146.	161.	133.	161.
S	414.	3104.	821.	554.
SR	173.	168.	152.	149.
CO&H2O	81800.	59300.	63300.	65200.
ZN	109.	77.	98.	113.
ZR	155.	194.	166.	152.
V	220.	160.	200.	240.
NI	140.	88.	128.	120.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-421 1529.0-1536.0	ST-422 1536.0-1537.5	ST-423 1537.5-1539.5	ST-424 1539.5-1540.0
SI	297140.	271750.	266440.	297510.
AL	93460.	66920.	86920.	82380.
FE	40910.	98680.	53920.	29920.
MG	22720.	29280.	8980.	2800.
CA	7770.	23450.	7760.	7260.
NA	8700.	5100.	8100.	10600.
K	37490.	17550.	30460.	35320.
TI	5720.	3020.	5180.	5100.
MN	1020.	1120.	770.	440.
BA	1400.	2000.	720.	680.
CO	54.	34.	38.	28.
CU	42.	38.	42.	29.
GA	26.	15.	20.	15.
LT	22.	14.	20.	14.
MO	1.	1.	1.	1.
PB	25.	25.	26.	35.
RB	176.	101.	170.	140.
S	326.	461.	717.	1518.
SR	151.	125.	137.	126.
CGH20	59400.	50300.	65400.	54700.
ZN	136.	70.	105.	93.
ZR	167.	116.	143.	163.
V	240.	160.	220.	200.
NI	144.	142.	114.	70.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-425 1540.0-1545.0	ST-426 1545.5-1551.0	ST-427 1551.0-1553.0	ST-428 1553.0-1555.0
SI	266090.	276750.	297090.	280270.
AL	88230.	89840.	64450.	88150.
FE	42060.	47160.	82480.	44130.
MG	6800.	6900.	9220.	9260.
CA	6750.	7280.	13020.	6800.
NA	7000.	9750.	8200.	5600.
K	28400.	25090.	7170.	17360.
TI	5510.	3420.	6770.	4950.
MN	730.	910.	1610.	480.
BA	560.	540.	540.	640.
CO	52.	42.	22.	42.
CU	42.	55.	24.	31.
GA	22.	29.	12.	22.
LI	21.	16.	10.	15.
MO	1.	1.	0.	1.
PB	27.	129.	7.	30.
PP	178.	161.	59.	164.
S	1250.	1117.	371.	2221.
SR	128.	150.	140.	158.
CE&H2O	90400.	75900.	75600.	117200.
ZN	127.	131.	55.	102.
ZR	137.	141.	88.	141.
V	260.	200.	100.	220.
NI	104.	116.	112.	128.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-429 1555.0-1560.0	ST-430 1560.0-1562.5	ST-431 1562.5-1563.0	ST-433 1564.0-1566.0
SI	313260.	295840.	276560.	294260.
AL	75290.	93790.	85730.	92380.
FE	29150.	45160.	57820.	29490.
MG	5160.	8660.	11380.	7660.
CA	31920.	7040.	7450.	5700.
NA	11000.	9700.	9800.	16900.
K	9540.	21030.	16610.	14360.
TI	2480.	5210.	4870.	5230.
MN	610.	520.	550.	590.
RA	700.	660.	820.	660.
CO	22.	46.	52.	46.
CU	15.	38.	32.	42.
GA	14.	27.	23.	24.
LI	8.	16.	17.	11.
MO	2.	1.	2.	2.
PB	10.	35.	49.	9.
RB	63.	176.	154.	86.
S	523.	1648.	3363.	221.
SR	159.	163.	197.	244.
COH ₂ O	45500.	90800.	148400.	68500.
ZN	50.	121.	121.	97.
ZR	118.	135.	128.	135.
V	120.	240.	200.	140.
NI	56.	136.	162.	122.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-434 1566.0-1569.0	ST-435 1569.0-1570.5	ST-436 1570.5-1571.0	ST-437 1571.0-1572.5
SI	281970.	280770.	286630.	270280.
AL	87520.	78530.	88370.	81040.
FE	58670.	35020.	21960.	56210.
MG	14800.	6480.	7480.	15080.
CA	16560.	21000.	9340.	15630.
NA	15500.	18700.	19200.	15800.
K	12240.	9150.	12990.	9680.
TI	4980.	4080.	5460.	4530.
MN	1090.	750.	550.	1050.
BA	880.	780.	620.	680.
CO	44.	36.	42.	36.
CU	45.	25.	33.	25.
GA	27.	21.	23.	21.
LI	11.	7.	9.	7.
MO	4.	1.	3.	0.
PB	2.	11.	11.	7.
RB	72.	39.	67.	52.
S	275.	136.	182.	105.
SR	266.	302.	223.	287.
CGH20	73500.	46300.	56700.	47900.
ZN	100.	76.	81.	63.
ZF	176.	124.	151.	153.
V	140.	100.	140.	126.
NT	124.	94.	94.	110.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-439 1976.5-1977.5	ST-440 1977.5-1982.0	ST-441 1982.0-1985.5	ST-442 1985.5-1990.5
SI	239390.	289080.	291760.	300830.
AL	82260.	53790.	88230.	85910.
FE	63250.	49380.	42920.	29170.
MG	7740.	8680.	80620.	9360.
CA	19120.	8410.	7450.	8270.
NA	15860.	12300.	10100.	10600.
K	9790.	19780.	22030.	17020.
TI	4620.	5540.	5560.	4630.
MN	1150.	810.	630.	570.
BA	760.	680.	1140.	560.
CO	28.	44.	50.	26.
CU	23.	41.	36.	19.
GA	23.	21.	23.	18.
LI	7.	17.	20.	11.
MO	0.	0.	1.	1.
PB	15.	35.	32.	18.
PB	0.	139.	150.	94.
S	162.	962.	1073.	444.
SR	280.	190.	158.	151.
CH20	50400.	61200.	76700.	52000.
ZN	90.	115.	107.	74.
ZR	169.	148.	145.	153.
V	140.	200.	220.	140.
NI	166.	132.	92.	74.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-443 1590.5-1595.0	ST-444 1595.0-1597.5	ST-445 1597.5-1600.5	ST-447 1601.0-1601.2
SI	286290.	246490.	279320.	236130.
AL	95076.	89900.	88190.	65480.
FE	43900.	59030.	47160.	69370.
MG	12220.	9000.	22400.	31940.
CA	8900.	7200.	7320.	6790.
NA	11500.	10700.	74700.	7800.
K	15520.	18030.	14780.	10870.
TI	4710.	5400.	5320.	4440.
MN	760.	760.	560.	1860.
BA	840.	580.	1020.	1180.
CO	32.	56.	56.	70.
CU	24.	35.	45.	35.
GA	19.	23.	16.	16.
IT	15.	17.	18.	15.
MO	0.	0.	1.	1.
PR	25.	32.	25.	187.
RB	105.	181.	115.	144.
S	399.	1547.	1474.	12169.
SR	178.	172.	147.	134.
CH20	57500.	84900.	160610.	184500.
ZN	88.	108.	91.	86.
ZR	169.	129.	123.	142.
V	143.	229.	200.	260.
NI	44.	156.	148.	276.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

	ST-448 1501.2-1605.0	ST-449 1605.0-1608.5	ST-451 1611.5-1613.0	ST-452 1613.0-1614.0
SI	284410.	282610.	307030.	300530.
AL	73790.	81880.	78690.	83010.
FE	41520.	48640.	29550.	35480.
MG	9260.	25080.	17340.	29520.
CA	7610.	9470.	17970.	33280.
NA	13800.	12200.	8800.	8700.
K	13430.	9480.	12570.	15620.
TI	4210.	3370.	3240.	4150.
MN	950.	850.	460.	570.
BA	600.	1120.	960.	1340.
CO	36.	36.	32.	42.
CU	36.	28.	29.	36.
GA	13.	12.	9.	16.
LI	15.	10.	12.	17.
MO	0.	0.	0.	0.
PB	18.	11.	19.	26.
PP	116.	73.	83.	138.
S	773.	439.	777.	1766.
SR	168.	189.	134.	183.
CO&H2O	69700.	61900.	46900.	67000.
ZN	89.	73.	70.	111.
ZR	144.	162.	108.	126.
V	240.	200.	200.	260.
NI	98.	82.	90.	120.

"TRANSITION ZONE"

ALL VALUES IN PARTS PER MILLION

ST-454
1614.2-1614.5

SI	264280.
AL	102650.
FE	26840.
MG	26080.
CA	9380.
NA	19100.
K	3200.
TI	2500.
MN	430.
BA	1000.
CO	42.
CU	3.
GA	22.
LT	9.
MO	0.
PB	10.
RB	0.
S	253.
SR	318.
CGH20	114700.
ZN	02.
ZR	137.
V	80.
NI	58.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-456 1617.5-1617.6	ST-458 1622.5-1623.0	ST-459 1623.0-1624.0	ST-462 1625.7-1626.0
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SI	253000.	294460.	289310.	277510.
AL	101910.	28860.	85910.	80580.
FE	22680.	47610.	34270.	21450.
MG	18940.	17500.	23920.	17760.
CA	9970.	7880.	9500.	8830.
NA	20110.	12600.	16700.	14900.
K	2410.	15420.	8530.	2410.
TI	5450.	5010.	3850.	1560.
MN	430.	630.	530.	430.
BA	640.	960.	1160.	600.
CO	40.	44.	40.	20.
CU	2.	59.	17.	4.
GA	26.	31.	24.	14.
LI	5.	17.	11.	11.
MO	0.	0.	0.	8.
PR	8.	59.	86.	11.
RB	0.	112.	46.	0.
S	25.	1584.	1781.	302.
SR	186.	168.	205.	124.
CH2O	127380.	86700.	92500.	168000.
ZN	39.	104.	65.	25.
ZR	72.	139.	154.	85.
V	40.	960.	140.	40.
NI	40.	102.	82.	50.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-464 1631.0-1632.5	ST-465 1633.5-1638.5	ST-466 1638.5-1640.0	ST-468 1641.0-1647.0
SI	273260.	294040.	257160.	267410.
AL	84460.	77540.	85250.	83300.
FE	37050.	43610.	34980.	58390.
MG	22540.	14280.	11000.	12460.
CA	3640.	9570.	9310.	7810.
NA	14000.	35500.	13000.	9200.
K	5630.	9020.	6150.	20350.
TI	3940.	6710.	4710.	5410.
MN	450.	920.	450.	1550.
BA	960.	860.	280.	840.
CO	40.	42.	48.	44.
CU	22.	37.	36.	37.
GA	21.	30.	35.	19.
LI	12.	11.	22.	17.
MO	0.	0.	1.	1.
PB	7.	17.	27.	31.
RB	21.	50.	37.	162.
S	372.	174.	1699.	289.
SR	148.	215.	261.	143.
CGH2O	188600.	82600.	229200.	64200.
ZN	61.	76.	107.	112.
ZR	117.	140.	218.	142.
V	160.	160.	80.	220.
NI	96.	100.	52.	114.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-469 1642.0-1652.0	ST-470 1652.0-1657.0	ST-471 1657.0-1662.0	ST-472 1662.0-1666.0
SI	297610.	293100.	287190.	286160.
AL	92140.	99600.	84550.	87560.
FE	44550.	40120.	49410.	42230.
MG	18960.	21440.	7260.	14800.
CA	7220.	6900.	6690.	6910.
NA	8300.	8700.	7100.	10900.
K	24500.	26320.	24840.	22850.
TI	5840.	5720.	5510.	5530.
MN	1090.	820.	520.	530.
BA	1120.	1180.	560.	920.
CO	56.	52.	68.	52.
CU	35.	29.	30.	33.
GA	21.	24.	22.	23.
LI	19.	15.	10.	18.
MO	1.	2.	2.	1.
PB	20.	31.	13.	24.
RB	157.	172.	147.	163.
S	225.	580.	645.	1202.
SR	132.	135.	128.	153.
CaH20	56900.	54600.	51800.	55400.
ZN	118.	130.	119.	151.
ZP	147.	144.	133.	148.
V	220.	220.	220.	220.
NI	116.	98.	90.	108.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-472 1660.0-1668.0	ST-474 1668.0-1672.0	ST-475 1672.0-1677.0	ST-476 1677.0-1683.0
SI	96.	276070.	267840.	286830.
AL	147.	86247.	80330.	94740.
FE	160.	36720.	46080.	48230.
MG	90.	5860.	7280.	14820.
CA	0.	13960.	7640.	7560.
NA	0.	14900.	9300.	8200.
K	0.	16770.	25560.	31270.
TI	0.	4460.	5600.	5780.
MN	0.	500.	1420.	1720.
DA	0.	700.	600.	960.
CO	235580.	46.	50.	50.
CU	36880.	34.	37.	37.
GA	39340.	21.	22.	26.
LI	10220.	19.	21.	23.
NO	8050.	2.	0.	0.
PB	8800.	26.	22.	17.
RB	21610.	148.	190.	204.
S	5340.	936.	289.	421.
SR	900.	144.	133.	144.
CaH2O	740.	56000.	57300.	58000.
ZN	40.	127.	115.	130.
ZR	21.	146.	132.	143.
V	21.	200.	240.	240.
NI	12.	112.	120.	140.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-477 1683.0-1684.0	ST-478 1684.0-1688.0	ST-479 1688.0-1689.0	ST-480 1689.0-1693.0
SI	174370.	270830.	190410.	295720.
AL	42320.	94150.	55390.	94270.
FE	188770.	42500.	187960.	39970.
MG	26120.	6840.	22780.	7240.
CA	54850.	7070.	31830.	6630.
NA	3200.	6490.	3100.	6800.
K	6770.	32940.	10410.	34860.
TI	2770.	5840.	3500.	5870.
MN	2950.	790.	1620.	500.
BA	440.	540.	540.	560.
CO	36.	72.	52.	76.
CU	42.	34.	32.	25.
GA	10.	27.	14.	30.
LI	11.	23.	15.	23.
MO	0.	0.	0.	0.
PB	77.	24.	12.	23.
RB	51.	210.	66.	214.
S	667.	959.	1053.	609.
SR	149.	136.	63.	131.
GH20	120600.	52460.	126200.	49200.
ZN	51.	146.	65.	0.
ZR	92.	142.	73.	139.
V	120.	240.	140.	260.
NI	558.	128.	218.	110.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-481 1693.0-1694.0	ST-482 1694.0-1697.0	ST-483 1697.0-1698.0	ST-484 1698.0-1702.0
SI	197340.	290880.	206870.	305840.
AL	59120.	91220.	69750.	91220.
FE	184690.	45430.	183960.	44320.
MG	21540.	10860.	22140.	16020.
CA	30910.	7190.	28210.	6830.
NA	2730.	6400.	3600.	6400.
K	17540.	29350.	17300.	34230.
TI	9590.	5760.	3280.	5410.
MN	1930.	530.	2080.	490.
BA	400.	760.	460.	960.
CO	58.	78.	44.	78.
CU	34.	15.	29.	25.
GA	10.	31.	19.	32.
LI	12.	22.	12.	20.
MO	0.	1.	0.	1.
PB	35.	20.	19.	29.
PB	67.	332.	70.	219.
S	1731.	781.	1567.	1071.
SR	59.	131.	54.	140.
CaH2O	109200.	49000.	114400.	50400.
ZN	68.	138.	44.	133.
ZR	70.	138.	66.	142.
V	140.	240.	120.	240.
NI	600.	116.	620.	136.

BEARDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-485 1702.0-1705.0	ST-486 1706.0-1707.0	ST-487 1707.0-1711.0	ST-488 1711.0-1715.5
SI	296920.	306860.	288540.	285670.
AL	89723.	97790.	84840.	85960.
FE	43920.	42750.	48110.	56730.
MG	17327.	10900.	9480.	9780.
CA	16860.	6850.	16080.	11990.
NA	13360.	9400.	11800.	14400.
K	18540.	29510.	15110.	14550.
TI	5180.	5330.	5010.	5300.
MN	950.	490.	950.	1130.
BA	960.	740.	660.	580.
CO	44.	34.	22.	46.
CU	43.	33.	37.	35.
GA	30.	32.	26.	31.
LI	12.	17.	9.	12.
MO	1.	0.	0.	1.
PR	21.	27.	28.	21.
RB	117.	202.	79.	107.
S	735.	939.	733.	492.
SR	203.	145.	240.	225.
CGH2O	45400.	57500.	68100.	76600.
ZN	96.	123.	86.	92.
ZK	144.	124.	155.	145.
V	100.	140.	80.	100.
NI	140.	154.	158.	164.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-490 1716.3-1721.0	ST-491 1727.0-1728.5	ST-492 1728.5-1729.0	ST-493 1728.0-1730.0
SI	28090.	28364.	27949.	29610.
AL	28410.	33030.	87650.	36840.
FE	46520.	52430.	51980.	48750.
MG	9380.	9760.	10370.	11100.
CA	10410.	9890.	8740.	8240.
NA	15100.	11950.	12300.	13000.
K	15310.	17030.	18060.	16220.
TI	5420.	5330.	5440.	5320.
MN	810.	890.	810.	510.
BA	560.	560.	540.	560.
CO	48.	48.	54.	48.
CU	36.	30.	29.	32.
GA	20.	24.	25.	26.
LI	12.	16.	17.	16.
MO	3.	2.	3.	2.
PB	18.	22.	29.	20.
PB	107.	129.	138.	123.
S	545.	332.	442.	1128.
SR	220.	217.	202.	205.
CGH2O	70600.	71400.	66800.	65800.
ZN	104.	120.	120.	113.
ZR	135.	142.	138.	136.
V	100.	100.	100.	100.
NI	148.	140.	156.	142.

BEARPAW FORMATION

ALL VALUES IN PARTS PER MILLION

ST-494
1730.0-1735.0

SI	290900.
AL	84740.
FE	48330.
MG	8240.
CA	8130.
NA	15000.
K	12350.
TI	4990.
MN	500.
BA	500.
CC	46.
CU	14.
GA	25.
LI	13.
MO	3.
PB	24.
PP	108.
S	1404.
SR	212.
C&H2O	77700.
ZN	100.
ZR	153.
V	80.
NI	160.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-495 1735.0-1736.0	ST-496 1736.0-1736.2	ST-497 1736.2-1739.5	ST-498 1739.5-1749.0
SI	287980.	261430.	303640.	293100.
AL	88280.	89430.	78530.	91890.
FE	45110.	39520.	42930.	45980.
MG	9320.	32700.	670.	5960.
CA	9590.	10870.	14630.	7960.
NA	17900.	19200.	12800.	14400.
K	5520.	3100.	8160.	12630.
TI	3900.	2540.	3830.	4950.
MN	480.	470.	600.	510.
BA	540.	400.	560.	520.
CO	42.	46.	34.	38.
CU	1.	24.	33.	26.
GA	25.	25.	14.	24.
LI	11.	7.	10.	14.
MO	2.	5.	1.	1.
PB	21.	35.	23.	31.
RR	331.	0.	59.	106.
S	1056.	1334.	1216.	1666.
SR	257.	280.	257.	215.
COH2O	77400.	84000.	65600.	69900.
ZN	65.	39.	65.	93.
ZR	130.	156.	179.	161.
V	40.	20.	60.	80.
NI	146.	156.	134.	140.

FLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-499 1742.0-1750.5	ST-500 1750.5-1753.5	ST-503 1753.0-1754.0	ST-504 1754.0-1755.5
SI	299090.	290620.	292170.	296570.
AL	76430.	80770.	92050.	91560.
FE	51350.	51600.	36870.	40990.
MG	5240.	7180.	6620.	6160.
CA	18120.	6730.	6250.	6710.
NA	12000.	10600.	13100.	12900.
K	9760.	19180.	18460.	27490.
TI	3620.	6120.	6070.	6440.
VN	820.	570.	430.	730.
BA	560.	440.	460.	440.
CO	28.	52.	40.	56.
CU	51.	50.	56.	42.
GA	18.	24.	20.	20.
LI	0.	20.	16.	17.
MO	0.	1.	1.	1.
PB	22.	25.	41.	10.
RB	58.	137.	121.	124.
S	1332.	1547.	225.	163.
SR	196.	196.	157.	149.
CGH2O	53500.	74600.	66300.	50700.
ZN	42.	125.	105.	134.
ZR	162.	134.	141.	150.
V	40.	180.	180.	160.
NI	150.	198.	148.	116.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-505 1755.5-1757.5	ST-506 1757.5-1759.0	ST-507 1759.0-1762.0	ST-508 1762.0-1765.0
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SI	284820.	287390.	288390.	306280.
AL	87290.	93110.	96810.	92630.
FE	41210.	32200.	21000.	32250.
MG	5100.	5440.	4700.	7820.
CA	45700.	6780.	6570.	6300.
NA	12400.	11500.	9400.	13200.
K	21720.	19420.	16230.	28740.
TI	4820.	6620.	6960.	6050.
MN	990.	570.	440.	450.
BA	560.	420.	380.	520.
CO	34.	52.	52.	46.
CU	40.	41.	46.	56.
GA	16.	18.	16.	17.
LI	32.	16.	16.	15.
MO	2.	1.	1.	1.
PB	14.	9.	8.	10.
RB	87.	102.	92.	116.
S	137.	267.	297.	187.
SR	166.	125.	116.	134.
CGH2O	39700.	100200.	121700.	52500.
ZN	93.	91.	86.	81.
ZR	147.	120.	110.	129.
V	80.	160.	180.	160.
NI	98.	112.	112.	124.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-509 1765.0-1767.0	ST-510 1767.0-1768.0	ST-512 1768.3-1769.0	ST-513 1769.0-1770.0
SI	25191.0	279830.	284170.	286100.
AL	81090.	95240.	88410.	94150.
FE	118520.	43020.	16140.	30740.
MG	11920.	6100.	5100.	6580.
CA	33970.	6790.	6470.	6700.
NA	9000.	11920.	9000.	12500.
K	12770.	17320.	17560.	21440.
TI	5860.	6820.	6560.	6410.
MN	1300.	560.	440.	470.
BA	540.	440.	500.	460.
CO	54.	63.	34.	50.
CU	45.	13.	22.	39.
GA	12.	18.	6.	16.
LI	12.	16.	23.	15.
MO	6.	1.	1.	1.
PB	5.	1.	1.	4.
RB	95.	144.	29.	87.
S	247.	296.	185.	229.
SR	177.	161.	60.	146.
CaH2O	67700.	117700.	197700.	91600.
ZN	60.	122.	9.	66.
ZP	143.	113.	65.	115.
V	129.	180.	100.	140.
NI	586.	148.	62.	116.

GUDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-515 1771.0-1771.5	ST-516 1771.5-1772.0	ST-517 1772.0-1772.5	ST-518 1772.5-1773.0
SI	291520.	299720.	298680.	312210.
AL	90800.	93630.	97590.	86700.
FF	30620.	29420.	35670.	34640.
MG	5960.	8660.	9080.	6240.
CA	7000.	9380.	6510.	7620.
NA	14700.	18000.	13100.	16100.
K	14550.	12390.	11830.	15190.
TI	5640.	4880.	6350.	5410.
MN	440.	540.	440.	460.
BA	560.	660.	540.	560.
CO	46.	46.	46.	40.
CU	35.	43.	36.	43.
GA	18.	19.	22.	82.
LI	12.	10.	12.	12.
MO	1.	2.	2.	3.
PR	2.	19.	10.	9.
FB	78.	53.	90.	87.
S	228.	150.	209.	98.
SR	185.	256.	195.	233.
CGH2O	36200.	34900.	24700.	45600.
ZN	71.	100.	60.	86.
ZR	127.	141.	126.	149.
V	120.	100.	160.	120.
NI	112.	120.	132.	120.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-520 1781.5-1782.5	ST-520 1782.5-1783.0	ST-521 1783.0-1784.0	ST-522 1784.0-1785.5
SI	308573.	311130.	317670.	300930.
AL	92913.	89126.	87060.	84410.
FE	36634.	38670.	30160.	62960.
MG	6123.	6800.	9640.	8280.
CA	6858.	7230.	7990.	9350.
NA	15200.	12600.	19800.	14300.
K	14150.	13250.	11850.	11100.
TI	5840.	5260.	4590.	5070.
MN	440.	430.	430.	1380.
BA	500.	560.	740.	600.
CO	40.	40.	34.	40.
CU	41.	28.	39.	34.
GA	22.	20.	14.	29.
LI	12.	9.	8.	9.
MO	2.	3.	1.	1.
PB	4.	11.	18.	16.
RB	108.	79.	69.	88.
S	167.	196.	174.	256.
SR	214.	215.	259.	245.
(CH ₂)	67300.	68700.	40200.	77400.
ZN	64.	55.	45.	77.
ZR	156.	164.	149.	161.
V	100.	126.	100.	100.
NI	132.	178.	154.	222.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-523 1785.5-1787.0	ST-524 1787.0-1788.5	ST-525 1788.5-1789.0	ST-526 1789.0-1790.5
SI	216260.	317090.	307700.	298840.
AL	90930.	83790.	89160.	89600.
FE	31940.	27550.	42050.	36410.
MG	7440.	6720.	21660.	8640.
CA	7690.	11530.	7720.	9180.
NA	18400.	19300.	15000.	19200.
K	11150.	8170.	13170.	10890.
TI	5470.	5230.	5430.	5040.
MN	450.	690.	450.	670.
BA	540.	580.	640.	520.
CO	36.	30.	54.	48.
CU	23.	38.	27.	25.
GA	25.	23.	30.	29.
LI	10.	7.	11.	8.
MO	2.	2.	2.	2.
PR	12.	15.	14.	18.
RB	73.	32.	93.	61.
S	176.	226.	80.	140.
SR	244.	295.	251.	282.
CaH2O	49200.	46500.	58600.	55200.
ZN	93.	72.	81.	90.
ZR	175.	186.	158.	181.
V	120.	100.	160.	120.
NI	84.	96.	90.	108.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	SI-527 1790.5-1793.0	ST-528 1792.0-1797.0	ST-529 1797.0-1798.5	ST-530 1798.5-1799.0
SI	313940.	306460.	316870.	314610.
AL	85213.	83250.	87060.	89990.
FE	31080.	27680.	36130.	37680.
MG	6240.	5580.	5980.	6420.
CA	9200.	20680.	7070.	7230.
NA	20100.	18900.	13200.	16900.
K	10170.	8380.	11470.	12210.
TI	4670.	4400.	5550.	5590.
MN	460.	660.	440.	440.
BA	640.	480.	460.	380.
CO	48.	46.	46.	62.
CU	19.	19.	35.	36.
GA	26.	25.	23.	21.
LI	7.	7.	9.	10.
MO	0.	2.	2.	1.
PB	14.	24.	11.	11.
RB	53.	25.	99.	114.
S	120.	176.	131.	277.
SR	292.	305.	270.	216.
(CH2)	44100.	34600.	55600.	73300.
ZN	63.	67.	55.	93.
ZR	176.	151.	167.	161.
V	100.	90.	160.	160.
NI	93.	108.	144.	154.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-531 1799.0-1800.5	ST-532 1800.5-1804.0	ST-533 1804.0-1806.0	ST-534 1806.0-1808.0
SI	263170.	322530.	308540.	316260.
AL	87610.	86790.	86010.	84740.
FE	43970.	45480.	37000.	28170.
MG	8600.	7290.	5740.	6360.
CA	3090.	9100.	7920.	9530.
NA	17000.	17700.	16800.	18600.
K	19840.	9320.	14910.	12720.
TI	4930.	4690.	5190.	5070.
MN	440.	640.	490.	520.
BA	1280.	520.	560.	660.
CO	54.	40.	48.	58.
CU	36.	41.	37.	21.
GA	25.	26.	27.	18.
LI	8.	8.	9.	8.
MO	1.	2.	1.	1.
PB	9.	13.	9.	13.
PB	92.	58.	106.	56.
S	221.	200.	130.	159.
SR	270.	283.	273.	270.
CaH2O	57300.	64360.	44500.	40600.
ZN	67.	77.	78.	65.
ZR	179.	194.	201.	249.
V	120.	100.	140.	120.
NI	146.	108.	124.	132.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-535 1808.0-1814.5	ST-536 1814.5-1815.5	ST-537 1815.5-1818.5	ST-538 1818.5-1819.0
SI	295130.	282670.	300250.	289180.
AL	81240.	86470.	91140.	86790.
FE	33850.	43010.	42430.	47910.
MG	7980.	8040.	8320.	8060.
CA	25720.	7290.	7890.	11080.
NA	19100.	14900.	14400.	18300.
K	9790.	15990.	18550.	11360.
TI	3930.	5040.	5850.	4810.
MN	910.	450.	480.	1000.
BA	750.	540.	600.	540.
CD	44.	50.	56.	50.
CU	26.	59.	57.	37.
GA	18.	22.	21.	23.
LI	6.	12.	12.	10.
MO	2.	2.	2.	2.
PB	25.	7.	14.	14.
RB	24.	115.	102.	50.
S	55.	244.	145.	171.
SR	277.	222.	238.	295.
GH20	29500.	80400.	53500.	56200.
ZN	49.	70.	90.	103.
ZR	412.	155.	179.	185.
V	60.	100.	140.	80.
NI	118.	172.	178.	188.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-539 1819.0-1821.0	ST-540 1821.0-1823.0	ST-541 1823.0-1825.5	ST-542 1825.5-1827.0
SI	303990.	302250.	306250.	287850.
AL	81590.	91570.	86790.	83500.
FE	55230.	39590.	48420.	43370.
MG	9840.	5740.	7200.	7740.
CA	7960.	6640.	7280.	7750.
NA	13200.	13200.	16700.	12200.
K	15780.	10990.	14750.	14780.
TI	5000.	5810.	5310.	5340.
MN	1020.	450.	450.	460.
BA	500.	520.	600.	500.
CO	50.	32.	46.	50.
CU	53.	46.	44.	45.
GA	21.	20.	23.	17.
LI	14.	14.	11.	15.
MO	3.	3.	1.	2.
PB	19.	9.	34.	17.
KB	94.	83.	96.	89.
S	351.	25.	213.	464.
SR	200.	203.	247.	194.
COH2O	76300.	58600.	53900.	134300.
ZN	93.	61.	105.	95.
ZR	191.	170.	212.	148.
V	120.	140.	120.	140.
NI	190.	138.	206.	138.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-543 1827.0-1830.0	ST-544 1830.0-1831.5	ST-545 1831.5-1833.0	ST-546 1833.0-1834.0
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SI	302300.	298570.	308510.	313620.
AL	85480.	85450.	90250.	88810.
FE	35430.	64820.	36890.	38080.
MG	7060.	10120.	5920.	7760.
CA	9060.	12640.	6840.	7350.
NA	17500.	16200.	14000.	15100.
K	12830.	9000.	11690.	13190.
TI	5140.	4540.	5520.	5240.
MN	490.	2310.	450.	450.
BA	460.	530.	440.	560.
CO	38.	38.	34.	30.
CU	38.	35.	34.	38.
GA	19.	24.	23.	20.
LI	11.	10.	11.	10.
MO	2.	1.	1.	1.
PB	27.	22.	5.	15.
RB	65.	39.	75.	69.
S	162.	107.	62.	83.
SR	271.	293.	215.	234.
CGH2O	59500.	72800.	54300.	57500.
ZN	91.	76.	47.	66.
ZR	107.	264.	309.	176.
V	100.	80.	100.	120.
NI	122.	156.	170.	122.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-547 1834.0-1835.5	ST-548 1835.5-1837.0	ST-549 1837.0-1844.0	ST-550 1844.0-1844.5
SI	303613.	327250.	304750.	309120.
AL	86930.	81040.	83450.	83060.
FE	41950.	26650.	28410.	38100.
MG	8300.	5280.	6120.	22720.
CA	7910.	7840.	15610.	7880.
NA	16590.	19920.	19300.	15400.
K	11380.	8990.	8550.	10600.
TI	5210.	4710.	4770.	5100.
MN	460.	440.	580.	460.
BA	590.	480.	620.	920.
CO	32.	38.	34.	38.
CU	39.	17.	28.	37.
GA	22.	14.	19.	27.
LI	11.	9.	3.	12.
MO	0.	1.	1.	3.
PB	19.	14.	22.	18.
RB	76.	49.	13.	87.
S	129.	510.	103.	195.
SR	253.	224.	329.	235.
CH2O	58100.	53800.	35500.	77500.
ZN	118.	42.	68.	59.
ZR	195.	160.	200.	184.
V	100.	69.	80.	200.
NI	132.	102.	124.	124.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-551 1844.5-1845.0	ST-552 1845.0-1846.0	ST-553 1846.0-1847.0	ST-554 1847.0-1850.0
SI	287830.	315600.	323200.	239310.
AL	95470.	83990.	88590.	81290.
FE	37360.	40260.	37150.	28270.
MG	3680.	26100.	9520.	16020.
CA	3860.	7160.	7360.	6670.
NA	15200.	16400.	16400.	17500.
K	6780.	12230.	11630.	3700.
TJ	3920.	5140.	5050.	4790.
MN	460.	460.	450.	440.
BA	560.	1000.	720.	980.
CO	34.	34.	22.	26.
CU	14.	36.	56.	26.
GA	19.	23.	21.	16.
LI	9.	13.	11.	8.
MO	2.	1.	1.	3.
PB	7.	6.	19.	9.
RB	34.	104.	64.	55.
S	230.	52.	192.	113.
SR	153.	236.	223.	218.
CGH20	143900.	58300.	55400.	38400.
ZN	71.	93.	71.	32.
ZR	142.	139.	171.	167.
V	60.	100.	80.	40.
NI	134.	90.	49.	64.

CLOWAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-555 1850.0-1851.0	ST-556 1851.0-1853.0	ST-557 1853.0-1853.5	ST-558 1853.5-1855.5
SI	306130.	298650.	364730.	311930.
AL	84220.	82570.	82360.	84590.
FE	38640.	36670.	37200.	32620.
MG	17120.	22400.	7160.	13720.
CA	7850.	3940.	7040.	7100.
NA	16800.	16930.	17000.	18400.
K	10140.	7680.	9230.	6480.
TI	4820.	3770.	4860.	3830.
MN	800.	1100.	460.	440.
BA	900.	840.	580.	340.
CO	36.	42.	36.	26.
CU	31.	34.	33.	23.
GA	21.	21.	17.	13.
LI	12.	11.	12.	8.
MO	2.	2.	3.	1.
PB	6.	19.	22.	7.
RB	74.	36.	63.	29.
S	520.	176.	162.	60.
SR	235.	275.	227.	231.
CGH2O	59300.	56200.	70200.	55400.
ZN	80.	65.	65.	30.
ZR	190.	177.	175.	140.
V	40.	40.	60.	40.
NI	176.	90.	92.	86.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-559 1855.5-1857.0	ST-560 1857.0-1857.5	ST-561 1857.5-1859.0	ST-563 1860.5-1861.5
SI	306480.	313110.	308880.	291940.
AL	79390.	46470.	82470.	86520.
FE	30750.	28620.	29810.	38550.
MG	14720.	9620.	14680.	15000.
CA	7230.	7550.	10420.	3240.
NA	17500.	17900.	20900.	17600.
K	6590.	5910.	5950.	8080.
TI	3640.	3380.	3610.	4020.
MN	440.	440.	510.	460.
BA	900.	720.	820.	900.
CO	30.	22.	32.	42.
CU	27.	19.	16.	26.
GA	14.	18.	18.	22.
LI	9.	10.	10.	10.
MO	1.	0.	2.	2.
PB	3.	10.	18.	21.
RB	33.	23.	14.	47.
S	207.	42.	172.	100.
SR	231.	244.	301.	279.
CGH2O	67500.	44800.	41200.	70800.
ZN	33.	21.	50.	63.
ZR	161.	159.	174.	184.
V	40.	40.	40.	40.
NI	86.	86.	120.	118.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-564 1861.5-1867.0	ST-565 1867.0-1868.0	ST-566 1868.0-1868.5	ST-567 1868.5-1873.0
SI	301760.	214210.	294030.	327490.
AL	88170.	79770.	86840.	78070.
FE	41320.	32390.	38950.	30290.
MG	16280.	10780.	17080.	4880.
CA	7790.	6880.	6760.	6780.
NA	17300.	16900.	14500.	13000.
K	9390.	7210.	9580.	7560.
TI	4320.	4570.	5130.	4600.
MN	460.	440.	450.	440.
BA	940.	740.	1000.	520.
CO	40.	34.	33.	44.
CU	43.	23.	59.	24.
GA	22.	18.	14.	15.
LI	10.	6.	10.	8.
MO	1.	4.	1.	2.
PB	15.	18.	14.	14.
PB	77.	40.	82.	46.
S	79.	93.	158.	114.
SR	265.	221.	199.	199.
GH20	66500.	65100.	90700.	53900.
ZN	67.	43.	95.	60.
ZR	198.	169.	163.	170.
V	66.	40.	120.	40.
NI	152.	70.	80.	124.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-568 1875.0-1878.0	ST-569 1878.0-1883.0	ST-570 1883.0-1886.0	ST-571 1886.0-1887.5
SI	307580.	311460.	295350.	304430.
AL	82310.	86110.	81610.	78130.
FE	43085.	43070.	44300.	31310.
MG	5240.	8480.	9100.	5460.
CA	6870.	8420.	7610.	6650.
NA	16700.	10000.	17100.	16200.
K	9930.	10430.	8960.	8470.
TI	4770.	4750.	4710.	5250.
MN	440.	480.	500.	440.
BA	580.	560.	540.	540.
CO	44.	46.	66.	34.
CU	26.	35.	35.	27.
GA	24.	20.	22.	18.
LI	15.	17.	19.	15.
MO	2.	1.	2.	1.
PB	13.	20.	15.	15.
RB	72.	70.	63.	58.
S	77.	72.	171.	81.
SR	238.	281.	259.	213.
U420	51700.	51000.	67000.	56500.
ZN	69.	92.	90.	86.
ZR	145.	154.	125.	156.
V	60.	60.	100.	80.
NI	166.	126.	190.	96.

OLDMAN FORMATION

ALL VALUES IN PARTS PER BILLION

	ST-572 1887.5-1892.5	ST-573 1892.5-1893.5	ST-574 1893.5-1895.0	ST-575 1895.0-1896.5
SI	313210.	329250.	294060.	310140.
AL	80150.	84060.	91150.	91150.
FE	40460.	23810.	45910.	48350.
MG	5260.	3280.	7560.	7860.
CA	6280.	6650.	7310.	7090.
NA	15700.	17500.	18100.	15700.
K	10320.	9690.	14610.	15070.
TI	5140.	4810.	5300.	5420.
MN	460.	440.	470.	480.
BA	460.	440.	520.	440.
CO	37.	36.	54.	54.
CU	27.	22.	44.	52.
GA	21.	17.	24.	26.
LI	16.	16.	20.	22.
MO	1.	1.	1.	2.
PB	13.	4.	7.	10.
RB	70.	60.	102.	118.
S	75.	34.	159.	123.
SR	224.	192.	256.	230.
CGH2O	44930.	44800.	61100.	64900.
ZN	62.	37.	133.	108.
ZP	196.	149.	192.	101.
V	61.	40.	140.	160.
NI	96.	70.	158.	184.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-576 1896.5-1898.5	ST-577 1898.5-1900.0	ST-578 1900.0-1906.0	ST-579 1906.0-1910.5
SI	297480.	291070.	286900.	336170.
AL	87810.	90550.	87040.	74500.
FE	41450.	42280.	30630.	26670.
MG	6620.	4860.	6940.	3860.
CA	7510.	8210.	12290.	6510.
NA	17300.	20500.	21500.	16900.
K	10440.	9480.	8600.	8180.
TI	4840.	4390.	4630.	5580.
MN	440.	470.	600.	450.
BA	540.	520.	560.	420.
CO	36.	46.	38.	24.
CU	31.	31.	21.	22.
GA	24.	24.	17.	10.
LI	15.	15.	13.	7.
MO	1.	3.	0.	2.
PB	74.	11.	18.	10.
RB	102.	72.	25.	55.
S	113.	84.	142.	17.
SR	267.	296.	324.	188.
CO ₂ H ₂ O	33400.	53700.	39500.	40000.
ZN	64.	90.	67.	36.
ZR	174.	208.	204.	168.
V	120.	100.	80.	60.
NI	124.	164.	100.	90.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-580 1910.5-1912.5	ST-581 1912.5-1914.5	ST-582 1914.5-1916.0	ST-583 1916.0-1920.0
SI	323610.	306260.	290440.	315780.
AL	83430.	85430.	71180.	96150.
FE	30900.	37030.	26730.	36480.
MG	5080.	5480.	3980.	12320.
CA	6600.	7390.	30770.	7290.
NA	15890.	16600.	16400.	18400.
K	10900.	13150.	10350.	12590.
TI	5010.	5200.	4360.	4920.
MN	470.	680.	930.	460.
BA	460.	540.	640.	340.
CO	50.	40.	30.	44.
CU	20.	25.	17.	31.
GA	15.	16.	13.	17.
LI	0.	30.	8.	9.
MO	2.	1.	1.	2.
PB	12.	14.	28.	13.
RB	67.	102.	39.	89.
S	108.	72.	35.	65.
SR	204.	222.	247.	245.
CO ₂ H ₂ O	45700.	55800.	30400.	47700.
ZN	51.	75.	52.	67.
ZR	177.	199.	204.	195.
V	80.	120.	60.	100.
NI	103.	116.	78.	104.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-584 1920.0-1921.0	ST-585 1921.0-1925.5	ST-586 1925.5-1927.5	ST-587 1927.5-1929.0
SI	303230.	301890.	292490.	285890.
AL	85370.	86370.	87250.	83480.
FE	39520.	40530.	44760.	44770.
MG	7840.	9460.	7485.	7380.
CA	6510.	6430.	6900.	7670.
NA	16400.	14200.	15600.	16000.
K	15470.	48320.	18210.	18620.
TI	5550.	5520.	5860.	5700.
MN	450.	450.	490.	520.
BA	660.	560.	656.	620.
CO	42.	42.	93.	76.
CU	43.	28.	49.	30.
GA	21.	19.	26.	26.
LI	10.	10.	16.	16.
MO	1.	2.	1.	1.
PB	3.	9.	9.	16.
RB	94.	90.	127.	81.
S	64.	55.	169.	474.
SR	233.	213.	245.	252.
UO ₂	59400.	47000.	55900.	57500.
ZN	42.	53.	106.	112.
ZR	132.	186.	194.	197.
V	140.	120.	112.	100.
NI	138.	138.	152.	166.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-588 1929.0-1930.5	ST-589 1930.5-1936.5	ST-590 1936.5-1936.8	ST-591 1936.8-1942.0
SI	223960.	282770.	281150.	294730.
AL	65780.	86840.	98270.	85450.
FE	122570.	47760.	50220.	40280.
MG	13600.	6700.	9340.	13960.
CA	19780.	6710.	7720.	7180.
NA	9500.	15600.	20000.	17200.
K	9820.	13620.	5220.	11180.
TI	4470.	5080.	2880.	5810.
MN	3820.	450.	460.	450.
BA	540.	620.	560.	820.
CO	42.	44.	42.	44.
CU	48.	44.	8.	27.
GA	18.	23.	29.	17.
LI	12.	11.	14.	11.
MO	0.	0.	3.	0.
PB	0.	7.	18.	6.
RB	55.	111.	20.	80.
S	336.	60.	89.	63.
SR	205.	252.	325.	257.
CGH2O	41600.	53300.	84200.	46600.
ZN	85.	71.	82.	54.
ZR	405.	195.	194.	134.
V	30.	100.	20.	60.
HI	372.	118.	90.	88.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-592 1942.0-1943.5	ST-593 1943.5-1944.5	ST-594 1944.5-1945.5	ST-595 1945.5-1947.0
SI	285490.	283030.	350310.	309980.
AL	76850.	65690.	55520.	83270.
FE	38740.	44840.	17140.	36720.
MG	13820.	6940.	11820.	6700.
CA	7930.	6370.	6000.	6080.
NA	18800.	14300.	10100.	12400.
K	11960.	19670.	9470.	15890.
TI	4550.	5880.	5320.	4550.
MN	1050.	480.	430.	450.
BA	360.	580.	700.	580.
CO	52.	50.	26.	40.
CU	22.	35.	23.	16.
GA	20.	16.	8.	14.
LI	11.	12.	6.	10.
MO	2.	1.	2.	2.
PB	35.	9.	10.	17.
RB	60.	60.	57.	104.
S	106.	55.	128.	308.
SR	285.	156.	122.	137.
CGH ₂ O	40100.	47600.	49900.	36200.
ZN	70.	54.	48.	73.
ZR	907.	172.	159.	230.
V	40.	100.	20.	40.
NI	106.	102.	40.	90.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-596 1947.0-1948.0	ST-597 1948.0-1953.0	ST-598 1953.0-1954.0	ST-599 1954.0-1955.5
SI	292640.	308180.	322440.	291250.
AL	83270.	77520.	75230.	79060.
FE	39810.	34600.	29630.	37100.
MG	10780.	8760.	5500.	7460.
CA	6050.	31900.	7090.	10980.
NA	13800.	10500.	14400.	10900.
K	15630.	17150.	15040.	17500.
TI	5710.	4460.	3180.	4550.
MN	460.	540.	500.	490.
BA	770.	600.	640.	620.
CO	46.	32.	28.	36.
CU	44.	25.	18.	23.
GA	15.	8.	9.	17.
LI	12.	10.	13.	10.
MO	2.	4.	0.	2.
PB	11.	6.	11.	12.
PP	103.	106.	39.	110.
S	144.	173.	98.	119.
SR	172.	151.	163.	171.
CH ₂ O	48800.	35600.	21900.	36800.
ZN	91.	70.	36.	64.
ZR	191.	226.	162.	222.
V	30.	60.	40.	60.
NI	92.	82.	38.	66.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-600 1955.5-1956.0	ST-601 1956.0-1958.0	ST-602 1958.0-1959.0	ST-603 1959.0-1959.7
SI	281840.	286110.	218800.	297780.
AL	75460.	71980.	48580.	62470.
FE	37890.	27500.	130590.	45630.
MG	9460.	15960.	15640.	12640.
CA	18630.	21100.	61910.	20470.
NA	12100.	9940.	5400.	8300.
K	16520.	17060.	11120.	15440.
TI	4680.	4150.	2940.	3750.
MN	520.	790.	12260.	550.
BA	600.	720.	500.	540.
CO	40.	36.	40.	28.
CU	24.	19.	32.	32.
GA	17.	13.	8.	11.
LI	10.	11.	9.	14.
MO	8.	2.	0.	2.
PB	16.	13.	10.	7.
RB	116.	105.	88.	100.
S	48.	17.	0.	86.
SR	179.	149.	145.	117.
CH2O	42300.	26800.	130400.	28900.
ZN	89.	73.	67.	62.
ZR	220.	218.	404.	277.
V	60.	60.	40.	60.
NI	114.	90.	510.	152.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-604 1959.7-1960.7	ST-605 1960.7-1960.9	ST-606 1960.9-1962.0	ST-607 1962.0-1963.3
SI	329230.	282160.	268900.	338810.
AL	78950.	67860.	72560.	68560.
FE	28760.	34410.	34150.	29270.
MG	3260.	13240.	6260.	5680.
CA	1530.	14790.	27190.	10100.
NA	13100.	11100.	12400.	10300.
K	2100.	10450.	14340.	10460.
TI	1100.	1020.	4090.	3150.
NO	100.	500.	1290.	540.
BA	140.	500.	550.	340.
CG	40.	34.	16.	30.
CO	14.	22.	19.	10.
GA	14.	19.	14.	16.
LI	2.	13.	9.	13.
MO	0.	3.	0.	0.
PB	20.	12.	12.	31.
RE	52.	134.	81.	47.
S	29.	9.	48.	246.
SR	152.	142.	180.	152.
CO ₂ H ₂ O	18300.	42900.	92300.	25300.
ZN	50.	68.	54.	43.
ZR	112.	213.	190.	150.
V	60.	120.	80.	60.
NI	68.	96.	94.	63.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-608 1963.3-1964.0	ST-609 1964.3-1966.0	ST-610 1966.0-1968.0	ST-611 1968.0-1970.5
SI	259900.	263970.	293120.	278710.
AL	92590.	76300.	87250.	78620.
FE	45230.	26570.	38610.	48930.
MG	8300.	7600.	7560.	21020.
CA	6580.	14580.	6950.	6810.
NA	15500.	22600.	18900.	11200.
K	13000.	9960.	13860.	17760.
TI	4950.	5440.	4780.	5160.
MN	470.	600.	460.	510.
BA	640.	780.	640.	880.
CO	52.	42.	26.	50.
CU	44.	16.	30.	45.
GA	35.	27.	26.	28.
LI	12.	11.	8.	13.
MO	1.	2.	1.	1.
PB	12.	13.	12.	33.
BR	52.	26.	72.	123.
S	31.	173.	197.	388.
SR	247.	373.	270.	193.
CaH ₂ O	57800.	28600.	42000.	52200.
ZN	59.	50.	41.	91.
ZR	262.	276.	193.	220.
V	140.	60.	140.	140.
NI	112.	56.	126.	168.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-612 1970.5-1974.0	ST-613 1974.5-1983.0	ST-614 1983.0-1983.5	ST-615 1983.5-1989.0
SI	318040.	291230.	288380.	296310.
AL	72620.	77690.	72740.	79550.
FE	26420.	26650.	31590.	23970.
MG	33300.	37060.	27800.	10560.
CA	5170.	13290.	17250.	13250.
NA	19700.	7200.	9100.	30800.
K	35350.	14860.	16020.	11480.
TI	4550.	4040.	3790.	3130.
MN	440.	570.	470.	470.
BA	680.	600.	620.	480.
CO	16.	18.	30.	20.
CU	21.	15.	17.	14.
GA	17.	18.	15.	13.
LI	0.	9.	12.	1.
MO	2.	2.	2.	0.
PB	23.	9.	10.	4.
RB	331.	69.	117.	48.
S	360.	231.	153.	129.
SR	129.	66.	155.	134.
COH2D	34800.	20000.	50100.	20700.
ZN	40.	29.	64.	26.
ZR	388.	232.	209.	160.
V	100.	60.	100.	40.
NI	82.	86.	114.	36.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-616 1989.0-1990.5	ST-617 1990.5-1993.5	ST-618 1993.5-1999.5	ST-619 1999.5-2000.5
SI	297080.	281140.	303200.	264970.
AL	67390.	81070.	63140.	67210.
FE	27010.	44500.	30530.	63140.
MG	7600.	14920.	19600.	23780.
CA	37020.	6070.	25210.	39970.
NA	11200.	11700.	5900.	6400.
K	12410.	23020.	20860.	26820.
TI	3510.	5400.	3750.	4290.
MN	760.	470.	540.	1330.
BA	540.	700.	480.	480.
CO	23.	36.	44.	22.
CU	17.	42.	19.	38.
GA	12.	22.	10.	21.
LI	15.	12.	11.	18.
MO	2.	1.	2.	4.
PB	16.	7.	4.	12.
RR	50.	152.	106.	161.
S	106.	118.	244.	202.
SR	135.	181.	81.	107.
CO&H2O	21300.	50700.	18800.	43000.
ZN	51.	110.	59.	101.
ZR	161.	197.	250.	307.
V	61.	180.	80.	140.
NI	42.	146.	120.	180.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-620 2006.5-2007.0	ST-621 2007.0-2012.0	ST-622 2012.0-2017.0	ST-624 2019.5-2021.5
SI	334390.	293680.	378480.	303430.
AL	58220.	58530.	50470.	87660.
FE	13820.	33310.	28510.	41850.
MG	21360.	35260.	12100.	20900.
CA	57330.	42840.	37530.	11410.
NA	4700.	5000.	3600.	10100.
K	11990.	11960.	7650.	21800.
TI	2350.	3810.	2080.	4940.
MN	780.	3070.	1440.	590.
BA	420.	400.	400.	980.
CO	8.	14.	10.	34.
CU	14.	10.	11.	27.
GA	8.	10.	6.	19.
LI	6.	11.	10.	16.
MO	2.	7.	1.	1.
PB	6.	6.	9.	7.
RB	80.	66.	11.	112.
S	82.	104.	245.	175.
SR	87.	58.	44.	166.
CO&H2O	9700.	18000.	14700.	44000.
ZN	26.	43.	24.	94.
ZR	114.	268.	120.	234.
V	40.	60.	60.	140.
NI	48.	74.	42.	102.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-625 2021.5-2027.0	ST-626 2027.0-2027.5	ST-627 2027.5-2032.5	ST-628 2032.5-2038.0
SI	396830.	377190.	279620.	359050.
AL	86810.	78900.	83060.	74210.
FE	35730.	75790.	28980.	29430.
MG	14400.	30500.	8980.	7680.
CA	24380.	15300.	40070.	9350.
NA	11000.	9900.	11100.	10500.
K	13190.	19810.	16210.	14780.
TI	4400.	4740.	4100.	4280.
MN	960.	3100.	930.	590.
BA	580.	3160.	900.	420.
CO	30.	42.	24.	22.
CU	21.	38.	20.	37.
GA	26.	20.	12.	10.
LI	13.	17.	11.	14.
MO	1.	0.	1.	0.
PB	7.	13.	6.	8.
PS	70.	116.	58.	52.
S	203.	210.	174.	103.
SR	162.	171.	150.	112.
CH2O	30700.	70800.	25900.	16200.
ZN	70.	101.	63.	55.
ZR	215.	328.	177.	150.
V	80.	140.	80.	40.
NI	44.	158.	94.	36.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-629 2023.0-2040.0	ST-630 2040.0-2041.0	ST-631 2041.0-2044.0	ST-632 2044.0-2045.5
SI	317910.	325040.	295930.	318510.
AL	70950.	76500.	82680.	85120.
FE	28870.	29440.	34920.	27700.
MG	25080.	40020.	17300.	18940.
CA	5960.	6000.	5860.	5800.
NA	11100.	12700.	11500.	10600.
K	14030.	12730.	26460.	26080.
TI	4190.	4180.	4210.	4150.
MN	470.	450.	450.	440.
BA	1040.	1160.	980.	960.
CO	28.	38.	28.	76.
CU	30.	19.	21.	25.
GA	18.	16.	19.	17.
LI	8.	7.	8.	9.
MO	4.	2.	2.	2.
PB	6.	10.	16.	12.
BR	123.	112.	178.	148.
S	0.	34.	47.	153.
SR	135.	149.	154.	121.
C&H2O	34900.	36100.	37300.	44800.
ZN	10.	19.	26.	100.
ZR	195.	192.	209.	198.
V	80.	60.	80.	100.
NI	62.	106.	114.	162.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-633 2045.5-2049.5	ST-634 2049.5-2050.5	ST-635 2050.5-2051.0	ST-636 2051.0-2054.0
SI	291830.	291860.	272840.	325470.
AL	34060.	92150.	82310.	82790.
FE	36770.	34700.	36350.	41010.
MG	43620.	12860.	10760.	11620.
CA	5860.	5870.	5980.	6230.
NA	11700.	11000.	10400.	11590.
K	22320.	16520.	15030.	28680.
TI	4510.	4780.	4780.	3990.
MN	460.	450.	460.	500.
BA	1290.	840.	740.	780.
CD	48.	32.	58.	34.
CU	41.	20.	21.	21.
GA	20.	23.	20.	16.
LI	13.	13.	16.	13.
MO	0.	2.	3.	0.
PB	7.	15.	25.	23.
RB	157.	152.	132.	142.
S	21.	28.	662.	791.
SR	141.	149.	107.	102.
CO&H2O	42500.	42600.	92900.	20100.
ZN	22.	45.	151.	53.
ZR	194.	192.	180.	250.
V	100.	100.	100.	80.
NI	134.	120.	158.	154.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-637 2054.0-2055.0	ST-638 2055.0-2056.0	ST-639 2056.0-2057.5	ST-640 2057.5-2059.5
SI	332190.	269240.	300100.	290330.
AL	98130.	68040.	87710.	73530.
FE	47170.	13740.	29450.	31240.
MG	12740.	14920.	35220.	38960.
CA	6160.	78360.	34550.	60580.
NA	7300.	7000.	9600.	13400.
K	49770.	19900.	45600.	30240.
TI	4990.	2450.	4240.	3250.
MN	590.	1700.	570.	590.
BA	740.	620.	600.	460.
CO	44.	18.	40.	36.
CU	41.	18.	34.	23.
GA	27.	13.	24.	15.
LI	18.	7.	27.	20.
MO	0.	1.	1.	0.
PB	25.	10.	19.	10.
RB	253.	73.	216.	116.
S	421.	614.	318.	362.
SR	129.	179.	129.	106.
CGH2O	25500.	5100.	24300.	14000.
ZN	109.	17.	93.	44.
ZR	247.	194.	234.	222.
V	140.	40.	100.	40.
NI	154.	70.	44.	36.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-641 2059.5-2062.5	ST-642 2062.5-2068.5	ST-643 2069.5-2074.5	ST-644 2074.5-2078.0
SI	314060.	298440.	281540.	307320.
AL	82630.	65720.	82200.	85950.
FE	36030.	19100.	19520.	39640.
MG	27250.	13660.	14340.	18940.
CA	29850.	79010.	30300.	15790.
NA	10700.	9100.	11600.	9900.
K	35100.	16500.	17600.	26990.
TI	3910.	2150.	2900.	4000.
MN	550.	950.	620.	520.
BA	520.	420.	440.	480.
CO	47.	26.	28.	30.
CU	20.	14.	15.	27.
GA	21.	12.	16.	17.
LI	10.	10.	12.	19.
MO	1.	0.	0.	0.
PB	8.	5.	30.	16.
RB	172.	72.	77.	153.
S	136.	229.	126.	65.
SR	132.	0.	97.	114.
C&H2O	25500.	5000.	8100.	22800.
ZN	59.	27.	20.	48.
ZR	233.	151.	145.	225.
V	80.	20.	40.	80.
NT	36.	34.	26.	36.

DIDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-645 2073.0-2083.0	ST-646 2083.0-2085.5	ST-647 2085.5-2086.0	ST-648 2086.0-2088.0
SI	268710.	265690.	255580.	278290.
AL	78290.	74270.	76300.	72350.
FE	37050.	25600.	44290.	34900.
MG	29700.	27160.	27520.	23200.
CA	41790.	74850.	41890.	78720.
NA	9390.	9000.	9200.	8600.
K	33640.	18210.	30550.	20770.
TI	3770.	3160.	2820.	2640.
MN	560.	980.	630.	840.
BA	560.	440.	520.	400.
CO	40.	32.	42.	34.
CU	31.	21.	31.	21.
GA	27.	13.	24.	20.
LI	20.	16.	25.	18.
MO	0.	4.	2.	2.
PB	10.	12.	16.	9.
RB	190.	93.	176.	119.
S	70.	156.	18.	55.
SR	122.	108.	105.	110.
CO ₂ H ₂ O	19200.	10800.	22100.	13300.
ZN	79.	40.	65.	49.
ZR	220.	247.	244.	272.
V	80.	40.	100.	40.
NI	42.	40.	44.	44.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-649 2088.0-2089.0	ST-650 2089.0-2093.5	ST-651 2093.5-2095.5	ST-652 2095.5-2097.0
SI	243000.	288850.	294060.	283640.
AL	66680.	58970.	87400.	84060.
FE	8520.	37520.	46890.	49920.
MG	28620.	14960.	5360.	5680.
CA	65100.	6000.	5960.	5910.
NA	8100.	10000.	9000.	11000.
K	24270.	14470.	12060.	17060.
TI	3530.	5590.	6060.	5730.
MN	3160.	470.	460.	470.
BA	520.	700.	460.	540.
CO	46.	36.	40.	46.
CU	24.	42.	49.	34.
GA	22.	12.	17.	16.
LT	17.	15.	15.	21.
NO	0.	2.	0.	0.
PB	5.	8.	3.	4.
RB	167.	119.	188.	152.
S	2.	54.	24.	84.
SR	101.	140.	169.	168.
CH20	27200.	33400.	43400.	40600.
ZN	72.	66.	57.	48.
ZK	351.	253.	205.	204.
V	89.	140.	180.	180.
NI	52.	40.	38.	48.

CLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-653 2097.0-2099.0	ST-654 2099.0-2101.0	ST-655 2101.0-2104.0	ST-656 2104.0-2108.0
SI	269880.	290150.	275810.	290920.
AL	89790.	79610.	82040.	77740.
FE	46210.	35660.	35690.	29590.
MG	7000.	11040.	16500.	16340.
CA	5810.	6310.	13080.	12750.
NA	11000.	10980.	9800.	9300.
K	19160.	19790.	21450.	11380.
TI	5550.	5020.	4750.	3510.
MN	460.	470.	510.	500.
BA	520.	560.	480.	480.
CD	61.	54.	38.	34.
CU	57.	23.	31.	12.
GA	22.	21.	15.	11.
LI	25.	22.	23.	15.
MO	0.	1.	1.	0.
PB	0.	15.	10.	29.
RB	146.	161.	152.	57.
S	139.	145.	205.	251.
SR	153.	136.	127.	81.
CaH2O	43000.	43500.	37100.	15600.
ZN	110.	76.	97.	33.
ZR	207.	207.	398.	192.
V	200.	140.	140.	80.
NI	80.	68.	46.	38.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	SI-657 2108.0-2114.0	SI-658 2114.0-2119.5	SI-659 2119.5-2125.5	SI-660 2125.5-2127.5
SI	343040.	330180.	335230.	286380.
AL	79770.	74950.	78840.	43140.
FE	23400.	22240.	21030.	59680.
MG	14160.	18320.	7100.	14100.
CA	23680.	41490.	19230.	52570.
NA	10500.	8100.	11400.	4800.
K	12040.	10030.	9390.	9250.
TI	3820.	3190.	3080.	1880.
MN	520.	620.	760.	2540.
BA	349.	380.	420.	300.
CO	25.	24.	20.	38.
CU	9.	19.	25.	32.
GA	14.	14.	14.	15.
LI	14.	15.	15.	11.
MO	8.	1.	0.	0.
PB	10.	11.	11.	8.
RB	56.	48.	39.	137.
S	168.	167.	145.	291.
SR	87.	91.	117.	138.
H ₂ O	10600.	21900.	11400.	41400.
ZN	31.	41.	45.	32.
ZR	185.	177.	317.	318.
V	60.	60.	80.	60.
NI	28.	30.	32.	54.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-661 2127.5-2128.5	ST-662 2129.5-2133.0	ST-663 2133.0-2135.5	ST-664 2135.5-2136.5
SI	262270.	279830.	269750.	277660.
AL	50470.	91850.	92640.	88270.
FE	29110.	54060.	53240.	43900.
MG	10280.	13760.	11020.	9680.
CA	64060.	6650.	6530.	7640.
NA	6500.	16100.	15100.	18700.
K	5080.	15480.	12290.	8930.
TI	1370.	5730.	5780.	6050.
MN	3160.	490.	610.	550.
BA	420.	520.	660.	540.
CO	32.	60.	60.	44.
CU	4.	28.	41.	20.
GA	12.	28.	23.	23.
LI	13.	22.	28.	19.
MO	0.	1.	0.	0.
PB	20.	8.	11.	2.
RB	10.	136.	86.	38.
S	94.	105.	132.	110.
SR	252.	219.	205.	225.
GH20	6800.	76500.	56500.	34200.
ZN	21.	82.	123.	78.
ZR	145.	178.	188.	209.
V	60.	120.	160.	120.
NI	48.	58.	76.	42.

GLDWIN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-665 2136.5-2138.5	ST-666 2139.5-2141.5	ST-667 2141.5-2143.5	ST-668 2143.5-2144.0
SI	321840.	272510.	295570.	285280.
AL	82150.	89390.	92100.	88580.
FE	31540.	43310.	33870.	56380.
MG	13300.	11840.	17280.	9220.
CA	5940.	7730.	6010.	6540.
NA	13600.	17200.	12700.	14000.
K	3350.	6560.	10820.	10230.
TI	5940.	5850.	6220.	5300.
MN	590.	620.	460.	850.
BA	740.	700.	960.	520.
CO	62.	50.	56.	52.
CU	40.	19.	44.	23.
GA	19.	21.	22.	24.
LI	21.	18.	22.	24.
MO	0.	1.	0.	0.
PB	5.	6.	7.	10.
RR	65.	31.	99.	55.
S	55.	123.	121.	90.
SR	160.	205.	150.	178.
CH2O	40500.	26800.	57300.	32100.
ZN	51.	56.	63.	93.
ZR	159.	106.	156.	232.
V	140.	127.	100.	140.
NI	62.	57.	48.	58.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-669 2144.0-2145.0	SI-670 2145.0-2145.5	ST-671 2145.5-2147.0	SI-672 2147.0-2149.5
SI	248800.	258420.	248660.	282260.
AL	85120.	91150.	82260.	100350.
FE	63310.	40160.	108460.	54060.
MG	13320.	7600.	12480.	10240.
CA	6130.	6050.	8100.	6050.
NA	31100.	14500.	30400.	16000.
K	13460.	13690.	11010.	74130.
TI	6050.	6020.	5660.	6290.
MN	880.	500.	800.	530.
BA	540.	480.	360.	400.
CO	76.	68.	88.	56.
CU	62.	65.	71.	50.
GA	24.	26.	19.	47.
LI	40.	25.	28.	27.
MO	0.	0.	0.	1.
PB	12.	8.	10.	17.
RB	99.	125.	86.	92.
S	357.	155.	160.	43.
SR	165.	200.	174.	200.
CH20	77400.	60200.	109100.	40900.
ZN	142.	116.	147.	99.
ZR	177.	190.	353.	216.
V	260.	200.	180.	180.
NI	103.	76.	90.	62.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-673 2149.5-2150.5	ST-674 2150.5-2151.0	ST-675 2151.0-2152.0	ST-676 2152.0-2153.0
SI	273650.	292490.	279160.	281020.
AL	92050.	93470.	95030.	90300.
FE	59010.	55980.	51480.	55890.
MG	12620.	11600.	13480.	9960.
CA	6100.	6250.	6150.	6080.
NA	17400.	14900.	12400.	14200.
K	15650.	15200.	16040.	13820.
TI	6420.	6390.	6470.	6140.
MN	530.	660.	550.	510.
BA	460.	460.	440.	440.
CO	76.	60.	66.	68.
CU	60.	57.	60.	47.
GA	28.	24.	22.	25.
LI	35.	45.	32.	27.
MO	9.	1.	2.	1.
PR	71.	6.	11.	5.
RB	109.	39.	114.	96.
S	135.	38.	149.	69.
SR	196.	189.	198.	205.
CO&H2O	52200.	45800.	57400.	39400.
ZN	130.	122.	129.	104.
ZR	217.	208.	202.	235.
V	220.	230.	200.	160.
NI	94.	75.	72.	76.

