

THE EVOLUTION OF HYDROTHERMAL FLUIDS AT THE PIPELINE  
GOLD MINE, LANDER COUNTY, NEVADA

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## ABSTRACT

Pipeline is a sediment-hosted, disseminated gold deposit located 120 km southwest of Elko, Nevada. Gold mineralization is argillization-hematite-silicification-gold in decalcified Roberts Mountains Formation. Pipeline and its extensions comprise a global resource of 13.13 million oz. gold and total mineralization reserves of 8.2 million oz.. Such large reserves and high tonnage make Pipeline an important deposit to study. In addition, samples could be collected at the commencement of mining activities before valuable information was lost by mining activities.

Until now, the genesis of Carlin-type deposits was considered enigmatic. Proposed sources of gold include magmatic, amagmatic, metamorphic and meteoric sources. Features of Carlin-type deposits remaining unanswered include the timing of gold mineralization, fluid sources, high-salinity fluid inclusions, the significance of carbonic fluid inclusions, a depositional mechanism, water-rock ratios for mineralizing fluids, and P-T conditions during gold mineralization. By applying a combination of analytical methods and field studies that are not widely used in Nevada, for the first time a coherent picture of mineralization processes and fluid sources of gold-bearing fluids was obtained that explain much of the contradictory evidence accumulated by previous studies. The objectives were to explore the genesis and timing of the Pipeline mineralization and to test the hypothesis that gold mineralization is coeval with decalcification in a Carlin-type deposit.

The study comprised field observations in addition to logging and sampling drillcore during 3 field seasons. Analytical methods applied include fluid inclusion

microthermometry, fluid inclusion gas analysis, fluid inclusion bulk crush leach,  $^{40}\text{Ar}/^{39}\text{Ar}$  dating, clay analysis, petrographic microscopy, reflected-light microscopy and electron microprobe analysis.

Pipeline mineralization occurs in sheared, brecciated and decalcified Roberts Mountain Formation below the Roberts Mountains thrust. Mineralization is quartz, minor sericite, hematite, goethite, minor calcite, and finely disseminated gold.

A paragenetic sequence for the Pipeline deposit is established. Stage 1 comprises dark petroliferous calcite. Stage 2 is represented by white calcite and is thought to be coeval with the Antler orogeny. Stage 3 is quartz-sericite-calcite-pyrite-gold with veins occurring beneath the deposit and that are considered the hydrothermal feeders to the deposit. The stage 3 veins are linked to gold mineralization within the deposit by age dating and only stage 3 veins have gold selvages associated with them. Oxidation characterizes stage 4 with pseudomorph replacement of sulfides by Fe-oxides. Vuggy calcite, which occurs in veins and open space fillings in the ore deposit, represents stage 5 that locally predates the Basin- and-Range faulting.

Pipeline fluid inclusion studies identify 3 inclusion types. Type 1a are aqueous dominated with a minor vapor bubble. Type 1b are aqueous dominated with a minor carbonic phase and bubble. Type 2 inclusions have  $\text{CO}_2$  and other gaseous species equal to or greater than the aqueous phase. Stage 1 calcite contains Type 1a inclusions, one population has methane-bearing clathrates with melting temperatures ( $T_m$ ) up to  $23.3^\circ\text{C}$  whereas the second population are low salinity fluids. Stage 2 white calcite inclusions are Type 2 and the salinity ranges up to 0.8 eq. wt. % NaCl. Stage 3 vein and ore quartz contain aqueous Type 1 inclusions and Type 2 inclusions. Stage 3 quartz Type 1 inclusion

salinities range from 5 to 25 eq. wt. % NaCl and homogenization temperatures ( $T_h$ ) range from 179° to 265°C. Hypersaline Type 1 inclusions have anomalous calcium-rich fluid with Ca/Na ratios of 0.8 to 1.4. Quartz-hosted stage 3, Type 2 inclusions are about 1:8 H<sub>2</sub>O-CO<sub>2</sub>, have salinities about 0.5 eq. wt. % NaCl and  $T_h$  ranges from 285° to 323°C. Calcite-hosted stage 3 inclusions are Type 1a, as are stage 5 calcite inclusions. Stage 3 calcite  $T_h$  values range from 219° to 235°C and calculated salinities are 3.0 to 3.3 eq. wt. % NaCl. Stage 5 calcite  $T_h$  values are ~125°C with low salinity values.

Gas analysis indicates stage 1 calcite inclusion fluids have 93.6 to 97.7 mol. % water and variable CO<sub>2</sub>/CH<sub>4</sub> ratios between 0.5 and 40. The N<sub>2</sub>/Ar ratios indicate meteoric and magmatic fluid components. Stage 2 calcite has high amounts of CO<sub>2</sub> that exceeds 50 mol. % for individual analyses, N<sub>2</sub>/Ar ratios are around 100 and CO<sub>2</sub>/CH<sub>4</sub> are about 100 indicating a meteoric source. Stage 3 quartz fluid inclusion gas analyses show that CO<sub>2</sub> varies from 0.5 to 8 mol. %. Carbon dioxide strongly correlates with H<sub>2</sub>S, which varies from 0.03 to 0.00001 mol. %, and CO<sub>2</sub> inversely correlates with salinity. Fluid inclusion N<sub>2</sub>/Ar ratios are >500 indicating a strong magmatic volatile component. Stage 5 calcite is dominated by fluids that have N<sub>2</sub>/Ar ratios less than 100 and CO<sub>2</sub>/CH<sub>4</sub> ratios ~1, indicating evolved fluids; total volatile contents are less than 1 mol. %.

Quartz bulk fluid inclusion crush leach followed by flame AA for cations and ion chromatography for anions show variable Ca/(Na+K) ratios. High ratios are paired with a high “missing” anion component, interpreted to be bicarbonate.

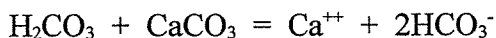
The only clay mineral present in ore zones is illite of 2M<sub>1</sub> polytype. FWHM values of the first order illite peak are positively correlated with decalcification intensity ( $R^2 = 0.41$ ).



Three thermal epochs are identified in the area. Mill Canyon stock biotite gives an  $^{40}\text{Ar}/^{39}\text{Ar}$  plateau age of  $152.2 \pm 0.3$  Ma. Stage 3 hydrothermal sericite from quartz-sericite-calcite veins at Pipeline are dated at  $92.0 \pm 0.3$  Ma that coincides with age dates of alteration minerals by others ranging from 92 to 105 Ma. Age spectra of illite from ore zones have a strong Early Cretaceous component. Inherited argon results in discordant age spectra for some illite samples whereas in other samples, 8% recoil loss accounts for ages slightly older than 92 Ma. Tertiary dikes in the Cortez area give biotite and K-feldspar ages of 35 ~ 36 Ma.

Trapping pressures of inclusions (Pt) are estimated by isochores, MACFLINCOR and from estimates of the geothermal gradient. Estimates of the geothermal gradient, pressure and inclusion Th's, for stage 1 give a depth of ~5 km. Stage 2 calcite pressure estimates calculated by MACFLINCOR are ~1.5 kbar, corresponding to a minimum lithostatic load of ~5km. Stage 3 quartz was deposited at a pressure ~2000 bars. Stage 3 calcite isochores confirm lower pressures for calcite than quartz at any given temperature, suggesting calcite was deposited under lower pressure conditions.

The range in  $\text{CO}_2$  contents of fluid inclusions, the range in fluid salinities that inversely correlate with  $\text{CO}_2$ , and correlation of  $\text{CO}_2$  with  $\text{H}_2\text{S}$  is consistent with decalcification driven by carbonic acid:



As  $\text{CO}_2$  is consumed, spent fluids should increase in ionic strength and  $\text{Ca}^{++}$ ; which is seen in both fluid inclusion and crush-leach analyses. The <1 % Fe in calcite released by calcite solution is available to form  $\text{FeS}_2$ , which explains the paired decrease in fluid inclusion  $\text{CO}_2$  and  $\text{H}_2\text{S}$ . Calculations of ore fluid pH is 4.66 whereas in spent fluid the calculated

average pH is 5.9. Theoretical gold solubility based on fluid inclusion salinity and gas analysis, is calculated to be ~200 ppb in ore fluid and <2 ppb in spent fluid. Gold deposition is attributed to wall rock attack and sulfidization reactions that lowered fluid  $H_2S$  and thus destabilizing Au bisulfide complexes.

Calculated mass-balances of ore fluid to rock give relatively low ratios that are consistent with mineralization by magmatic fluids. Consumption of  $CO_2$  during decalcification, Ca-production and change of gold solubility, are consistent with a water-rock ratio of about 6:1 by weight and explains the very localized alteration commonly observed in Carlin-type deposits.

Conclusions are that prior to gold mineralization were two periods of calcite veining in response to regional magmatic and tectonic events that did not produce gold mineralization. Gold mineralization was coeval with alteration and deposition of quartz during stage 3, around 92 Ma. Fluids derived from an intrusive body and charged with  $CO_2$  penetrated the country rock through fractures and these fluids entered the permeable shear zones within the Roberts Mountains Formation. Decalcification occurred, liberating  $Fe^{++}$  which reacted with  $H_2S$  causing sulfidation. Spent ore fluids were Ca-rich brine that had salinities up to 25 eq. wt. % NaCl. The depletion of  $H_2S$  in ore solutions destabilized the gold bisulfide complexes and initiated gold deposition. Oxidization of the ore body was most likely by subsurface oxygenated waters and not a result of weathering. Following ore-body oxidation was calcite mineralization by evolved waters, and then Basin-and-Range faulting.

This work presents a internally self consistent body of data that yields an understanding of how Pipeline formed, and a genetic model that satisfies mass balance

calculations. Many Pipeline geochemical and physical characteristics are reported in other Carlin-type deposits. The implication is that most Carlin-type deposits have a similar genesis. That is, the driving force and major fluid source is magmatic. The CO<sub>2</sub> and H<sub>2</sub>S charged fluids associated with an intrusive body provide a fluid that serves both to introduce gold and cause decalcification in one event. Gold mineralization is in response to sulfidization reactions. Fluid quantities are limited, hence there are low water-rock ratios and a localized alteration halo. Gold is associated with quartz and sericite mineralization. Depths can be as deep as 8 km, with mineralization under lithostatic pressure, hence, fluid inclusion Th measurements can yield far lower temperatures than mineralizing fluids. Carbonic fluid inclusions are the product of mild varying CO<sub>2</sub> composition that boiled when occasionally highly charged with CO<sub>2</sub>. The oxidation event that replaced pyrite by Fe-oxides may not necessarily be supergene. Multiple intrusive and hydrothermal events occurred at or near the gold deposit, but principally one event introduced to gold.

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*The biggest risk that one could take in life is not taking one at all*

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## CHAPTER 1

### Introduction

The United States of America is currently the world's second biggest gold producer. The greatest domestic gold production occurs in Nevada from Carlin-type gold deposits. Exploration for these deposits commenced in the 1960's following the discovery of gold in the Carlin area (Teal and Jackson, 1997). Subsequent discoveries were made along a linear trend passing through the Carlin mine and elsewhere in north central Nevada. Discovered during the past ten years, Pipeline is one of the largest gold deposits in Nevada. The Pipeline Gold Mine is located in Lander County, approximately 120 km southwest of Elko, Nevada (Fig. 1.1) along a mineralized belt named the Battle Mountain/Eureka trend. Pipeline and its extensions comprise a global resource of 13.13 million oz. gold and total mineralization reserves of 8.2 million oz. (R.C. Hays, pers. comm.).

Carlin-type deposits are hydrothermal gold mineralization hosted in carbonate rocks. These deposits feature finely disseminated gold with low silver to gold ratios, exhibit a similar alteration style, and have a strong structural control. Occurring along regional mineralization trends, these deposits have northwest and northeast-trending faults, and are associated with elevated concentrations of As, Sb, Hg and Te. Pipeline exhibits features typical of Carlin-type deposits including decalcification (calcite removal), argillization, sub-micron gold, carbonate host rocks and mineralization control by shear zones.

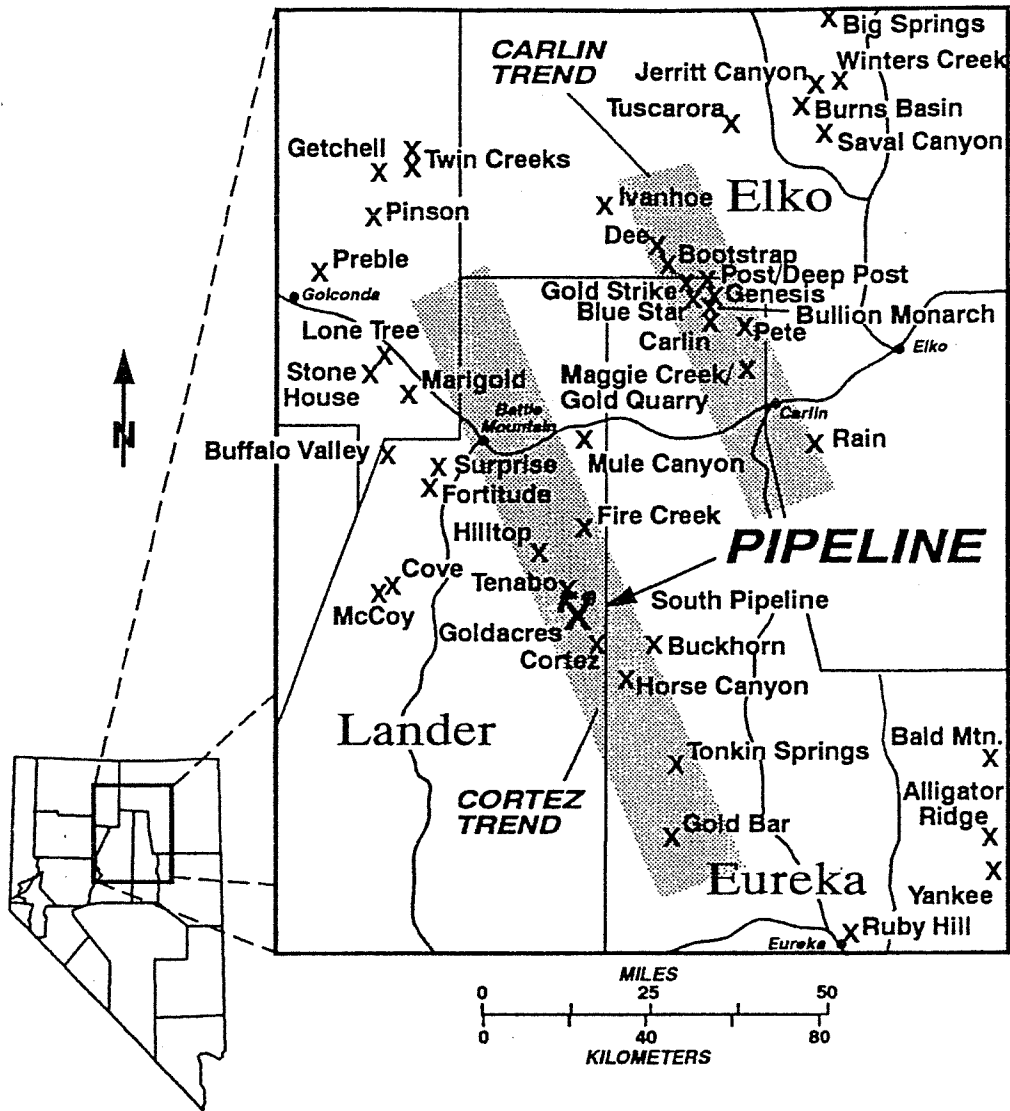


Figure 1.1 Location of the Pipeline deposit and several other gold deposits in Nevada (with permission from Foo et al., 1996). Shaded are the Battle Mountain-Eureka and Carlin trends.

Exploration of Carlin deposits has been driven by economic factors that dictate large, high-tonnage deposits that can be mined in an open pit. An understanding of Carlin-type deposit genesis is necessary for the successful exploration of new deposits, and the formation of predictive strategies to locate hidden reserves nearby known mineralization.

Important milestones influencing our understanding of Carlin-type deposits were made in the past 15 years. The concept of decalcification (also referred to as decarbonation) is recognized as the most prominent alteration style in Carlin-type deposits (Teal and Jackson, 1997). Decalcification refers to the dissolution of calcite to create a suitably porous and permeable host rock by decalcifying fluids. It was first documented at Carlin (Kuehn, 1989; Bakken 1990). These two studies describe hydrothermal fluid being focused along structural conduits and favorable stratigraphic units resulting in pre-ore decalcification, loss of density, coupled with increase of porosity and permeability. Decalcification of the silty limestone protolith at Carlin is more widespread and intense, this being attributed to the original porosity and permeability of the host rock (Teal and Jackson, 1997). In contrast, at Meikle, hydrothermal fluids did not react readily with the biosparitic protolith and therefore decalcification tends to be restricted to near high-angle conduits (Teal and Jackson, 1997). Decalcification is generally regarded as a ground-preparation event that is economically unimportant and separate in time from gold mineralization. However, calcite destruction and mineralization are commonly considered coeval in skarn and base metal replacements deposits. This leads to the question whether separate alteration and mineralization events are required in Carlin-type deposits.



Sulfidation is common in all Carlin-type deposits and is well documented at Twin Creeks by Stenger et al., 1998. Sulfur is introduced by hydrothermal fluid but Fe is locally sourced from ferroan-dolomites. Sulfide minerals are regarded as an important factor in Carlin-type deposits due to their strong association with gold, particularly arsenopyrite (Arehart et al., 1993a).

A variety of characteristics specific to individual deposits has prevented the development of one genetic model that would explain all Carlin-type deposits. In some deposits the mineralization controls are stratigraphic (Carlin and Pete) and in others faults control the mineralization (Gold Quarry and Griffin). Shear as opposed to breccia-style mineralization is also used by Teal and Jackson (1997) to contrast the differences within the greater group of Carlin-type deposits.

Dating of gold mineralization in Carlin-type deposits is restricted by the lack of datable minerals that are paragenetically linked with gold mineralization. In addition, Carlin-type deposits may be complicated by the potential for repeated hydrothermal activity driven by igneous events that span the Jurassic, Cretaceous, and Tertiary. Five gold-bearing events are reported (Groff et al., 1997) at Getchell and Twin Creeks, with the major gold mineralizing events occurring at 83 Ma and 42 Ma. Sub-micron gold is commonly associated with altered, decalcified sedimentary rocks as well as silicification and fine-grained pyrite (Kuehn, 1989; Bakken et al., 1989; and J. Cline, pers. comm.). In these alteration and mineralization conditions, the growth of potassium-rich minerals is not favored. As a result, age dating of Carlin-type deposits is restricted to alteration products, such as illite and sericite (Arehart et al., 1993), and potassium-bearing minerals from igneous rocks that pre or postdate gold mineralization (Groff, 1996.).

The timing of gold mineralization in Carlin-type deposits is strongly debated. Argon isotope dating of adularia has provided conclusive ages for Eocene hydrothermal events, particularly at Jerritt Canyon (Hofstra et al., 1999). Conclusive evidence for five gold mineralizing events is found at Getchell (Groff et al., 1997). Dating of clays from Carlin-type deposits (Arehart et al., 1993b) are generally problematic and inconclusive. It is unclear if gold mineralization and alteration require multiple events to form a Carlin-type deposit or if mineralization and alteration occur in a single event. Another issue that remains unresolved is whether the Eocene events documented in northeastern Nevada apply to their western counterparts along the Battle Mountain/Eureka trend. If the Eocene is such an important event, then why is the 83 Ma event at Getchell an important gold contributor?

The sources of gold-bearing fluids in Carlin-type deposits remain enigmatic (Arehart et al., 1993b; Kuehn and Rose, 1995; Cline et al., 1996; and Stenger et al., 1998). Meteoric fluids are regarded as important at Jerritt Canyon (Hofstra et al., 1999). Fluid inclusion microthermometry and O-H stable isotope analyses for the Carlin (Kuehn, 1989) and Cortez (Rye et al., 1974) mines led to the hypothesis that Tertiary volcanism causes circulating meteoric water which then leaches gold from crustal rocks. However, the spatial relationship of Carlin-type gold deposits with porphyry systems near the Bingham Canyon mine, Utah and the Bau district, Malaysia, led Sillitoe and Bonham (1990) to propose a magmatic component in the mineralizing fluids. In a similar theme to the magmatic hypothesis, Seedorf (1991) proposes a metamorphic model where the heat is provided by magmatic bodies. Ilchik and Barton (1996) propose an amagmatic model whereby gold is leached by basinal fluids which then are focused along faults. Since

multiple events are recognized at Getchell (Groff, 1996), it is reasonable to hypothesize multiple fluid sources and that their composition changed in time.

The Pipeline deposit provides an opportunity to examine an economically significant, large tonnage Carlin-type deposit prior to commencement of mining activities. Study of Pipeline is important because the genesis and timing of gold mineralization has not been documented, the deposit is economically significant, is a major gold producer in Nevada, mining was just starting and so the deposit could be observed in a pristine state before mining destroyed key evidence, and considerable drillcore was generated by an aggressive exploration program.

### **Objective**

My objective is to determine the genesis of the Pipeline mineralization. Specifically, my objectives are to understand the gold depositional process, the chemistry of gold-ore solutions, the chemical signatures of dissolved gases that enable fluid source recognition, and to determine the age of mineralization. In so doing, I test the hypothesis that gold mineralization is coeval with decalcification in a Carlin-type deposit.

## CHAPTER 2

### BACKGROUND

#### History and Discovery

Mining activities in the Pipeline district (Fig. 2.1) began in 1862 with the discovery of silver in the Cortez and Mill Canyon areas (Foo et al., 1996). The production from these mining activities is uncertain, however, a flourishing community at the time suggests a lucrative operation. The Hilltop deposit was discovered in 1907 with gold hosted in quartz veins and breccia. Mining occurred between 1910 and 1934 (Lisle and Desrochers, 1988). The first mining activities at the Gold Acres deposit (Fig. 2.1) in 1935 produced >500,000 troy oz. of gold (Foo et al., 1996).

Placer Dome U.S., formerly known as American Exploration and Mining Co. (AMEX), began exploration within the district in 1959 and joined forces with Kennecott to form the Cortez Joint Venture (hereafter referred to as the CJV). Placer Dome U.S. controls 60% of the CJV stock and are the operators of the Pipeline mine whereas Kennecott hold the remaining 40%. During the 1960's, the United States Geological Survey (USGS) conducted mapping and sampling programs throughout the area. They reported anomalous gold hosted by oxidized and weathered silty carbonate outcroppings adjacent to the range front (Wells et al., 1969). Drilling by AMEX at the site led to the discovery of the Cortez Gold deposit which has produced 872,870 troy oz. of gold from 1969 to 1973 (Foo et al., 1996). The present unmined gold reserves at Cortez are estimated at 250,000 troy oz..