OLDMAN FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-677 2153.0-2154.0	ST-678 2154.0-2161.0	ST-679 2161.0-2162.0	ST-680 2162.0-2163.5
SI	276590.	256240.	271740.	271270.
AL	91550.	89800.	101940.	94740.
FE	52920.	36520.	51360.	48870.
MG	11040.	8360.	11400.	10220.
CA	6150.	31420.	6140.	6530.
NA	12800.	16700.	11500.	14800.
K	14140.	10030.	13280.	12380.
TI	6210.	3650.	6300.	5390.
MN	570.	1000.	610.	670.
BA	420.	420.	440.	520.
CO	60.	54.	62.	54.
CU	54.	24.	47.	27.
GA	23.	25.	27.	20.
LI	32.	19.	32.	21.
MO	1.	2.	2.	2.
PB	8.	4.	6.	9.
RB	100.	44.	94.	51.
S	170.	101.	135.	254.
SR	202.	202.	201.	179.
CGH2O	49300.	20400.	48400.	28300.
ZN	108.	64.	106.	84.
ZR	202.	188.	195.	164.
V	180.	120.	180.	120.
NI	72.	58.	80.	50.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-683 2166.0-2166.5	ST-684 2166.5-2167.5	ST-685 2167.5-2169.0	ST-686 2169.0-2172.0
SI	289700.	284430.	266270.	269740.
AL	89000.	89900.	88630.	85950.
FE	36960.	38650.	41390.	45180.
MG	10600.	10500.	9140.	12720.
CA	5920.	5930.	6070.	7150.
NA	11500.	11500.	12200.	11500.
K	12540.	13730.	11260.	12790.
TI	5220.	5400.	5640.	5740.
MN	470.	460.	470.	600.
BA	403.	740.	720.	820.
CO	49.	57.	64.	60.
CU	34.	61.	38.	38.
GA	23.	23.	25.	17.
LI	19.	16.	25.	28.
MO	1.	2.	2.	1.
PB	9.	12.	19.	9.
RB	309.	127.	105.	99.
S	158.	287.	354.	212.
SR	197.	183.	186.	190.
CH ₂ O	51400.	57500.	54200.	63700.
ZN	36.	72.	90.	90.
ZR	181.	160.	104.	181.
V	105.	160.	140.	160.
NI	52.	84.	76.	80.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-687 2172.0-2173.5	ST-688 2173.5-2176.5	ST-689 2176.5-2178.0	ST-690 2178.0-2178.5
SI	264280.	249260.	267840.	261700.
AL	95080.	96520.	91750.	87090.
FE	55230.	51430.	53920.	51480.
MG	11700.	14500.	10700.	16980.
CA	5230.	6110.	6400.	6490.
NA	12800.	12200.	15500.	12700.
K	12960.	12620.	12500.	12710.
TI	6020.	6180.	6030.	6450.
MN	530.	540.	740.	590.
BA	600.	760.	560.	720.
CO	64.	76.	68.	70.
CU	45.	50.	48.	50.
GA	17.	22.	21.	16.
LI	29.	27.	26.	31.
MO	2.	2.	1.	2.
PB	5.	15.	3.	8.
RB	69.	93.	62.	64.
S	134.	506.	135.	271.
SR	200.	193.	191.	184.
CH2O	48300.	98000.	47300.	105700.
ZN	99.	115.	100.	108.
ZR	208.	174.	202.	179.
V	160.	240.	140.	200.
NI	76.	110.	88.	96.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-692 2179.0-2181.5	ST-693 2181.5-2183.5	ST-694 2183.5-2184.0	ST-695 2184.0-2186.0
SI	287250.	27295.	274810.	259600.
AL	84960.	83000.	86470.	92690.
FE	34140.	45190.	42900.	74500.
MG	6760.	13320.	9300.	14180.
CA	5980.	8010.	7950.	9660.
NA	11500.	11200.	12700.	14200.
K	10880.	9880.	8690.	10630.
TI	5,60.	4590.	4700.	5460.
MN	450.	680.	750.	1070.
BA	540.	620.	440.	720.
CO	50.	50.	54.	55.
CU	35.	30.	34.	30.
GA	16.	16.	15.	21.
LI	16.	19.	16.	20.
MO	2.	2.	2.	3.
PR	7.	17.	18.	17.
RB	30.	55.	52.	61.
S	153.	178.	325.	221.
SR	190.	187.	165.	210.
SH20	63800.	43000.	67000.	54400.
ZN	31.	72.	56.	94.
ZR	172.	194.	204.	240.
V	160.	100.	100.	140.
NI	52.	56.	58.	64.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-696 2186.0-2187.5	ST-698 2188.0-2189.0	ST-699 2189.0-2193.0	ST-700 2193.0-2194.0
SI	235930.	249570.	272500.	271760.
AL	92590.	100580.	89550.	97940.
FE	51130.	62910.	41920.	46100.
MG	15740.	7340.	8860.	14820.
CA	6400.	6140.	5950.	6040.
NA	12000.	11500.	15000.	14200.
K	10630.	7970.	11400.	13160.
TI	5550.	5620.	6180.	6430.
MN	1370.	480.	490.	500.
BA	850.	580.	800.	800.
CO	66.	54.	76.	58.
CU	60.	34.	41.	55.
GA	33.	24.	28.	26.
LI	26.	22.	17.	21.
MO	4.	1.	1.	2.
PB	19.	10.	20.	15.
SR	88.	98.	101.	101.
S	179.	63.	190.	93.
SR	222.	208.	224.	216.
H ₂ O	91600.	85600.	58800.	60700.
ZN	291.	35.	86.	130.
ZR	300.	150.	139.	204.
V	222.	160.	220.	220.
NI	110.	50.	86.	70.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-701 2194.0-2196.0	ST-702 2196.0-2199.5	ST-703 2199.5-2201.5	ST-704 2201.5-2203.0
SI	265870.	271310.	266260.	281670.
AL	92150.	91350.	92960.	98030.
FE	53290.	41780.	48540.	46350.
MG	7380.	13940.	9120.	15720.
CA	6140.	6680.	6130.	6170.
NA	13500.	12700.	12900.	13700.
K	9550.	5760.	12680.	14270.
TI	5310.	6100.	5740.	6150.
MN	490.	680.	470.	490.
BA	600.	720.	560.	740.
CO	60.	62.	52.	76.
CU	25.	49.	34.	68.
GA	16.	22.	23.	22.
LI	17.	24.	16.	21.
MO	1.	0.	2.	1.
PB	10.	14.	21.	25.
RB	60.	93.	119.	109.
S	120.	53.	96.	108.
SR	210.	226.	237.	223.
CaH2O	56500.	65200.	59700.	59000.
ZN	86.	123.	130.	115.
ZR	181.	190.	175.	167.
V	140.	320.	220.	200.
NI	70.	70.	54.	88.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-705 2203.0-2209.0	ST-706 2209.0-2213.0	ST-707 2213.0-2214.0	ST-708 2214.0-2218.5
SI	266570.	257440.	222790.	254910.
AL	93430.	91020.	68270.	94360.
FE	53140.	51750.	46930.	37550.
MG	13480.	19530.	3860.	12180.
CA	7140.	22870.	74080.	24340.
NA	16600.	19200.	12100.	21200.
K	12370.	9010.	8770.	6910.
TI	6150.	5280.	3850.	7990.
MN	590.	750.	1330.	1140.
RA	600.	660.	500.	580.
CO	62.	56.	52.	52.
CU	49.	39.	42.	19.
GA	21.	21.	20.	18.
LI	25.	19.	19.	14.
MO	3.	2.	2.	2.
PR	12.	10.	0.	20.
RB	72.	41.	51.	33.
S	152.	7.	196.	0.
SR	247.	292.	289.	208.
CH ₂ O	48300.	28800.	71800.	18500.
ZN	102.	76.	65.	78.
ZR	204.	202.	251.	191.
V	180.	170.	160.	160.
NI	82.	68.	66.	64.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	SI-709 2218.5-2219.5	SI-710 2219.5-2226.0	SI-711 2226.0-2227.0	SI-712 2227.0-2232.5
SI	229960.	252170.	263860.	273140.
AL	71380.	81180.	84280.	87510.
FE	55990.	60680.	61110.	69690.
MG	64368.	9440.	16523.	18700.
CA	76590.	8560.	7100.	10280.
NA	14350.	19100.	12300.	18200.
K	7433.	9480.	12350.	12050.
TI	4250.	5640.	5820.	5820.
MN	1620.	820.	880.	1050.
BA	930.	480.	560.	680.
CO	90.	58.	62.	64.
CU	31.	22.	60.	53.
GA	23.	12.	24.	25.
LI	18.	19.	27.	25.
MO	3.	1.	0.	0.
PR	8.	32.	6.	12.
RB	25.	35.	80.	49.
S	112.	276.	156.	53.
SR	279.	262.	220.	276.
SH20	40800.	29010.	65800.	51600.
ZN	72.	76.	121.	113.
ZR	278.	316.	209.	255.
V	160.	140.	180.	180.
NI	112.	30.	96.	80.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-718 2242.5-2244.0	ST-719 2244.0-2246.0	ST-720 2246.0-2247.0	ST-721 2247.0-2248.0
SI	274460.	183960.	284230.	276670.
AL	79440.	81240.	96850.	85120.
FE	53950.	56560.	52900.	40580.
MG	8340.	13040.	10240.	7200.
CA	6330.	6640.	6290.	6140.
NA	14400.	15700.	13500.	14500.
K	7420.	10910.	13460.	9740.
TI	5460.	5800.	5730.	5880.
MN	610.	620.	500.	490.
BA	460.	500.	440.	420.
CO	44.	62.	56.	52.
CU	41.	52.	56.	39.
GA	16.	17.	20.	13.
LI	13.	22.	21.	16.
MO	2.	1.	2.	1.
PB	6.	7.	4.	7.
RB	57.	82.	90.	69.
S	83.	170.	129.	197.
SR	269.	257.	249.	235.
C&H2O	62700.	65400.	62800.	62000.
ZN	54.	106.	99.	84.
ZR	187.	206.	207.	186.
V	180.	220.	220.	200.
NI	52.	80.	74.	54.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-722 2248.0-2252.5	ST-723 2252.5-2255.5	ST-724 2255.5-2256.5	ST-725 2256.5-2259.5
SI	268630.	243510.	233420.	266510.
AL	81610.	78350.	92590.	90000.
FE	44310.	67060.	56330.	52290.
MG	11760.	9300.	13460.	11920.
CA	6140.	10070.	7140.	6330.
NA	24100.	13800.	12400.	13800.
K	9910.	11360.	6010.	11530.
TI	5850.	5460.	5360.	6010.
MN	500.	1050.	760.	520.
BA	440.	440.	560.	500.
CO	66.	70.	68.	58.
CU	32.	58.	44.	24.
GA	15.	22.	32.	24.
LI	21.	21.	22.	22.
MO	2.	2.	13.	0.
PB	5.	5.	15.	8.
RB	83.	79.	30.	82.
S	316.	58.	132.	138.
SR	244.	280.	301.	230.
C&H2O	47900.	55600.	69700.	64600.
ZN	58.	106.	95.	104.
ZR	186.	236.	256.	192.
V	220.	340.	260.	240.
NI	84.	78.	98.	72.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-726 2259.5-2261.0	ST-727 2261.0-2265.5	ST-728 2265.5-2266.5	ST-729 2266.5-2271.0
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SI	269550.	262900.	264680.	271010.
AL	84640.	88890.	86370.	90800.
FE	43400.	53840.	55390.	62720.
MG	11360.	12940.	9780.	9360.
CA	6200.	6640.	6370.	7010.
NA	12760.	14100.	14900.	15600.
K	10630.	9560.	10400.	10440.
TI	6080.	5650.	6000.	5930.
MN	640.	620.	730.	1140.
BA	660.	620.	500.	580.
CO	50.	58.	62.	60.
CU	86.	48.	55.	49.
GA	21.	25.	25.	28.
LI	16.	17.	19.	20.
MO	0.	0.	2.	1.
PB	3.	18.	5.	11.
RB	87.	60.	84.	63.
S	131.	69.	73.	102.
SR	235.	255.	249.	255.
CGH2O	54300.	43900.	54300.	60000.
ZN	86.	86.	100.	88.
ZR	193.	223.	221.	231.
V	220.	180.	200.	200.
NI	60.	66.	84.	70.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-720 2271.0-2275.5	ST-731 2275.5-2279.0	ST-732 2279.0-2279.5	ST-733 2279.5-2281.0
SI	253790.	254470.	258580.	257710.
AL	82470.	83220.	88380.	83960.
FE	56130.	57630.	60460.	54300.
MG	4340.	13960.	18200.	12700.
CA	7780.	6330.	6700.	6710.
NA	16000.	11500.	15500.	13200.
K	8730.	12590.	10750.	13030.
TI	5390.	6040.	5840.	6080.
MN	860.	580.	540.	790.
BA	580.	760.	720.	640.
CO	52.	62.	62.	60.
CU	42.	39.	48.	47.
GA	24.	33.	41.	29.
LI	18.	19.	21.	24.
MO	1.	1.	1.	1.
PB	31.	18.	19.	15.
RB	51.	92.	82.	101.
S	140.	59.	61.	78.
SR	285.	253.	335.	258.
C&H2O	43400.	54300.	45800.	57000.
ZN	77.	84.	135.	127.
ZR	215.	217.	270.	205.
V	160.	220.	180.	240.
NI	72.	72.	66.	56.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-734 2281.0-2286.5	ST-735 2286.5-2289.0	ST-736 2289.0-2292.0	ST-737 2292.0-2297.5
SI	259840.	256910.	283520.	258200.
AL	88120.	84060.	84170.	86320.
FE	55280.	52970.	34890.	58350.
MG	15480.	19080.	5960.	12540.
CA	6200.	6370.	6070.	6280.
NA	14600.	12800.	15200.	12900.
K	13170.	11760.	10620.	10360.
TI	6190.	6400.	6440.	6250.
MN	610.	660.	470.	610.
BA	740.	740.	440.	480.
CO	64.	80.	50.	66.
CU	51.	46.	2.	64.
GA	100.	27.	20.	30.
LI	27.	29.	17.	34.
MO	1.	1.	1.	1.
PB	35.	29.	9.	11.
RB	101.	86.	80.	90.
S	106.	226.	16.	145.
SR	240.	209.	215.	227.
COH2O	55500.	70900.	49500.	60500.
ZN	116.	146.	58.	134.
ZR	201.	186.	167.	204.
V	220.	220.	180.	200.
NI	60.	110.	38.	70.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-738 2297.5-2298.0	ST-739 2298.0-2299.5	ST-740 2298.5-2301.0	ST-741 2301.0-2302.7
SI	253860.	259400.	239030.	259360.
AL	84490.	92000.	78070.	86270.
FE	54990.	51240.	106840.	58720.
MG	10760.	8200.	9800.	12200.
CA	7070.	8260.	8730.	6740.
NA	16500.	17300.	17800.	15500.
K	10570.	9150.	9330.	10780.
TI	5980.	5160.	5390.	6140.
MN	810.	690.	3200.	890.
BA	480.	440.	420.	420.
CO	60.	56.	58.	64.
CU	42.	34.	59.	53.
GA	19.	15.	21.	20.
LI	26.	21.	21.	25.
MO	2.	0.	0.	1.
PB	6.	14.	20.	13.
RB	76.	50.	66.	79.
S	155.	102.	221.	151.
SR	237.	237.	219.	224.
C&H2O	46400.	38000.	49500.	53100.
ZN	90.	85.	104.	99.
ZR	229.	201.	349.	235.
V	160.	140.	140.	180.
NI	52.	44.	52.	60.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-742 2302.7-2303.0	ST-743 2303.0-2304.0	ST-744 2304.0-2310.0	ST-745 2310.0-2315.0
SI	25920.	267940.	273340.	27050.
AL	82950.	87350.	87150.	87660.
FE	41990.	43760.	62200.	51880.
MG	9500.	9420.	10660.	10400.
CA	6300.	6040.	9440.	7980.
NA	13500.	14900.	17900.	13500.
K	10930.	12360.	10590.	9580.
TI	5780.	6000.	5780.	5660.
MN	530.	490.	820.	640.
BA	440.	460.	420.	400.
CO	56.	50.	60.	72.
CU	40.	46.	50.	39.
GA	18.	19.	20.	20.
LI	21.	19.	20.	23.
MO	0.	0.	0.	1.
PB	12.	5.	12.	26.
RB	82.	92.	70.	52.
S	449.	86.	85.	183.
SR	221.	221.	253.	251.
C&H2O	71100.	53200.	42400.	113900.
ZN	81.	100.	84.	84.
ZR	164.	184.	230.	212.
V	200.	220.	180.	160.
NI	48.	42.	56.	66.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-746 2315.0-2319.0	ST-747 2319.0-2324.0	ST-748 2324.0-2325.0	ST-749 2325.0-2325.5
SI	292070.	256430.	283450.	127180.
AL	90350.	83640.	93230.	25680.
FE	39130.	45130.	48820.	94810.
MG	6140.	7600.	10700.	8880.
CA	17680.	52860.	8150.	65270.
NA	20400.	19800.	19200.	5800.
K	7550.	7700.	12410.	3670.
TI	4650.	5520.	5880.	1200.
MN	1070.	970.	570.	116090.
BA	420.	440.	460.	440.
CO	54.	54.	58.	62.
CU	20.	28.	40.	24.
GA	17.	18.	24.	6.
LI	15.	14.	18.	6.
MO	1.	1.	0.	0.
PB	19.	15.	13.	1.
RB	32.	23.	58.	0.
S	114.	122.	237.	125.
SR	210.	298.	307.	346.
CO&H2O	19000.	24200.	47400.	107500.
ZN	61.	66.	97.	15.
ZR	198.	249.	211.	375.
V	160.	160.	220.	140.
NI	40.	44.	48.	46.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-750 2325.5-2326.0	ST-751 2326.0-2326.5	ST-752 2326.5-2328.0	ST-753 2328.0-2333.0
SI	272530.	269470.	265860.	264590.
AL	91350.	91650.	91200.	92740.
FE	46610.	35630.	59410.	52180.
MG	9780.	7140.	11320.	9800.
CA	7610.	31620.	7140.	12470.
NA	16400.	17300.	13700.	19500.
K	13720.	7360.	13060.	9860.
TI	5870.	6720.	6140.	6210.
MN	610.	1490.	900.	830.
BA	540.	460.	480.	420.
CO	58.	52.	60.	58.
CU	49.	11.	48.	27.
GA	22.	18.	21.	20.
LI	17.	14.	21.	20.
MO	0.	2.	0.	3.
PB	10.	17.	6.	10.
RB	87.	22.	52.	24.
S	165.	86.	119.	89.
SR	269.	224.	262.	230.
C&H20	59100.	17200.	54800.	2990.
ZN	87.	51.	106.	85.
ZR	195.	277.	163.	172.
V	200.	145.	220.	160.
NI	52.	38.	50.	42.

FURFURST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-754 2333.0-2335.0	ST-755 2335.0-2337.0	ST-756 2337.0-2339.0	ST-757 2339.0-2342.0
SI	274450.	270920.	272810.	244090.
AL	89390.	92000.	91050.	77800.
FE	45770.	41060.	43990.	81810.
MG	3560.	11560.	9460.	9060.
CA	6600.	6230.	6300.	35150.
NA	14800.	14900.	16400.	18100.
K	11000.	12120.	13350.	10060.
TI	5690.	6070.	5860.	4990.
MN	480.	490.	500.	2340.
BA	500.	540.	540.	480.
CO	42.	54.	46.	48.
CU	37.	48.	41.	58.
GA	22.	21.	21.	20.
LI	16.	21.	17.	16.
MO	1.	1.	1.	0.
PB	10.	18.	5.	5.
RB	49.	51.	51.	35.
S	128.	212.	138.	115.
SR	261.	228.	243.	338.
CO ₂	44700.	51800.	43400.	28400.
ZN	100.	96.	82.	102.
ZR	169.	166.	161.	162.
V	200.	200.	160.	180.
NI	36.	50.	32.	42.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-758 2342.0-2344.0	ST-759 2344.0-2345.0	ST-760 2345.0-2349.0	ST-761 2349.0-2351.5
SI	254640.	271160.	276670.	264040.
AL	85170.	92300.	92640.	87400.
FE	52570.	48820.	43560.	51480.
MG	11960.	10540.	9280.	13440.
CA	24390.	7120.	6610.	8390.
NA	12200.	17800.	17800.	18800.
K	9570.	12780.	12660.	10500.
TI	7190.	5980.	5900.	5880.
MN	1130.	570.	640.	560.
BA	540.	500.	560.	560.
CO	64.	48.	46.	58.
CU	34.	50.	42.	45.
GA	21.	16.	15.	18.
LI	21.	20.	17.	22.
MO	3.	1.	2.	3.
PB	12.	4.	6.	18.
RB	24.	0.	0.	0.
S	108.	85.	141.	174.
SR	205.	243.	252.	288.
CGH2O	70900.	44300.	42000.	38300.
ZN	95.	87.	85.	91.
ZR	110.	165.	167.	174.
V	180.	160.	120.	120.
NI	56.	46.	40.	53.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-762 2351.5-2352.0	ST-763 2352.0-2357.0	ST-764 2357.0-2361.5	ST-765 2361.5-2362.5
SI	262550.	258970.	265920.	275050.
AL	91250.	81020.	85640.	92100.
FE	56150.	38500.	55430.	39300.
MG	17920.	6280.	10300.	20020.
CA	3220.	56870.	8510.	6450.
NA	17200.	16300.	17900.	13800.
K	11760.	8640.	9080.	12410.
TI	6240.	4360.	5860.	5920.
MN	590.	1420.	660.	500.
BA	640.	440.	500.	880.
CO	58.	46.	50.	66.
CU	47.	25.	36.	44.
GA	21.	13.	14.	18.
LI	25.	15.	21.	19.
MO	2.	1.	1.	1.
PB	9.	11.	21.	15.
RB	0.	0.	0.	0.
S	174.	146.	113.	260.
SR	265.	304.	228.	232.
CGH20	46400.	19100.	29800.	53500.
ZN	108.	66.	71.	94.
ZR	173.	138.	167.	151.
V	140.	100.	120.	160.
NI	56.	42.	44.	70.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-766 2362.5-2364.5	ST-767 2364.5-2369.0	ST-768 2369.0-2370.0	ST-769 2370.0-2371.0
SI	274850.	273940.	288910.	266420.
AL	85900.	93620.	83750.	96420.
FE	42560.	54410.	27290.	53050.
MG	11540.	10420.	5440.	8630.
CA	6570.	6540.	6030.	6210.
NA	16100.	13900.	11800.	11800.
K	11350.	12790.	10590.	17490.
TI	6140.	6340.	6510.	6440.
MN	960.	710.	480.	520.
BA	680.	560.	500.	560.
CO	50.	56.	40.	48.
CU	38.	52.	35.	66.
GA	22.	20.	19.	23.
LI	16.	27.	14.	20.
MO	1.	1.	0.	0.
PB	21.	48.	31.	75.
RB	74.	81.	82.	123.
S	158.	109.	67.	135.
SR	226.	214.	185.	247.
CGH2O	61900.	57400.	45300.	61900.
ZN	67.	104.	56.	71.
ZR	151.	145.	151.	142.
V	130.	160.	140.	240.
NI	50.	68.	36.	62.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-770 2371.0-2372.5	ST-771 2372.5-2374.0	ST-772 2374.0-2375.5	ST-773 2375.5-2377.0
SI	269320.	269700.	255870.	255900.
AL	93870.	91900.	91400.	94160.
FE	59080.	46140.	62440.	59680.
MG	7940.	7920.	9880.	13180.
CA	6490.	6330.	8510.	6720.
NA	13300.	13400.	15800.	14000.
K	13830.	14400.	10610.	13530.
TI	6230.	6190.	6770.	6430.
MN	1450.	680.	670.	770.
BA	540.	540.	460.	500.
CO	110.	52.	56.	72.
CU	55.	50.	31.	35.
GA	24.	23.	26.	26.
LI	20.	20.	22.	32.
MO	2.	0.	2.	1.
PB	23.	14.	6.	27.
RB	103.	97.	45.	87.
S	283.	296.	222.	217.
SR	252.	241.	259.	233.
C&H2O	65400.	62400.	34400.	60700.
ZN	212.	113.	113.	135.
ZR	150.	158.	189.	148.
V	220.	200.	180.	200.
NI	136.	64.	54.	84.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-774 2377.0-2377.5	ST-775 2377.5-2379.0	ST-776 2379.0-2380.0	ST-777 2380.0-2383.5
SI	263280.	257550.	271940.	263970.
AL	95320.	87450.	98220.	89550.
FE	60360.	49170.	62910.	48310.
MG	9380.	10160.	11360.	8380.
CA	6650.	6420.	6690.	6540.
NA	12500.	14300.	15400.	15300.
K	12770.	13210.	13330.	11350.
TI	6290.	6400.	6360.	6080.
MN	1570.	530.	990.	720.
BA	540.	520.	460.	480.
CO	58.	54.	70.	56.
CU	54.	61.	41.	41.
GA	21.	21.	10.	19.
LI	22.	25.	26.	20.
MO	1.	1.	1.	0.
PP	9.	7.	12.	10.
RB	74.	72.	68.	65.
S	124.	132.	105.	114.
SR	251.	237.	228.	228.
C&H2O	63200.	56500.	48400.	48500.
ZN	125.	128.	109.	97.
ZR	152.	150.	159.	151.
V	220.	240.	300.	160.
NI	60.	50.	80.	54.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-773 2383.5-2385.5	ST-779 2385.5-2387.0	ST-780 2387.0-2389.0	ST-781 2389.0-2389.5
SI	267140.	267050.	283520.	260580.
AL	89850.	91750.	89240.	94010.
FE	55830.	55440.	26630.	62150.
MG	11220.	8760.	5040.	11120.
CA	6930.	8490.	6120.	6520.
NA	14100.	15600.	14100.	16300.
K	10400.	10000.	9400.	14720.
TI	5930.	7080.	6370.	6010.
MN	610.	740.	460.	530.
BA	480.	400.	500.	520.
CO	70.	50.	46.	70.
CU	41.	31.	27.	108.
GA	21.	19.	13.	27.
LI	24.	21.	14.	22.
MO	2.	1.	2.	1.
PR	4.	18.	14.	28.
RB	51.	47.	52.	67.
S	161.	114.	76.	102.
SR	216.	204.	193.	240.
C&H2O	35100.	29100.	43700.	46000.
ZN	86.	79.	49.	126.
ZR	164.	182.	118.	145.
V	180.	140.	120.	200.
NI	72.	54.	32.	74.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-782 2389.5-2391.0	ST-783 2391.0-2391.5	ST-784 2391.5-2392.0	ST-785 2392.0-2393.5
SI	259470.	265770.	261440.	265130.
AL	94010.	94450.	94310.	92640.
FF	64580.	63470.	53630.	53140.
MG	11620.	12480.	9920.	8700.
CA	6430.	6640.	6420.	7090.
NA	13000.	13800.	14000.	16300.
K	15240.	12800.	14150.	10960.
TI	6300.	6070.	5920.	5530.
MN	540.	570.	520.	590.
BA	540.	520.	500.	480.
CO	64.	46.	38.	42.
CU	48.	44.	40.	32.
GA	25.	21.	25.	7.
LI	26.	25.	22.	20.
MO	0.	1.	1.	2.
PB	22.	26.	17.	24.
RB	68.	58.	67.	37.
S	77.	100.	113.	148.
SR	238.	231.	242.	257.
C&H2O	52000.	44300.	52700.	41800.
ZN	107.	110.	84.	80.
ZR	425.	149.	136.	141.
V	220.	180.	200.	180.
NI	66.	60.	48.	46.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-786 2393.5-2394.0	ST-787 2394.0-2394.5	ST-788 2394.5-2396.5	ST-789 2396.5-2399.0
SI	260220.	260950.	256920.	259900.
AL	94260.	91350.	91300.	94500.
FE	39470.	43910.	59440.	63730.
MG	7700.	8380.	10260.	7560.
CA	6170.	6360.	6180.	6500.
NA	15200.	14200.	14400.	16000.
K	12230.	13040.	14610.	12900.
TI	5900.	6030.	6150.	6250.
MN	500.	570.	500.	840.
BA	500.	520.	540.	520.
CO	64.	42.	102.	64.
CU	47.	45.	49.	45.
GA	25.	29.	28.	26.
LI	19.	19.	20.	16.
MO	2.	2.	3.	2.
PB	15.	4.	38.	24.
RB	74.	88.	87.	76.
S	161.	43.	69.	27.
SR	233.	243.	246.	243.
C&H2O	57900.	62500.	56400.	59500.
ZN	91.	111.	109.	114.
ZR	135.	163.	158.	180.
V	220.	220.	220.	190.
NI	64.	46.	64.	72.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-790 2399.0-2400.0	ST-791 2400.0-2402.5	ST-792 2402.5-2403.5	ST-793 2403.5-2405.0
SI	256650.	257600.	244100.	252880.
AL	91300.	89140.	84960.	88790.
FE	70590.	71070.	54160.	56640.
MG	12680.	9520.	11320.	10160.
CA	6320.	6530.	6350.	6360.
NA	13200.	14400.	13600.	14300.
K	14140.	11940.	13760.	14780.
TI	6230.	5900.	6150.	6000.
MN	550.	600.	600.	810.
BA	500.	460.	540.	560.
CO	50.	40.	46.	42.
CU	50.	29.	51.	53.
GA	33.	26.	23.	30.
LI	28.	21.	26.	22.
MO	2.	3.	4.	3.
PB	26.	3.	16.	4.
RB	81.	61.	89.	96.
S	64.	98.	67.	92.
SR	228.	243.	241.	249.
CGH2O	56800.	41800.	59800.	57300.
ZN	122.	92.	117.	106.
ZR	158.	170.	154.	156.
V	240.	160.	220.	180.
NI	62.	56.	78.	64.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-794 2405.0-2406.5	ST-795 2406.5-2407.5	ST-796 2407.5-2410.0	ST-797 2410.0-2416.0
SI	250460.	250140.	256630.	250200.
AL	86730.	87760.	88120.	95370.
FE	59490.	59200.	56330.	45900.
MG	10960.	12640.	11760.	6840.
CA	6660.	6420.	6460.	7620.
NA	14900.	14600.	13900.	21200.
K	14320.	13490.	14320.	7600.
TI	6140.	6090.	6220.	5670.
MN	1170.	620.	590.	580.
BA	520.	500.	620.	440.
CO	48.	60.	46.	34.
CU	57.	61.	51.	17.
GA	15.	16.	20.	14.
LI	23.	23.	24.	15.
MO	1.	2.	1.	1.
PB	27.	25.	17.	18.
RB	68.	63.	63.	21.
S	192.	192.	175.	90.
SR	225.	219.	238.	153.
C&H2O	61500.	60900.	55300.	14600.
ZN	111.	116.	110.	64.
ZR	150.	148.	148.	138.
V	200.	200.	200.	120.
NI	66.	126.	64.	44.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-798 2416.0-2419.0	ST-799 2419.0-2425.0	ST-800 2425.0-2427.0	ST-801 2427.0-2428.0
SI	249390.	255620.	230770.	260060.
AL	96380.	84220.	47200.	79440.
FE	42850.	50730.	52850.	37760.
MG	5680.	8300.	5160.	6360.
CA	23880.	7330.	60790.	16940.
NA	18500.	20700.	13000.	16400.
K	7280.	8400.	6230.	8870.
TI	5560.	5590.	4350.	5270.
MN	940.	530.	2290.	820.
BA	480.	420.	460.	540.
CO	32.	34.	44.	40.
CU	23.	22.	26.	23.
GA	10.	14.	13.	18.
LI	14.	16.	10.	12.
MO	0.	1.	1.	5.
PR	41.	37.	60.	37.
RB	24.	18.	11.	37.
S	148.	122.	144.	43.
SR	186.	218.	318.	293.
C&H2O	23900.	26400.	35800.	40000.
ZN	65.	61.	42.	54.
ZR	126.	155.	155.	151.
V	120.	100.	80.	100.
NI	44.	44.	46.	48.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-802 2428.0-2431.0	ST-803 2431.0-2431.5	ST-804 2431.5-2432.5	ST-805 2432.5-2434.0
SI	248480.	190310.	254120.	240330.
AL	83910.	45210.	94790.	79990.
FE	49500.	47780.	56160.	58900.
MG	5200.	3700.	12820.	9300.
CA	30240.	71690.	7670.	15740.
NA	19400.	22620.	13800.	20100.
K	6560.	4670.	13810.	8560.
TI	5020.	2500.	6110.	5480.
MN	1520.	470.	570.	990.
BA	440.	1460.	680.	480.
CD	34.	34.	38.	44.
CU	19.	13.	50.	28.
GA	18.	14.	31.	19.
LI	13.	8.	27.	19.
MD	4.	0.	4.	5.
PB	48.	32.	13.	17.
RB	4.	0.	67.	17.
S	0.	0.	45.	33.
SR	260.	1392.	252.	305.
C&H2O	17900.	52100.	55700.	25200.
ZN	44.	43.	99.	77.
ZR	132.	243.	149.	155.
V	80.	80.	180.	100.
NI	40.	48.	72.	68.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-806 2434.0-2435.5	ST-807 2435.5-2438.0	ST-808 2438.0-2439.5	ST-809 2439.5-2442.0
SI	251950.	236780.	253950.	258770.
AL	91700.	88270.	87810.	94940.
FE	52730.	57210.	59150.	43460.
MG	11620.	12280.	11900.	7560.
CA	6580.	6600.	7820.	6360.
NA	13100.	12600.	17600.	15500.
K	12510.	13410.	11740.	13790.
TI	5970.	5880.	6110.	5840.
MN	700.	720.	730.	460.
BA	640.	480.	520.	580.
CO	40.	42.	44.	36.
CU	58.	53.	45.	41.
GA	23.	28.	23.	17.
LI	20.	23.	23.	18.
MO	4.	4.	2.	1.
PB	19.	43.	21.	45.
RB	62.	78.	63.	82.
S	0.	73.	165.	135.
SR	243.	245.	251.	259.
C&H2O	49600.	58200.	54500.	54900.
ZN	91.	114.	104.	78.
ZR	149.	132.	161.	143.
V	160.	200.	240.	160.
NI	64.	68.	72.	60.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-810 2442.0-2444.0	ST-811 2444.0-2447.5	ST-812 2447.5-2449.0	ST-813 2449.0-2453.0
SI	248720.	256270.	239170.	256070.
AL	87090.	90250.	82950.	89750.
FE	58810.	56330.	58760.	55810.
MG	9220.	14320.	10700.	12340.
CA	12020.	6830.	7030.	6540.
NA	18600.	13400.	19400.	10300.
K	10720.	13550.	10960.	13310.
TI	5100.	6290.	5960.	6400.
MN	800.	620.	570.	570.
BA	520.	560.	560.	480.
CO	36.	50.	42.	58.
CU	36.	51.	41.	55.
GA	19.	22.	14.	19.
LI	16.	24.	23.	23.
MO	2.	1.	0.	1.
PB	34.	16.	15.	22.
RB	39.	69.	45.	75.
S	141.	137.	44.	92.
SR	300.	228.	251.	222.
C&H2O	32900.	48200.	34500.	52600.
ZN	93.	116.	103.	109.
ZR	144.	156.	161.	135.
V	120.	180.	160.	200.
NI	68.	72.	58.	90.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-814 2453.0-2455.0	ST-815 2455.0-2457.5	ST-816 2457.5-2466.0	ST-817 2466.0-2470.0
SI	249200.	264870.	255910.	255440.
AL	79120.	84540.	80260.	90200.
FE	53470.	40900.	35500.	56880.
MG	7640.	5940.	5200.	15940.
CA	11440.	6620.	55040.	7450.
NA	14630.	16800.	19400.	17500.
K	8440.	8270.	6680.	12890.
TI	5440.	6230.	4150.	6010.
MN	1000.	1630.	1540.	540.
BA	440.	440.	400.	680.
CO	40.	32.	32.	58.
CU	34.	22.	16.	43.
GA	17.	14.	13.	21.
LI	17.	14.	11.	21.
MO	1.	1.	1.	1.
PB	27.	3.	14.	2.
RB	38.	60.	22.	63.
S	142.	106.	194.	90.
SR	248.	235.	273.	283.
CGH2O	33800.	44800.	18800.	52900.
ZN	76.	60.	49.	127.
ZR	140.	158.	131.	158.
V	100.	140.	100.	180.
NI	50.	30.	40.	66.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-818 2470.0-2471.5	ST-819 2471.5-2475.0	ST-820 2475.0-2478.0	ST-821 2478.0-2479.5
SI	255290.	260040.	259740.	236160.
AL	83270.	89090.	91550.	83910.
FE	72390.	71820.	55890.	49450.
MG	10180.	11920.	15260.	12200.
CA	13080.	6890.	7380.	24540.
NA	21500.	12800.	16100.	16700.
K	8470.	13320.	13490.	7390.
TI	6180.	6170.	6220.	6010.
MN	920.	560.	610.	900.
BA	440.	520.	640.	520.
CO	46.	48.	50.	60.
CU	29.	45.	54.	24.
GA	13.	18.	22.	14.
LI	17.	20.	24.	20.
MO	0.	1.	0.	0.
PB	3.	12.	15.	10.
PB	28.	69.	65.	9.
S	128.	156.	128.	128.
SR	336.	263.	259.	302.
C&H2O	27000.	51800.	57900.	47900.
ZN	79.	112.	122.	58.
ZR	183.	151.	153.	154.
V	140.	220.	220.	180.
NI	56.	66.	70.	76.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-822 2479.5-2481.0	ST-823 2481.0-2486.0	ST-824 2486.0-2486.5	ST-825 2486.5-2488.0
SI	260850.	253770.	242270.	254780.
AL	94060.	94840.	87760.	85540.
FE	40020.	47270.	55400.	61490.
MG	7620.	8760.	11520.	9540.
CA	6820.	13970.	11330.	9760.
NA	16500.	22600.	17300.	21600.
K	11630.	9590.	9080.	8780.
TI	5280.	5880.	5430.	5420.
MN	680.	740.	560.	610.
BA	560.	540.	680.	520.
CO	36.	46.	52.	42.
CU	33.	29.	42.	27.
GA	20.	26.	19.	23.
LI	11.	15.	17.	18.
MO	0.	0.	0.	0.
PB	9.	22.	66.	28.
RB	55.	12.	5.	6.
S	22.	119.	386.	59.
SR	269.	225.	359.	332.
C&H2O	55300.	33400.	85200.	29500.
ZN	50.	79.	82.	73.
ZR	143.	140.	170.	158.
V	200.	140.	200.	180.
NI	36.	54.	64.	48.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-826 2488.0-2491.0	ST-827 2491.0-2493.0	ST-828 2493.0-2498.5	ST-829 2498.5-2503.5
SI	255120.	268140.	241880.	251420.
AL	87870.	81880.	92100.	91050.
FE	55680.	31970.	40220.	37270.
MG	11520.	6660.	7420.	7120.
CA	7380.	6540.	14400.	10210.
NA	15300.	15900.	24600.	21500.
K	12300.	9190.	8590.	8080.
TI	6060.	5730.	6250.	6630.
MN	620.	470.	720.	570.
BA	480.	516.	500.	580.
CO	50.	36.	46.	46.
CU	46.	26.	25.	23.
GA	29.	19.	25.	18.
LI	18.	10.	12.	11.
MO	0.	1.	1.	0.
PB	18.	8.	15.	22.
RB	44.	32.	11.	11.
S	136.	76.	174.	166.
SR	276.	245.	333.	290.
C&H2O	51500.	40900.	24700.	22700.
ZN	105.	63.	73.	67.
ZR	162.	160.	173.	135.
V	220.	180.	200.	200.
NI	64.	34.	52.	40.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-830 2503.5-2508.5	ST-831 2508.5-2515.0	ST-832 2515.0-2517.0	ST-833 2517.0-2520.0
SI	247100.	214650.	252400.	254920.
AL	85220.	64830.	86680.	85540.
FE	57890.	34650.	46990.	57810.
MG	7380.	6280.	9880.	10260.
CA	9160.	72620.	7080.	7630.
NA	24900.	14500.	9500.	18100.
K	10240.	6290.	10670.	11410.
TI	5570.	2890.	5640.	5650.
MN	640.	1790.	470.	510.
BA	600.	460.	580.	600.
CO	44.	44.	50.	54.
CU	40.	23.	43.	42.
GA	17.	11.	16.	15.
LI	13.	9.	10.	13.
MO	0.	0.	0.	0.
PB	19.	28.	10.	20.
RB	36.	4.	47.	49.
S	109.	12.	61.	38.
SR	268.	321.	269.	325.
C&H2O	19500.	15200.	52100.	46100.
ZN	87.	38.	42.	95.
ZR	146.	129.	137.	148.
V	180.	140.	220.	240.
NI	44.	42.	54.	64.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-834 2520.0-2525.0	ST-835 2525.0-2525.5	ST-836 2525.5-2531.0	ST-837 2531.0-2532.0
SI	246420.	235410.	249700.	254750.
AL	87660.	86890.	84590.	92690.
FE	53870.	67760.	58170.	54690.
MG	9400.	10860.	10260.	12900.
CA	11290.	11510.	16550.	7900.
NA	18100.	23500.	24700.	18000.
K	6970.	6640.	7210.	12160.
TI	6510.	5420.	7770.	6070.
MN	550.	750.	750.	660.
BA	820.	1140.	1020.	520.
CO	58.	68.	56.	60.
CU	27.	37.	30.	52.
GA	18.	17.	15.	18.
LI	13.	12.	14.	20.
MO	0.	0.	1.	1.
PB	28.	41.	35.	1.
BB	10.	12.	0.	54.
S	93.	418.	76.	65.
SR	373.	311.	364.	283.
C&H2O	25700.	49000.	24500.	49700.
ZN	68.	77.	95.	107.
ZR	173.	137.	224.	154.
V	220.	280.	240.	240.
NI	52.	60.	54.	72.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-838 2532.0-2533.5	ST-839 2533.5-2535.0	ST-840 2535.0-2537.0	ST-841 2537.0-2538.0
SI	258620.	260880.	253980.	263630.
AL	90200.	90250.	81340.	88530.
FE	56300.	59960.	52340.	34120.
MG	15008.	14560.	10740.	9040.
CA	7800.	7710.	26870.	6850.
NA	18600.	14700.	16600.	13800.
K	12160.	14450.	8990.	11450.
TI	5970.	6180.	6610.	6010.
MN	620.	610.	1200.	480.
BA	708.	680.	640.	740.
CO	41.	42.	32.	32.
CU	50.	60.	31.	43.
GA	15.	16.	14.	12.
LI	17.	23.	14.	12.
MO	1.	1.	1.	1.
PB	13.	16.	5.	21.
FB	45.	62.	16.	47.
S	19.	134.	20.	277.
SR	304.	274.	351.	246.
C&H2O	47000.	50800.	29600.	90200.
ZN	97.	123.	80.	49.
ZR	155.	146.	211.	139.
V	244.	280.	220.	240.
NI	68.	84.	62.	62.