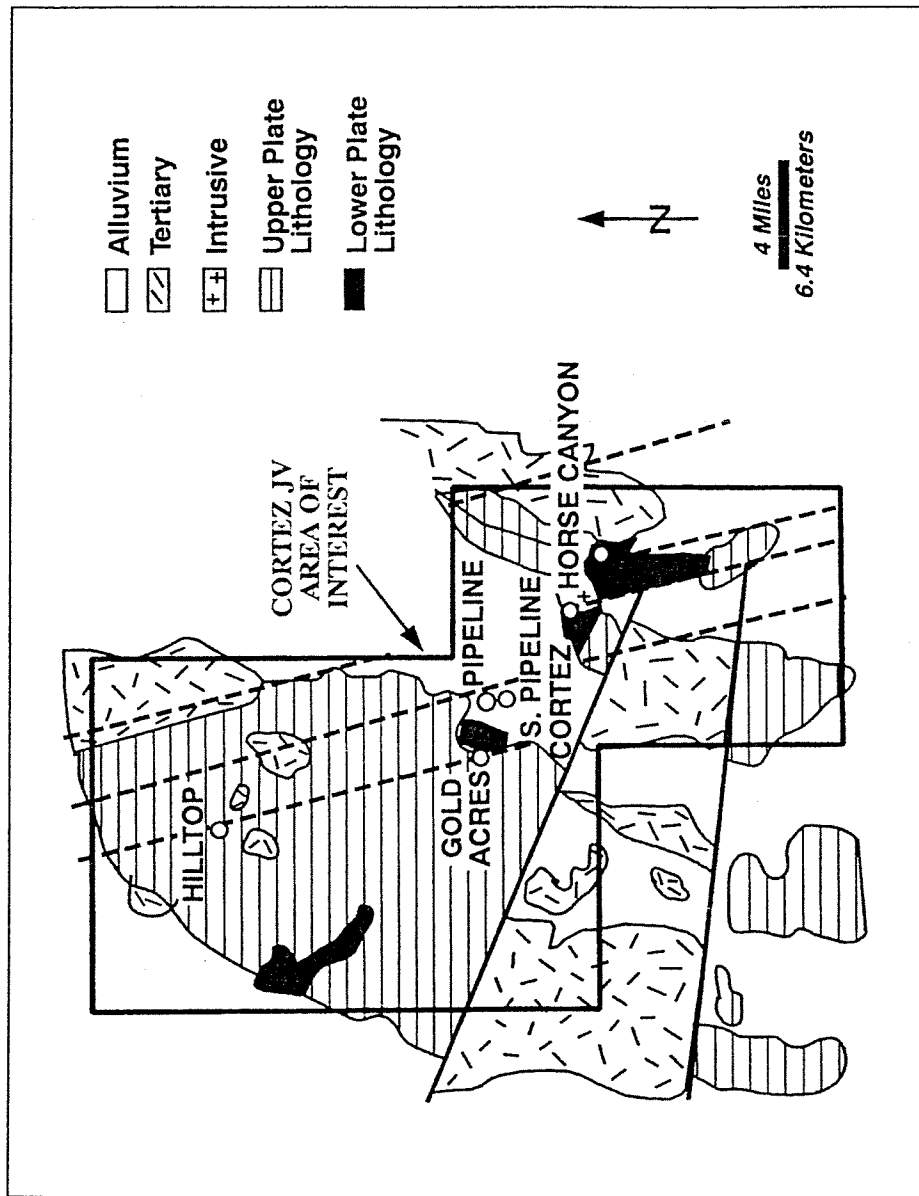


Figure 2.1. Simplified geology of the CJV area of interest. The Pipeline deposit is located along the eastern flank of the Shoshone range within a buried erosional window (Foo et al., 1996).

The Horse Canyon deposit, 6 km southeast of the Cortez Gold Mines mill site, was discovered in 1976. Approximately 385,000 troy oz. of gold were produced from 1983 to 1987 (Foo and Hebert, 1995).

The 1991 discovery of the Pipeline deposit resulted from condemnation drilling for Gold Acres heap leach pads (Foo et al., 1996). Two reverse-circulation drillholes were planned. Both intersected alteration and drillhole 91907 had a 35 m intersection averaging 10.5 g/ton gold (Foo et al., 1996). Pipeline's name refers to a water pipeline that traversed the area supplying water to the Gold Acres operations (R.C. Hays, pers. comm.).

## **Geological Setting**

### *North Central Nevada Geologic History*

During the Mississippian, northeastern Nevada was situated along a stable paleocontinental margin as indicated by regional stratigraphy and isotopic data (Stewart, 1980). A prism shaped, westward-thickening package of sediment was deposited from the outer margins of the paleocontinental shelf into an oceanic basin and facies changes led to a gradation from eastern shelf sediments into western deep basin equivalents (Teal and Jackson, 1997). Subsequent eastward-directed compressional tectonism associated with the Antler orogeny during the Late Devonian through Middle Mississippian resulted in region-scale north-south folding and imbricate thrusting of the western assemblage over the eastern assemblage (Roberts et al., 1958). The region continued to experience three less important, yet similar, compressional tectonic events during the Late Pennsylvanian

through Permian with the Humbolt orogeny, the Early Triassic Sonoma orogeny, and finally the Early Cretaceous Sevier orogeny (Teal and Jackson, 1997). It is unclear whether NNW-trending antiforms are a result of one specific compressional event or formed during more than one of the above mentioned events. Mid-Tertiary extension between 40 and 30 Ma is regarded by Hofstra et al. (1999) as the most important event in terms of gold mineralization in Nevada. "Dilation of faults and fractures during mid-Tertiary northwest-southeast extension may have controlled emplacement of igneous dikes and underlying intrusions, provided connections between deep fluid reservoirs and the meteoric-dominated regime in the upper crust, and served to focus flow of convecting meteoric water" (Hofstra et al., 1999).

Episodic intrusive activity that spans Late Triassic to Late Tertiary time indicates the gold belts of the Great Basin were subjected to high heat flow. There is a close spatial association between many of the Great Basin gold deposits and intrusive rocks of multiple ages. However, the role of igneous rocks in the possible formation of Great Basin gold deposits has remained enigmatic (Cline et al., 1996). In the Ely district evidence suggests that intrusive bodies are the source for gold in Carlin-type deposits (Seedorf, 1991). In other areas of Nevada the relationship is unclear and the timing of gold mineralization relative to intrusive bodies is poorly constrained.

### *Geology*

The stratigraphy of central Nevada is comprised of shelf and deeper marine sediments. Terminology most commonly used in Nevada refers to miogeosynclinal and eugiosynclinal sediments. Thrusting has brought these time equivalent sediments, that

were once spatially separated on the continental shelf, into close proximity. Stratigraphy is therefore described in order of the Lower Plate rocks, also referred to as Eastern Assemblage, followed by the Upper Plate rocks or Western assemblage rocks. The stratigraphy of the region is complicated by facies changes within some units. The lower and upper plate assemblages are discussed separately.

*Lower plate rocks:* The oldest lower plate unit in Central Nevada is Middle Cambrian Hamburg Dolomite (Gilluly and Masursky, 1965). Gilluly and Gates (1965) describe this unit as being “composed almost wholly of highly broken and irregularly bedded dolomite.” Hamburg dolomite is coarsely granular and largely recrystallized. Approximately 150 m thickness is exposed along the Northern Shoshone Range (Gilluly and Gates, 1965). Exposures of the Hamburg at Cortez are metamorphosed to a marble where it is in contact with the Mill Canyon stock (Gilluly and Masursky, 1965).

The Ordovician Eureka Quartzite overlies the Hamburg Dolomite and is a well sorted medium grained quartzite of high purity with accessory silt-sized grains, heavy minerals and pyrite. Corals and cross bedding within the Eureka quartzite suggest a shallow sea depositional environment.

The Hanson Creek Formation conformably overlies the Eureka Quartzite and comprises alternating beds of dark gray and very light gray dolomite with occasional thin limestone beds. The top of the formation contains interbedded chert with a prominent chert capping (for Type section, see Nolan et al., 1956).

Silurian Roberts Mountains Formation (SRM) conformably overlies the Hanson Creek Formation. It comprises thinly bedded to laminated carbonaceous silty limestones



and calcareous siltstones. Microscopically, the formation is about 80% calcite and 20% silt, comprised of 15% quartz, about 5% K-feldspar and minor muscovite flakes. Organic carbon and authigenic pyrite crystals are present. Graded bedding is observed in the thickest beds and fossil hash may be present. Formation thickness is estimated at 200 to 300 m. The Roberts Mountains Formation depositional environment is interpreted to be the transition between the siliceous rocks of the basin facies and the carbonate shelf facies (Gilluly and Masursky, 1965).

Devonian Wenban limestone postdates, and has a gradational boundary with the Roberts Mountains Limestone (Gilluly and Masursky, 1965) and the base of the Wenban is the first bioclastic bed above the thinly bedded SRM. The formation comprises thickly bedded bioclastic limestone with thinly bedded argillaceous limestone. Devonian Wenban differs from the Roberts Mountains Formation in age; bed thickness, which is generally 10 cm to 1 m; and siliceous content (Gilluly and Gates, 1965). Deposition is interpreted to have been within the moderately deep outer shelf environment (Stewart, 1980).

*Upper plate rocks:* Cambrian age rocks of upper plate are not exposed in the district. The first upper plate rocks are the Ordovician Valmy Formation which comprises a wide variety of rock types including quartzite, chert, greenstone, sandstone, siltstone, shale and very minor limestone.

Overlying the Valmy formation is the Silurian Elder Sandstone, comprised of predominantly fine-grained sandstone and interbedded siltstones. Most of the beds are laminated although some are crossbedded or ripple marked and do not part along the bedding as readily as the Roberts Mountains Formation (Gilluly and Gates, 1965).

The Devonian System overlying the Elder Sandstone comprises the Slaven Chert. Slaven Chert consists predominantly of black chert that has partings of dark carbonaceous shale and thinly bedded sandstone (Gilluly and Masursky, 1965).

### *Structural setting*

Gold mining districts in north-central Nevada are aligned along the Carlin, Battle Mountain, and Getchell trends (Fig. 1.1). The Battle Mountain/Eureka, and Carlin trends were originally recognized by Roberts (1960) to be related to alignment of tectonic windows although the origin of these gold belts is not clear. Roberts proposed that the belts were related to “third order structures of Precambrian age” but that additional work is required to clarify the origin of the belts (Roberts, 1960). The trend also corresponds to a basement gravity gradient, consistent with either a terrane boundary, a strike-slip fault, or a major structure that is Jurassic or older in age (Grauch et al., 1995).

The Pipeline deposit is located along the Battle Mountain/Eureka trend in north-central Nevada, near the eastern flank of the Shoshone Range (Fig. 2.1). The deposit occurs within an erosional window of the Roberts Mountains thrust on the west side of Crescent Valley. Upper plate rocks above the Roberts Mountains thrust comprise allochthonous deep water siliceous sediments and volcanic rocks that have been thrust approximately 80 km during the Late Devonian Antler Orogeny over its time-equivalent, the Silurian Roberts Mountains Formation (Foo et al., 1996). The timing of structural and igneous events within the CJV area of interest is summarized in Table 2.1.

The major structural events that impacted the CJV from Jurassic times to the present are the NNW-trending Cortez fault and the Basin-and-Range extension. A model

<b>Structure or intrusive</b>	<b>Date</b>	<b>Reference</b>
Roberts Mountains Thrust	Late Devonian to Early Mississippian	Roberts et al., 1958
Mill Canyon Stock	151 K-Ar biotite	Guilluly and Masursky, 1965
Gold Acres Stock	149.6±6.9Ma U/Pb zircon	J.K.Mortensen, 2000, unpublished
Gold Acres Stock	104.8±0.02Ma U/Pb zircon	J.K.Mortensen, 2000, unpublished
Gold Acres Stock	98.8±2.0 Ma biotite	Silberman and McKee, 1971
Gold Acres Stock	92.8±1.0 K-Ar altered stock	Silberman and McKee, 1971
Quartz porphyry dike	94.3±1.9 K-Ar sericite	Silberman and McKee, 1971
Cortez dikes	34.5 Ma sericite + biotite	Wells et al., 1971
Caetano volcanics	34.4±1.1 Ma K-Ar biotite	J.D.Obradovich, unpublished
Caetano volcanics	32.6±1.1 Ma K-Ar sanidine	J.D.Obradovich, unpublished
Basin and range extension	11 Ma	McCormack and Hays, 1996

Table 2.1 Tectonic and intrusive dates for the CJV area.

to reconstruct the area is described by McCormack and Hays (1996) and is based on gravity, geologic, magnetic and topographic data. This model incorporates reversal of movement along low-angle detachment faults related to Basin and Range extension around 11 Ma, as well as strike-slip movement along the Cortez and Pipeline faults, connecting the Mill Canyon and Gold Acres stocks (Fig. 2.2).

### **Pipeline Deposit**

#### *Igneous rocks*

The Mill Canyon stock has a 1000 m vertical exposure at Mount Tenabo. The stock is dominantly biotite-quartz monzonite but is variable in composition from a quartz diorite to an alaskite (Gilluly and Masursky, 1965). It may evolve through time from the former to the latter. In general the rock is porphyritic with feldspar phenocrysts containing An ranging from 25 to 55%. Biotite commonly has a reddish-brown hue and quartz commonly forms polycrystalline aggregates. Accessory minerals include magnetite, zircon and minor apatite. All are set in a mosaic of perthitic microcline. Sometimes hornblende is present but does not appear to be altered. Biotite is commonly poikilitic, enclosing plagioclase and quartz (Gilluly and Masursky, 1965).

Three dike types are reported within the area and have compositions of quartz porphyry, alaskite (like the stock), and augite syenite (Gilluly and Masursky, 1965). Quartz porphyry dikes are considered to be magmatically allied to the Caetano Tuff (Gilluly and Masursky, 1965). Dikes are mostly N to NNW trending and are controlled by

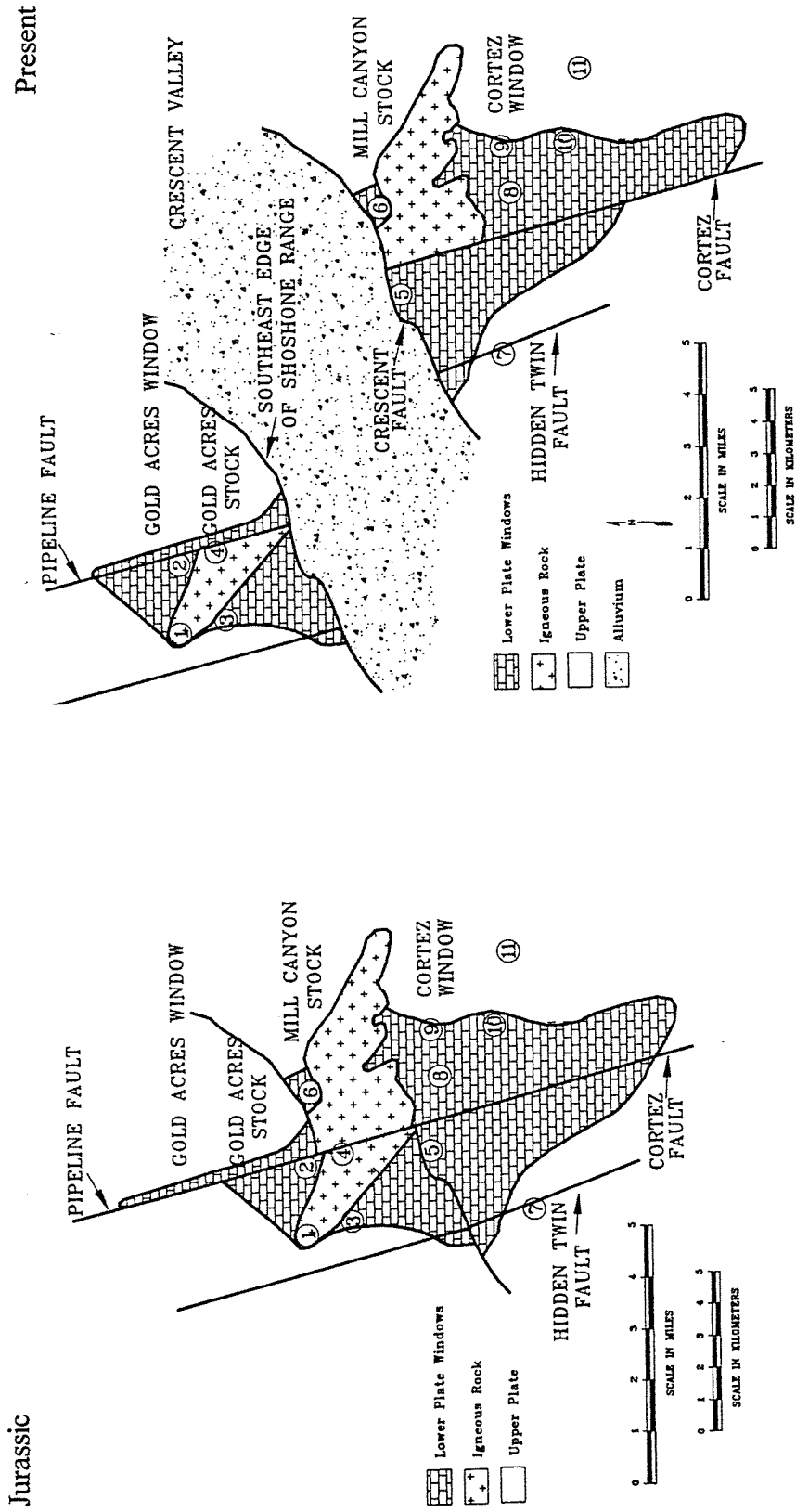


Figure 2.2 Foo et al. (1996) model for reconstruction of the Crescent Valley. The figures show the present (right) and reconstructed (left) positions of faults and intrusive bodies.

parallel faults. In the Cortez pits these dikes also turn parallel to bedding to form sills that were subsequently altered to smectite.

The Caetano Tuff is a body of welded and water-laid tuff with associated conglomerate and sandstone with outcrops starting a few km's south of the Pipeline Mine and continuing south into the Toiyabe Range. The thickness of the Caetano is estimated at 2500 m (Gilluly and Masursky, 1965).

### *Geology*

Pipeline is located near the eastern flank of the Shoshone Range within Lander County, Nevada. The main ore zone, is 150 to 180 m below the surface, varying in thickness from 15 to 105 m, is tabular in shape, and dips at a low angle to the east. This zone extends about 760 m in the northerly direction and about 460 m in the easterly direction (Foo et al., 1996).

Pipeline was a "blind" deposit covered by alluvium and hosted within the Silurian Roberts Mountains Formation (SRM). Unaltered SRM is gray to black silty carbonate, thin to medium-bedded, thinly laminated with normal graded beds of 5 to 12 mm thickness. Carbonaceous content is estimated at 0.03% and the pyrite content is estimated at 0.003 to 0.01%; both are variable. Unaltered rock comprises silt-size particles of calcite ( $\pm 80\%$ ), quartz ( $\pm 15\%$ ), K-feldspar ( $\pm 5\%$ ) and muscovite flakes ( $< 1\%$ ) (Gilluly and Masursky, 1965). Roberts Mountains formation within the deposit is invariably altered to some degree. Altered SRM typically comprises 50 to 80% fine-grained to clay-sized quartz, 0 to 40% calcite, 5 to 50% illite, as well as accessory iron-oxides (Foo et al., 1996; and personal observations). Carbon has been removed by oxidation that

extends below the water table and to as much as 300 m below the surface, giving a gray-buff color to the SRM.

The Devonian Wenban limestone (DW) is exposed across the NNW-trending fault on the west side of the pit. It is not economically important because DW has not reacted to hydrothermal fluids like the SRM.

Bedding in the SRM generally dips 15-20° to the east, a product of Basin-and-Range tectonism (Foo et al., 1996). Within the deposit bedding is variable due to shearing, thrusting, and duplex formation. The primary ore controlling structure is a low-angle shear zone that varies from 3 m in thickness on the edge of the deposit to 105 m within the deposit (R.C. Hays, pers. comm.). Within the shear zone the rocks are sheared, deformed and brecciated; individual shear planes commonly exhibit fault drag of the immediately overlying strata. Shear zones are regarded as zones of imbricate thrusting subparallel to and beneath the Roberts Mountains Thrust (Foo et al., 1996).

High-angle faults are well documented by pit mapping and include a NNW-fault that strikes N15W to N20W. The Pipeline fault is the most prominent of these faults and dips 75-85° to the east, is sympathetic to the Cortez trend, and is interpreted to be an offset extension of the Cortez fault (McCormack and Hays, 1996). A N35W subvertical fault is recognized to truncate deep mineralization, but this in turn is truncated by a younger NE-striking, high-angle fault set of which the Fence fault is the most important (Fig. 2.3). Normally conjugate shear planes of the same age develop at about 30° or 60° to each other, however, although the faults are about 60° to each other, the lineations measured for these faults suggest that they are co-active rather than conjugate pairs (C. Tarnocai, pers. comm.). Movement along the NNW faults are reported as normal oblique

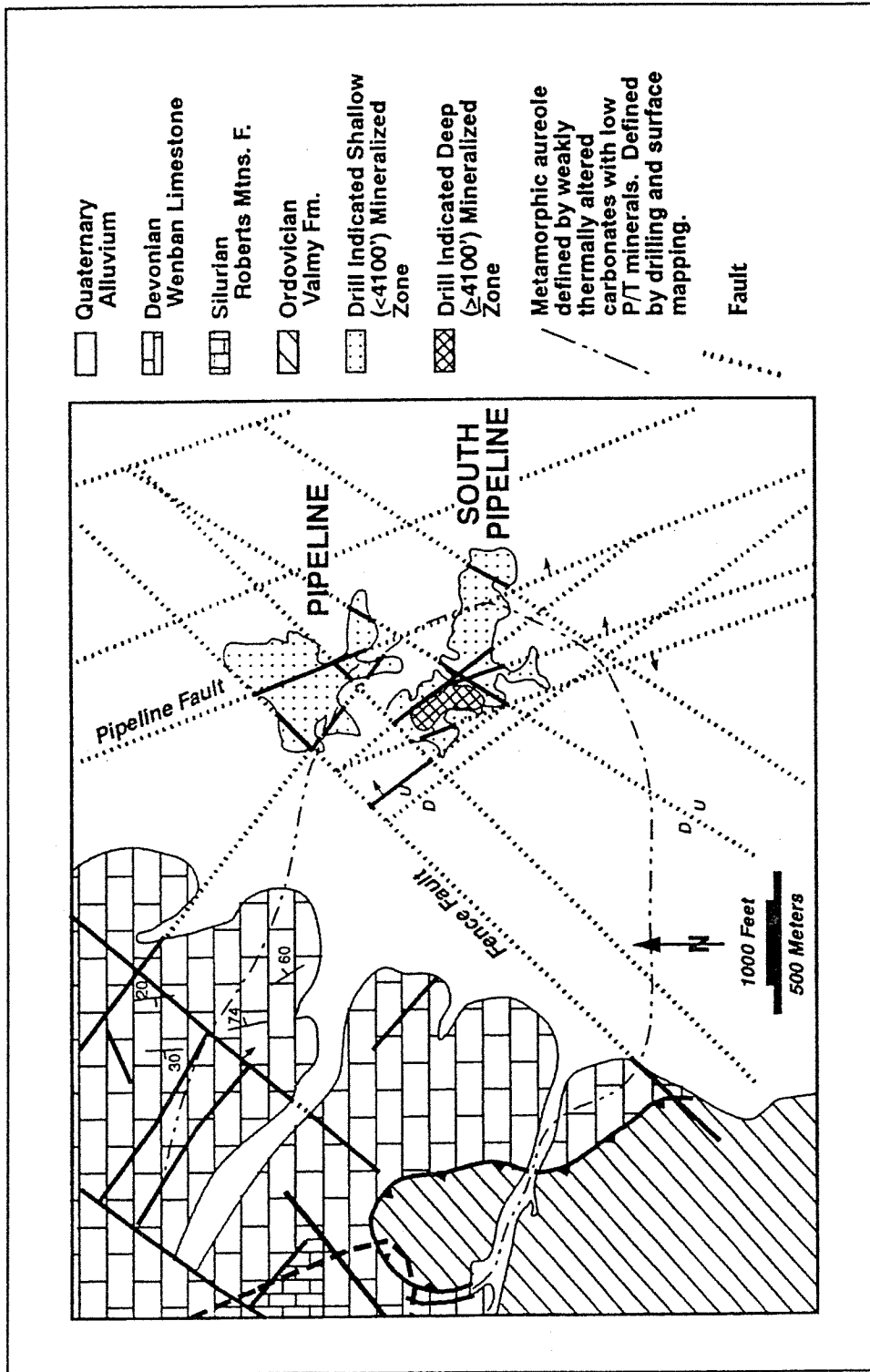


Figure 2.3. Simplified geologic map of the Pipeline and South Pipeline deposit areas showing faulting and outline of gold mineralization (Foo et al., 1996).



right slip whereas the NE faults have some normal movement with significant left slip (Foo et al., 1996). Both the NNW- and NE-trending faults are important ore controls.

### *Alteration*

Alteration types include decalcification, silicification and argillization.

Decalcification intensity is measured at the Pipeline mine by the reaction of the rock to 6:1 HCl acid. The amount of decalcification is visually estimated by the intensity of effervescence and by comparing this intensity to descriptions made on SRM of known decalcification intensity. Silicification is also documented within the Pipeline deposit. The silicification intensity is measured by comparing analytically determined intensities of silicification to a rock's response to a steel dental tool. Steel left behind on a drillcore after a steel dental tool has been scraped across the surface has a starting limit of 20% silicification. Argillization refers to the increase in argillic content. Most commonly this is a result of decalcification whereby the removal of calcite increases the bulk concentration of the insoluble components, including clay. The term sericitization refers to the growth of sericite such that new material is added without other components being removed.

### *Gold Mineralization*

According to Foo et al. (1996) gold is not confined to a single alteration type, nor confined to shear zones. However, the most favorable host to gold mineralization occurs within shear zones that are decalcified, sericitized, and oxidized. Microscopically visible gold was reported by Foo et al. (1996) who concluded that "much of the gold occurs as submicroscopic, disseminated grains." Also, gold "was observed in and on silica, in and

on hematite, on pyrite, and in illitic or sericitic matrix material as well as discrete grains in open spaces and on fracture surfaces” (Foo et al., 1996). A link between gold and pyrite is inferred “from limonite and hematite pseudomorphs.”

### **Previous Geochemical Studies**

#### *Fluid inclusion studies*

*Microthermometry:* Studies of Carlin-type gold deposits incorporating fluid inclusion microthermometry include Radtke et al. (1980), Rye (1985), Kuehn and Rose (1995), Lamb (1995), Groff (1996), Kamali (1996), Cline et al. (1996), Simon (1999) and Cline et al. (2000). A common observation from many of the studies are homogenization temperatures ranging from 180° to 220°C. Most studies also report salinities of 1 to 7 eq. wt. % NaCl, however, some higher salinities near 20 eq. wt. % NaCl are reported at Purple Vein and Post/Betze (Lamb, 1995), at Lone Tree (Kamali, 1996), Getchell and Twin Creeks for main ore stage (Groff, 1996), and Turquoise Ridge (Cline et al., 2000). Hypersaline inclusions with daughter halite crystals are reported from Lone Tree (Kamali, 1996), Getchell and Twin Creeks (Groff, 1996).

Fluid inclusion microthermometry and interpretations at the Carlin mine by Radtke et al. (1980) suggest that gold mineralization and boiling during late-stage mineralization occurred at depths of <1 km. Recognition of CO<sub>2</sub>-bearing inclusions at Jerritt Canyon (Hofstra et al., 1988) and Carlin (Kuehn, 1989) has led to the conclusion that gold mineralization occurred at depths of 1-5 km. Depth estimates at Getchell are a minimum of 1.2 km (Cline et al., 2000).

*Gases:* Known studies of Carlin-type deposits that involve fluid inclusion gas analysis are restricted to Bendrick (1989), Graney et al. (1991), Groff (1996), Kamali (1996) and Cline et al. (2000). Work by Bendrick (1989) added to the microthermometry of Kuehn (1989) and shows that volatile contents decrease in time whereas H<sub>2</sub>S increases. The focus of both Groff (1996) and Kamali (1996) was to recognize fluid sources. In addition, Groff (1996) is able to show that gold mineralization is associated with fluids that have a high methane content and labeled the fluid as "organic-rich". Fluid source categorization based on He-N<sub>2</sub>-Ar ternary discrimination diagrams identified magmatic, crustal, and meteoric components to fluids trapped within different minerals as fluid inclusions. In contrast, J. Cline (pers. comm.) uses gas analysis to test for differences between fluid inclusion populations rather than applying source recognition.

#### *Radiometric dating within the CJV*

Within the CJV, multiple dates are reported that span the Jurassic, Cretaceous and Tertiary (Table 2.1). A K/Ar age of 151 Ma is reported for fresh biotite for the Mill Canyon stock (Guilluly and Masursky, 1965). Despite the Crescent Valley reconstruction model of McCormack and Hays (1996) placing the Mill Canyon stock and Gold Acres stock in juxtaposition, only one date for the Gold Acres stock is within error of the 151 Ma date. Dating of zircon by U/Pb gives two ages, i.e., 149.6±6.9 Ma and 104.8±0.02 Ma (J.K. Mortensen, unpublished data). The sample submitted for dating was a composite from drillcuttings (R.C. Hays, pers. comm.) and therefore the existence of two discrete intrusive bodies should be considered. Biotite from the Gold Acres stock yields an age of 98.8±2.0 Ma and altered stock gives a K-Ar age of 92.8±1.0 Ma (Silberman and

McKee, 1971). Sericite from a quartz porphyry dike in the area gives a K-Ar date of  $94.3 \pm 1.9$  Ma (Silberman and McKee, 1971). The variance of ages for the Gold Acres stock presumably reflects thermal events and/or alteration that impacted the stock.

A hiatus separates Cretaceous igneous activity from Tertiary volcanism. Dikes at Cortez are dated as 34.5 Ma (sericite + biotite; Wells et al., 1971) and biotite from the Caetano volcanics to the south gives a K-Ar age of  $34.4 \pm 1.1$  Ma and sanidine gives  $32.6 \pm 1.1$  Ma (J.D. Obradovich, unpublished).

## CHAPTER 3

### ANALYTICAL METHODS

#### *Field studies*

More than 110 samples were collected and described during 3 field seasons (Appendix A). During this time, I logged several thousand feet of drillcore and had access to the open pit. Most vein material sampled originated from drillcore and was intact, whereas the material from the open pit was broken and displaced by blasting. Access to previously drilled core was granted, however, key drillcore intersecting ore zones in the original drilling program had been removed for metallurgical testing. Additional core was removed during skeletonization and only limited core remains.

#### *Fluid Inclusions*

I studied fluid inclusions by geothermometry, gas geochemistry, and bulk analysis of major ions. The basic assumptions are (1) the chemistry of fluid inclusions have not been modified since trapping occurred, and (2) the P-T-V conditions measured reflect the conditions at the time of trapping.

A Linkham TH600 heating-freezing stage and temperature controller is used to accomplish microthermometry. Doubly polished, 100-300  $\mu\text{m}$  thick, rock sections for analysis were prepared by Spectrum Petrographics. Sections are removed from the microscope-slide backing by soaking in acetone prior to analysis. The instrument calibration is checked daily by use of a  $\text{H}_2\text{O}$  standard, and each week the calibration is checked using at least three standards. Data obtained between shifts in the calibration are

discarded. The analytical error in melting point determinations near 0°C is 0.1°C, whereas error in Th measurements in the temperature range of 200°C is 0.5°C.

The analysis of volatile species is done in vacuum using by the CFS (crush-fast scan) method (Norman et al., 1996). Samples are cleaned with potassium hydroxide, then distilled water, and then oven dried at about 60°C (at 100°C He is rapidly lost). Samples are then placed in crushers and evacuated while heating to about 60°C until a pressure  $<10^{-7}$  Torr ( $10^{-8}$  mPascals) is attained. The analysis is performed by means of a Balzers QME125 quadrupole mass spectrometer operating in a fast-scan, peak-hopping mode. The CFS method involves opening inclusions by a swift crush in the vacuum chamber housing the mass spectrometer. Volatiles released are quickly removed by the vacuum pumping system within two seconds. Meanwhile, the pulse of inclusion volatiles is recorded by operating the quadrupole in a fast scan mode with measurements every 150 to 200 msec. The mass peak areas are used to determine the concentration of each species using predetermined sensitivity factors and a peak-stripping algorithm designed by D.I. Norman. Opening a 10 to 20  $\mu\text{m}$  inclusion, or group of smaller inclusions of equivalent volume, provides the ideal amount of volatiles for CFS analysis. Opening a 40  $\mu\text{m}$  inclusion swamps the vacuum system and the system crashes. Five to twenty sequential crushes are made on about a 200 mg sample with the expectation that some crushes will be failures by opening too many or too few inclusions. Species routinely recorded are  $\text{H}_2$ , He,  $\text{CH}_4$ ,  $\text{H}_2\text{O}$ ,  $\text{N}_2$ ,  $\text{O}_2$ ,  $\text{H}_2\text{S}$ , Ar,  $\text{C}_3\text{H}_8$ ,  $\text{CO}_2$  and  $\text{SO}_2$ . In addition several crushes are done on a sample while monitoring  $\text{CH}_4$ ,  $\text{CO}_2$ , C2-4 alkenes and alkanes, benzene and toluene. Ammonia is rarely detected because of the interference of secondary water peaks at  $m/e = 17$  and 16; He at concentrations below 10 ppm is interfered with by the tail on the

H<sub>2</sub> peak; and CO peaks fall on those of CO<sub>2</sub>, N<sub>2</sub>, CH<sub>4</sub> and C2-7 organic species. Small amounts of admixed air is commonly detected during CFS measurements, which is estimated from the amount of O<sub>2</sub> measured. The source of air contamination is most likely air trapped on grain boundaries and micro-cracks. The concentrations of inclusion N<sub>2</sub>, Ar and CO<sub>2</sub> can be corrected for air contamination assuming all O<sub>2</sub> measured represents admixed air. In general, analyses indicating admixed air are discarded because of the uncertainties in making an air correction. Air contamination is eliminated by prolonged baking. However, in the interest of expediency, and to minimize H<sub>2</sub> and He diffusion from inclusions, prolonged baking of samples is not done.

The instrument is calibrated with commercial gas mixtures, artificial inclusions filled with gas mixtures, and an in-house fluid inclusion standard. The gas water ratio of the standard inclusions (HF1) is known to about 0.1% by Penfield-tube analysis, thus allowing water calibration with an error less than 0.2%. Measurement precision is <5% for major gaseous species, and ~10% for the minor species.

Crush-leach analysis is done in order to measure ratios of fluid inclusion anions and cations. Methods used are described in detail in Norman et al. (1987) and Shepherd and Rankin (1998). In excess of 10 gm of quartz is placed in nitric acid to destroy any calcite. Samples are boiled in nitric acid to clean the surfaces. The nitric acid is decanted and the samples washed several times in deionized water. Samples then are boiled several times in ultra-pure, reverse osmosis, deionized water prior to placing them in electrolytic cells. The water in the electrolytic cells is changed daily until the current does not increase in a days operation from freed ions. Dried samples are placed in clean stainless steel tubes and crushed in a hydraulic press to open fluid inclusions. The powder produced is placed on a

sieve and a reverse osmosis leach bath removes the fluid inclusion salts. The leachate is reduced by evaporation in Teflon containers, then analyzed at the New Mexico Bureau of Mines and Mineral Resources by atomic absorption and ion chromatographic methods.

### *Argon Geochronology*

The  $^{40}\text{Ar}/^{39}\text{Ar}$  technique is an extension of the K-Ar technique. The sample must be irradiated with fast neutrons in a reactor thus converting some  $^{39}\text{K}$  into  $^{39}\text{Ar}$ . Unlike the K-Ar technique which requires the K concentration to be known precisely, ratios between Ar isotopes are analyzed. Also, the sample is incrementally heated *in vacuo* and the argon released during each heating step is analyzed separately to produce an apparent age spectrum. Another common form of display is the isochron plot. The  $^{40}\text{Ar}/^{39}\text{Ar}$  technique is a relative method and requires the use of monitors of known age to determine a sample age. These monitors are used to determine the neutron flux parameter referred to as J. The  $^{40}\text{Ar}/^{39}\text{Ar}$  technique also requires the measurement of  $^{37}\text{Ar}$  and  $^{36}\text{Ar}$  to determine interfering argon isotopes produced from K and Ca.

The K-bearing minerals found in the Pipeline deposit are very fine-grained illite and hydrothermal sericite. Some geologists regard illite and sericite to be the same mineral, however, sericite has slightly more potassium. Dating such fine-grained clay minerals may be problematic in that the recoil distance for  $^{39}\text{Ar}$  radiation is comparable to the grain-size of illite. A brief explanation of recoil is given below to enable a better understanding of this potential problem in dating fine-grained materials.



Samples analyzed by the  $^{40}\text{Ar}/^{39}\text{Ar}$  technique require irradiation in nuclear reactors. By absorbing a neutron,  $^{39}\text{K}$  emits a proton and transmutes to  $^{39}\text{Ar}_\text{K}$  and this reaction is expressed as  $^{39}\text{K} (n,p) ^{39}\text{Ar}$ . The produced  $^{39}\text{Ar}_\text{K}$ , recoils with an energy of 177 keV (Onstott et al., 1995) displacing the  $^{39}\text{Ar}_\text{K}$  from its original site by about 800 Å (McDougall and Harrison, 1988). Recoil may invalidate the assumption “that the  $^{39}\text{Ar}_\text{K}$  produced during irradiation is distributed in a manner similar to the  $^{40}\text{K}$  in a sample” (McDougall and Harrison, 1988). It is possible for  $^{39}\text{Ar}_\text{K}$  to recoil out of the clay grain from where it was produced and embed itself in an adjacent grain. The effect of recoil can produce discordant age spectra in clay minerals, exsolved minerals, and altered minerals.

### *Clay Mineralogy*

I selected seventeen samples for XRD analysis; i.e. two fault gouges and other samples which were primarily collected along section line 59200 where drillcore exists and different alteration types occur. This allows a comparison between alteration type relative to clay data.

Clay samples for XRD analysis are individually ground with deionized water in a mortar and pestle, and the resulting fluid is poured into a beaker. Deionized water is added to dilute the clay-water mixture and the sample is allowed to settle under gravity. After about 4 hours, a pipette is used to extract about 4 ml of solution from near the surface in order to capture a  $<4 \mu\text{m}$  fraction. The solution is allowed to coat one side of a glass slide and then left to evaporate. The clays in suspension are concentrated on the surface of the slide producing a basal section of the clay for XRD analysis. Clay-coated slides are placed in a Rigaku XRD spectrometer using monochromatic X-rays (using

curved crystals) from a Cu tube set to 40 kV and 25 mA. The goniometer is set to 0.03 °2θ per second. After the spectra are collected, X-ray patterns are produced using the WINJADE computer program.

Randomly orientated slides for polytype identification are produced by collecting about 1-2 gm of <4 μm clay material. Clay is allowed to dry and is then broken up and sprinkled onto a glass slide that is coated with petroleum jelly to act as an adhesive. The slide is immediately analyzed using the XRD spectrometer by the same method as previously described except that the dwell is increased about 5 to 10 times. Random mounts are used to examine the polytypes of illite where distinctive spectral lines enable the identification of each polytype (Table 3.1).

1M			2M <sub>1</sub>		
	<i>d</i> (Å)	Intensity		<i>d</i> (Å)	Intensity
1	4.35	1½	1	4.29	1
2	4.12	1	2	4.09	1
3	3.66	5	3	3.88	3
4	3.07	5	4	3.72	3
5	2.93	1	5	3.49	3
6	2.69	2	6	3.20	3
			7	2.98	3½
			8	2.86	3
			9	2.79	2½

2M <sub>2</sub>			3T		
	<i>d</i> (Å)	Intensity		<i>d</i> (Å)	Intensity
1	4.34	2	1	3.87	3½
2	3.90	3	2	3.60	3
3	3.68	4	3	3.11	3
4	3.52	4	4	2.88	4
5	3.21	4	5	2.68	1
6	3.07	4			
7	2.87	2			
8	2.81	2			

Table 3.1. Diagnostic XRD lines for 1M, 2M<sub>1</sub>, 2M<sub>2</sub> and 3T polytypes of illite (Bailey, 1980).

## CHAPTER 4

### OBSERVATIONS AND RESULTS

#### **Mine Geology**

##### *Alteration*

Observations of the alteration styles confirmed those reported by Foo et al. (1996) and described by mine geologists. Several additional observations were made, particularly a paragenetic sequence of vein types.

*Decalcification:* Removal of calcite is commonly documented in drillcore at Pipeline. Total decalcification occurs in shear zones, however, a progressive decrease in the intensity of decalcification is documented perpendicular to the shear zones. Fresh, undecalcified SRM (Fig. 4.1) has a well-developed lamination that is emphasized by dusty pyrite. In the shear zones where decalcification is total, the lamination spacing decreases and laminations are enhanced by hematite (Fig. 4.2).

Decalcification has affected most of the deposit with shear zones exhibiting the strongest intensity. Locally, there is no reaction of the SRM to acid. Totally decalcified SRM is confined to the shear zones. Totally decalcified rock exhibits high porosity such that water dripped onto the rock surface is immediately absorbed and hand samples are discernibly less dense.

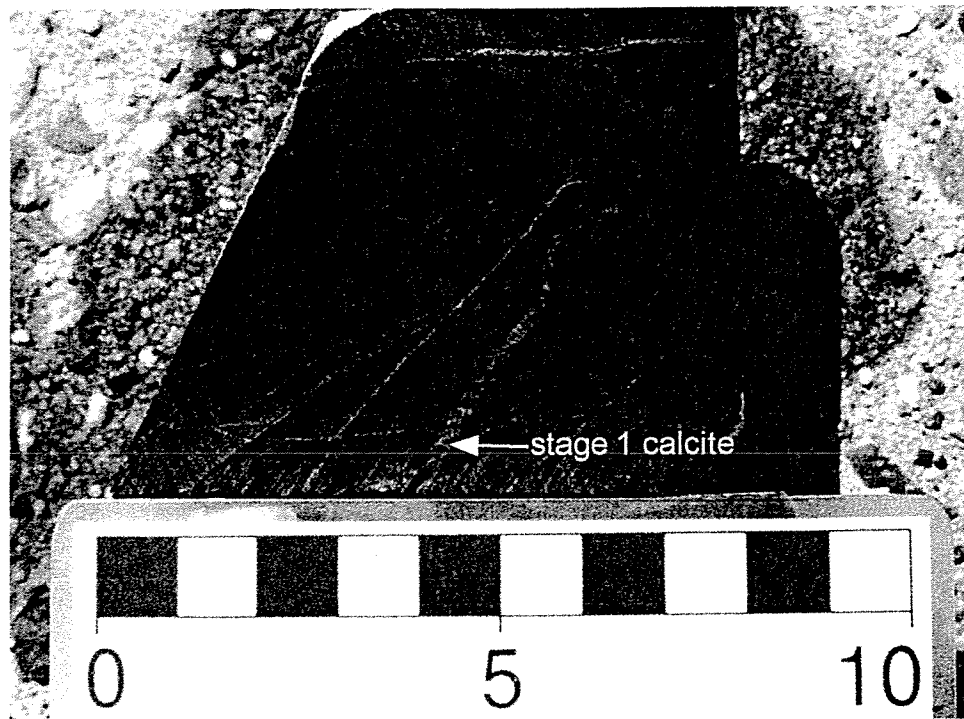


Figure 4.1 Photograph of fresh, carbonaceous SRM crosscut by a stage 1 dark calcite vein. The scale is in cm.



Figure 4.2 Photograph of totally decalcified, argillized and oxidized SRM. The mm-scale lamination is emphasized by hematite. The scale is in cm.

*Silicification:* Silicification occurs pervasively and as halos to quartz veins.

Observations of thin sections and polished surfaces show that the filling of open space by quartz is the most common occurrence, whereas replacement by silica is less common. An example of silicification controlled by a fracture is shown in Figure 4.3 and emphasizes how silica penetrates the host rock to a depth of a few mm. Although the term “silicification” is commonly used by Nevada. At Pipeline, petrographic analysis indicated that silica was deposited as quartz rather than chalcedony; therefore, the term “ore quartz” is used to represent silicification.

*Sulfidation:* Pyrite-bearing haloes of up to 10 mm wide occur next to quartz carbonate veins below the deposit (Fig. 4.4). Sulfidation is not as extensive as decalcification and in Figure 4.3 the light brown decalcified halo extends beyond the dark specks that represent pseudomorph replacement of pyrite by Fe-oxides. Evidence for sulfidation within the ore zones is obscured by subsequent pseudomorph replacement to Fe-oxides.

*Oxidation:* Oxidation is divided into two types, iron-oxide development and carbon removal from dark carbonaceous SRM to produce a light yellow-brown colored rock. The entire ore zone is oxidized and the oxidation halo can extend to >300 m. Observations of drillcore confirm that Fe-oxide replacement of sulfides occurs slightly ahead of carbon removal.

Two iron-oxides are present, hematite and goethite. Red-colored hematite is spatially associated with shear zones and immediately above the shear zones where



Figure 4.3 Photograph showing silicification of wallrock adjacent to a quartz vein. Note the decalcified halo (light brown) extends beyond the silicified halo as well as the halo of Fe-oxide that forms as pseudomorph replacement after pyrite. The scale is in cm.

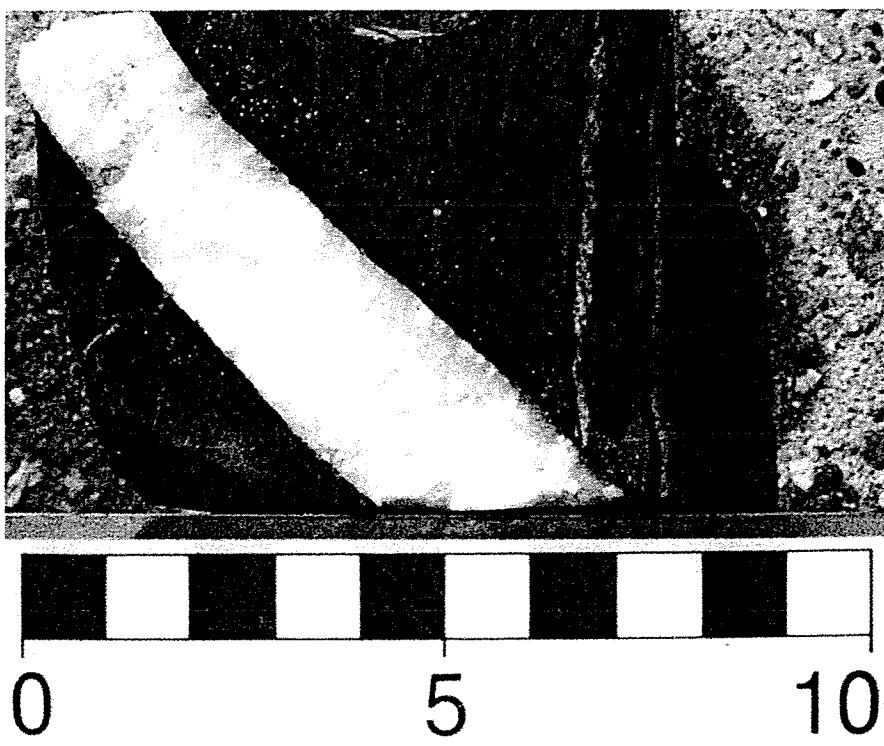


Figure 4.4 Photograph of a stage 3 quartz-calcite vein in fresh SRM. Note the sulfidized halo that extends beyond the vein for several mm's. The scale is in cm.

decalcification is prominent. Hematite concentration is based on color intensity comparisons to known standards. Red laminations bearing fine-grained hematite are most common (Fig. 4.2), however, it also occurs in argillized zones where moderate to total decalcification has occurred. Goethite, is orange-brown and occurs as laminations and replacements. An interesting observation is that laminated goethite forms a zone above hematite. Interlaminated goethite and hematite is common. Goethite also occurs as pseudomorph replacements after pyrite.

*Argillization:* In most of the deposit the intensity of argillization is low but locally in shear zones argillization is so intense that rock has the consistency of putty. Argillization commonly is a residual accumulation of clay released by decarbonization of SRM and the rock has a light brown color. A second argillization type is the growth of illite to produce a distinctive off-white clay that occurs locally within the pit (Fig. 4.5). This off-white clay is commonly associated with good gold values and is thought to be the same material as the hydrothermal sericite that occupies quartz-calcite veins.