FOREMOST FORMATION

ALL VALUES IN PARTS PER MILLION

	ST-843 2538.0-2538.7	ST-844 2539.0-2540.0	ST-845 2540.0-2541.0
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SI	261150.	255560.	25540.
AL	93970.	95230.	90400.
FE	55990.	52340.	51890.
MG	12240.	14820.	9860.
CA	6640.	6850.	7460.
NA	13900.	15380.	16700.
K	14780.	12620.	10470.
TI	6420.	6110.	5810.
MN	550.	610.	530.
BA	540.	760.	620.
CO	32.	44.	34.
CU	60.	43.	34.
GA	16.	20.	21.
LI	22.	18.	14.
MO	1.	0.	1.
PR	19.	15.	4.
PB	67.	46.	27.
S	185.	178.	75.
SR	256.	257.	297.
C&H2O	58100.	60900.	42800.
ZN	125.	98.	104.
ZR	155.	152.	163.
V	240.	240.	180.
NI	62.	96.	66.

Appendix 2

Classifications for the Standard Groups
Marine vs Continental-Brackish 24 Variables

SAMPLE SIZE GROUP
1 2 3
83
23

GROUP CON BRACK	MEANS	44679.15625	12478.55078	16309.51563	14432.11719	15161.68359	4718.07031
27600.43750	82933.43750	37.01204	31.19218	26.22882	12.33735	1.37349	22.38553
754.68873	754.68873	204.91565	79244.56250	86.20482	143.00000	165.30119	113.85541
92.65059	766.14453						
GROUP MARINE	MEANS	67647.56250	13566.79688	12624.79688	8608.00000	22158.79688	5093.19922
263710.75000	81248.00000	49.48000	32.35999	22.23999	133.59999	203.64600	24.39999
1005.19995	716.00000	141.59999	68660.00000	104.51999	133.59999	203.64600	172.71999
149.71999	855.43994						

POOLED DISPERSION MATRIX

ROW SI	679947008.00000	169606656.00000	-480516352.00000	-37897376.00000	-226522080.00000	22313800.00000	
	88354352.00000	-6154923.00000	-5639952.00000	1646958.00000	3276.56888	-241294.00000	
	48432.10938	31942.80078	2062.07959	-9595.14844	63695.00000	-116739.00000	
	-86851.06250	-276093952.00000	90396.00000	197521.62500	19856.81250	-116739.00000	
ROW AL	169606656.00000	106019776.00000	-170395766.00000	-6212583.00000	-99432320.00000	15799143.00000	
	28952894.00000	2847048.00000	-2271416.00000	216887.43750	41429.73438	-8605.00000	
	32045.91406	14641.12891	2061.34668	-12223.94822	21717.93750	-1313268.00000	
	-86680.56234	-11554549.00000	-41768.46875	-61148.98047	74698.25000	-355604.93750	
ROW FE	-170395766.00000	-170395766.00000	824346368.00000	648441264.00000	135343728.00000	-43071264.00000	
	-58589296.00000	-7947551.00000	8653642.00000	-890494.43750	32813	78698.00000	
	-39565.86719	-1230.10156	-7025.39844	28036.26172	-310236.06250	523591.00000	
	-372805.88750	256015952.00000	-82867.00000	-297148.06250	-344765.31250	2080256.00000	
ROW MG	-37897376.00000	-6212583.00000	648441264.00000	40584816.00000	9817160.00000	3083261.00000	
	-1223252.00000	-2224392.00000	727998.75000	887023.37500	19165.85547	-1504.51133	
	-5742.23961	-1649.63506	-612.34961	33427.90334	-76922.18750	2405198.00000	
	-60609.55469	71133792.00000	-27515.60156	-36393.44141	-48720.00781	170218.43750	
ROW CA	-99432320.00000	135343728.00000	135343728.00000	9817160.00000	199742704.00000	-10772847.00000	
	-3142298.00000	-4505438.00000	1811208.25000	-43979.66016	-52885.40663	-2336.73438	
	31742.94722	-30194.69331	-318.04346	-57087.43359	-376765.42500	-292843.00000	
	204732.93750	-122962416.00000	-87086.93750	-57533.38672	-2733534.62500	277038.43750	
ROW NA	15799143.00000	-43071264.00000	-43071264.00000	3083261.00000	-10772847.00000	48173712.00000	
	-882629.00000	284068.13750	-57286.25000	7177.50000	1786.54346	-1675.95679	
	69572.06250	27203832.00000	-19677.94688	-24033.60156	-377254.00000	-122354.00000	
				9543.97266	-23599.88203	-10041.56250	
ROW K	88354352.00000	-29952864.00000	-58589296.00000	-11223262.00000	-37452688.00000	-8626206.00000	
	6891728.00000	412687.95009	-519076.93750	583978.25000	34811.17578	3341.60156	
	233569.51663	-12603.12500	11972.25000	17063.18991	313803.67500	202945.00000	
	-12603.12500	-96607980.00000		53308.27344	238990.56250	-113229.31250	
ROW JI	6154923.00000	2847048.00000	-7947551.00000	-2224392.00000	-4503638.00000	284068.18750	
	4166800.00000	953908.13750	-5225.29178	-17232.37500	2254.44141	4133.36719	
	23375.86670	3048.76350	1728.52734	852.48460	24516.87500	7959.37500	
	-1011.60059	-4308410.00000		6492.73074	21623.83594	-1741.75391	
ROW MN	-5639952.00000	-2271410.00000	8653642.00000	727998.75000	1811208.00000	-572861.25000	
	-570078.93750	-52272.28125	140548.43750	-1037.09880	3281.1584	3998.96598	
	-494.76007	-256.28366	-108.54732	-1267.96850	-261.50001	7959.37500	
	-2782.53760	1488921.00000	-40.11182	-2666.11893	-3936.55420	22771.92198	
ROW BA	1646958.00000	219987.43750	-890494.43750	887023.37500	-43979.66016	71717.50000	
	583978.25000	-17523.37500	-3027.01880	625760.50000	2972.91700	4260.82022	
	18.73138	117.43790	-65.20282	7430.26172	1435.97072	4260.82022	
	-1533.16382	-1698828.00000	463.22803	447.39869	2283.44434	-381.61874	
ROW CO	32676.54688	41849.73438	7173.32813	19195.85547	-52885.40663	1786.54346	
	34811.17578	3254.44141	-16.93554	496.91602	126.59159	22.34290	
	26.70425	25.44954	0.000893	84.90852	280.51440	583.97620	
	-131.32045	82743.31250	110.18311	17.71158	74.45527	16.72901	
ROW CU	-12604.69531	-8605.73047	78998.00000	-1504.61133	-20336.73438	-1675.95679	
	33341.60156	4130.26719	1395.96558	-5.62420	22.64660	122.24950	
	13.949531	-21.67598	-2.31826	40.84300	175.24464	72.52200	
	-86.22597	864.85547	184.11195	24.92940	273.65405	236.01540	

ROW GA	48432.10218	32065.91406	-39568.86718	-5712.35371	-31428.07422	-387.66968
	25859.51563	2375.86670	-494.72607	14.22389	250.70425	13.99531
	36.89009	11.12428	-1.27389	9.72795	130.03610	-293.79932
	46.81683	-24624.98828	71.27892	59.72795	21390103	-82.85709
ROW LI	31942.80078	14641.12891	-17230.10156	-16449.43506	-30794.69521	-3638.12305
	24427.35547	2048.79346	-256.25366	117.43790	25.67321	61.67538
	11.22428	18.47684	0.07115	25.51125	122.14732	1300.94092
	-93.67456	34045.51563	7.31264	19.82820	143.39091	-28.18898
ROW MD	2062.07959	2061.34668	-7025.39844	-612.20282	-3184.04366	723.93092
	-1432.08350	-58.67319	-109.54742	-65.20282	0.00898	723.93092
	-1.27389	3.71113	-1.03001	-2.10323	-3.76712	-132.34226
	-3.51861	16210.10156	-1.70434	-3.38290	3.76712	-12.21729
ROW PB	-9594.14844	-12223.94922	28036.26172	33427.30234	-57087.43359	-24033.60156
	17063.12891	552.4642	1327.38550	750.26172	84.90847	230.83066
	9.74282	28.51992	-2.70323	503.62495	313.24707	23377.70703
	-239.99214	194395.12500	123.24995	48.42397	195.10895	313.76906
ROW RB	639195.00000	217217.93750	-310336.98250	-76922.18750	-376765.12500	-37725.85547
	313803.87500	24519.18750	-3643.51001	14355.07176	280.51440	175.24664
	130.03610	1638.14732	7239.37500	317.24707	3368.89844	16318.59375
	-814.81348	-260670.62500	823.96045	325.74588	1600.48682	-306.88916
ROW S	-2416194.00000	-1313269.00000	5232591.00000	2495128.00000	-2328438.00000	-1223342.00000
	202945.00000	-72107.25000	72539.37500	42408.98047	5834.16406	722.52100
	-293.79932	1300.94092	1300.94092	23377.70703	16338.09375	1645099.00000
	-16821.05469	14567632.00000	2951.19200	1215.42847	78993.41406	28091.94141
ROW SR	-86951.06250	-8680.65234	-372805.68750	-60693.55469	204732.93750	69372.06250
	-126053.12500	-1071.60959	-2782.53750	-153.16382	-131.32045	-86.22557
	46.81683	-93.67456	-3.17861	-32.32205	-84.8248	-14821.65469
	2206.52759	-686217.93750	58.15709	590.25269	-1048.05713	-12255.26001
ROW CGH2	-27609395.00000	-11557549.00000	256015952.00000	71133792.00000	-123962416.00000	27200832.00000
	-96594080.00000	-4302410.00000	148921.00000	-199365.00000	82743.31250	864.85547
	24624.98828	34045.51563	16216.10156	194395.12500	-260670.62500	17567632.00000
	-68621.93750	1364362240.00000	-148282.81250	-285948.06250	212995.87500	820061.87500
ROW ZN	90396.00000	41768.46875	-82867.00000	-27515.60156	-87096.93750	-19677.04688
	119721.25000	17269.52734	-401.11182	423.22805	110.18311	184.11195
	71.16992	73.31264	-1.70434	123.22805	823.96045	2951.17920
	56.15709	-148282.81250	962.11841	25.23599	684.07349	-190.16074
ROW ZR	197531.62500	61148.98047	-297148.06250	-36393.44141	-57532.39672	9511.97256
	53308.27344	6492.73047	-26226.12182	44.35889	37.7158	24.92940
	27.42755	19.62820	-3.38290	48.42397	325.2488	1215.42847
	530.25269	-285948.06250	251.23599	631.45142	91.35092	-789.34717
ROW V	198586.81250	74508.25000	-344705.31250	-48720.00781	-275334.62500	-29599.08203
	238200.54250	21623.83594	-2336.55420	2283.44434	1600.48682	273.65425
	1048.05713	443.39091	3.76712	19.10955	4834.31172	7893.41426
	-1048.05713	212995.87500	684.07349	91.35092	-939.39307	-939.39307
ROW NI	-113268.00000	-35504.93750	2050256.00000	170216.43750	277038.43750	-10041.56250
	-113268.00000	17424.18391	2277.92188	-3819.16724	169.72967	2249.01540
	-42.85709	820061.87500	-1.21789	313.78906	-306.88912	2809.94141
	-12205.26001	820061.87500	-190.16074	-789.34717	-939.39307	7113.07813
COMMON MEANS	274319.68750	82282.62500	49842.20313	12730.26563	15456.55469	13082.39652
	16781.36719	4804.90234	808.05493	745.73999	39.89810	31.66362
	22.40739	13.64615	1.20370	22.89813	105.86104	729.81271
	190.25919	76794.37500	90.44437	140.85404	174.14807	127.48160
GENERALIZED MAHALANOBIS D-SQUARE			148.727157593			

DISCRIMINANT FUNCTION CON BRACK

CONSTANT * COEFFICIENTS				
-672.121093750	0.002302214	0.003894767	0.001746852	-0.00094850
	0.003474343	-0.000335249	0.001326657	0.009732164
	0.031533159	-0.001753531	-0.0228197813	-0.696543455
	-2.655446053	2.2432856569	-0.197466195	0.588289559
	-0.154583931	-0.002759227	-0.705316424	-0.000884702
	-0.016881760	0.041593067	0.208988130	-0.052475989

DISCRIMINANT FUNCTION MARINE				
CONSTANT * COEFFICIENTS				
-655.823486328	0.002271105	0.003866632	0.001748435	-0.000912192
	0.003433480	-0.000346826	0.001681390	0.009432122
	0.034335159	-0.006129816	-0.117014527	-0.825383980
	-2.722186089	2.798332269	-0.444887409	0.280963723
	-0.155018508	-0.003336020	0.667390281	-0.000913283
	-0.004104771	0.058920398	0.213495333	-0.036533283

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

GROUP CON BRACK

OBSERVATION PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION LARGEST FUNCTION NO.

1	0.95641	
2	0.97317	
3	0.99735	
4	0.99995	
5	0.99445	
6	0.97705	
7	0.94336	
8	0.99923	
9	0.92537	
10	0.57081	
11	0.90888	
12	0.96523	
13	0.91155	
14	0.99558	
15	0.98051	
16	0.98679	
17	0.95804	
18	0.98739	
19	0.99852	
20	0.97605	
21	0.98211	
22	0.99341	
23	0.99820	
24	0.99888	
25	0.99202	
26	0.99114	
27	0.99266	
28	0.53449	
29	0.95777	
30	0.58463	
31	0.99987	
32	0.99269	
33	0.99337	
34	0.99254	
35	0.99039	
36	0.99113	
37	0.99290	
38	0.89267	
39	0.99393	
40	0.99273	
41	0.99352	
42	0.79077	
43	0.99077	
44	0.99255	
45	0.73925	
46	0.99198	
47	0.94288	
48	0.94257	
49	0.59722	
50	0.98110	
51	0.94400	
52	0.99886	
53	0.99802	
54	0.99886	
55	0.99119	
56	0.99771	
57	0.97215	
58	0.99110	
59	0.98184	
60	0.99744	
61	0.86602	
62	0.99004	
63	0.92223	
64	0.99744	
65	0.99150	
66	0.97150	
67	0.97168	
68	0.64335	
69	0.80984	
70	0.81961	
71	0.79760	
72	0.99779	
73	0.99167	
74	0.94855	
75	0.99555	
76	0.68716	
77	0.99579	
78	0.99377	
79	0.99891	
80	0.98282	
81	0.91413	
82		
83		

GROUP MARINE	OBSERVATION	PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION	PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION	LARGEST FUNCTION NO.
	1	0.91239	0.91238	N
	2	0.96550	0.96550	N
	3	0.79221	0.79221	N
	4	0.91237	0.91237	N
	5	0.91236	0.91236	N
	6	0.98566	0.98566	N
	7	0.98333	0.98333	N
	8	0.96019	0.96019	N
	9	0.98386	0.98386	N
	10	0.89417	0.89417	N
	11	0.95866	0.95866	N
	12	0.99239	0.99239	N
	13	0.99598	0.99598	N
	14	0.99778	0.99778	N
	15	0.99867	0.99867	N
	16	0.99860	0.99860	N
	17	0.99239	0.99239	N
	18	0.99598	0.99598	N
	19	0.99778	0.99778	N
	20	0.99867	0.99867	N
	21	0.99885	0.99885	N
	22	0.99889	0.99889	N
	23	0.99885	0.99885	N
	24	0.99885	0.99885	N
	25	0.99875	0.99875	N

Appendix 3

Classifications for the Standard Groups
Continental vs Brackish 24 Variables

DISCRIMINANT ANALYSIS.....CONTINENTAL VS BRACKISH TWENTY FOUR

NUMBER OF GROUPS 2
 NUMBER OF VARIABLES 24
 SAMPLE SIZES
 GROUP 1 20
 GROUP 2 63

GROUP	CONTINENTAL	MEANS	15079.00000	11172.00000	14500.00000	10005.00000	4391.00000
1	27875.50000	85059.00000	26.34999	20.34999	12.20000	1.80000	13.59999
2	531.50000	751.00000	26.34999	71.34999	131.59999	20.00000	83.89999
	73.25000	531.75000	111046.00000				

GROUP BRACKISH MEANS
 27539.75000 81921.52250 47294.44141 11653.01563 17940.47266 14407.93359 16798.72656 4821.90334
 779.57129 755.87280 3815873 33.73075 3815873 33.73075 3815873 33.73075
 98.80951 840.55542 21111110 69155.75306 90.92662 148.37777 151.42856 12.33659

PROBLED DISPERSION MATRIX

ROW SI	433781.7600	1006494.4800	00000	-70500288.00000	-14420065.00000	-177414560.00000	6594936.00000
	57208087.00000	-2238813.18750	00000	-116233889.00000	6864630.62500	235899.01172	10880.62000
	213375.45234	17940.47266	00000	-2119713.76895	-2119713.76895	483704.75000	-8864600.50000
	-372877.43750	-140504928.00000	00000	-554481.62881	22334.62260	-95391.25000	-29999.71172
ROW AL	107464448.00000	78197936.00000	00000	-40449588.00000	2060160.00000	-85957840.00000	14981632.00000
	19236826.00000	10423360.28750	00000	-3872289.00000	-185558.97750	343348.82350	4126.64263
	248355.12109	380246484	00000	1099.95288	-113408.17016	124444.12500	-1034000.31950
	-52801.97266	38112544.00000	00000	-766.39990	13275.93750	-571827.26453	8957.19322
ROW FE	-17520288.00000	-40483588.00000	00000	212742809.00000	24960366.00000	-4705878.00000	-18412889.00000
	-453765.00000	1522289.00000	00000	-269203.00000	365344.18750	13778.65931	658931.62000
	3643.49146	17940.47266	00000	-2776.86795	52700.20703	90667.75000	3066799.00000
	-62330.17168	64081360.00000	00000	163589.25000	-12476.88906	163148.06250	3068675.50000
ROW HG	-1420065.00000	2060160.00000	00000	24960366.00000	40305420.00000	3467573.00000	7341768.00000
	-375025.00000	-1673319.00000	00000	369862.31250	1092221.00000	28525.24375	-832.47000
	91504	288.33613	00000	-1088.48047	47661.66094	-38233.66875	3177204.00000
	-18267.2693	3569776.00000	00000	-68822.50000	-68822.66016	-62409.41797	64235.52734
ROW JA	-174415.00000	-859774.00000	00000	-4705878.00000	3467573.00000	7341768.00000	-7089466.00000
	50000	-357256.00000	00000	305831.50000	324720.87500	-85491.51563	-40383.20703
	33367.7344	1512.41504	00000	-2599.82482	-76719.12500	-399169.62250	-1525079.00000
	51391.8123	-181389840.00000	00000	-68822.50000	-19714.88672	-173142.00000	-1525079.00000
ROW NA	652428.00000	14981632.00000	00000	-18432880.00000	7341768.00000	-7089466.00000	60084976.00000
	-1689347.00000	-697639379.00000	00000	-383366.00000	21129.18359	7326.24219	-2028.93115
	51391.8123	1512.41504	00000	-2599.82482	-76719.12500	-399169.62250	-1525079.00000
	-21429.4570	-21429.4570	00000	95588.43750	12881.83906	-52107.25781	-22493.10938
ROW K	5779872.00000	3736776.00000	00000	-658760.00000	-375005.00000	-38017200.00000	12880357.00000
	6071880.00000	3139674.00000	00000	-14026.75000	544859.25000	1662.40663	33997.36375
	-21429.4570	-21429.4570	00000	95588.43750	12881.83906	-52107.25781	-22493.10938
ROW LI	2028913.18750	1093842.68750	00000	1523297.90000	-1670319.00000	-3579256.00000	-90763.97750
	211159.80567	6071880.00000	00000	403337.90000	-58527.92219	1329.27168	4820.4916
	-9776.8639	337328.00000	00000	15005.12109	345.6623	29842.25781	-47174.17500
ROW MN	-159889.00000	-97209.00000	00000	269203.00000	369862.31250	305391.50000	-363206.02250
	-113027.35000	403337.90000	00000	65248.28265	1093842.68750	305391.50000	1080.34559
	-27.4663	2275.63316	00000	1572.84937	-293.89390	3932.79164	8074.58250
ROW RA	686539.00000	-185258.93750	00000	676944.18750	1092921.00000	321720.00000	21729.18359
	54906.28500	-152207.53119	00000	10880.62000	61870.62260	40.07663	6.28032
	-278.13039	-149840.00000	00000	-68822.50000	-380.69033	1933.22912	62466.5053
ROW CO	3582.91172	38346.97594	00000	13778.92578	28925.34375	-65491.51563	7921.2397
	1682.33625	2729.27148	00000	0.31735	401.623159	208.60093	7000.5375
	-141.80473	13811.52250	00000	107.04831	21.17055	6.57664	199.77820
ROW CU	10887.62500	4120.64063	00000	65933.62669	-832.47900	-40283.20743	-2068.97115
	38397.42375	4850.41016	00000	10880.62000	48.99619	21.97197	726.6872
	-14.82731	28.65515	00000	25.84027	43.88092	40.67673	203.6233
ROW GA	21375.62234	25355.12109	00000	3963.49146	-642.91504	-30567.88844	-2452.6429
	18530.6072	165.90867	00000	-7.76888	-106.22108	84.97159	-396.13696
	36.2660	9.2660	00000	59.03900	43.22305	-	34.8612

ROW MO	1098.48047 -110.52297 -110.32892 -4.94145	288.33113 25.03626 168.58248 139.31808	-31928.74890 -5.17.51113 1844.38575 65.88057	729.36058 21.50259 -142.49232 -1.98477
ROW PB	47081.96094 876.00073 6.3789581	47081.96094 876.00073 6.3789581	-33742.17188 45.80022 30.347.20031 417.85532	-33742.17188 45.80022 30.347.20031 417.85532
ROW PB	30667.99.00000 88172.82250 90347.32031 2435.87865	30667.99.00000 88172.82250 90347.32031 2435.87865	-60736.78936 212.96150 21787.80078 27784.14453	-60736.78936 212.96150 21787.80078 27784.14453
ROW S	1029.89795 -73.72500 -2.46281 -3.44946	50667.75000 -391.91164 -31.91530 698.17480	-398188.06250 236.00093 3543.91968 1767.77930	-398188.06250 236.00093 3543.91968 1767.77930
ROW PB	146244.12500 18564.17188 1160.52420 129968.31250	146244.12500 18564.17188 1160.52420 129968.31250	-4574689.00000 82.00000 21787.80078 15852.55469	-4574689.00000 82.00000 21787.80078 15852.55469
ROW S	1029.89795 -73.72500 -2.46281 -3.44946	50667.75000 -391.91164 -31.91530 698.17480	-398188.06250 236.00093 3543.91968 1767.77930	-398188.06250 236.00093 3543.91968 1767.77930
ROW SR	17275.43750 -2425.83750 -1.13890 23.88957	17275.43750 -2425.83750 -1.13890 23.88957	313981.81250 -141.84473 -21991.22344 -439.98428	313981.81250 -141.84473 -21991.22344 -439.98428
ROW CMH	38172544.00000 3827344.00000 1284139776.00000	38172544.00000 3827344.00000 1284139776.00000	49008832.00000 33987.16016 23859744.30000 4424660.62500	49008832.00000 33987.16016 23859744.30000 4424660.62500
ROW ZN	15075.12000 -1762.39090 -137.75500	163589.25000 -293.69390 119.88105	-68832.50000 107.04831 688.17480 852.02295	-68832.50000 107.04831 688.17480 852.02295
ROW ZR	12881.53000 42.80809	12881.53000 42.80809	-17714.86672 171.70059 122.62000 77.58405	-17714.86672 171.70059 122.62000 77.58405
ROW V	29195.03750 -130.06650	162148.06250 3932.79781 139.37898 852.02295	-173146.00000 167.58034 127.70059 5098.13672	-173146.00000 167.58034 127.70059 5098.13672
ROW HI	2898.50001 3.89012 -42.82422	308675.50000 3086.67651 1.83744 494.06641	-23403.10938 202.60233 27394.44233 1334.34009	-23403.10938 202.60233 27394.44233 1334.34009
COMMON MEANS	8203.43750 2718.05641 26.45242 20.91256	44479.14453 748.67432 12.37340 86.20471	16309.50391 37.019275 92.86054 165.30115	16309.50391 37.019275 92.86054 165.30115
GENERALIZED MAHALANOBIS D-SQUARE				
233.293853760				

DISCRIMINANT FUNCTION CONTINENTAL
CONSTANT * COEFFICIENTS

-663.836914063
0.001065866
0.0037445059
0.0085531731
-0.47198009
-0.103220462
0.031175487

0.005096551
-0.00979842
0.02331993
4.81001918
-0.004615175
0.107873261

0.00623112
0.000236548
-0.420441498
-0.24834908
0.55876783
0.22805041

-0.00061675
0.011023881
-0.71316922
0.53589746
0.00088826
-0.009582460

DISCRIMINANT FUNCTION BRACKISH
CONSTANT * COEFFICIENTS

-642.076415016
0.01030019
0.00333584
0.00351614
-0.50971878
-0.107948840
0.006873950

0.004912760
-0.00023482
0.00343194
4.823438319
-0.00130236
0.11144411

0.00759572
0.00023532
-0.17747928
0.10712328
0.18617591
0.18617591

-0.00583826
0.00716029
-0.71316922
0.4076845
0.0000000
0.01225812

Appendix 4

Classifications for the Standard Groups
Marine vs Continental-Brackish 12 Variables

DISCRIMINANT ANALYSIS.....CON BRACK VS MARINE TWELVE VAR

NUMBER OF GROUPS 12
 NUMBER OF VARIABLES 25
 SAMPLE SIZES
 GROUP 1 83
 GROUP 2 25

GROUP CON BRACK MEANS 754.69873 37.01204 31.19276 22.45782 12.33735 204.91565
 4718.07031 748.67456 143.00000 165.30119
 79244.56250 86.20482

GROUP MARINE MEANS 716.00000 49.48000 32.35999 22.23999 18.00000 141.59999
 5092.19922 1095.19995 133.59999 203.51999

POOLED DISPERSION MATRIX

ROW TI 953963 31250 -52272.28125 -17523.37500 3254.44141 4130.36719 2375.86670
 2048.79346 -1071.60059 -17269.52734 6492.73047 27623.83594

ROW MN -52272.28125 140948.43750 -2782.53760 -3027.01880 126.99159 22.64600 26.70425
 -256.23956 -2782.53760 1488921.00000 1488921.00000 -107.18311 17.77158 74.49567

ROW BA -17523.37500 -1027.01880 -1533.16382 -62596.50000 496.91602 447.35889 13.89831
 117.43790 -1533.16382 -1698828.00000 463.22803 24.92940 275.65405

ROW CO 3254.44141 -167.93584 -131.32045 496.91602 126.99159 22.64600 26.70425
 25.44954 -131.32045 82743.31250 82743.31250 110.18311 17.77158 74.49567

ROW CU 4130.36719 1395.96558 -86.22597 -5.65242 22.64600 24.92940 13.89831
 21.67538 -86.22597 864.85547 184.11195 19.52820 143.39091

ROW GA 2375.86670 -494.72607 46.81683 18.73138 26.70425 13.99531 36.69009
 11.12428 -46.81683 -24624.98828 71.16992 58.42735 21.90103

ROW LI 2048.79346 18.47684 -256.25366 117.43790 25.44954 19.52820 11.12428
 18.47684 -256.25366 34045.51563 73.31264 19.52820 143.39091

ROW SR -1071.60059 -2782.53760 2206.52759 -1533.16382 -131.32045 86.22597 46.81683
 -93.67456 2206.52759 -686217.93750 -686217.93750 56.15709 -1048.05713

ROW C6H2 -43202410.00000 1488921.00000 -686217.93750 1364362240.00000 -82743.31250 864.85547 224624.98828
 34045.51563 -686217.93750 -686217.93750 -148282.81250 -285948.06250 212995.87500

ROW ZN 17269.92734 -401.11182 56.15709 463.23903 110.18311 184.11195 71.16992
 73.31264 56.15709 -148282.81250 982.11841 251.23599 684.07346

ROW ZR 6492.73047 19.52820 -2626.12183 590.25269 -17.77158 24.92940 59.42735
 19.52820 -2626.12183 -285948.06250 251.23599 631.45142 91.35092

ROW Y 27623.83594 -143.39091 2336.55420 -1048.05713 2283.44434 212295.87500 21.90103
 143.39091 -2336.55420 -1048.05713 212295.87500 684.07349 91.35092 4834.51172

COMMON MEANS 4304.90234 808.05493 745.73999 76794.37500 38.89810 31.46295 22.40739
 13.64815 190.25619 76794.37500 98.44457 140.82404 174.14807

GENERALIZED MAHALANOBIS D-SQUARE 122.741928101

DISCRIMINANT FUNCTION CON BRACK CONSTANT *
 -66.758499146
 -0.605764309
 -0.028128639
 0.000167535

DISCRIMINANT FUNCTION MARINE CONSTANT *
 -64.052671704
 0.003346049
 -0.164303243
 -0.000122587

GROUP CON BRACK	OBSERVATION	PROBABILITY	ASSOCIATED WITH	LARGEST
		LARGEST DIS	FUNCTION	FUNCTION NO.
	1	0.97834		
	2	0.99870		
	3	0.98540		
	4	0.97258		
	5	0.95964		
	6	0.95123		
	7	0.92803		
	8	0.91468		
	9	0.84342		
	10	0.85356		
	11	0.95901		
	12	0.94694		
	13	0.91711		
	14	0.94283		
	15	0.95338		
	16	0.94441		
	17	0.92715		
	18	0.98003		
	19	0.90796		
	20	0.92445		
	21	0.92688		
	22	0.92829		
	23	0.95276		
	24	0.9227		
	25	0.98091		
	26	0.77290		
	27	0.96570		
	28	0.92500		
	29	0.92500		
	30	0.93488		
	31	0.95227		
	32	0.95227		
	33	0.9315		
	34	0.95451		
	35	0.76470		
	36	0.72825		
	37	0.73653		
	38	0.55293		
	39	0.74954		
	40	0.70262		
	41	0.89203		
	42	0.93388		
	43	0.93388		
	44	0.71225		
	45	0.96834		
	46	0.9989		
	47	0.9989		
	48	0.9930		
	49	0.9799		
	50	0.9927		
	51	0.93382		
	52	0.57382		
	53	0.76825		
	54	0.9825		
	55	0.79711		
	56	0.99320		
	57	1.00000		
	58	0.9322		
	59	0.8885		
	60	0.70003		
	61	0.64938		
	62	0.9322		
	63	0.9825		
	64	0.8712		
	65	0.9322		
	66	0.9549		
	67	0.9949		
	68	0.9949		
	69	0.9949		
	70	0.9949		
	71	0.9949		
	72	0.9949		
	73	0.9949		
	74	0.9949		
	75	0.9949		
	76	0.9949		
	77	0.9949		
	78	0.9949		
	79	0.9949		
	80	0.9949		
	81	0.9949		
	82	0.9949		
	83	0.9949		
	84	0.9949		
	85	0.9949		
	86	0.9949		
	87	0.9949		
	88	0.9949		
	89	0.9949		
	90	0.9949		
	91	0.9949		
	92	0.9949		
	93	0.9949		
	94	0.9949		
	95	0.9949		
	96	0.9949		
	97	0.9949		
	98	0.9949		
	99	0.9949		
	100	0.9949		

GROUP	MARINE	PROBABILITY LARGEST DISCR	ASSOCIATED WITH MINORANT FUNCTION	LARGEST FUNCTION NO.
1		0.94813		1
2		0.94102		2
3		0.93631		2
4		0.93224		2
5		0.93216		2
6		0.93234		2
7		0.93237		2
8		0.93210		2
9		0.93213		2
10		0.93214		2
11		0.93212		2
12		0.93221		2
13		0.93221		2
14		0.93221		2
15		0.93221		2
16		0.93221		2
17		0.93217		2
18		0.93217		2
19		0.93217		2
20		0.93217		2
21		0.93217		2
22		0.93217		2
23		0.93217		2
24		0.93217		2
25		0.93217		2

Appendix 5

Classifications for the Standard Groups
Continental vs Brackish 16 Variables

NUMBER OF GROUPS
NUMBER OF VARIABLES
SAMPLE SIZES
GROUP

2
16
20
63
1
2

GROUP CONTINENTAL MEANS
15079.0000 14500.0000 4391.00000 591.50000 751.00000 33.39999 26.34999
20.34999 12.20000 73.25000 111040.0000 71.34999 131.09999 209.00000

GROUP BRACKISH MEANS
11652.01563 14407.93359 16798.72656 4821.90234 755.87280 39.15872 32.73015
23.12693 12.38095 98.80951 211.11110 69150.75000 90.92062 146.77777 151.42856

POOLED DISPERSION MATRIX

ROW VG
40205446.00000 7341068.00000 -3750905.00000 -1670319.00000 369862.31250 1092921.00000
28525.34375 -643.91504 -2452.64429 -5187.51172 -39233.46875 -18267.26953
3597740.00000 -5587.50000 -6822.66016 -62409.41797

ROW NA
7241068.00000 60084976.00000 -12880257.00000 3118775.00000 -363606.06250 21729.18359
7821.24310 -2048.93115 -2452.64429 -5187.51172 -60736.78906 57190.30859
4902892.00000 -39259.67578 -7680.08984 -53107.25781

ROW K
-3750905.00000 -12880257.00000 60718384.00000 3118775.00000 -114022.37500 549659.62500
19621.40625 38397.34375 15830.80078 22966.81250 268564.31250 -224594.93750
-2955556.00000 95188.43750 12861.53906 291954.93750

ROW TT
-1670319.00000 -90763.93750 3118775.00000 962802.31250 40391.55469 -55297.49219
2729.27143 4450.41016 1653.90967 1806.02467 18544.17188 -9779.86328
3347364.00000 15345.12100 1292.75366 29842.25781

ROW MN
369862.31250 -363606.06250 -114022.37500 40391.55469 65459.28125 10855.53125
57.68272 1060.30469 -27.76688 4.29925 -391.18164 5.40623
32756.03516 1572.84937 -293.49390 3932.79761

ROW BA
1092921.00000 21729.18359 569659.62500 -55297.49219 10855.53125 67344.12500
491.22437 6.82602 -106.22116 52.53119 497.47095 -2783.12016
-1449940.00000 -618.48682 -396.49023 1933.22974

ROW CO
28525.34375 7821.24219 19621.40625 2729.27148 57.68272 491.02637
98.21150 32.97397 21.39410 25.09361 -141.80473
164311.56250 107.94831 21.77055 67.57634

ROW CU
-822.47900 -2048.93115 38397.34375 4850.41016 1060.30469 6.82602
52.97397 141.56596 17.24321 26.65515 212.96150 8.82602
33697.16016 205.84027 20.95697

ROW LI	289.02313	-5187.51172	22966.81250	1806.03467	4.29925	52.53119	-106.22116
	25.09361	26.65515	9.26600	19.18579	160.52440	-134.15045	18.18893
	61736.91016	76.33862	9.80155	139.37808			
ROW RH	-39233.46075	-60736.78906	266564.31250	18544.17188	-391.18164	497.47095	
	206.03993	212.96150	84.97159	160.52440	3543.91968	-1388.29150	
	122966.31250	698.17480	122.62601	1767.77930			
ROW SR	-18267.26953	57190.20859	-224594.93750	-9779.96328	5.40623	-2788.12036	
	-141.80473	-148.20731	18.18993	-134.15045	-1388.29150	2312.88037	
	-15844.87500	-200.11333	429.90809	-1306.06250			
ROW CRH2	39597760.00000	49002832.00000	-29535664.00000	3347364.00000	32750.03516	-1449840.00000	
	164311.56250	33997.16016	18387.50391	61736.91016	122996.31250	-515544.87500	
	1286139776.00000	90137.75000	-77354.75000	42055.29297			
ROW ZN	-6687.80000	-29359.67578	95588.43750	15045.12109	1572.84937	-618.48682	
	107.04837	205.84027	59.03900	76.33862	698.17480	-200.11333	
	88137.75000	795.00000	119.58105	852.02295			
ROW ZR	-6682.66016	-7680.08384	12881.53906	1292.75366	-293.49390	-380.49023	
	21.77055	20.95697	43.22305	9.80155	122.62601	429.90859	
	-77054.75000	119.58105	560.54956	77.55405			
ROW V	-82409.41797	-53107.25781	261954.93750	29842.825781	3932.79761	1933.22974	
	6757624	409.76733	-3.14104	139.37808	1767.77930	-1306.06250	
	42055.29297	852.02295	77.55405	5098.13672			
COMMON MEANS	12478.56078	14630.10547	15161.67188	4718.06641	748.67432	754.69849	
	37.01202	31.19275	22.43782	12.33734	92.65054	204.91556	
	79244.50000	86.20471	142.99989	165.30115			
GENERALIZED MAHALANOBIS D-SQUARE	161.353622437						
DISCRIMINANT FUNCTION CONTINENTAL CONSTANT * COEFFICIENTS	-73.719580233 *	0.000157554	-0.000037940	0.000290766	0.007028900		
		0.003115894	0.026661061	-0.282257547	0.039703250		
		-0.19773819	1.965945475	0.041430663	0.325023361		
		0.000189272	-0.213716447	0.029654499	0.022531826		
DISCRIMINANT FUNCTION BRACKISH CONSTANT * COEFFICIENTS	-79.568618774 *	-0.000245353	0.000070451	0.000716941	0.086231286		
		0.011671495	0.027534287	-0.028423373	0.043120325		
		-0.400927782	1.719291687	0.043033693	0.351169348		
		0.000167543	-0.150811217	0.041280117	-0.014962699		