Several differences are recognizable between unaltered SRM several meters above the shear zones and the strongly altered ore horizon. Unaltered SRM is gray, calcareous, and has bedding planes of 3 to 15 mm separation containing syngenetic pyrite (Fig. 4.1). In contrast, altered SRM is off-white, totally decalcified, and has a ~1 mm bedding lamination separation emphasized by brick-red colored fine-grained hematite laminae (Fig. 4.2).



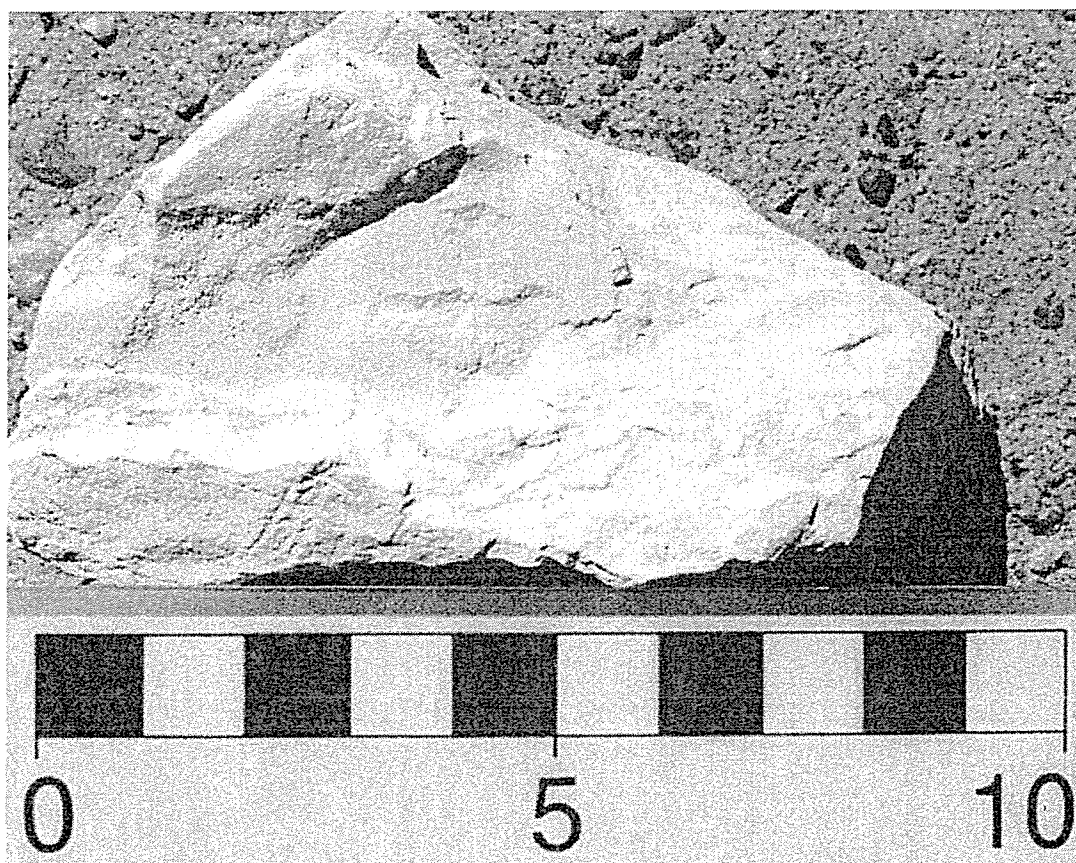


Figure 4.5 Strongly argillized, totally decalcified ore. This sample assayed 21 ppm gold. The scale is in cm.

## *Veins*

Four vein types are recognized. Dark petroliferous calcite veins (VC-1) can be found above and below ore and shear zones. The distribution of these veins is unaffected by shear zones. Fluid inclusion sections show the dark coloration to be micron-sized carbonaceous matter.

A second vein set forms a stockwork of white undeformed-calcite veins (VC-2) and comprises up to 30% of the SRM that spatially underlies the shear zones but do not occur within the shear zones. The veins are anastomosing with a subvertical preferred orientation and crosscut stylonites.

Quartz-sericite-calcite veins (VQ-3) occur beneath the deposit, whereas none are observed above the ore. A similarity is drawn between these veins and the vein systems that develop beneath massive sulfide deposits because they appear to be feeders to the tabular ore body. These quartz-sericite-calcite veins have a paragenetic sequence of sericite and quartz followed by the growth of euhedral quartz into open space, followed by calcite. The wallrock immediately adjacent to the vein has a silicified and sulfidized halo that is commonly 5 mm wide but does not exceed 10 mm. In two fresh SRM samples, scattered pyrite grains up to 1 mm occur (Fig. 4.4). Silicification is more difficult to observe in hand specimens than in thin section. In oxidized samples, the pyrite is replaced by Fe-oxides whereas the silicification is emphasized by a color contrast (Fig. 4.3). In oxidized samples, a decalcified halo that manifests itself as a paler shade between the grey-colored silicification and the slightly darker undecalcified rock (Fig. 4.3) is observed. The decalcified halo is larger than the silicified halo.

Vuggy calcite veins (VC-5) crosscut gold mineralization and are more abundant peripheral to the deposit than within it. Calcite crystals are commonly light brown in color and the habits observed include dogtooth spar, cockscomb and stubby drusey crystals. Most crystals are clear to translucent.

### *Gold Mineralization*

Access to gold values obtained from logged core was limited. Section lines compiled by the author and mine geologists show a correlation between shear zones and gold values. All samples collected were examined with a binocular microscope for gold. Visible gold is rare, and polished ore thin sections fail to reveal gold, despite assays confirming good gold values. Two polished resin-impregnated samples of ore zones did not exhibit visible gold using a reflected-light microscope despite neutron activation confirming ppm levels of gold. The highest gold values of 21 ppm assayed by neutron activation came from a sample (NB-87) that is off white in color, totally decalcified, strongly sericitized, unsilicified, porous and hosted within a shear zone (Fig. 4.5).

One blasthole drilled in the Pipeline pit during 1998, yielded >2 oz per ton gold. Visible gold grains as large as 1 mm were recovered from the panned concentrate. These grains are the only case of visible gold observed by the author. In this concentrate, gold is intimately associated with Fe-oxide. Using the electron microprobe in SEM mode, crystalline gold with hopper-like surface textures is revealed (Fig. 4.6); this is inconsistent with the sub-micron sized gold generally associated with Carlin mineralization. The gold purity of these grains is high with microprobe analyses giving only up to 0.5% Ag, the remainder being gold. Some visible gold grains are associated with Fe-oxide (Fig. 4.7)

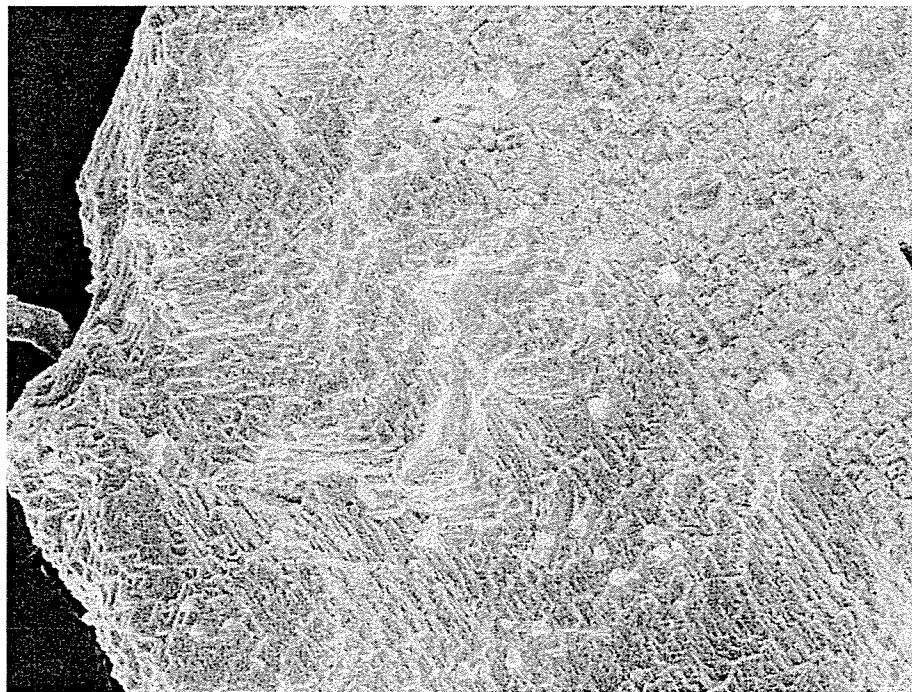


Figure 4.6 Electron microprobe image in SEM mode of a gold grain showing a hopper-like crystal growth pattern. The field of view is about 200  $\mu\text{m}$ .



Figure 4.7 Electron microprobe image in SEM mode of a gold grain showing a close association with Fe-oxides (granular material). The field of view is about 100  $\mu\text{m}$ .

although there is no information suggesting the relative timing of either phase. The images do, however, confirm the intimate association of gold and a Fe-oxide.

Fire assays from drillcore that hosted stage 1, 2 or 5 veins showed no gold values. In contrast, the sulfidized selvages of four stage 3 veins assayed by fire assay all confirmed gold values that varied from 0.3 to 1.0 ppm. The gold content of the wall rocks beyond the pyrite selvages is below detection.

### **Paragenetic Relationships**

The paragenetic relationships at the Pipeline mine were determined from observations made in core, observations within the pit, regional crosscutting relationships and dating of K-bearing minerals. The mineral paragenesis is summarized in Table 4.1.

#### *Crosscutting veins*

The earliest mineralization (stage 1) are dark petroliferous calcite veins (Fig. 4.1). Stage 1 veins are, crosscut by all other veins, and are commonly deformed and crosscut by shear planes.

The dark-colored stage 1 veins are cut by VC-2 stage 2 veins (Fig. 4.8). These veins are not observed as fragments within the ore zones and their absence is attributed either to decalcification in the ore zones or the locations of drillholes.

Stage 3 quartz-sericite-calcite veins crosscut stage 1 and 2 veins. In one locality a stage 3 vein is truncated by a shear plane but this plane could be related to Basin-and-Range extension.

Time	Pre-Antler Orogeny	Antler Orogeny	Cretaceous	Pre Basin and Range	Basin and Range
Event	Stage 1	Stage 2	Stage 3	Stage 4	Stage 5
Dark calcite	—				
White calcite		—	—		
Sericite					
Quartz			—		
Pyrite			—		
Gold			—		
Orpiment			?		
Vuggy calcite					—
<b>Alteration</b>					
Silicification			—		
Decalcification			—		
Argillization			—		
Oxidation				—	
<b>Structural</b>					
Shearing		—			
Brecciation		—			?

Table 4.1 Paragenetic sequence as recognized by veining, alteration and shearing at the Pipeline mine.

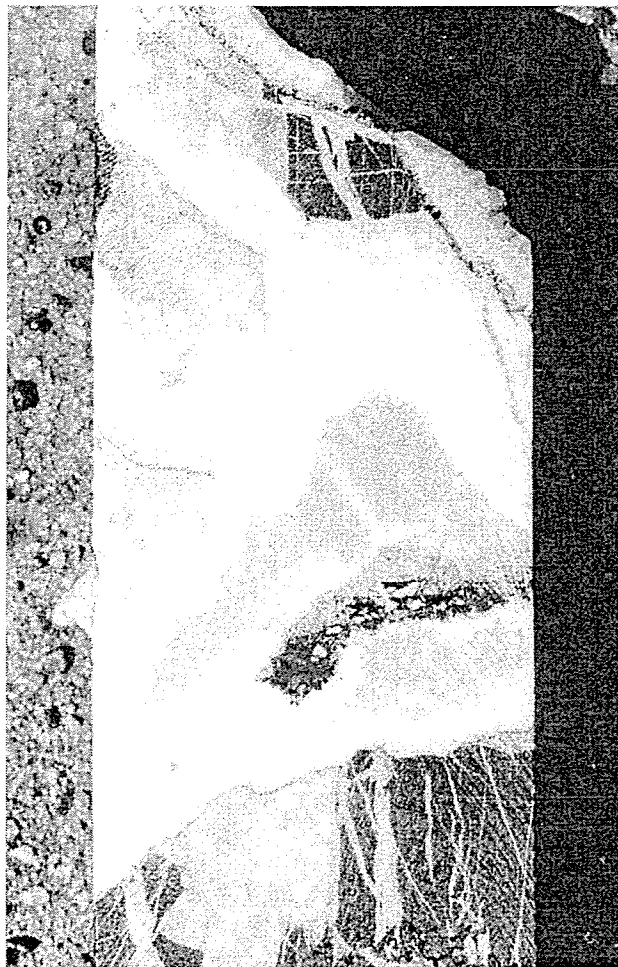


Figure 4.8 Photograph of stage 2 white calcite stockwork, crosscut by stage 6 calcite vein. The width of the drillcore is approximately 6 cm.

Oxidation postdates stage 3. Fresh pyrite is associated with stage 3 veins at depths >300 m whereas in the oxidized zone, pyrite is replaced by Fe-oxides.

Crosscutting both stage 3 veins and the oxidized ore body are vuggy, calcite veins (stage 5). Dipping layers of calcareous sediment (Fig. 4.9) have the same inclination as surrounding sediments. Since the local 10 to 20° dip is indicated to be the result of Basin-and-Range faulting, the sediment must predate this event. These veins must also postdate stage 4 oxidation. It is expected that acid fluids produced by the oxidation of pyrite would destroy calcite in stage 5 veins.

#### *Ore deposit*

Paragenetic relationships within the Pipeline deposit are poorly constrained. Unlike several other Carlin-type deposits (Cortez, Meikle), no intrusive bodies occur within Pipeline and so dating crosscutting igneous rocks is precluded. The Crescent Valley reconstruction model (McCormack and Hays, 1996) indicates that NNW-trending faulting postdates the Mill Canyon stock. The location of Pipeline on these NNW-trending lineaments suggests that the deposit must have formed after 152 Ma, the age of the Mill Canyon stock. NE-trending faults are observed and economic gold mineralization is abruptly terminated on the Fence fault. Poor gold values occur on the NW side of the Fence fault. This may indicate that major gold mineralization predated the NE-trending fabric but that minor remobilization could postdate the Fence fault.

No examples of early calcite veins are seen crosscutting the deposit. The only vein identified that crosscuts the deposit is stage 5 calcite. Ore zones within the deposit are



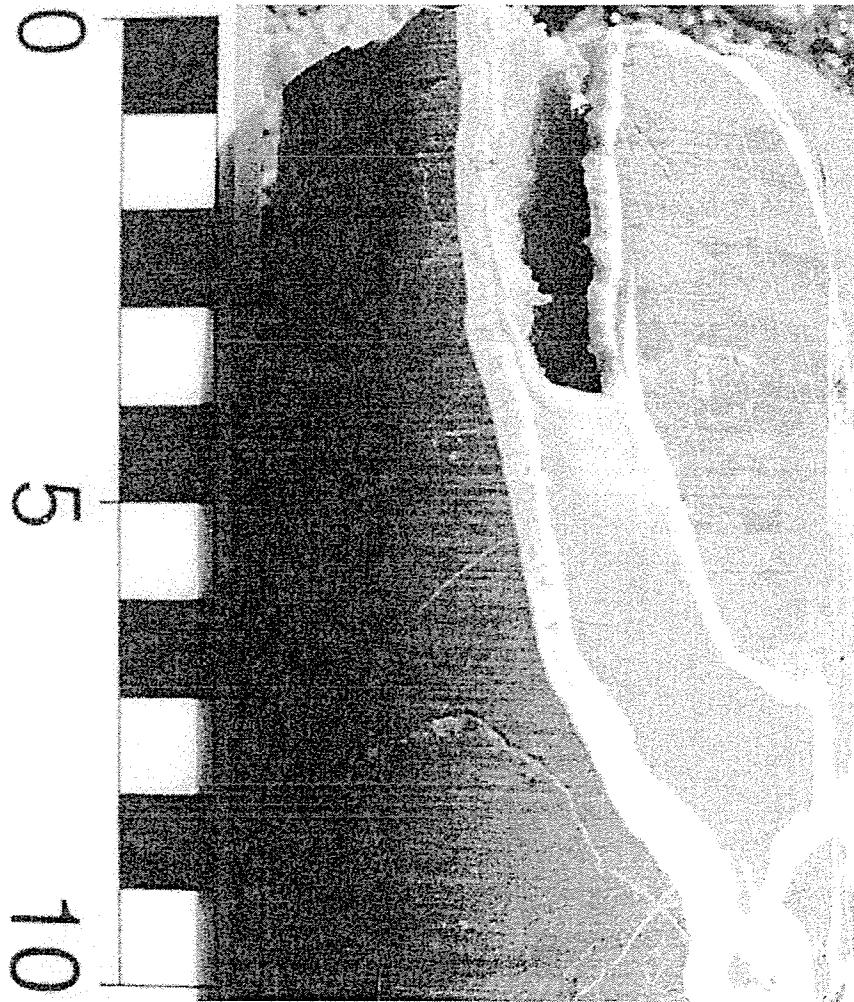


Figure 4.9 Photograph of a stage 4 vein showing the laminated calcareous sediment. The scale is in cm.

generally located along shear zones sympathetic to and underlying the Roberts Mountains thrust and must therefore postdate the Roberts Mountains thrust.

Ore zones are decalcified, gold-bearing, and exhibit local sericitization and silicification (ore quartz). A halo of oxidation extends beyond the ore zones and within this halo, Fe-oxides replace all sulfide minerals.

The link between gold mineralization in the deposit and the stage 3 veins below the deposit is made as follows. Only stage 3 veins have gold-bearing selvages. Sericite associated with stage 3 and in the ore zone illite give similar dates; this will be discussed later in the argon geochronology section.

Ore zones are currently represented by residual material after decalcification, that have up to 1 % hematite and gold is closely associated with the Fe-oxide. Oxidation of pyrite to form hematite is a potential decalcification mechanism in that acid is produced by the oxidation of pyrite. However, the  $\leq 1$  % hematite content of decalcified rock implies that insufficient acid could be produced during oxidation to account for removing  $>80$  % of the rock volume by pyrite oxidation alone. Two decalcification events must have occurred at Pipeline. Oxidation of pyrite provides a sulfur source and therefore the oxidation event is coeval with the sporadic occurrence of barite peripheral to the deposit.

## Fluid Inclusions

### *Microthermometry*

Twenty-five fluid inclusion sections were studied. Microthermometry results are reported in Appendix B. The convention used to classify Pipeline fluid inclusions is based on the number of phases and the composition of these phases (Table 4.2).

Primary inclusions hosted in quartz are abundant, 5 to 20  $\mu\text{m}$  in size, invariably elongated, and irregular in shape. Clusters of inclusions form zones that mimic the crystal habit of quartz (Fig. 4.10). Secondary inclusions occur either individually or as trails of

<b>Inclusion Type</b>	<b>Description:</b>
Type 1a (Fig. 4.11)	Two phase liquid and vapor inclusion that is liquid-dominated (aqueous) with a vapor bubble that is smaller than the aqueous phase. The inclusion may or may not exhibit clathrate melting behavior.
Type 1b (Fig. 4.12)	Three phase, liquid-dominated inclusion that has a vapor bubble that is smaller than the aqueous phase and minor liquid $\text{CO}_2$ at $10^\circ\text{C}$ . The inclusion exhibits clathrate melting.
Type 2 (Fig. 4.13)	Three phase aqueous, $\text{CO}_2$ -dominated inclusions that at $10^\circ\text{C}$ have a small rim of aqueous fluid and $>50\%$ by wt. of liquid and gaseous mixture of $\text{CO}_2$ and other gaseous species.

Table 4.2 Fluid inclusion classification as recognized at Pipeline.

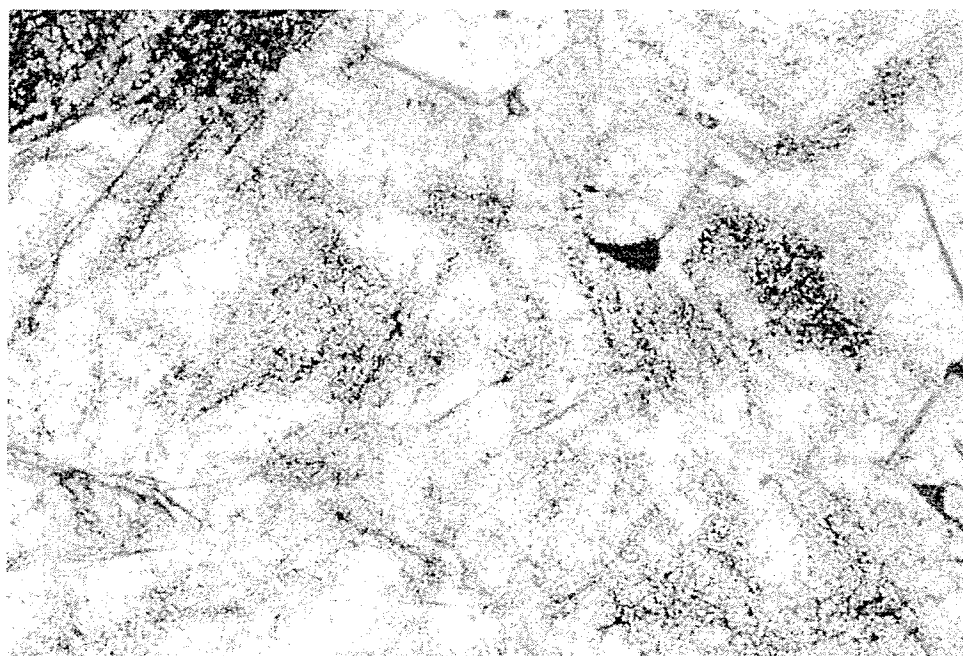


Figure 4.10 Stage 3 quartz grain (sample NB-99) showing primary, zoned fluid inclusions which mimic the crystal shape. The field of view is about 1200  $\mu\text{m}$ .

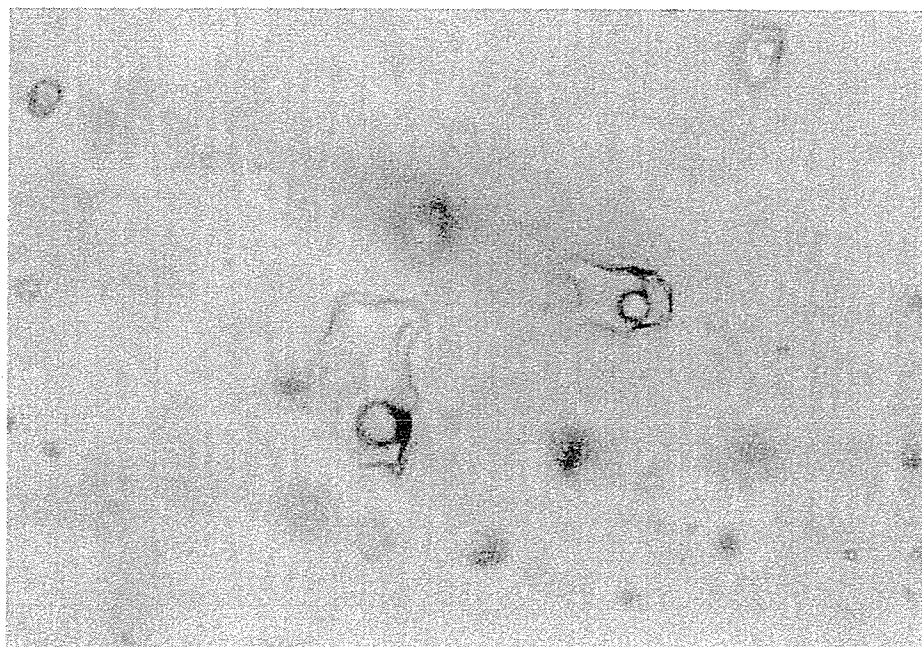


Figure 4.11 Type 1a fluid inclusions (stage 3 quartz; sample NB-33) comprising a dominant aqueous phase and a minor vapor phase. No carbonic phase is visible. The field of view is about 120  $\mu\text{m}$ .

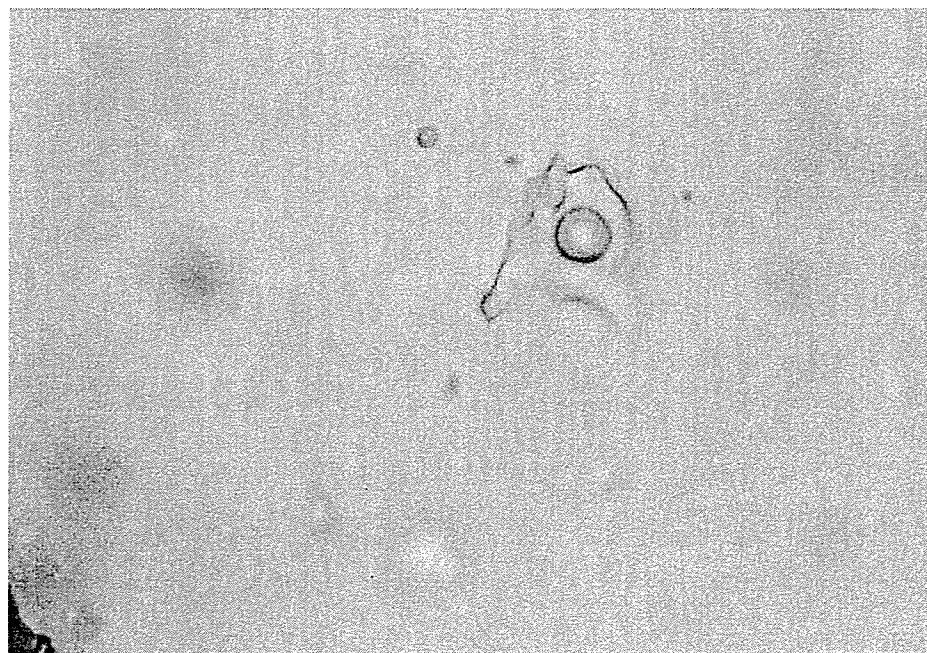


Figure 4.12 Type 1b fluid inclusion hosted in stage 3 quartz (sample NB-107). The inclusion comprises a major aqueous phase and a minor bubble. The bubble shows a vapor phase in the center, rimmed by liquid CO<sub>2</sub>. The field of view is about 120  $\mu\text{m}$ .

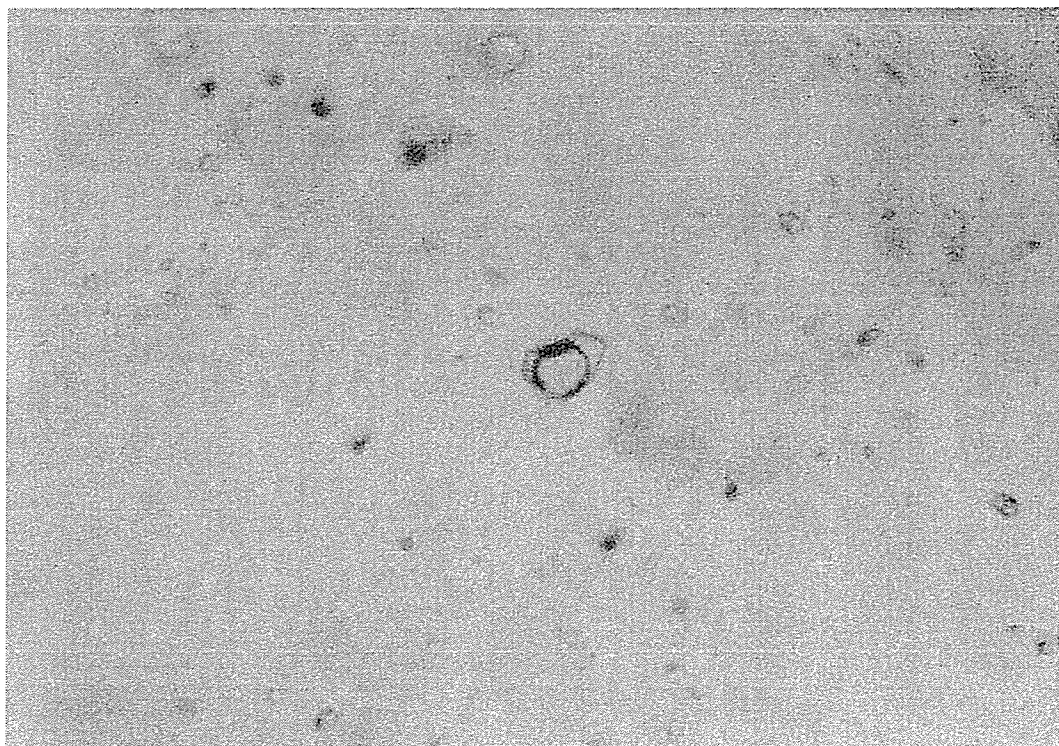


Figure 4.13 Type 2 fluid inclusion hosted in stage 3 quartz (sample NB-104). The inclusion comprises a dominant carbonic phase and a minor aqueous phase. The carbonic phase homogenizes to a liquid. The field of view is about 100  $\mu\text{m}$ .

weakly orientated inclusions of 8 to 15  $\mu\text{m}$ .

Inclusions hosted in calcite are commonly submicron in size, however, sparse visible inclusions of up to 8  $\mu\text{m}$  occur. These visible inclusions are invariably rectangular.

Type 1a inclusions are aqueous-dominated with a vapor bubble generally exceeding 10% by volume (Fig. 4.11). On heating, the aqueous phase expands at the expense of the vapor phase until the inclusion homogenizes to a liquid at which point the bubble disappears. Upon freezing, ice forms at the expense of liquid and during subsequent thawing, the salinity of the inclusion in eq. wt. % NaCl is determined from the melting depression of ice below 0°C. Unlike the gentle melting of ice in contact with brine, clathrate melting occurs very rapidly and the disintegration of the solid phase occurs almost instantaneously. Final melting occurs above 0°C for inclusions that exhibit clathrate melting behavior. Inclusions are heated at a ramp rate of 2°C/min between -20° and 0°C to help stabilize the clathrate.

Type 1b inclusions are aqueous dominated, but at 10 °C annular rings of liquid CO<sub>2</sub> are visible (Fig. 4.12). The liquid CO<sub>2</sub> and vapor bubble may homogenize to a liquid or a vapor. All Type 1b inclusions exhibit clathrate melting behavior. Total homogenization is always to an aqueous phase.

Type 1 inclusions appear to have a broad range of CO<sub>2</sub>. Those inclusions with very little CO<sub>2</sub> exhibit ice melting behavior. As the CO<sub>2</sub> content increases the melting behavior changes to clathrate melting and with more CO<sub>2</sub>, visible rings of liquid CO<sub>2</sub> occur. The characteristics defining Type 1 inclusions reflect end member compositions of which an entire spectrum of compositions are present.

Type 2 inclusions are sparse and have a small aqueous phase (generally 10% by volume, perhaps none visible) and the remainder comprises a CO<sub>2</sub>-rich phase that homogenizes to a liquid between 10° and 31°C (Fig. 4.13). Type 2 inclusions homogenize around 300°C from a major supercritical CO<sub>2</sub> phase and a minor aqueous phase, to a carbonic phase. On freezing, the CO<sub>2</sub> phase forms solid CO<sub>2</sub> between -90° and -100°C. This solid phase melts between -57° and -60°C. All Type 2 inclusions show clathrate melting behavior of the aqueous phase. Often it is impossible to discern if Type 2 inclusions are primary or secondary, however, in one case four Type 2 inclusions occurred in a line suggesting that they are secondary.

*Stage 1 inclusions:* Only one inclusion section out of four has visible aqueous inclusions. Black calcite has primary and secondary, 5 to 10 µm, Type 1a inclusions with about 98% fill. Submicron carbonaceous material is observed under the microscope and possibly represent polymerized hydrocarbons that were once hosted within fluid inclusions. Homogenization temperature (Th) measurements vary from 142° to 152°C. Melting temperature measurements (Tm) are bimodal. Ice melting temperatures (Tm<sub>ice</sub>) are -0.8 ±0.4°C; inclusions exhibiting clathrate melting have Tm<sub>cl</sub> from +1° to +23.2°C. The salinities of inclusions with Tm between -0.4° and -1.2°C calculated range from 0.7 to 2.2 eq. wt. % NaCl. Owing to clathrate melting behavior in hydrocarbon-rich inclusions, the salinity cannot be accurately determined. Fluid-inclusion salinity can be estimated from clathrate melting, provided the gaseous species are known. Black calcite gas analyses presented below shows considerable analysis to analysis variation of the clathrate



forming species  $\text{CO}_2$ ,  $\text{CH}_4$ , and  $\text{C}_3\text{H}_8$ , therefore estimating inclusion salinity from the clathrate melting temperatures is not possible. However, clathrate melting temperatures above  $10.7^\circ\text{C}$  indicate the presence of methane, and clathrate melting temperatures above  $16^\circ\text{C}$  suggest inclusions contain mixtures of  $\text{CH}_4$  with heavier hydrocarbon species (Katz et al., 1959).

*Stage 2 inclusions:* The one fluid inclusion section examined was host to abundant fluid inclusions. All VC-2 fluid inclusions are primary, Type 2, 8 to 15  $\mu\text{m}$  in size, and comprise about equal proportions by volume of water and a  $\text{CO}_2$ -rich phase. Homogenization of  $\text{CO}_2$ -liquid and vapor ( $T_{\text{hCO}_2}$ ) to liquid occurs between  $+23.2^\circ$  and  $+25.5^\circ\text{C}$ . These measurements correspond to a  $\text{CO}_2$  density range of 0.72 to 0.75. Decrepitation of inclusions start at  $200^\circ\text{C}$ ; all the inclusions decrepitated by  $276^\circ\text{C}$  before  $T_{\text{hTOTAL}}$  was reached. Measurement of  $T_{\text{mcl}}$  varies from  $+9.6^\circ$  to  $+11.5^\circ\text{C}$ . The  $T_{\text{mcl}}$  measured could result from additions of methane, which is confirmed by gas analysis, or attributed to either clathrate metastability or high pressure (Katz et al., 1959). The stability of  $\text{CO}_2$  clathrate is extended to higher temperatures as the partial pressure of  $\text{CO}_2$  increases (R. Bakker, pers. comm.). Fluid inclusion salinity of about 0.8 eq. wt. % NaCl is estimated assuming  $\text{CO}_2$ -clathrate melting.

*Stage 3 inclusions:* From ten stage 3 inclusion sections, a subset of six sections which were not contaminated by secondary inclusion trails were selected. Thermometric analyses of vein quartz and ore quartz analyses show similar results, therefore are discussed together. Quartz is host to primary Type 1a, 1b, and sparse Type 2 inclusions

of 2 to 20 mm in size (Fig. 4.10). Type 1 inclusion Th measurements range from 179° to 265°C (Fig. 4.14) and Tm measurements range from -26.0° to +10.1°C (Fig. 4.15). A general observation is that Th values of Type 1b are higher than Type 1a inclusions. Calculated inclusion salinities cluster in a large group with 5 to 10 eq. wt. % NaCl with some extraneous values as high as 25 eq. wt. % NaCl (Fig. 4.16). Samples that have salinities near 25 eq. wt. % NaCl exhibit eutectic melting of salt-hydrate to brine at temperatures of -21.1° to -26.0°C. Assuming that the potassium contribution can be added to the Na budget, then the Ca/Na ratio of the inclusion is determined by the transition temperature of hydrohalite to ice (see Shepherd et al., 1985, p. 103). The range of calculated Ca/Na ratios for these very saline inclusions is 0.8:1 to 1.4:1.

Some Type 1a inclusions exhibit clathrate melting behavior. Liquid CO<sub>2</sub> is not observed in these inclusions (Fig. 4.11), however, this does not preclude that small annular rings of liquid CO<sub>2</sub> are present which could not be seen in the small-size inclusions. Measurements of sample NB99 zoned quartz crystals show a change in fluid chemistry with time. Fluid inclusions in the core have T<sub>m<sub>ice</sub></sub> (ice melting temperature) values in the region of -5°C. Toward the outside of the same crystal, fluid inclusions exhibit clathrate melting behavior and T<sub>m<sub>cl</sub></sub> (clathrate melting temperature) about +7°C (Fig. 4.17). The calculated salinities from T<sub>m<sub>ice</sub></sub> and T<sub>m<sub>cl</sub></sub> measurements are about 7 eq. wt. % NaCl.

In Type 1b inclusions liquid-CO<sub>2</sub> and vapor homogenize to liquid (Fig. 4.12), and T<sub>m<sub>CO2</sub></sub> ranges from +13° to +23°C. A general increase in Th values are observed for Type 1b inclusions in comparison to Type 1a. The highest Type 1 inclusion Th of 265°C was measured on a Type 1b inclusion.

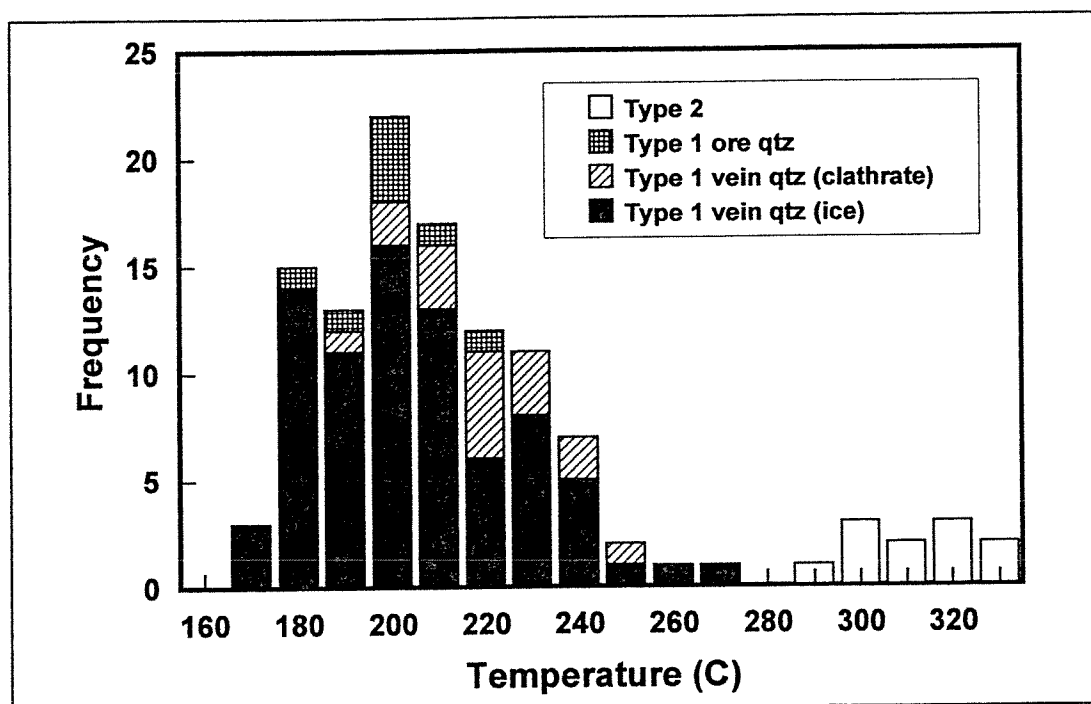


Figure 4.14 Histogram of Th's measured for all inclusions hosted in stage 3 quartz. Note that Type 2 inclusions have higher Th measurements than Type 1.

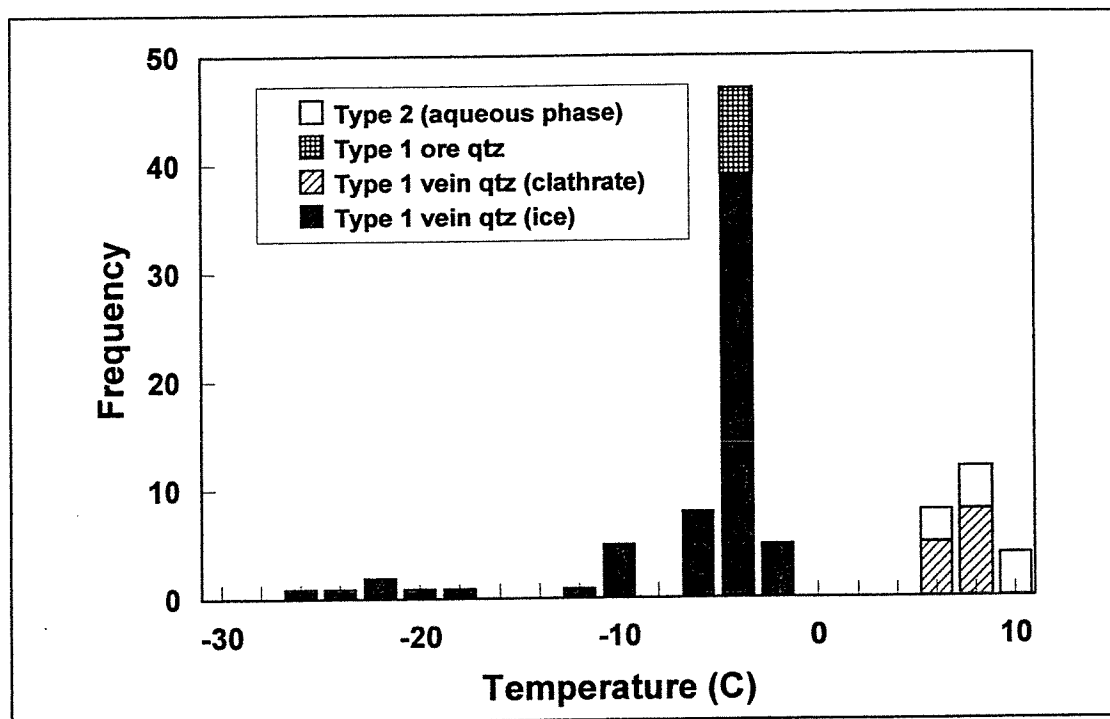


Figure 4.15 Histogram of  $T_m$  values measured for all inclusions hosted in stage 3 quartz.

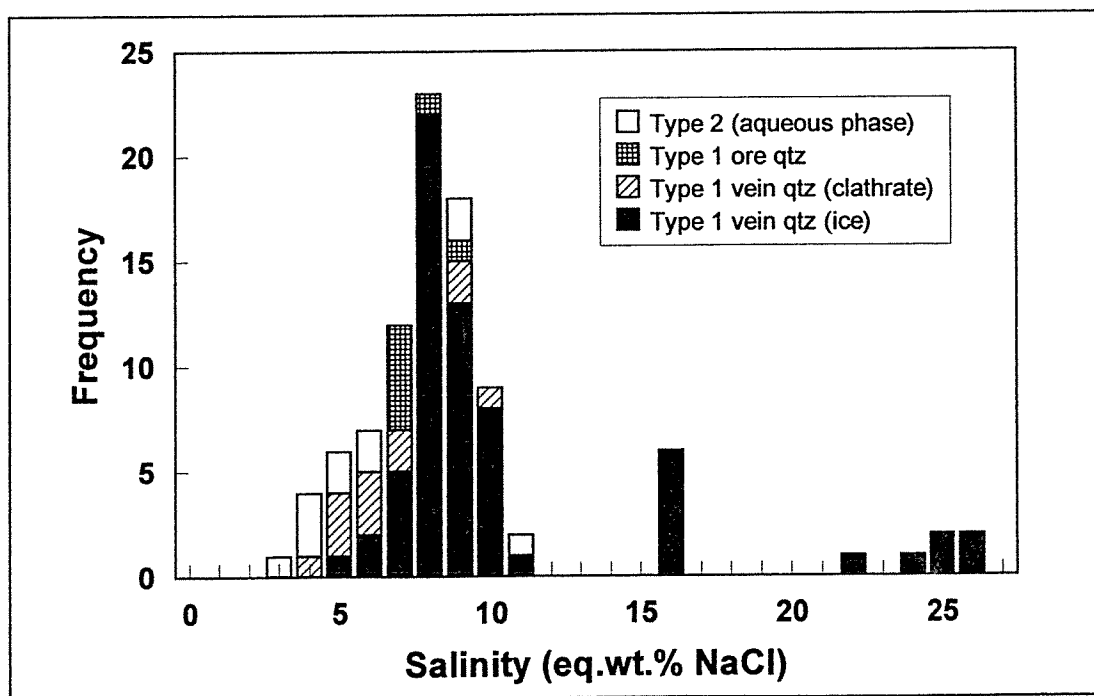


Figure 4.16 Histogram of salinity determined for all inclusions hosted in stage 3 quartz.

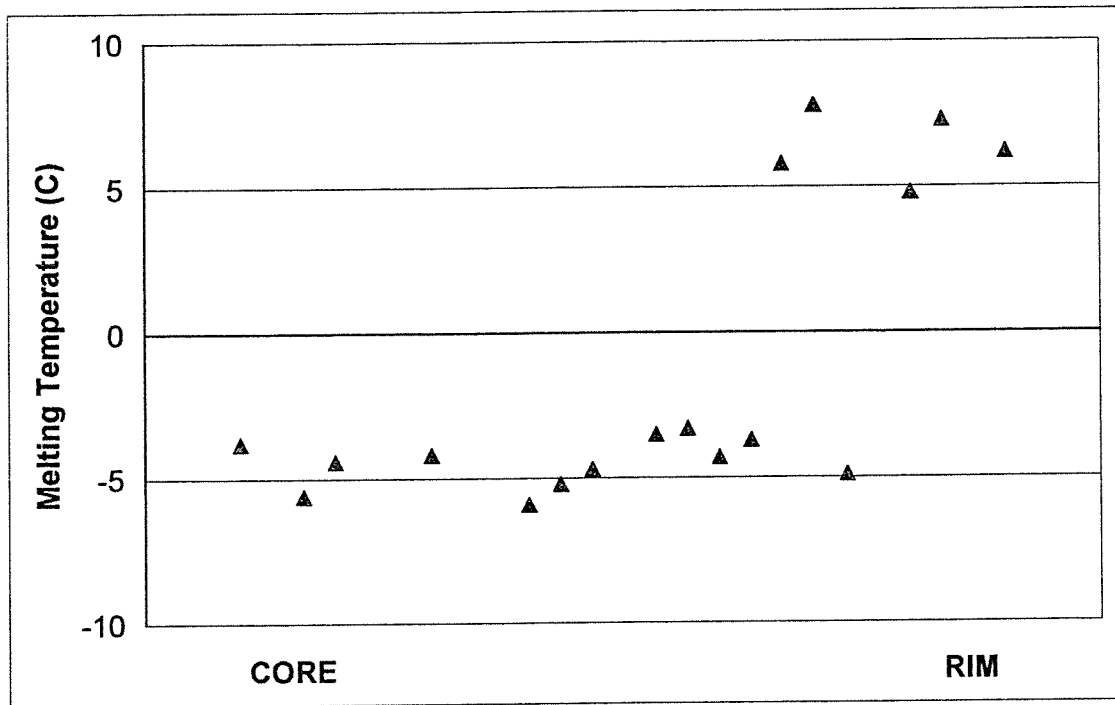


Figure 4.17 Distribution of T<sub>m</sub> values for sample NB-99 (stage 3 quartz) showing ice melting behavior within the crystal core and clathrate melting at the rims.