GROUP IDENTIFICATION	PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION	LARGEST FUNCTION NO.
1	C.96957	1
2	C.99128	1
3	C.62326	1
4	1.00000	1
5	C.99123	1
6	C.98642	1
7	C.99867	1
8	C.90878	1
9	C.99969	1
10	C.84175	1
11	C.96043	1
12	C.99909	1
13	C.99251	1
14	C.99797	1
15	C.99649	1
16	C.99034	1
17	C.90872	1
18	C.99907	1
19	C.78400	2
20	C.96423	1

GROUP BACKLISH	PROBABILITY ASSOCIATED WITH LARGEST DISCRIMINANT FUNCTION	LARGEST FUNCTION NO.
1	C.91934	2
2	C.72818	1
3	C.95548	2
4	C.94436	2
5	C.54569	1
6	C.96095	2
7	C.97801	2
8	C.63523	2
9	C.99990	2
10	C.99976	2
11	C.69195	2
12	C.90086	2
13	C.99996	2
14	C.89861	2
15	C.96896	2
16	C.98336	2
17	C.99976	2
18	C.69846	2
19	C.99972	2
20	C.96984	2
21	C.99169	2
22	C.99994	2
23	C.69965	2
24	C.99779	2
25	C.67899	2
26	C.69762	2
27	C.69744	2
28	C.99841	2
29	C.99814	2
30	C.98332	2
31	C.78944	1
32	C.69423	2
33	C.76590	2
34	C.86270	2
35	C.69923	2
36	C.99963	2
37	C.99995	2

Appendix 6

Classifications for the Unknown Samples in the
Groups Marine vs Continental-Brackish 12 Variables

DISCRIMINANT ANALYSIS.....CON BRACK VS MARINE TWELVE VAR
 NUMBER OF GROUPS
 NUMBER OF VARIABLES 12 2
 SAMPLE SIZE
 GROUP 2
 189
 189

DISCRIMINANT FUNCTION: CONTINENTAL BRACKISH

CONSTANT * COEFFICIENTS
 -66.7584991455 *
 0.0057643093
 0.0145713352
 -0.0281286389
 -0.03833433700
 0.0407248761
 0.10477086120
 0.0209555700
 0.0827211142
 0.2165119848
 0.0237405486

DISCRIMINANT FUNCTION: MARINE

CONSTANT * COEFFICIENTS
 -64.0528717041 *
 0.0053260486
 0.0182240329
 -0.023703232
 -0.1401119232
 0.15124540329
 -0.1190724373
 0.0170597844
 1.5124540329
 0.1011859179
 0.16498944186
 0.1852390888
 0.0276229951

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
1	598.5	0.99157	CONTINENTAL BRACKISH
2	600.0	0.74658	MARINE
3	602.0	0.89243	MARINE
4	603.2	0.96704	MARINE
5	603.4	0.97970	MARINE
6	605.7	0.97977	MARINE
7	607.4	0.98457	MARINE
8	611.5	0.98936	MARINE
9	612.0	0.99024	MARINE
10	618.0	0.99238	MARINE
11	622.0	0.99299	MARINE
12	624.0	0.99353	MARINE
13	624.0	0.99353	MARINE
14	624.0	0.99353	MARINE
15	624.0	0.99353	MARINE
16	624.0	0.99353	MARINE
17	624.0	0.99353	MARINE
18	633.3	0.99353	MARINE
19	633.3	0.99353	MARINE
20	635.0	0.99353	MARINE
21	638.0	0.99353	MARINE
22	644.5	0.99353	MARINE
23	644.5	0.99353	MARINE
24	645.0	0.99353	MARINE
25	650.5	0.99353	MARINE
26	652.0	0.99353	MARINE
27	653.0	0.99353	MARINE
28	657.0	0.99353	MARINE
29	657.0	0.99353	MARINE
30	661.0	0.99353	MARINE
31	662.0	0.99353	MARINE
32	663.0	0.99353	MARINE
33	663.0	0.99353	MARINE
34	667.0	0.99353	MARINE
35	667.0	0.99353	MARINE
36	667.0	0.99353	MARINE
37	667.0	0.99353	MARINE
38	667.0	0.99353	MARINE
39	667.0	0.99353	MARINE
40	673.0	0.99353	MARINE
41	673.0	0.99353	MARINE
42	673.0	0.99353	MARINE
43	673.0	0.99353	MARINE
44	673.0	0.99353	MARINE
45	673.0	0.99353	MARINE
46	673.0	0.99353	MARINE
47	673.0	0.99353	MARINE
48	683.0	0.99353	MARINE
49	683.0	0.99353	MARINE
50	683.0	0.99353	MARINE
51	683.0	0.99353	MARINE
52	683.0	0.99353	MARINE
53	683.0	0.99353	MARINE
54	683.0	0.99353	MARINE
55	683.0	0.99353	MARINE
56	683.0	0.99353	MARINE
57	683.0	0.99353	MARINE
58	683.0	0.99353	MARINE
59	683.0	0.99353	MARINE
60	683.0	0.99353	MARINE
61	683.0	0.99353	MARINE
62	683.0	0.99353	MARINE
63	683.0	0.99353	MARINE
64	683.0	0.99353	MARINE
65	683.0	0.99353	MARINE
66	683.0	0.99353	MARINE
67	683.0	0.99353	MARINE
68	683.0	0.99353	MARINE
69	683.0	0.99353	MARINE
70	683.0	0.99353	MARINE

DISCRIMINANT ANALYSIS.....CON BRACK VS MARINE TWELVE VAR

NUMBER OF GROUPS 12 2
 NUMBER OF VARIABLES 12 2
 SAMPLE SIZES 199 199
 GROUP 1 2

DISCRIMINANT FUNCTION CONTINENTAL BRACKISH

CONSTANT * COEFFICIENTS
 -66.7584991455 0.0857663093 0.0145713352 0.0205557011 0.0827211142
 -0.0201288889 -0.0383433700 -0.0383433700 1.0502348761 0.2157119488
 0.0001675350 -0.1302070022 0.1047086120 0.1047086120 0.0237405486

DISCRIMINANT FUNCTION MARINE

CONSTANT * COEFFICIENTS
 -64.0528717041 0.0053460486 0.0182699372 0.0176597844 0.1649864186
 -0.1643032632 0.0001225670 -0.140119232 1.5124540329 0.1943398488
 0.0001225670 -0.1190724373 0.1011859179 0.1011859179 0.0276229531

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
1	1539.0	0.64460	CONTINENTAL BRACKISH
2	1540.0	0.93309	MARINE
3	1545.0	0.87376	CONTINENTAL BRACKISH
4	1545.5	0.68377	MARINE
5	1551.0	0.91497	CONTINENTAL BRACKISH
6	1553.0	0.65498	MARINE
7	1553.0	0.84706	CONTINENTAL BRACKISH
8	1562.0	0.95660	CONTINENTAL BRACKISH
9	1564.0	0.99332	CONTINENTAL BRACKISH
10	1566.0	0.99387	CONTINENTAL BRACKISH
11	1569.0	0.99167	CONTINENTAL BRACKISH
12	1570.0	0.98622	CONTINENTAL BRACKISH
13	1571.0	0.98115	CONTINENTAL BRACKISH
14	1573.0	0.98175	CONTINENTAL BRACKISH
15	1577.0	0.57075	MARINE
16	1582.0	0.57856	CONTINENTAL BRACKISH
17	1585.0	0.55836	MARINE
18	1590.0	0.85426	CONTINENTAL BRACKISH
19	1597.0	0.88335	MARINE
20	1601.0	0.60777	CONTINENTAL BRACKISH
21	1601.0	0.60985	MARINE
22	1611.0	0.82672	CONTINENTAL BRACKISH
23	1613.0	0.74352	CONTINENTAL BRACKISH
24	1614.0	0.91527	CONTINENTAL BRACKISH
25	1617.0	0.93396	CONTINENTAL BRACKISH
26	1622.0	0.92843	CONTINENTAL BRACKISH
27	1623.0	0.93910	CONTINENTAL BRACKISH
28	1625.0	0.93921	CONTINENTAL BRACKISH
29	1633.0	0.99208	CONTINENTAL BRACKISH
30	1638.0	0.98282	CONTINENTAL BRACKISH
31	1642.0	0.97826	CONTINENTAL BRACKISH
32	1644.0	0.95196	CONTINENTAL BRACKISH
33	1652.0	0.97761	CONTINENTAL BRACKISH
34	1656.0	0.85892	CONTINENTAL BRACKISH
35	1662.0	0.00000	CONTINENTAL BRACKISH
36	1666.0	0.39889	MARINE
37	1677.0	0.99902	CONTINENTAL BRACKISH
38	1677.0	0.99504	MARINE
39	1682.0	0.99424	MARINE
40	1688.0	0.99369	MARINE
41	1693.0	0.99940	MARINE
42	1693.0	0.99934	MARINE
43	1698.0	0.99924	MARINE
44	1703.0	0.99126	MARINE
45	1705.0	0.98204	MARINE
46	1707.0	0.74107	CONTINENTAL BRACKISH
47	1715.0	0.99704	CONTINENTAL BRACKISH
48	1716.0	0.91201	CONTINENTAL BRACKISH
49	1721.0	0.92001	CONTINENTAL BRACKISH

Appendix 7

Classification for the Unknown Samples in the Groups
Continental vs. Brackish 16 Variables

DISCRIMINANT ANALYSIS.....CONTINENTAL VS BRACKISH SIXTEEN VAR

NUMBER OF GROUPS 2
 NUMBER OF VARIABLES 16
 SAMPLE SIZES:
 GROUP 1 189
 2 189

DISCRIMINANT FUNCTION CONTINENTAL

CONSTANT * COEFFICIENTS
 -73.7195892334
 0.0001575540
 0.0031158940
 -0.1977338195
 0.0001892720
 -0.000379400
 0.0266610908
 1.9659404755
 -0.2137164474
 0.002907659
 -0.2823676467
 0.0414306633
 0.0296544991
 0.0070889001
 0.0397032499
 0.329033612
 0.0225318260

DISCRIMINANT FUNCTION BRACKISH

CONSTANT * COEFFICIENTS
 -79.5686187744
 -0.0002453530
 0.0116714947
 -0.4009277821
 0.0001675430
 0.000704510
 0.0275342874
 1.7192916870
 -0.1808112168
 0.007169410
 -0.0284233727
 0.0430336930
 0.0412801169
 0.0062712856
 0.0431203246
 0.3511693478
 -0.0149626993

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

SAMPLE CLASSIFICATION

PROBABILITY

DEPTH

SAMPLE NO.

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
1	0	0.000000	CONTINENTAL
1	1	0.000000	CONTINENTAL
1	2	0.000000	CONTINENTAL
1	3	0.000000	CONTINENTAL
1	4	0.000000	CONTINENTAL
1	5	0.000000	CONTINENTAL
1	6	0.000000	CONTINENTAL
1	7	0.000000	CONTINENTAL
1	8	0.000000	CONTINENTAL
1	9	0.000000	CONTINENTAL
1	10	0.000000	CONTINENTAL
1	11	0.000000	CONTINENTAL
1	12	0.000000	CONTINENTAL
1	13	0.000000	CONTINENTAL
1	14	0.000000	CONTINENTAL
1	15	0.000000	CONTINENTAL
1	16	0.000000	CONTINENTAL
1	17	0.000000	CONTINENTAL
1	18	0.000000	CONTINENTAL
1	19	0.000000	CONTINENTAL
1	20	0.000000	CONTINENTAL
1	21	0.000000	CONTINENTAL
1	22	0.000000	CONTINENTAL
1	23	0.000000	CONTINENTAL
1	24	0.000000	CONTINENTAL
1	25	0.000000	CONTINENTAL
1	26	0.000000	CONTINENTAL
1	27	0.000000	CONTINENTAL
1	28	0.000000	CONTINENTAL
1	29	0.000000	CONTINENTAL
1	30	0.000000	CONTINENTAL
1	31	0.000000	CONTINENTAL
1	32	0.000000	CONTINENTAL
1	33	0.000000	CONTINENTAL
1	34	0.000000	CONTINENTAL
1	35	0.000000	CONTINENTAL
1	36	0.000000	CONTINENTAL
1	37	0.000000	CONTINENTAL
1	38	0.000000	CONTINENTAL
1	39	0.000000	CONTINENTAL
1	40	0.000000	CONTINENTAL
1	41	0.000000	CONTINENTAL
1	42	0.000000	CONTINENTAL
1	43	0.000000	CONTINENTAL
1	44	0.000000	CONTINENTAL
1	45	0.000000	CONTINENTAL
1	46	0.000000	CONTINENTAL
1	47	0.000000	CONTINENTAL
1	48	0.000000	CONTINENTAL
1	49	0.000000	CONTINENTAL
1	50	0.000000	CONTINENTAL
1	51	0.000000	CONTINENTAL
1	52	0.000000	CONTINENTAL
1	53	0.000000	CONTINENTAL
1	54	0.000000	CONTINENTAL
1	55	0.000000	CONTINENTAL
1	56	0.000000	CONTINENTAL
1	57	0.000000	CONTINENTAL
1	58	0.000000	CONTINENTAL
1	59	0.000000	CONTINENTAL
1	60	0.000000	CONTINENTAL
1	61	0.000000	CONTINENTAL
1	62	0.000000	CONTINENTAL
1	63	0.000000	CONTINENTAL
1	64	0.000000	CONTINENTAL
1	65	0.000000	CONTINENTAL
1	66	0.000000	CONTINENTAL
1	67	0.000000	CONTINENTAL
1	68	0.000000	CONTINENTAL
1	69	0.000000	CONTINENTAL
1	70	0.000000	CONTINENTAL
1	71	0.000000	CONTINENTAL
1	72	0.000000	CONTINENTAL
1	73	0.000000	CONTINENTAL
1	74	0.000000	CONTINENTAL
1	75	0.000000	CONTINENTAL
1	76	0.000000	CONTINENTAL
1	77	0.000000	CONTINENTAL
1	78	0.000000	CONTINENTAL
1	79	0.000000	CONTINENTAL
1	80	0.000000	CONTINENTAL
1	81	0.000000	CONTINENTAL
1	82	0.000000	CONTINENTAL
1	83	0.000000	CONTINENTAL
1	84	0.000000	CONTINENTAL
1	85	0.000000	CONTINENTAL
1	86	0.000000	CONTINENTAL
1	87	0.000000	CONTINENTAL
1	88	0.000000	CONTINENTAL
1	89	0.000000	CONTINENTAL
1	90	0.000000	CONTINENTAL
1	91	0.000000	CONTINENTAL
1	92	0.000000	CONTINENTAL
1	93	0.000000	CONTINENTAL
1	94	0.000000	CONTINENTAL
1	95	0.000000	CONTINENTAL
1	96	0.000000	CONTINENTAL
1	97	0.000000	CONTINENTAL
1	98	0.000000	CONTINENTAL
1	99	0.000000	CONTINENTAL
1	100	0.000000	CONTINENTAL

DISCRIMINANT ANALYSIS.....CONTINENTAL VS BRACKISH SIXTEEN VAR

NUMBER OF GROUPS 2
NUMBER OF VARIABLES 16
SAMPLE SIZES:
GROUP 1 199
2 199

DISCRIMINANT FUNCTION CONTINENTAL
CONSTANT * COEFFICIENTS

-73.7195892334 *
0.0001575540
0.0031158940
-0.1977338195
0.0001892720
-0.0000379400
0.0266610908
1.9659404755
-0.2137164474
0.0002907659
-0.2823676467
0.0414306633
0.0296544991
0.0070289001
0.0397032499
0.3290313612
0.0225318260

DISCRIMINANT FUNCTION BRACKISH
CONSTANT * COEFFICIENTS

-79.5686187744 *
-0.0002453530
0.0116714947
-0.4009277821
0.0001675430
0.000704510
0.0275542874
1.7192916870
-0.1908112168
0.0007169410
-0.0284233727
0.0431203246
0.3511693478
-0.0149626993

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
4424	5.0	0.0	CONTINENTAL
4425	0.9	0.0	CONTINENTAL
4426	1.2	0.0	CONTINENTAL
4427	0.0	0.0	CONTINENTAL
4428	0.0	0.0	CONTINENTAL
4429	0.0	0.0	CONTINENTAL
4430	0.0	0.0	CONTINENTAL
4431	0.0	0.0	CONTINENTAL
4432	0.0	0.0	CONTINENTAL
4433	0.0	0.0	CONTINENTAL
4434	0.0	0.0	CONTINENTAL
4435	0.0	0.0	CONTINENTAL
4436	0.0	0.0	CONTINENTAL
4437	0.0	0.0	CONTINENTAL
4438	0.0	0.0	CONTINENTAL
4439	0.0	0.0	CONTINENTAL
4440	0.0	0.0	CONTINENTAL
4441	0.0	0.0	CONTINENTAL
4442	0.0	0.0	CONTINENTAL
4443	0.0	0.0	CONTINENTAL
4444	0.0	0.0	CONTINENTAL
4445	0.0	0.0	CONTINENTAL
4446	0.0	0.0	CONTINENTAL
4447	0.0	0.0	CONTINENTAL
4448	0.0	0.0	CONTINENTAL
4449	0.0	0.0	CONTINENTAL
4450	0.0	0.0	CONTINENTAL
4451	0.0	0.0	CONTINENTAL
4452	0.0	0.0	CONTINENTAL
4453	0.0	0.0	CONTINENTAL
4454	0.0	0.0	CONTINENTAL
4455	0.0	0.0	CONTINENTAL
4456	0.0	0.0	CONTINENTAL
4457	0.0	0.0	CONTINENTAL
4458	0.0	0.0	CONTINENTAL
4459	0.0	0.0	CONTINENTAL
4460	0.0	0.0	CONTINENTAL
4461	0.0	0.0	CONTINENTAL
4462	0.0	0.0	CONTINENTAL
4463	0.0	0.0	CONTINENTAL
4464	0.0	0.0	CONTINENTAL
4465	0.0	0.0	CONTINENTAL
4466	0.0	0.0	CONTINENTAL
4467	0.0	0.0	CONTINENTAL
4468	0.0	0.0	CONTINENTAL
4469	0.0	0.0	CONTINENTAL
4470	0.0	0.0	CONTINENTAL
4471	0.0	0.0	CONTINENTAL
4472	0.0	0.0	CONTINENTAL
4473	0.0	0.0	CONTINENTAL
4474	0.0	0.0	CONTINENTAL
4475	0.0	0.0	CONTINENTAL
4476	0.0	0.0	CONTINENTAL
4477	0.0	0.0	CONTINENTAL
4478	0.0	0.0	CONTINENTAL
4479	0.0	0.0	CONTINENTAL
4480	0.0	0.0	CONTINENTAL
4481	0.0	0.0	CONTINENTAL
4482	0.0	0.0	CONTINENTAL
4483	0.0	0.0	CONTINENTAL
4484	0.0	0.0	CONTINENTAL
4485	0.0	0.0	CONTINENTAL
4486	0.0	0.0	CONTINENTAL
4487	0.0	0.0	CONTINENTAL
4488	0.0	0.0	CONTINENTAL
4489	0.0	0.0	CONTINENTAL
4490	0.0	0.0	CONTINENTAL
4491	0.0	0.0	CONTINENTAL
4492	0.0	0.0	CONTINENTAL
4493	0.0	0.0	CONTINENTAL
4494	0.0	0.0	CONTINENTAL
4495	0.0	0.0	CONTINENTAL
4496	0.0	0.0	CONTINENTAL
4497	0.0	0.0	CONTINENTAL
4498	0.0	0.0	CONTINENTAL
4499	0.0	0.0	CONTINENTAL
4500	0.0	0.0	CONTINENTAL
4501	0.0	0.0	CONTINENTAL
4502	0.0	0.0	CONTINENTAL
4503	0.0	0.0	CONTINENTAL
4504	0.0	0.0	CONTINENTAL
4505	0.0	0.0	CONTINENTAL
4506	0.0	0.0	CONTINENTAL
4507	0.0	0.0	CONTINENTAL
4508	0.0	0.0	CONTINENTAL
4509	0.0	0.0	CONTINENTAL
4510	0.0	0.0	CONTINENTAL

Appendix 8

Classification for the Unknown Samples in the Groups
Marine vs. Continental-Brackish 24 Variables

DISCRIMINANT ANALYSIS.....CON. BRACK VS MARINE TWENTY FOUR

NUMBER OF GROUPS 2
 NUMBER OF VARIABLES 24
 SAMPLE SIZES 189
 GROUP 1
 2

DISCRIMINANT FUNCTION CONTINENTAL BRACKISH
 CONSTANT * COEFFICIENTS

-672.1210937500 *
 0.0023922140
 0.00132266519
 0.00132266569
 -0.00132266569
 -0.2281978130
 -0.1974661946
 0.5982895589
 0.7053162244
 0.2089881301
 -0.0009948500
 -0.0097321644
 -0.096544554
 0.5982895589
 0.000887020
 -0.00222475988

DISCRIMINANT FUNCTION MARINE
 CONSTANT * COEFFICIENTS

-655.8234363281 *
 0.0022711051
 -0.0036666320
 -0.0036666320
 -0.0036666320
 -0.0061298102
 2.7983722687
 -0.0033960200
 -0.0583203984
 0.0017484350
 0.0011681900
 -0.1170145273
 -0.4444887638
 0.6673902869
 0.0008191429
 -0.0565382838

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
1	599.5	0.75306	CONTINENTAL BRACKISH
2	600.0	0.72686	CONTINENTAL BRACKISH
3	600.0	0.71989	MARINE
4	603.2	0.61210	MARINE
5	603.4	0.58998	MARINE
6	605.7	0.98443	MARINE
7	607.2	0.99442	MARINE
8	617.45	0.94612	CONTINENTAL BRACKISH
9	612.0	0.93324	MARINE
10	618.0	0.93324	MARINE
11	622.0	0.94223	MARINE
12	622.0	0.71200	MARINE
13	623.0	0.93354	MARINE
14	624.0	0.93583	MARINE
15	631.0	1.00000	CONTINENTAL BRACKISH
16	632.3	0.93944	MARINE
17	633.8	0.94819	CONTINENTAL BRACKISH
18	635.0	0.99185	CONTINENTAL BRACKISH
19	638.0	0.99755	CONTINENTAL BRACKISH
20	642.0	0.99939	CONTINENTAL BRACKISH
21	644.5	0.99994	CONTINENTAL BRACKISH
22	645.0	0.99990	CONTINENTAL BRACKISH
23	645.0	0.99988	CONTINENTAL BRACKISH
24	650.0	0.99608	CONTINENTAL BRACKISH
25	650.0	0.73570	CONTINENTAL BRACKISH
26	650.0	1.00000	CONTINENTAL BRACKISH
27	653.8	0.99908	CONTINENTAL BRACKISH
28	655.0	0.99908	CONTINENTAL BRACKISH
29	655.0	0.99954	CONTINENTAL BRACKISH
30	660.0	0.99999	CONTINENTAL BRACKISH
31	660.0	0.99999	CONTINENTAL BRACKISH
32	660.0	0.99999	CONTINENTAL BRACKISH
33	662.0	0.99982	CONTINENTAL BRACKISH
34	662.0	0.99982	CONTINENTAL BRACKISH
35	667.0	0.99994	CONTINENTAL BRACKISH
36	667.0	0.99775	CONTINENTAL BRACKISH
37	667.0	0.99775	CONTINENTAL BRACKISH
38	667.0	0.99775	CONTINENTAL BRACKISH
39	668.0	0.99692	MARINE
40	668.0	0.99692	MARINE
41	673.0	0.97981	CONTINENTAL BRACKISH
42	673.0	0.94740	CONTINENTAL BRACKISH
43	674.5	0.94200	CONTINENTAL BRACKISH
44	675.5	0.97350	CONTINENTAL BRACKISH
45	677.0	0.95944	CONTINENTAL BRACKISH
46	679.0	0.83599	CONTINENTAL BRACKISH
47	679.0	0.80699	CONTINENTAL BRACKISH
48	682.0	0.97272	CONTINENTAL BRACKISH
49	683.0	0.73436	MARINE
50	685.0	0.00000	MARINE
51	685.0	0.97146	CONTINENTAL BRACKISH
52	685.0	0.99998	CONTINENTAL BRACKISH