Type 2 inclusions are sparsely distributed, are secondary and vary from 3 to 20  $\mu\text{m}$  in size (Fig. 4.13). The aqueous phase of Type 2 inclusions exhibits clathrate melting (Fig. 4.15). Type 2 inclusion  $T_h$  values vary from 295° to 323°C (Fig. 4.14). However, measurements are few because Type 2 inclusions readily decrepitate at temperatures >250°C. The inner non-aqueous liquid in Type 2 inclusions melts at about -59° to -58°C and corresponds to 9-12 mol. %  $\text{CH}_4$  in the carbonic phase (Shepherd and Rankin, 1985). The inner liquid and vapor homogenize to liquid at +13° to +23°C. These measurements correspond to a  $\text{CO}_2$  density range of 0.76 to 0.85. Calculated brine salinity ranges from 5 to 6 eq. wt. % NaCl, and the calculated salinity of the inclusion fluid as a whole is about 0.5 eq.wt. % NaCl.

Calcite exhibits primary fluid inclusions that commonly occur in zones (Fig. 4.18). Calcite-hosted fluid inclusions are generally submicron (Fig. 4.19) but some as large as 8  $\mu\text{m}$  provide practical geothermometry measurements. Secondary inclusions are not observed. Calcite  $T_{m_{\text{ice}}}$  measurements range from -1.8° to -2.0°C and  $T_h$  values range from 219° to 235°C. Calculated salinities are 3.0 to 3.3 eq. wt. % NaCl.

A single quartz-orpiment vein was recovered from a NNW-trending fracture within the Pipeline pit that shows some differences from the stage 3 quartz below the ore zones. This is possibly a stage 3 vein and it is therefore mentioned together with stage 3. The quartz is host to primary and pseudosecondary Type 1a and 1b fluid inclusions. These inclusions exhibit clathrate melting behavior;  $T_{m_{\text{cl}}}$  measurements range from +6.8° to +7.9°C. The  $T_{m_{\text{CO}_2}}$  values for Type 1b inclusions range from -60.2° to -60.7°C and  $T_{h_{\text{CO}_2}}$  was measured from 21° to 27°C as homogenization proceeds to a liquid. Type 1a inclusion  $T_h$  varies from 192.9° to 233.1°C. Type 1b  $T_h$  values range from 303.3° to



Figure 4.18 Primary, zoned fluid inclusions hosted in stage 3 calcite. The field of view is about 1200  $\mu\text{m}$ .

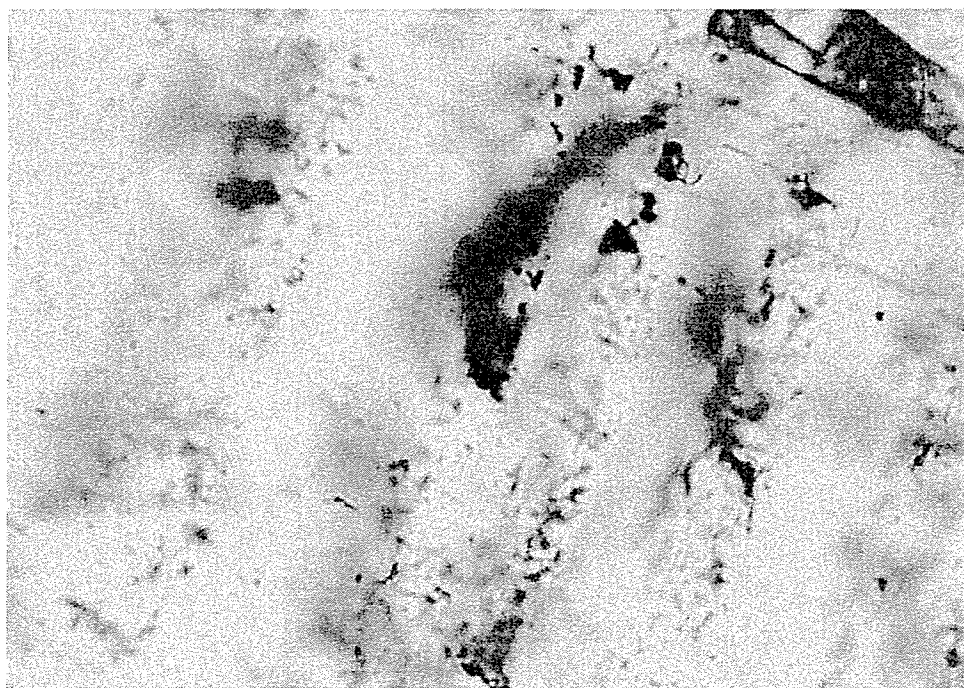


Figure 4.19 Primary, submicron, Type 1 fluid inclusions hosted in stage 3 calcite. The field of view is about 100  $\mu\text{m}$ .

312.8°C. Estimated inclusion salinities, assuming CO<sub>2</sub> clathrate is observed, range from 5.15 to 6.88 eq. wt. % NaCl. Estimated inclusion CH<sub>4</sub>/CO<sub>2</sub> ratios from the CO<sub>2</sub> melting point (Shephard et al., 1985) range from 0.31 to 0.34.

### *Gas Chemistry*

The individual gas analyses from the quadrupole mass spectrometer are given in Appendix C. Forty-four samples (calcite = 21, quartz = 21, pyrite = 1, barite = 1) were analyzed yielding 531 analyses of the major volatile species and 118 analyses of the organic species. Table 4.3 gives representative analyses of each mineral analyzed.

*Stage 1 and stage 2 calcite:* Gaseous species comprise 2.27 to 6.43 mol.% of volatiles in VC-1 calcite and 50.88 to 70.05 % in VC-2 calcite. These ratios are in line with observations made on inclusion liquid to vapor relationships. On a CO<sub>2</sub>/CH<sub>4</sub>-N<sub>2</sub>/Ar diagram (Fig 4.20; template from Norman et al., 1998), VC-1 inclusions show a range in composition from those with N<sub>2</sub>/Ar <100 and CO<sub>2</sub> >CH<sub>4</sub> to inclusions that have N<sub>2</sub>/Ar >100 and CH<sub>4</sub> >CO<sub>2</sub>. In contrast all VC-2 analyses indicate similar CO<sub>2</sub>/CH<sub>4</sub> ratios and a small range in N<sub>2</sub>/Ar ratios (Fig. 4.20).

*Stage 3 sericite-quartz-calcite:* Quartz inclusion analyses show gaseous species ranging from 0.54 to 13.21 mol. %. The H<sub>2</sub>S content is highly variable ranging from 0.00001 to 0.03 mol. % and CO<sub>2</sub> ranges from 0.22 to 11.3 mol. %.



Vein	VC-1	VC-2	VQ3	VC3	VC-4
Mineral	calcite	calcite	quartz	calcite	calcite
H2	0.718	0.095	0.085	0	0
He	0.0019	0.0065	0.00059	0.00019	0.0016
CH4	2.05	0.48	1.04	0.11	0.063
H2O	95.24	35.6	93.1	99.3	99.7
N2	0.197	0.36	0.19	0.031	0.14
O2	0.0106	0	0	0	0.025
H2S	0.00012	0.0027	0.013	0.0003	0.00022
Ar	0.00047	0.0028	0.00036	0.00033	0.0021
C3H8	0.01707	0.19	0.012	0.00104	0.00041
CO2	1.76	63.3	5.55	0.58	0.041
SO2	0.00014	0.0002	0.00004	0.00001	0.00004
CO2	95.8		84.4	91.2	
CH4	3.78		15.0	8.3	
C2H4	0.076		0.024	0.020	
C2H6	0.096		0.26	0.126	
C3H6	0.089		0.084	0.093	
C3H8	0.13		0.18	0.187	
C4H8	0.00007		0.011	0.0024	
C4H10	0.0015		0.004	0.0070	
C5H10	0		0	0	
C6H6	0.00001		0.00054	0.0021	
C7H8	0		0.00021	0.00046	

Table 4.3 Typical gas analysis for the sampled vein sets. The upper group are the traditional geothermal species that are analyzed. The lower group represent the carbon-bearing species, normalized to 100%.

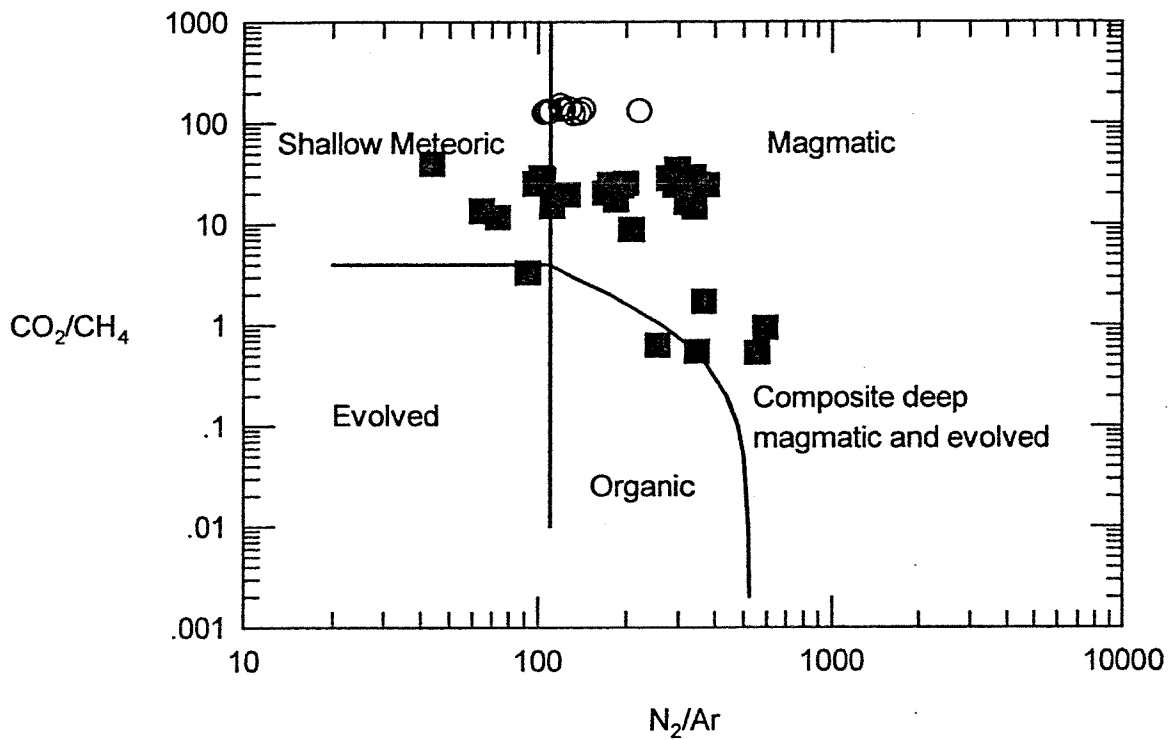


Figure 4.20 Discrimination  $\text{CO}_2/\text{CH}_4$  vs  $\text{N}_2/\text{Ar}$  diagram for the stage 1 (solid squares) and stage 2 (open circles) calcite veins.

Plotting the quartz data on a CO<sub>2</sub>/CH<sub>4</sub>-N<sub>2</sub>/Ar diagram shows a broad spread of CO<sub>2</sub>/CH<sub>4</sub> ratios (Fig. 4.21). Most N<sub>2</sub>/Ar ratios are well above 500 indicating a significant magmatic component.

A linear relationship exists between CO<sub>2</sub>/CH<sub>4</sub> and H<sub>2</sub>S (Fig. 4.22a and b). Analyses made on quartz samples bearing inclusions with 5 to 10 eq. wt. % NaCl salinities have higher H<sub>2</sub>S levels than analyses of quartz that contain inclusions with 15 to 25 eq. wt. % NaCl (Fig. 4.22). A CO<sub>2</sub> versus total gas content shows a highly linear relationship between CO<sub>2</sub> and gas content of fluid inclusions, and that CO<sub>2</sub> and CH<sub>4</sub> concentrations are not coupled (Fig. 4.23). There is also no discernible relationship between N<sub>2</sub>/Ar and total gas content.

Calcite inclusions generally have lower concentration of gaseous species and a different gas chemistry than inclusions hosted in quartz. Calcite gaseous species mostly range from 0.24 to 1.5 mol. %, although a few analyses indicate up to 5 mol. %. Calcite CO<sub>2</sub>/CH<sub>4</sub> ratios are similar to those measured in quartz, but the N<sub>2</sub>/Ar ratios are much lower (Fig. 4.21). There is appreciably less H<sub>2</sub>S in calcite-hosted inclusions; analyses range from 0.001 to 0.00001 mol. % H<sub>2</sub>S. Calcite analyses show a mixing relationship between a shallow meteoric and a composite magmatic-sedimentary sources (Fig. 4.21). A linear trend between between two end member compositions is shown in Figure 4.24 for calcite analyses.

*Stage 5 vuggy calcite:* The five samples of vuggy calcite analyzed had similar results for thirty-nine analyses. On a CO<sub>2</sub>/CH<sub>4</sub>-N<sub>2</sub>/Ar diagram the data plots in the evolved field (Fig. 4.25).

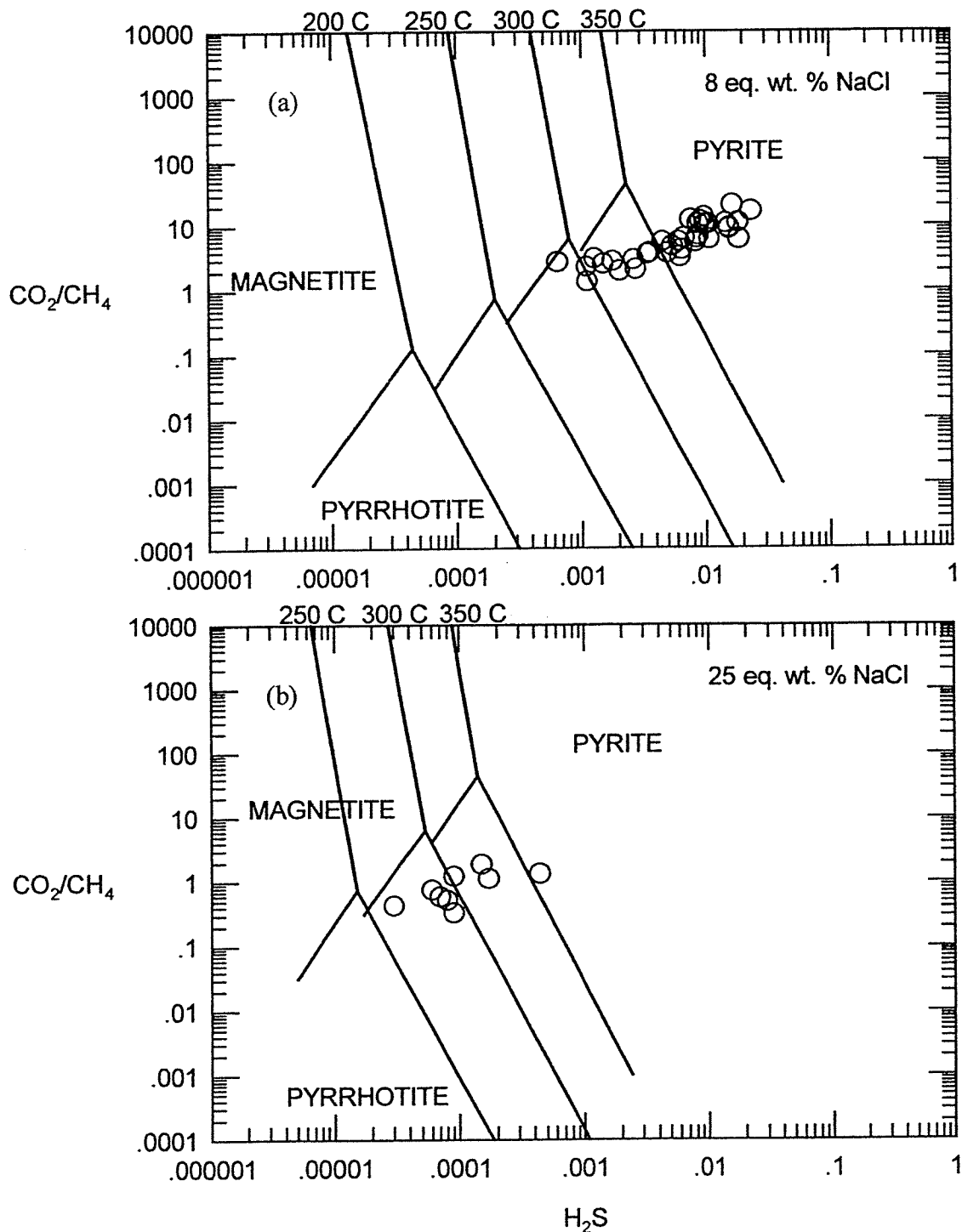


Figure 4.22 Plot of  $\text{CO}_2/\text{CH}_4$  vs  $\text{H}_2\text{S}$  for non-hypersaline (a) and hypersaline stage 3 quartz. Corresponding stability fields for the magnetite-pyrite-pyrrhotite system are shown at varying temperature, calculated for 8 eq. wt. % NaCl (a) and 25 eq. wt. % NaCl (b). Note that the data points have a  $\text{H}_2\text{S}$  content that ranges from 0.001 to 0.03 mol. % for non-hypersaline samples whereas the  $\text{H}_2\text{S}$  content of hypersaline samples varies from 0.00003 to 0.0004 mol. %. This  $\text{H}_2\text{S}$  content corresponds to pyrite stability  $>300^\circ\text{C}$ .

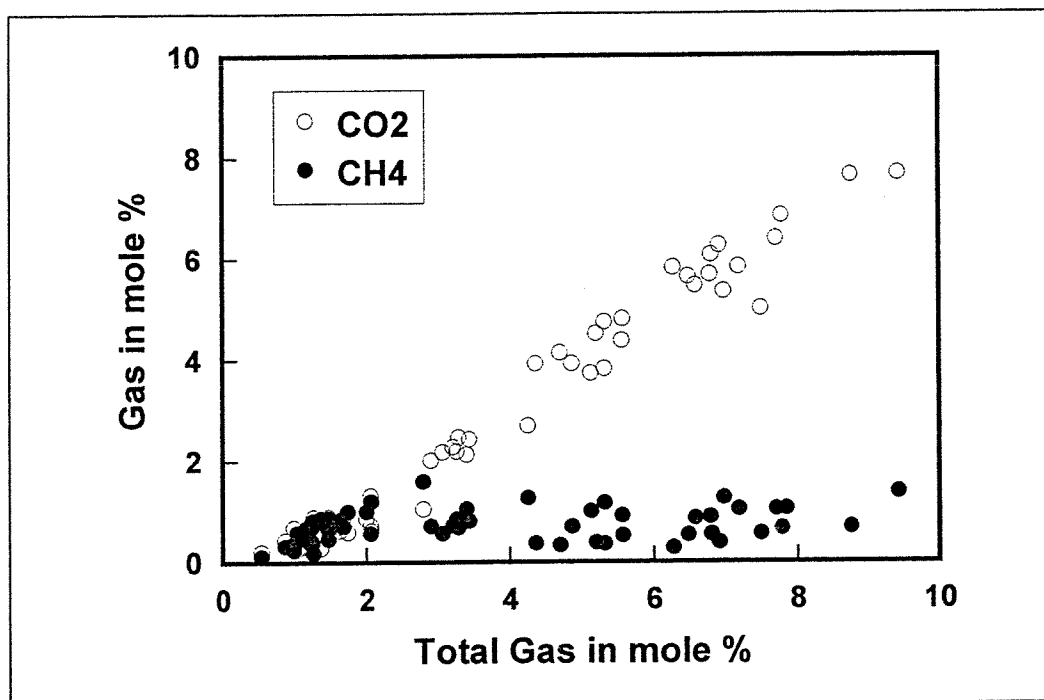


Figure 4.23 Comparison between CO<sub>2</sub> and CH<sub>4</sub> concentration as a function of total gas (excluding water) for the stage 3 quartz. Note that as the CO<sub>2</sub> content decreases, so does the total gas whereas CH<sub>4</sub> is constant.

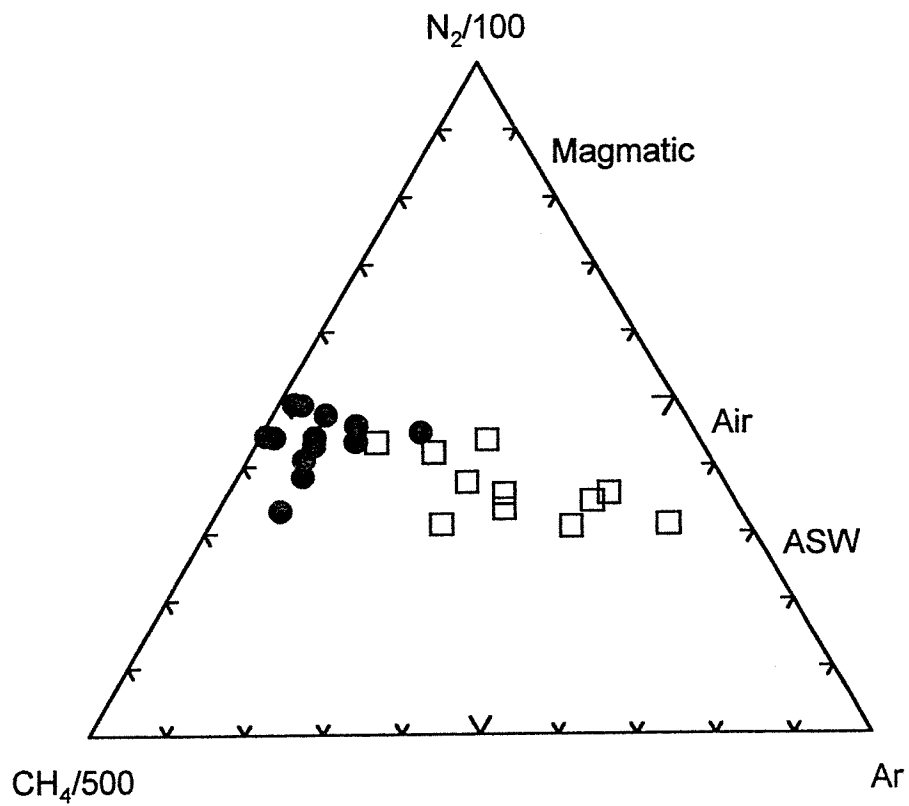


Figure 4.24 Comparison between the calcite (open squares) and quartz (solid circles) from the stage 3 vein set (sample NB-33 only) using the  $CH_4$ - $N_2$ - $Ar$  discrimination diagram. The calcite data plots in a line that has end member compositions corresponding to the quartz gas signature and air saturated water. Mixing is inferred.

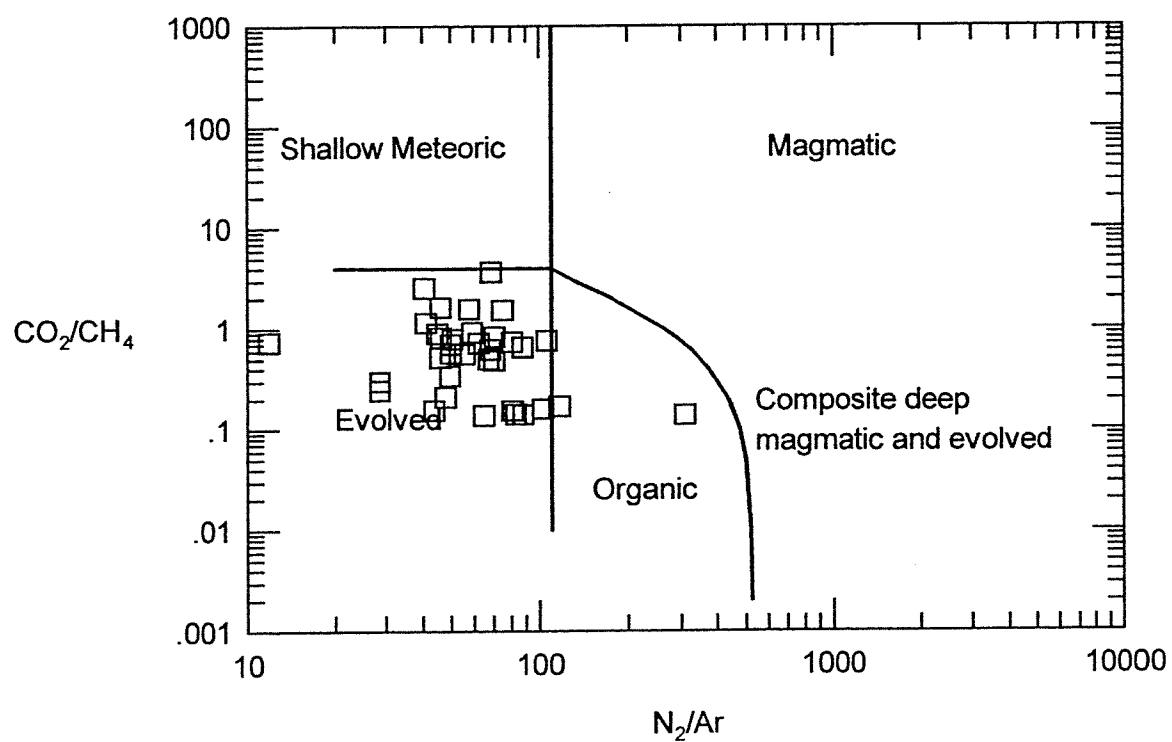


Figure 4.25 Discrimination CO<sub>2</sub>/CH<sub>4</sub> vs N<sub>2</sub>/Ar diagram for the stage 5 vuggy calcite.