DISCRIMINANT ANALYSIS.....CON BRACK VS MARINE TWENTY FOUR

NUMBER OF GROUPS 2
 NUMBER OF VARIABLES 24
 SAMPLE SIZES
 GROUP 1 199
 GROUP 2 199

DISCRIMINANT FUNCTION CONTINENTAL BRACKISH

CONSTANT * COEFFICIENTS
 -672.1210937500 *
 0.0023022140
 0.0034743431
 0.0015331593
 -2.24232565689
 0.1545892954
 -0.0168817602
 0.0038947670
 -0.0003552490
 -0.0017535309
 2.24232565689
 -0.0027592271
 0.0415930673
 0.0017466519
 -0.0013260569
 -0.221978130
 0.882885520
 0.000387020
 -0.0522475988

DISCRIMINANT FUNCTION MARINE

CONSTANT * COEFFICIENTS
 -655.8234863281 *
 0.0022711051
 0.0034354799
 0.0043331588
 -2.7221869886
 0.1550195084
 -0.0041047707
 0.0038666320
 -0.0009121930
 -0.0011681900
 -0.1170145273
 -0.4444887638
 0.6673903869
 0.00088191423
 -0.2134951525
 -0.0009121930
 -0.004515420
 -0.3353826802
 0.5841433545
 0.00088191423
 -0.2565532833

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
1529	1	0.9248	CONTINENTAL BRACKISH
1530	2	0.9088	MARINE
1531	1	0.94870	CONTINENTAL BRACKISH
1532	0	0.98767	MARINE
1533	1	0.98161	CONTINENTAL BRACKISH
1534	0	0.9359	MARINE
1535	0	0.9876	CONTINENTAL BRACKISH
1536	0	0.9392	MARINE
1537	0	0.9303	CONTINENTAL BRACKISH
1538	0	0.9309	MARINE
1539	0	0.9329	CONTINENTAL BRACKISH
1540	1	0.9783	MARINE
1541	1	0.9293	CONTINENTAL BRACKISH
1542	1	0.9267	MARINE
1543	0	0.9307	CONTINENTAL BRACKISH
1544	0	0.7497	MARINE
1545	0	0.5296	CONTINENTAL BRACKISH
1546	0	0.6844	MARINE
1547	0	0.9241	CONTINENTAL BRACKISH
1548	0	0.9241	MARINE
1549	0	0.9241	CONTINENTAL BRACKISH
1550	0	0.9241	MARINE
1551	0	0.9241	CONTINENTAL BRACKISH
1552	0	0.9241	MARINE
1553	0	0.9241	CONTINENTAL BRACKISH
1554	0	0.9241	MARINE
1555	0	0.9241	CONTINENTAL BRACKISH
1556	0	0.9241	MARINE
1557	0	0.9241	CONTINENTAL BRACKISH
1558	0	0.9241	MARINE
1559	0	0.9241	CONTINENTAL BRACKISH
1560	0	0.9241	MARINE
1561	0	0.9241	CONTINENTAL BRACKISH
1562	0	0.9241	MARINE
1563	0	0.9241	CONTINENTAL BRACKISH
1564	0	0.9241	MARINE
1565	0	0.9241	CONTINENTAL BRACKISH
1566	0	0.9241	MARINE
1567	0	0.9241	CONTINENTAL BRACKISH
1568	0	0.9241	MARINE
1569	0	0.9241	CONTINENTAL BRACKISH
1570	0	0.9241	MARINE
1571	0	0.9241	CONTINENTAL BRACKISH
1572	0	0.9241	MARINE
1573	0	0.9241	CONTINENTAL BRACKISH
1574	0	0.9241	MARINE
1575	0	0.9241	CONTINENTAL BRACKISH
1576	0	0.9241	MARINE
1577	0	0.9241	CONTINENTAL BRACKISH
1578	0	0.9241	MARINE
1579	0	0.9241	CONTINENTAL BRACKISH
1580	0	0.9241	MARINE
1581	0	0.9241	CONTINENTAL BRACKISH
1582	0	0.9241	MARINE
1583	0	0.9241	CONTINENTAL BRACKISH
1584	0	0.9241	MARINE
1585	0	0.9241	CONTINENTAL BRACKISH
1586	0	0.9241	MARINE
1587	0	0.9241	CONTINENTAL BRACKISH
1588	0	0.9241	MARINE
1589	0	0.9241	CONTINENTAL BRACKISH
1590	0	0.9241	MARINE
1591	0	0.9241	CONTINENTAL BRACKISH
1592	0	0.9241	MARINE
1593	0	0.9241	CONTINENTAL BRACKISH
1594	0	0.9241	MARINE
1595	0	0.9241	CONTINENTAL BRACKISH
1596	0	0.9241	MARINE
1597	0	0.9241	CONTINENTAL BRACKISH
1598	0	0.9241	MARINE
1599	0	0.9241	CONTINENTAL BRACKISH

Appendix 9

Classification for the Unknown Samples in the Groups
Continental vs. Brackish 24 Variables

DISCRIMINANT ANALYSIS.....CONTINENTAL VS BRACKISH TWENTY FOUR

NUMBER OF GROUPS 2
 NUMBER OF VARIABLES 24
 SAMPLE SIZES *
 GROUP 1 189
 GROUP 2 189

DISCRIMINANT FUNCTION COEFFICIENTS
 -663.8369140625 *
 0.0019659661
 0.0034450591
 0.0655317307
 -2.4971886063
 -0.1932204628
 0.00311754867
 0.0050696507
 -0.00079820
 0.0233819932
 4.810519180
 -0.0046755746
 0.1078732610
 0.0006231421
 -0.00000616750
 -0.000262941
 -0.7451632619
 0.5155697465
 0.0008883561
 -0.0095824599

DISCRIMINANT FUNCTION BRACKISH CONSTANT * COEFFICIENTS
 -642.0764160156 *
 0.0019000189
 0.0034254899
 0.0655261142
 -2.5129718781
 -0.1079488397
 0.0068739504
 -0.0049727596
 -0.0005764819
 0.0244941637
 4.5443363190
 -0.0030409261
 0.1114441156
 0.0007596740
 0.0000295020
 -1.1779478980
 -0.7116590278
 0.4894944429
 0.0007662520
 0.1816170812

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
1	598.5	0.97837	CONTINENTAL
2	0.0	0.98535	CONTINENTAL
3	0.0	0.99998	CONTINENTAL
4	603.0	1.00000	CONTINENTAL
5	603.2	0.99984	CONTINENTAL
6	605.7	0.99992	CONTINENTAL
7	607.7	0.99997	CONTINENTAL
8	611.5	0.99997	CONTINENTAL
9	612.3	1.00000	CONTINENTAL
10	612.0	0.99998	CONTINENTAL
11	614.3	0.99994	CONTINENTAL
12	618.0	0.99998	CONTINENTAL
13	623.0	0.99985	CONTINENTAL
14	623.1	0.99985	CONTINENTAL
15	624.0	0.99977	CONTINENTAL
16	631.0	0.99976	CONTINENTAL
17	632.3	0.99976	CONTINENTAL
18	633.8	0.99979	CONTINENTAL
19	635.0	0.99979	CONTINENTAL
20	638.0	0.99978	CONTINENTAL
21	640.0	0.99978	CONTINENTAL
22	644.0	0.99996	CONTINENTAL
23	645.0	0.99996	CONTINENTAL
24	645.0	0.99996	CONTINENTAL
25	648.0	0.99996	CONTINENTAL
26	650.5	1.00000	CONTINENTAL
27	652.5	1.00000	CONTINENTAL
28	653.5	1.00000	CONTINENTAL
29	657.0	1.00000	CONTINENTAL
30	658.0	1.00000	CONTINENTAL
31	660.5	1.00000	CONTINENTAL
32	661.0	0.99996	CONTINENTAL
33	662.0	0.99996	CONTINENTAL
34	663.5	0.99999	CONTINENTAL
35	664.5	0.99999	CONTINENTAL
36	667.9	0.99999	CONTINENTAL
37	667.9	0.99999	CONTINENTAL
38	668.1	0.99999	CONTINENTAL
39	673.0	0.99984	CONTINENTAL
40	673.5	0.99984	CONTINENTAL
41	673.5	0.99984	CONTINENTAL
42	675.5	0.99985	CONTINENTAL
43	677.0	0.99990	CONTINENTAL
44	679.0	0.99961	CONTINENTAL
45	679.5	0.99318	CONTINENTAL
46	682.0	0.99306	CONTINENTAL
47	685.0	0.99635	CONTINENTAL
48	685.2	0.99184	CONTINENTAL
49	689.0	0.99997	CONTINENTAL
50	693.0	0.99999	CONTINENTAL

DISCRIMINANT ANALYSIS.....CONTINENTAL VS BRACKISH TWENTY FOUR

NUMBER OF GROUPS 2
 NUMBER OF VARIABLES 24
 SAMPLE SIZES...
 GROUP
 1 199
 2 199

DISCRIMINANT FUNCTION CONTINENTAL
 CONSTANT * COEFFICIENTS

-663.8369140625 *
 0.0019659661 0.0050696507 0.0006231421 -0.0000616750
 0.0034450591 -0.0007798420 -0.0005365841 0.0110289907
 0.0655317307 0.0233819932 -1.4350414276 -0.7451632619
 -2.4571886063 4.8100319180 0.2483490050 0.5155697465
 -0.1032204628 -0.0046755746 0.5587678552 0.0008383561
 0.0311754867 0.1078732610 0.2280504107 -0.0095824599

DISCRIMINANT FUNCTION BRACKISH
 CONSTANT * COEFFICIENTS

-642.0764160156 *
 0.0019000189 0.0049727596 0.0007596740 -0.0005858261
 0.0034354839 -0.0005764819 0.0000255920 0.0106478557
 0.0655161142 0.0244941637 -1.1779479980 -0.7116690278
 -2.5129718781 4.5443363190 0.3072032928 0.4894944429
 -0.1079488397 -0.0030409261 0.5783316493 0.0007662550
 0.0068739504 0.1114441156 0.1816170812 0.0122591124

EVALUATION OF CLASSIFICATION FUNCTIONS FOR EACH OBSERVATION
 GROUP CONTINENTAL

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
ST-424	1539.5-1540.0	0.99986	CONTINENTAL
ST-425	1540.0-1545.5	0.99957	CONTINENTAL
ST-426	1545.5-1551.0	0.99110	CONTINENTAL
ST-427	1551.0-1555.0	0.96419	CONTINENTAL
ST-428	1555.0-1555.0	0.51519	CONTINENTAL
ST-429	1555.0-1560.0	0.82911	CONTINENTAL
ST-430	1560.0-1562.5	0.90265	CONTINENTAL
ST-431	1562.5-1563.0	0.99642	CONTINENTAL
ST-433	1564.0-1566.0	0.99945	CONTINENTAL
ST-434	1566.0-1569.0	0.99987	CONTINENTAL
ST-435	1569.0-1570.5	0.99998	CONTINENTAL
ST-436	1570.5-1571.0	0.99917	CONTINENTAL
ST-437	1571.0-1572.5	0.99955	CONTINENTAL
ST-439	1573.5-1577.5	1.00000	CONTINENTAL
ST-440	1577.5-1582.0	0.99988	CONTINENTAL
ST-441	1582.0-1585.5	0.91800	BRACKISH
ST-442	1585.5-1590.5	0.50513	CONTINENTAL
ST-443	1590.5-1595.0	0.85714	CONTINENTAL
ST-444	1595.0-1597.5	0.99989	CONTINENTAL
ST-445	1597.5-1600.5	0.99898	CONTINENTAL
ST-447	1601.0-1601.2	0.99998	CONTINENTAL
ST-448	1601.2-1605.0	0.70370	CONTINENTAL
ST-449	1605.0-1608.5	0.99781	BRACKISH
ST-451	1611.5-1613.0	0.99788	BRACKISH
ST-452	1613.0-1614.0	0.99999	BRACKISH
ST-454	1614.2-1614.5	0.99978	BRACKISH
ST-456	1617.5-1617.6	0.99948	BRACKISH
ST-458	1622.5-1623.0	0.99929	BRACKISH

ST-464	1631.0-1633.5	0.99990	BRACKISH
ST-465	1633.5-1638.5	1.00000	BRACKISH
ST-466	1638.5-1640.0	0.61642	BRACKISH
ST-468	1641.0-1647.0	0.99948	BRACKISH
ST-469	1642.0-1652.0	0.98599	CONTINENTAL
ST-470	1652.0-1657.0	0.74785	CONTINENTAL
ST-471	1657.0-1662.0	0.50305	BRACKISH
ST-472	1662.0-1666.0	0.99865	CONTINENTAL
ST-473	1666.0-1668.0	0.98949	CONTINENTAL
ST-474	1668.0-1672.0	1.00000	CONTINENTAL
ST-475	1672.0-1677.0	0.99766	CONTINENTAL
ST-476	1677.0-1683.0	0.99941	CONTINENTAL
ST-477	1683.0-1684.0	0.98569	CONTINENTAL
ST-478	1684.0-1688.0	1.00000	CONTINENTAL
ST-479	1688.0-1689.0	1.00000	CONTINENTAL
ST-480	1689.0-1693.0	1.00000	CONTINENTAL
ST-481	1693.0-1694.0	1.00000	CONTINENTAL
ST-482	1694.0-1697.0	1.00000	CONTINENTAL
ST-483	1697.0-1698.0	1.00000	CONTINENTAL
ST-484	1698.0-1702.0	1.00000	CONTINENTAL
ST-485	1702.0-1705.0	0.99880	CONTINENTAL
ST-486	1705.0-1707.0	0.99933	CONTINENTAL
ST-487	1707.0-1711.0	0.99638	CONTINENTAL
ST-488	1711.0-1715.5	0.99999	CONTINENTAL
ST-490	1716.0-1721.0	1.00000	CONTINENTAL
ST-491	1721.0-1725.5	0.99997	CONTINENTAL
ST-492	1725.5-1728.0	1.00000	CONTINENTAL
ST-493	1728.0-1730.0	0.99996	CONTINENTAL
ST-494	1730.0-1735.0	0.99999	CONTINENTAL
ST-495	1735.0-1736.0	0.99986	CONTINENTAL
ST-496	1736.0-1736.2	0.91467	CONTINENTAL
ST-497	1736.2-1739.5	0.99994	CONTINENTAL
ST-498	1739.5-1743.0	0.99996	CONTINENTAL
ST-499	1743.0-1750.5	1.00000	CONTINENTAL
ST-500	1750.5-1751.5	0.99994	CONTINENTAL
ST-503	1753.0-1754.0	0.95797	CONTINENTAL
ST-504	1754.0-1755.5	1.00000	CONTINENTAL
ST-505	1755.5-1757.5	1.00000	CONTINENTAL
ST-506	1757.5-1759.0	0.99290	CONTINENTAL
ST-507	1759.0-1762.0	0.51684	CONTINENTAL
ST-508	1762.0-1765.0	0.99959	BRACKISH
ST-509	1765.0-1767.0	1.00000	CONTINENTAL
ST-510	1767.0-1768.0	0.99305	CONTINENTAL
ST-512	1768.3-1769.0	0.99982	CONTINENTAL
ST-513	1769.0-1770.0	0.99964	BRACKISH
ST-515	1771.0-1771.5	0.99677	CONTINENTAL
ST-516	1771.5-1778.0	0.99989	CONTINENTAL
ST-517	1778.0-1779.5	0.86371	CONTINENTAL
ST-519	1779.5-1781.5	0.99841	CONTINENTAL
ST-520	1781.5-1782.5	0.99554	CONTINENTAL
ST-521	1782.5-1783.0	0.99999	CONTINENTAL
ST-522	1783.0-1784.0	0.99983	CONTINENTAL
ST-523	1784.0-1785.5	0.99999	CONTINENTAL
ST-524	1785.5-1787.0	0.98260	CONTINENTAL
ST-525	1787.0-1788.5	0.99953	CONTINENTAL
ST-526	1788.5-1789.0	0.99776	CONTINENTAL
ST-527	1789.0-1790.5	0.99990	CONTINENTAL
ST-528	1790.5-1793.0	0.99995	CONTINENTAL
ST-529	1793.0-1797.0	1.00000	CONTINENTAL
ST-530	1797.0-1798.5	0.99894	CONTINENTAL
ST-531	1798.5-1799.0	0.99991	CONTINENTAL
ST-532	1799.0-1800.5	1.00000	CONTINENTAL
ST-533	1800.5-1804.0	0.99994	CONTINENTAL
	1804.0-1806.0	1.00000	CONTINENTAL

ST-534	1806.0-1808.0	1.00000	CONTINENTAL
ST-535	1808.0-1814.5	1.00000	CONTINENTAL
ST-536	1814.5-1815.5	1.00000	CONTINENTAL
ST-537	1815.5-1818.5	1.00000	CONTINENTAL
ST-538	1818.5-1819.0	1.00000	CONTINENTAL
ST-539	1819.0-1821.0	1.00000	CONTINENTAL
ST-540	1821.0-1823.0	0.98071	CONTINENTAL
ST-541	1823.0-1825.5	1.00000	CONTINENTAL
ST-542	1825.5-1827.0	0.99290	CONTINENTAL
ST-543	1827.0-1830.0	0.99984	CONTINENTAL
ST-544	1830.0-1831.5	0.99998	CONTINENTAL
ST-545	1831.5-1833.0	0.99946	CONTINENTAL
ST-546	1833.0-1834.0	0.98777	CONTINENTAL
ST-547	1834.0-1835.5	0.98921	CONTINENTAL
ST-548	1835.5-1837.0	0.99978	CONTINENTAL
ST-549	1837.0-1844.0	0.99996	CONTINENTAL
ST-550	1844.0-1844.5	0.99876	CONTINENTAL
ST-551	1844.5-1845.0	0.81534	BRACKISH
ST-552	1845.0-1846.0	0.99452	BRACKISH
ST-553	1846.0-1847.0	0.96102	CONTINENTAL
ST-554	1847.0-1850.0	0.80746	BRACKISH
ST-555	1850.0-1851.0	0.99893	CONTINENTAL
ST-556	1851.0-1853.0	0.61844	CONTINENTAL
ST-557	1853.0-1853.5	0.99886	CONTINENTAL
ST-558	1853.5-1855.5	0.92123	CONTINENTAL
ST-559	1855.5-1857.0	0.92484	CONTINENTAL
ST-560	1857.0-1857.5	0.99781	CONTINENTAL
ST-561	1857.5-1859.0	0.99715	CONTINENTAL
ST-563	1860.5-1861.5	0.99946	CONTINENTAL
ST-564	1861.5-1867.0	0.99455	CONTINENTAL
ST-565	1867.0-1868.0	0.99766	CONTINENTAL
ST-566	1868.5-1868.5	0.88955	BRACKISH
ST-567	1868.5-1873.0	0.99994	CONTINENTAL
ST-568	1873.0-1878.0	0.99999	CONTINENTAL
ST-569	1878.0-1883.0	0.99987	CONTINENTAL
ST-570	1883.0-1886.0	1.00000	CONTINENTAL
ST-571	1886.0-1887.5	0.98878	CONTINENTAL
ST-572	1887.5-1892.5	0.99918	CONTINENTAL
ST-573	1892.5-1893.5	0.96498	CONTINENTAL
ST-574	1893.5-1895.0	0.99996	CONTINENTAL
ST-575	1895.0-1896.5	0.99974	CONTINENTAL
ST-576	1896.5-1898.5	0.98799	CONTINENTAL
ST-577	1898.5-1900.0	1.00000	CONTINENTAL
ST-578	1900.0-1906.0	0.99994	CONTINENTAL
ST-579	1906.0-1910.5	0.99406	CONTINENTAL
ST-580	1910.5-1912.5	0.99999	CONTINENTAL
ST-581	1912.5-1914.5	0.99976	CONTINENTAL
ST-582	1914.5-1916.0	0.99999	CONTINENTAL
ST-583	1916.0-1920.0	0.99984	CONTINENTAL
ST-584	1920.0-1921.0	0.99996	CONTINENTAL
ST-585	1921.0-1925.5	1.00000	CONTINENTAL
ST-586	1925.5-1927.5	1.00000	CONTINENTAL
ST-587	1927.5-1929.0	1.00000	CONTINENTAL
ST-588	1929.0-1930.5	1.00000	CONTINENTAL
ST-589	1930.5-1936.5	1.00000	CONTINENTAL
ST-590	1936.5-1936.8	0.99989	CONTINENTAL
ST-591	1936.8-1942.0	0.99984	CONTINENTAL
ST-592	1942.0-1943.5	1.00000	CONTINENTAL
ST-593	1943.5-1944.5	1.00000	CONTINENTAL
ST-594	1944.5-1945.5	0.53862	BRACKISH
ST-595	1945.5-1947.0	1.00000	CONTINENTAL
ST-596	1947.0-1948.0	0.99998	CONTINENTAL
ST-597	1948.0-1953.0	0.99998	CONTINENTAL
ST-598	1953.0-1954.0	0.99998	CONTINENTAL
ST-599	1954.0-1955.5	1.00000	CONTINENTAL
ST-600	1955.5-1956.0	1.00000	CONTINENTAL

SAMPLE NO.	DEPTH	PROBABILITY	SAMPLE CLASSIFICATION
ST-601	1956.0-1958.0	0.99983	CONTINENTAL
ST-602	1958.0-1959.0	1.00000	CONTINENTAL
ST-603	1959.0-1959.7	0.99994	CONTINENTAL
ST-604	1959.7-1960.7	0.99998	CONTINENTAL
ST-605	1960.7-1960.9	0.99063	CONTINENTAL
ST-606	1960.9-1962.0	0.99835	CONTINENTAL
ST-607	1962.0-1963.3	0.99597	CONTINENTAL
ST-608	1963.3-1964.0	0.99915	CONTINENTAL
ST-609	1964.0-1966.0	1.00000	CONTINENTAL
ST-610	1966.0-1968.0	0.99974	CONTINENTAL
ST-611	1968.0-1970.5	0.99968	CONTINENTAL
ST-612	1970.5-1974.0	0.74651	BRACKISH
ST-613	1974.0-1983.0	0.69854	CONTINENTAL
ST-614	1983.0-1983.5	0.96751	BRACKISH
ST-615	1983.5-1989.0	0.99513	CONTINENTAL
ST-616	1989.0-1990.5	0.99756	CONTINENTAL
ST-617	1990.5-1993.5	0.99843	CONTINENTAL
ST-618	1993.5-1999.5	0.99991	CONTINENTAL
ST-619	1999.5-2000.5	0.99823	CONTINENTAL
ST-620	2000.5-2007.0	0.99964	BRACKISH
ST-621	2007.0-2012.0	0.99998	BRACKISH
ST-622	2012.0-2017.0	0.99958	BRACKISH
ST-624	2019.5-2021.5	0.56140	CONTINENTAL
ST-625	2021.5-2027.0	0.97466	CONTINENTAL
ST-626	2027.0-2027.5	0.92007	CONTINENTAL
ST-627	2027.5-2032.5	0.99918	CONTINENTAL
ST-628	2032.5-2038.0	0.82661	CONTINENTAL
ST-629	2038.0-2040.0	0.79150	CONTINENTAL
ST-630	2040.0-2041.0	0.99895	BRACKISH
ST-631	2041.0-2044.0	0.99997	CONTINENTAL
ST-632	2044.0-2045.5	1.00000	CONTINENTAL
ST-633	2045.5-2048.5	0.90890	BRACKISH
ST-634	2048.5-2050.5	0.96636	CONTINENTAL
ST-635	2050.5-2051.0	0.99967	CONTINENTAL
ST-636	2051.0-2054.0	1.00000	CONTINENTAL
ST-637	2054.0-2055.0	1.00000	CONTINENTAL
ST-638	2055.0-2056.0	0.99994	CONTINENTAL
ST-639	2056.0-2057.5	0.99218	CONTINENTAL
ST-640	2057.5-2059.5	0.61057	CONTINENTAL
GROUP	BRACKISH		
ST-641	2059.5-2062.5	0.99821	CONTINENTAL
ST-642	2062.5-2068.5	0.99701	CONTINENTAL
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ST-845	2540.0-2541.0	1.00000	CONTINENTAL

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