### *Bulk cation and anion analysis*

Five samples were analyzed for their anion and cation components. Results are shown in Table 4.4 and are graphically presented in Figure 4.26. The diagram shows a broader range in Ca than for Na and K, and two analyses show  $Ca > Na$ . One of these high Ca samples, NB-100, is host to the hypersaline fluid inclusions from which individual microthermometry measurements gave Ca/Na ratios as high as 1.4. The bulk cation analysis confirms microthermometry observations. The Na/K ratio varies from about 4 to 1. Applying the Fournier geothermometer (Fournier, 1981) yields values from 307° to 515°C. The geothermometer was calibrated to give acceptable values over the temperature range of 150° to 300°C and fluids with lower salinity.

Sample	NB-99	NB-100	NB-102	NB-103	NB-107
Na	5	12	13	21	22
K	4	3	13	5	11
Ca	41	35	24	24	17
Cl	7	30	11	37	40
F	1	1	3	2	2
Br	0	0	0	0	0
SO <sub>4</sub> <sup>2-</sup>	19	10	18	0	0
HCO <sub>3</sub> <sup>-</sup>	23	9	18	11	8

Table 4.4 Results of bulk ion leach converted into percentage of total ion budget (Appendix D). Cations comprise 50% of the total budget and the “missing” anion component is attributed to bicarbonate.

Major anions were analyzed and the results are shown in Table 4.4. Comparing the total cation charge against the total anion charge, the cations always exceed the anions (Appendix D). This “missing” anion component is attributed to bicarbonate. The bicarbonate component in % vs. the Ca/Na ratio is plotted in Figure 4.27. Samples with



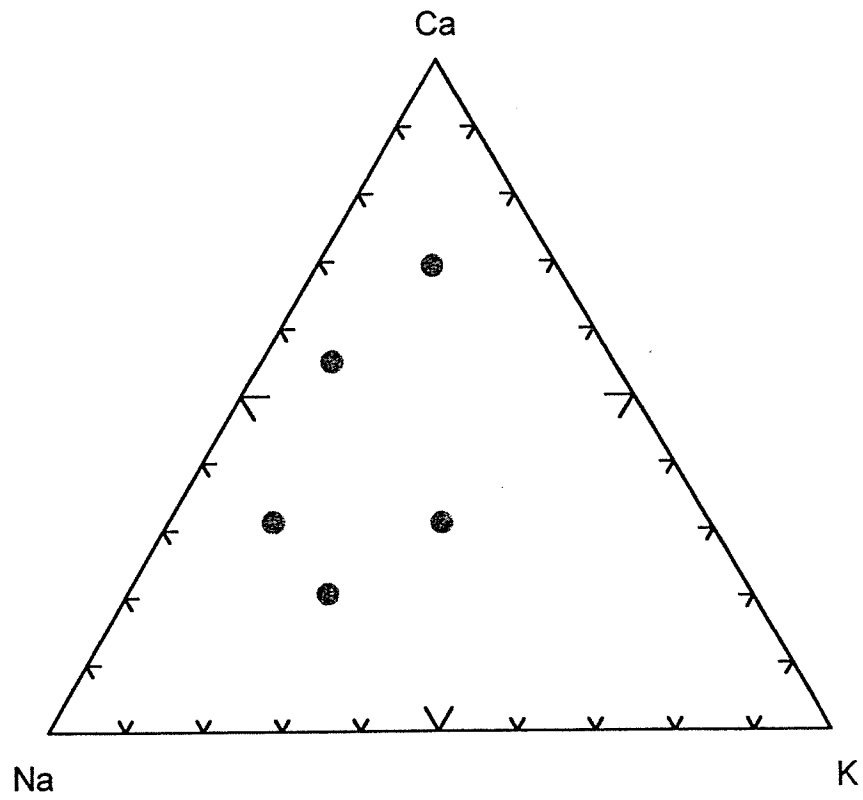


Figure 4.26 Ternary diagram for Ca-Na-K from the bulk cation leach. The high-Ca data corresponds to the hypersaline sample.

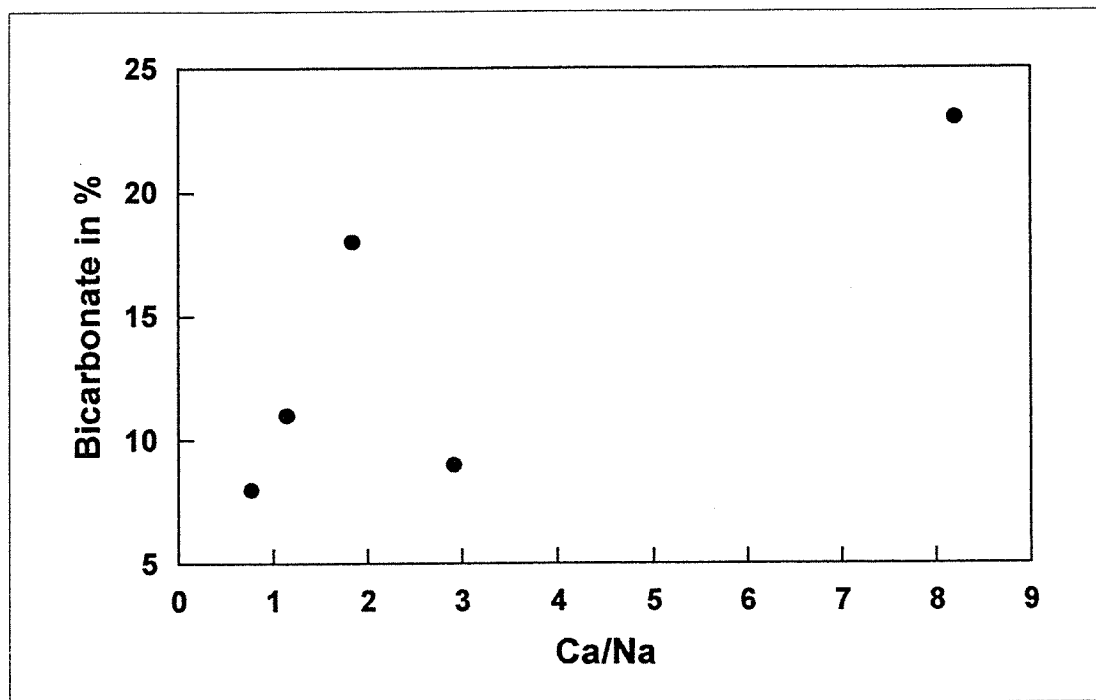


Figure 4.27 Plot of bicarbonate component in % vs. Ca/Na ratio. Highest bicarbonate correlates with highest Ca/Na whereas lowest bicarbonate correlates with lowest Ca/Na.

highest bicarbonate are those with high Ca/Na ratios, whereas samples with a low bicarbonate have low Ca/Na ratios.

### Argon Geochronology

The furnace incremental heating age spectrum method was used to analyze all samples. Abbreviated analytical methods for the dated samples are given in Appendix E. The argon isotopic results are listed in Appendix F; all errors are  $2\sigma$  unless otherwise stated.

Both the K-feldspar and biotite from sample 93271 collected at South Trench exhibit simple age spectra with a plateau for greater than 90% of the gas release (Fig. 4.28b). The biotite has a weighted mean age for steps C through I of  $35.88 \pm 0.14$  Ma with an MSWD for these steps of 4.93. Slightly elevated MSWD indicate scatter which can not be accounted for by analytical uncertainties. The radiogenic yield for the plateau steps is about 95%, and the K/Ca ratio decreases towards the final heating steps. The K-feldspar has a weighted mean age for all the steps of  $35.72 \pm 0.06$  Ma and an MSWD of 1.04.

The biotite and K-feldspar pair from Cortez have slightly younger apparent ages than the South Trench sample. Biotite has a plateau for ~89% of the  $^{39}\text{Ar}$  released giving a weighted mean age of  $35.80 \pm 0.24$  Ma and is analytically indistinguishable from the biotite in sample 93271 (Fig. 4.28a). In contrast, the Cortez K-feldspar heating spectrum

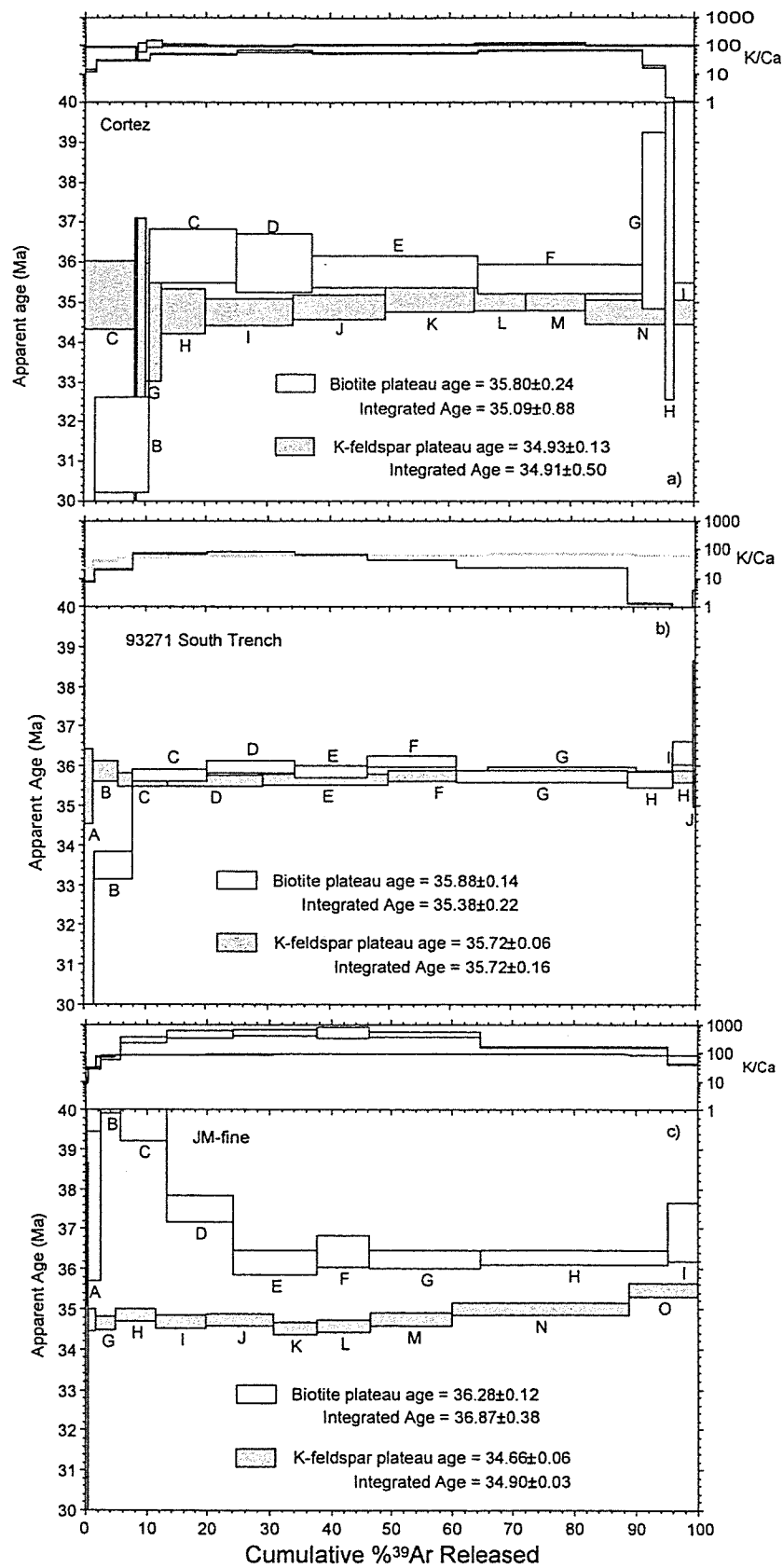


Figure 4.28 Age spectra for all K-feldspar - biotite pairs collected from Eocene dikes.

is flat for 100% of the gas released with a weighted mean age of  $34.93 \pm 0.13$  Ma (MSWD is 0.93).

The biotite and K-feldspar pair from the dike that crosscuts the Mill Canyon stock in a drillhole is referred to as JM-fine. The age spectra for the biotite and K-feldspar are more complex than the Cortez and 93271 biotites (Fig. 4.28c). The biotite age spectrum is disturbed and exhibits ages that are older than the biotite in the Cortez and 93271 samples. Initial heating steps yield old ages and are followed by a plateau segment with an age of  $36.28 \pm 0.12$  Ma (Fig. 4.28c). In contrast, the K-feldspar has an age spectrum that is flat for the first ~50% of the gas released with a plateau age of  $34.66 \pm 0.06$  Ma. The final three steps rise to ~35.5 Ma.

Isochron analyses are reported for several samples. The isochron plots are shown in Figure 4.29 for the samples yielding Eocene apparent ages and the results are reported in Appendix F. The isochron ages are analytically indistinguishable from the plateau ages, however, there are greater uncertainties associated with the isochron ages in comparison to the plateau ages. The final three heating steps from the JM-fine K-feldspar lie on a relatively poor isochron with a MSWD of 11.1. The isochron has a trapped initial  $^{40}\text{Ar}/^{36}\text{Ar}$  value of  $603 \pm 100$  and an apparent age of  $34.78 \pm 0.47$  Ma. This age is within error of the plateau age determined for the initial heating steps and may indicate that the apparent age gradient is related to excess argon in large diffusion domains (Foster et al., 1990).

The Mill Canyon stock is intersected by a reverse-circulation drillhole on the east side of the valley. The sample of Mill Canyon stock is referred to as JM-coarse and is host

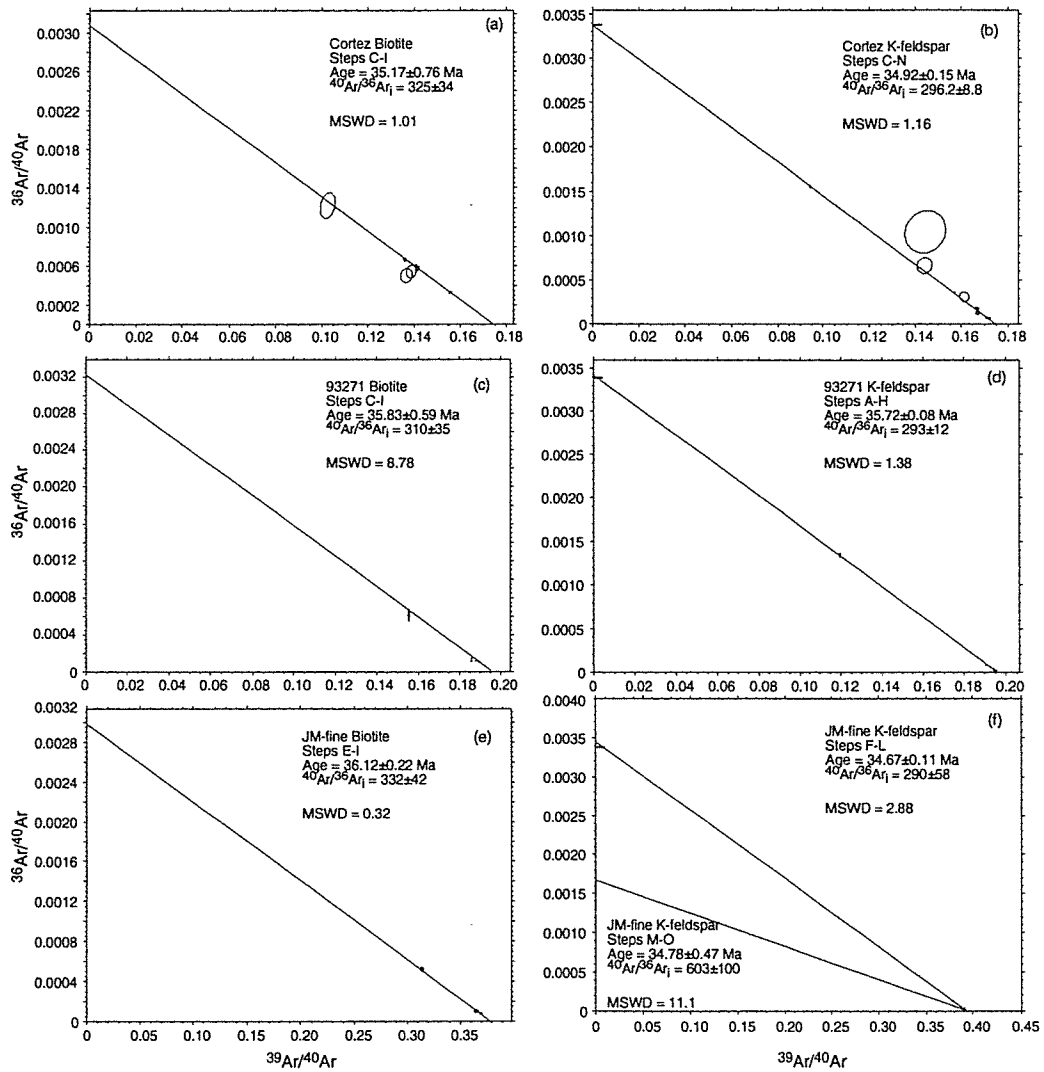


Figure 4.29 Isochron diagrams for biotite and K-feldspars from samples that yield Eocene apparent ages.

to coarse, fresh biotite and K-feldspar. The biotite has a flat age spectrum with a plateau age of  $152.24 \pm 0.33$  Ma, whereas the K-feldspar yields an age gradient ranging from about 50 to 150 Ma (Fig. 4.30).

Sample NB-102 is the only stage 3 vein that is host to hydrothermal sericite. Thin section shows the sericite has variable grain size with a maximum grain size of  $\sim 20$   $\mu\text{m}$  (Fig. 4.31). In contrast, electron microprobe backscatter images show that the material used for dating comprises a mosaic of fine-grained white mica (Fig. 4.32), closely associated with quartz. Using the electron microprobe in point quantitative analysis mode, the sericite was analyzed and the  $\text{K}_2\text{O}$ ,  $\text{Al}_2\text{O}_3$  and  $\text{SiO}_2$  are reported in Table 4.5.

#	$\text{Al}_2\text{O}_3$	$\text{P}_2\text{O}_5$	$\text{TiO}_2$	$\text{MgO}$	$\text{CaO}$	$\text{MnO}$	$\text{Na}_2\text{O}$	$\text{K}_2\text{O}$	$\text{Al}_2\text{O}_3$	$\text{SiO}_2$	Total	$\text{K}_2\text{O}/\text{Al}_2\text{O}_3$	$\text{SiO}_2/(\text{Al}_2\text{O}_3 + \text{K}_2\text{O})$
1	4.00	0.02	0.00	0.09	0.05	0.01	0.01	1.12	4.00	70.69	76.00	0.28	13.8
2	3.08	0.02	0.03	0.08	0.04	0.02	0.02	0.76	3.08	83.81	87.85	0.25	21.8
3	1.62	0.01	0.00	0.05	0.03	0.03	0.04	0.41	1.62	94.27	96.45	0.24	46.4
4	1.81	0.01	0.01	0.04	0.04	0.01	0.00	0.44	1.81	75.39	77.78	0.25	33.5
5	2.57	0.06	0.00	0.11	0.05	0.00	0.03	0.65	2.57	94.11	97.58	0.27	29.2
6	2.82	0.00	0.01	0.07	0.05	0.00	0.02	0.75	2.82	92.35	96.07	0.29	25.9
7	3.45	0.03	0.00	0.08	0.02	0.00	0.02	1.00	3.45	82.39	87.01	0.29	18.5
9	2.18	0.00	0.03	0.08	0.05	0.00	0.03	0.49	2.18	81.06	83.94	0.27	30.3
10	2.75	0.00	0.00	0.10	0.05	0.00	0.03	0.74	2.75	82.27	85.94	0.27	23.6

Table 4.5 Electron microprobe analysis of NB-102 sericite. Note the consistent  $\text{K}_2\text{O}/\text{Al}_2\text{O}_3$  ratios whereas the  $\text{SiO}_2/(\text{Al}_2\text{O}_3 + \text{K}_2\text{O})$  ratios are variable.

The sericite displays a complex age spectrum (Fig. 4.33a). Overall there is a decrease in the apparent ages from heating steps A to J, followed by a dramatic drop in apparent age for the ensuing steps. The drop in apparent age observed for steps K through P coincides with a decrease in radiogenic yield and the lowest K/Ca ratios.

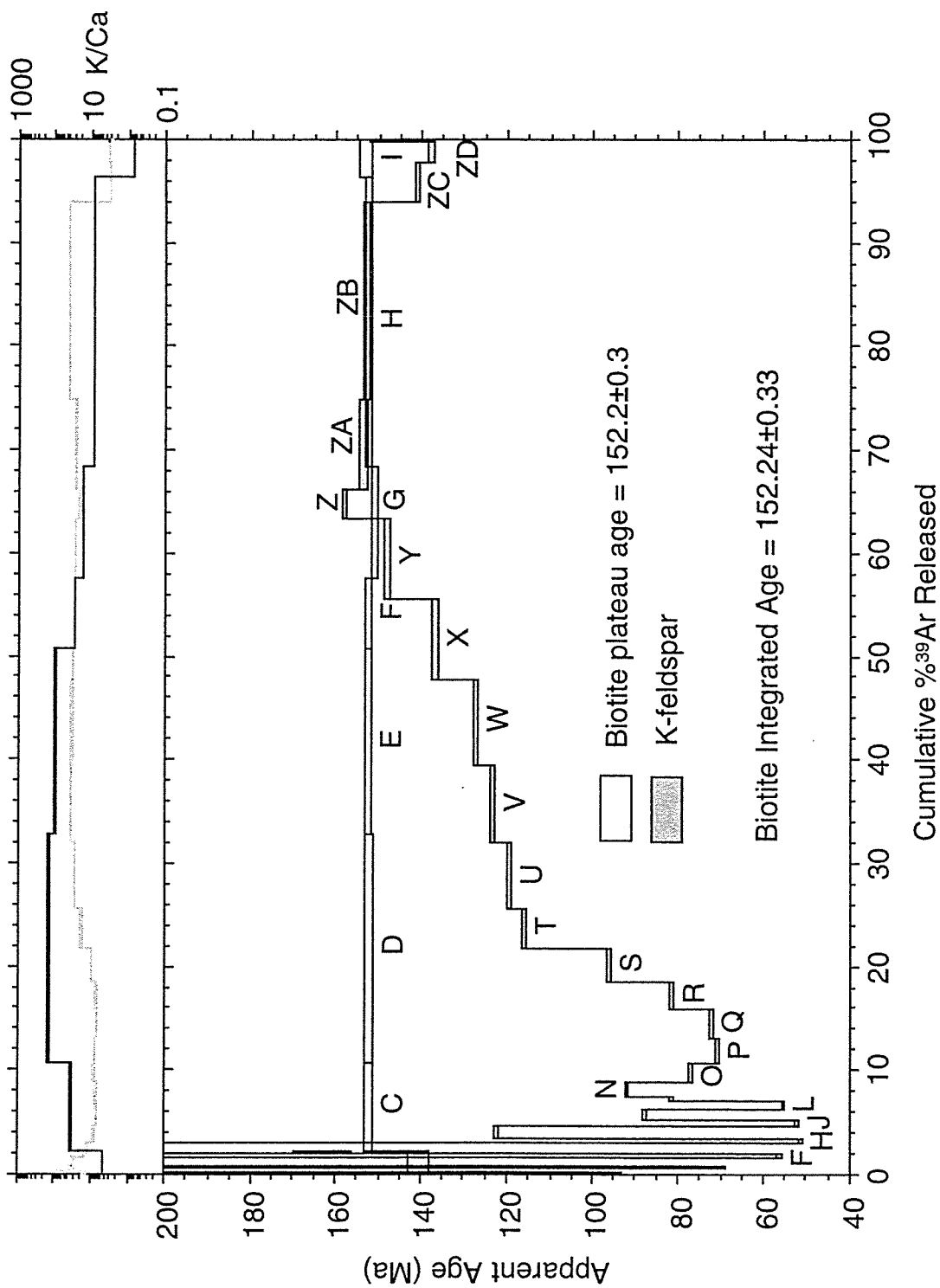


Figure 4.30 Mill Canyon stock (JM-coarse), biotite and K-feldspar age spectra. This sample was collected from the Mill Canyon stock near Cortez Gold Mines.



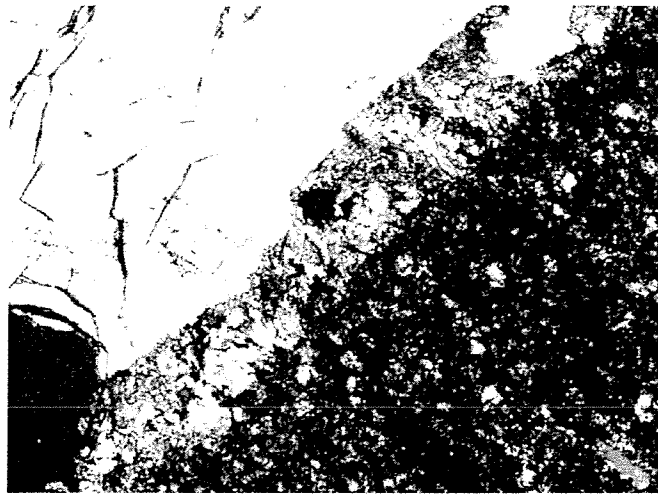


Figure 4.31 Photograph of stage 3 coarse-grained, hydrothermal sericite. The field of view is 1200  $\mu\text{m}$ .

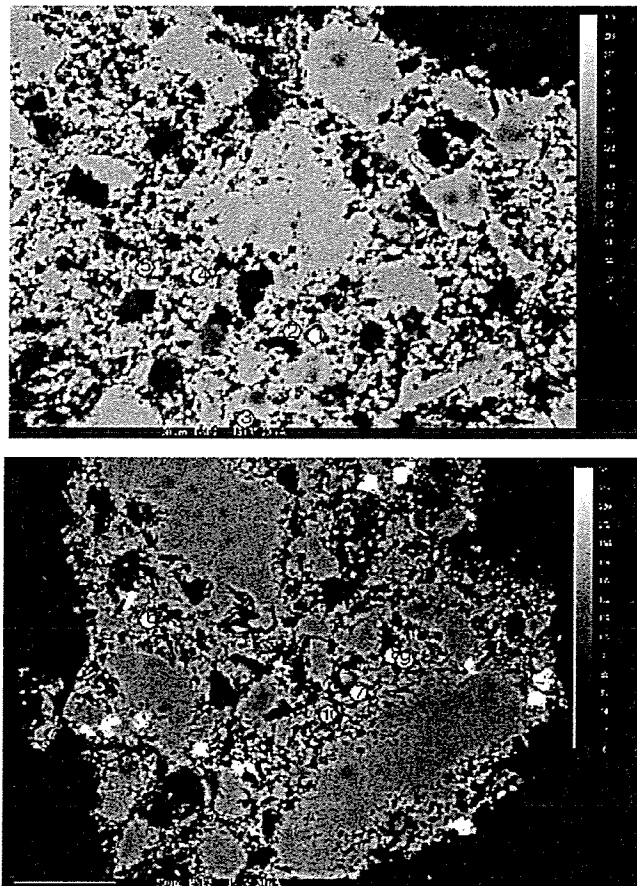


Figure 4.32 Electron microprobe image in backscatter mode of stage 3 sericite and quartz. The image shows a mosaic of fine-grained sericite and closely associated quartz. The uniform grey areas are quartz. Point analyses are indicated.

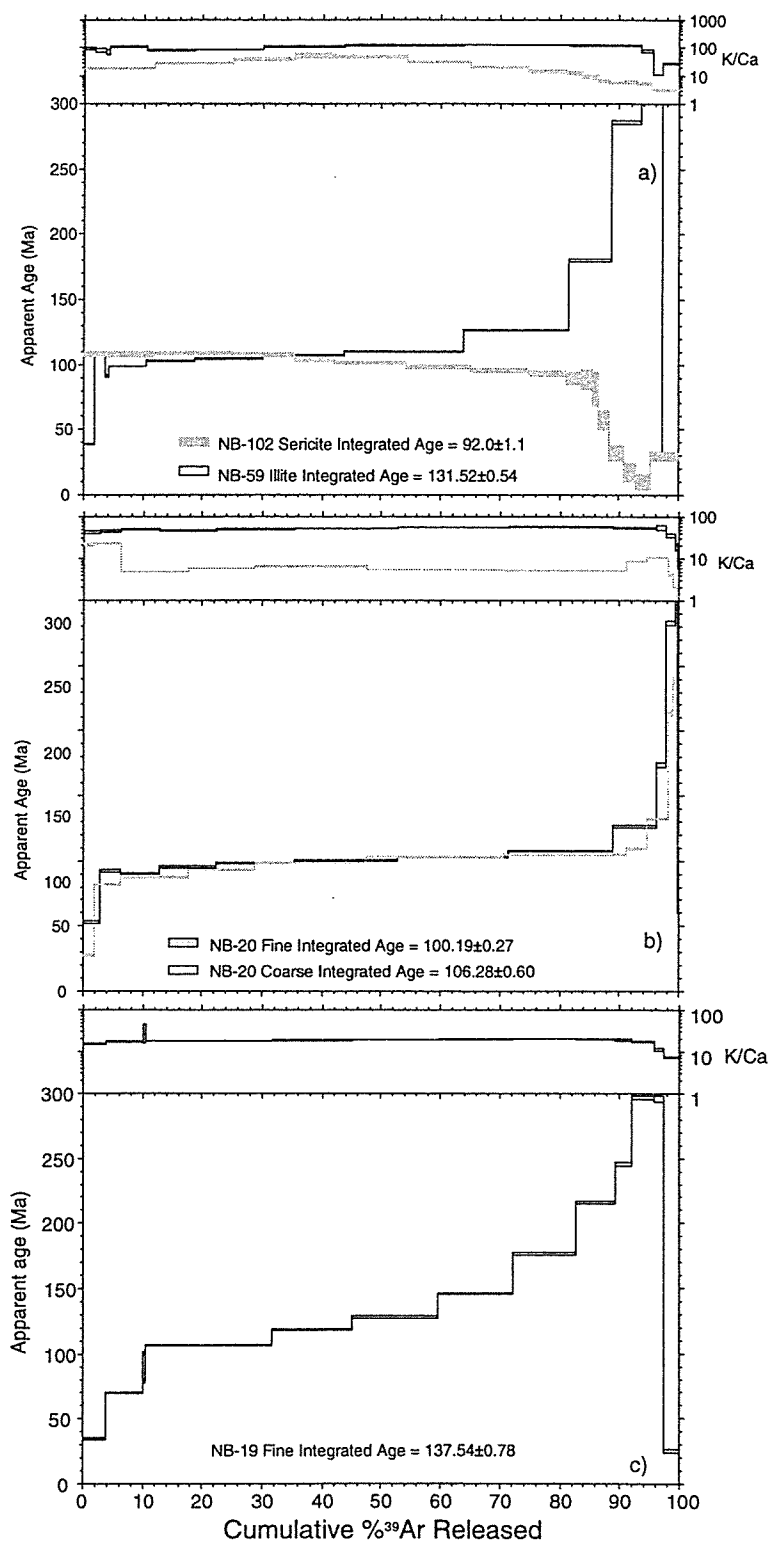


Figure 4.33 Illite age spectra from mineralized zones, argillized zones and faults.

A sample of illite from a mineralized zone (sample NB-20) was separated into a coarse and fine clay fraction. Both coarse and fine-grained fractions show discordant age spectra that steadily climb from about 90 to greater than 250 Ma (Fig. 4.33b). Both size fractions yield nearly identical results, however, the K/Ca values for the fine fraction is almost an order of magnitude lower than the coarse fraction. The radiogenic yield is 100% for nearly all the heating steps.

Illite from a very strongly argillized zone (sample NB-59), also shows a discordant age spectrum (Fig. 4.33a). The spectrum is dominated by steps with apparent ages between 100 and 110 Ma followed by a sharp rise to ages as old as 400 Ma, accompanied by a large drop at the fusion step. The radiogenic yield is almost 100% for heating steps E through N.

An argillized sample from which the clay minerals have been separated is represented by sample NB-19. The age spectrum is discordant with the first heating step being about 35 Ma followed by an age increase for ensuing steps (Fig. 4.33c). There is no plateau evident although there are several heating steps giving ages older than Cretaceous. As with the other illite spectra, the ages climb to very old values near the end of the heating steps followed by a drop for the fusion steps.

### Clay Mineralogy

Clay minerals in the Fence Fault gouge and a NNW-trending fault in the Crescent Pit are illite and kaolinite in a 6:4 ratio (see Fig. 4.34). The first order illite peaks are

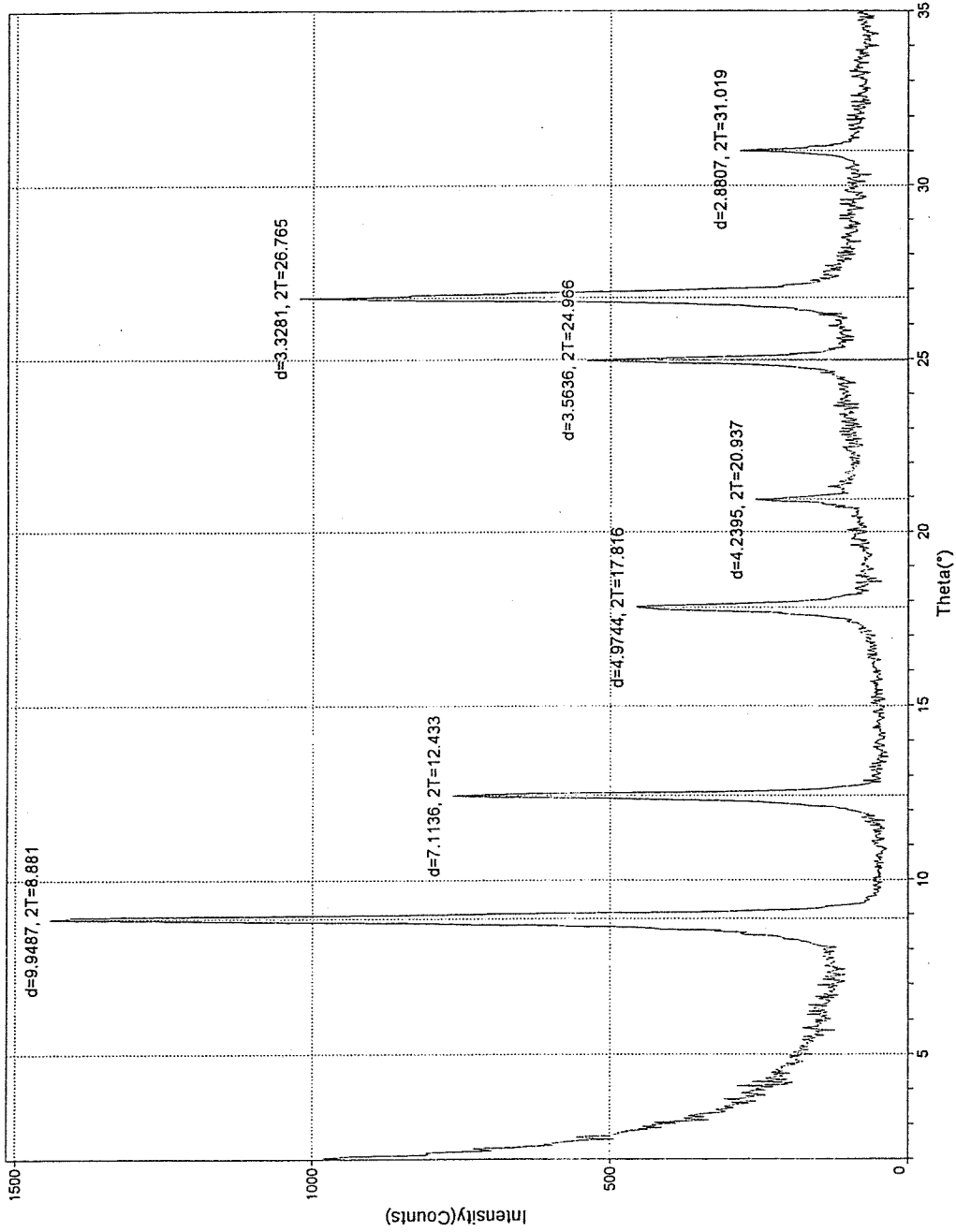


Figure 4.34 Basal section x-ray diffraction pattern for the clay fraction separated from the fault gouge of the Fence Fault. The d-spacing and intensity of the peaks correspond to illite and kaolinite in 6:4 ratio.

sharp. The clay mineralogy of the other fault gouges comprise illite with less than 5% kaolinite or smectite.

Illite is the only clay present in samples collected from mineralized zones (Fig. 4.35). Kaolinite is absent in all samples tested from mineralized zones but was detected in some unaltered samples outside the ore zones. Random mount spectral analysis shows that illite  $2M_1$  polytype dominates, but the presence of 1M polytype is not ruled out (see Fig. 4.36; the diagnostic spectral lines for each polytype are reported in Table 3.1). Spectral lines corresponding to 1M polytype are barely discernible, but identification of the  $2M_1$  polytype is conclusive.

Sixteen analyses show that the clay minerals analyzed from mineralized and/or altered SRM collected along section line 59200, and in drillhole DP104, are exclusively illite. However, in drillhole DP104, accessory kaolinite is present.

The FWHM refers to the full width of the XRD peak at half maximum intensity (Drits, et al., 1997) and is also known as the Kubler Index (Kubler, 1964). Smaller FWHM values correspond to a high degree of sample crystallinity. Samples with broader peaks and higher FWHM values are indicative of more poorly crystalline materials. The crystallinity index of illite is calculated using the FWHM of the 001 illite XRD reflection and the data is reported in Table 4.6. The FWHM of all illite analyzed ranges from 0.198 to 0.418. Comparing FWHM to alteration type (Table 4.6), the FWHM correlates with decalcification intensity ( $R^2 = 0.2$ ) and to argillization intensity ( $R^2 = 0.41$ ).

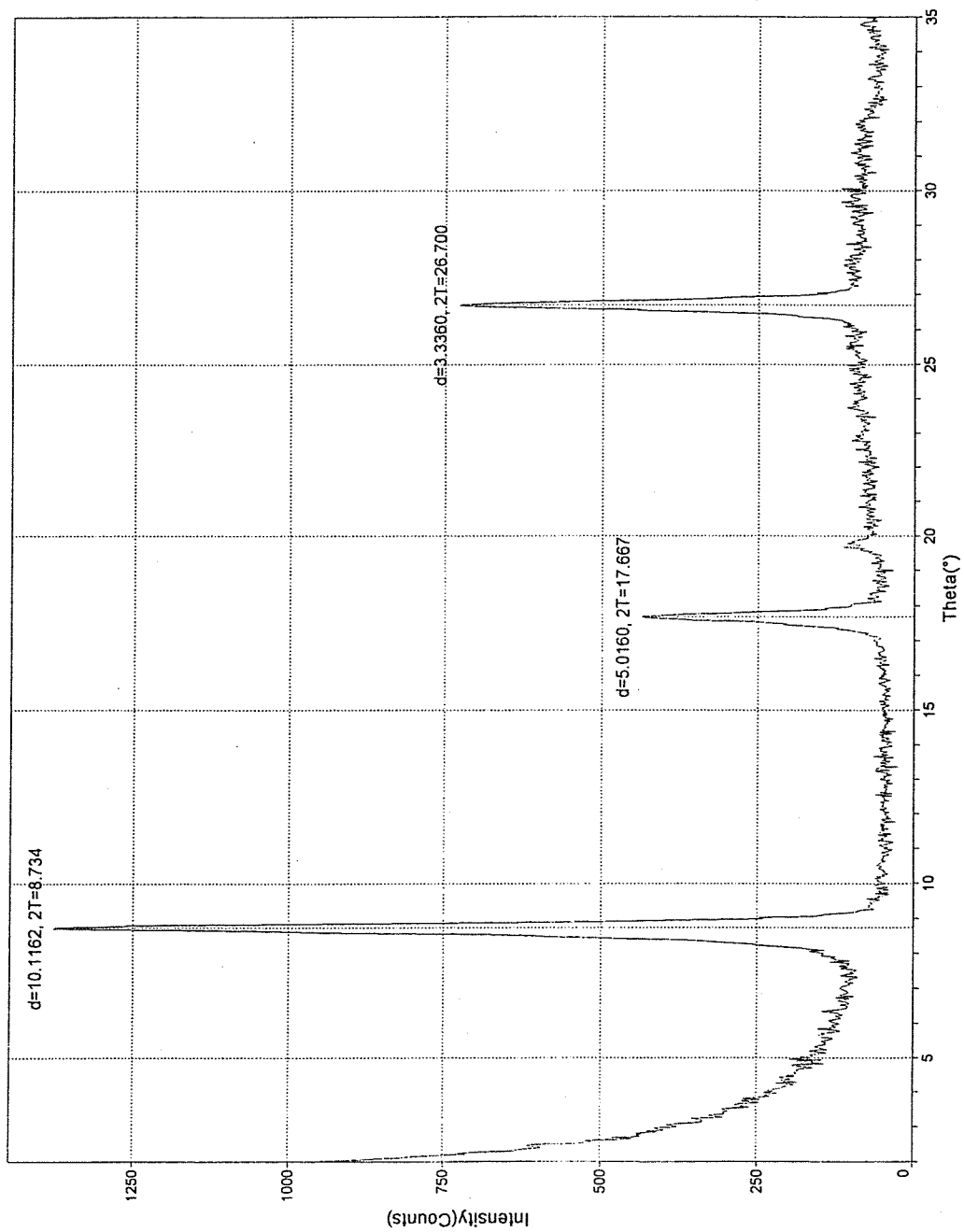


Figure 4.35 Basal section x-ray diffraction pattern for the clay fraction separated from a gold-rich ore zone (Sample NB-20). The d-spacing of these peaks correspond to illite.

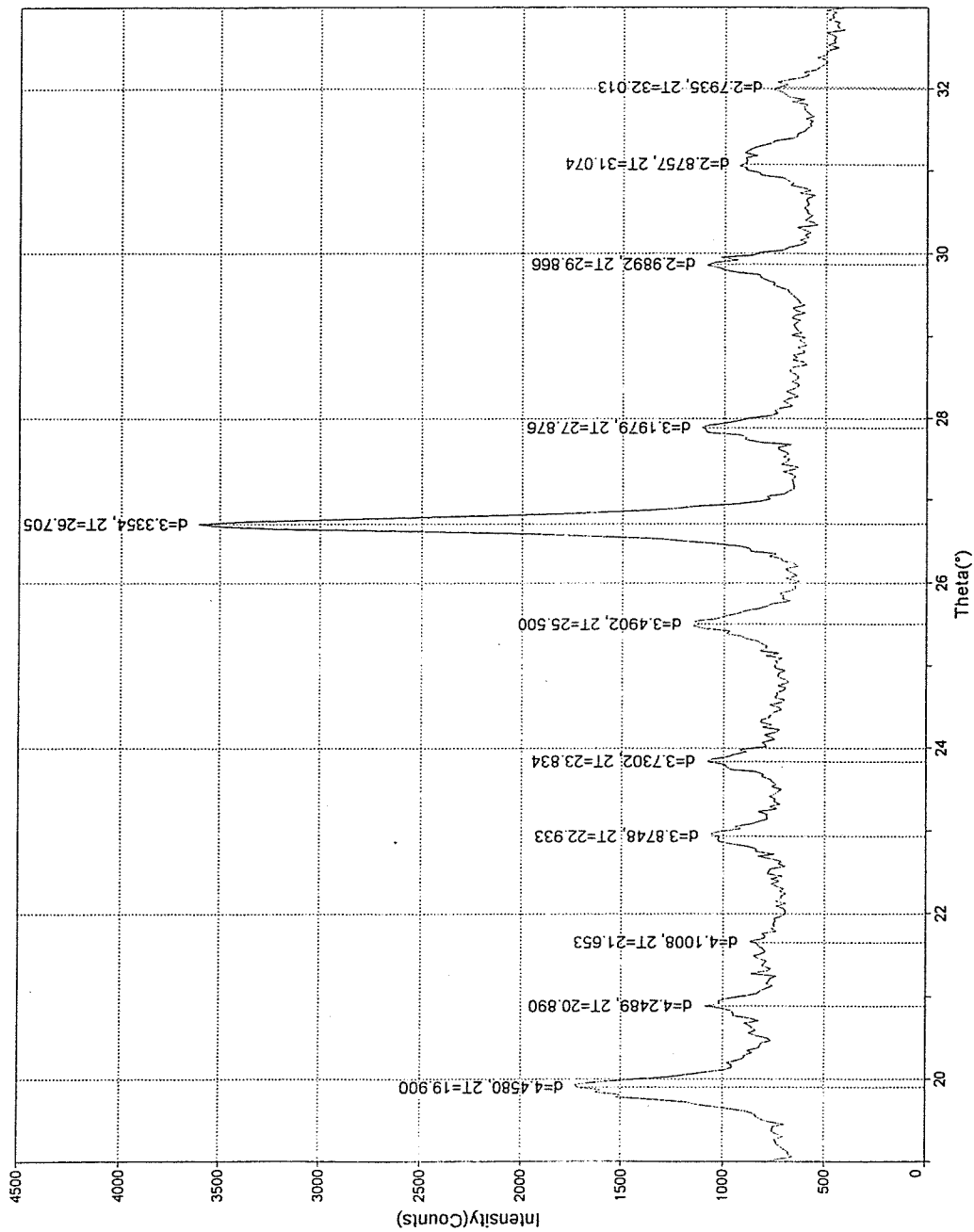


Figure 4.36 Random mount x-ray diffraction pattern for the clay fraction separated from a gold-rich ore zone (Sample NB-20). The d-spacing of these peaks correspond to the illite 2M<sub>1</sub> polytype.

Sample	FWHM	Decalcification intensity in %	Argillization intensity in %	Silicification intensity in %	Fe-oxide content in %
NB-19	0.326	100	30	20	
NB-20	0.341	100	30	0	0.3
NB-57	0.355	40	30	0	0
NB-58	0.334	20	30	0	0
NB-59	0.357	100	30	0	0.05
NB-60	0.345	100	30	0	0.3
NB-62	0.289	100	20	10	0
NB-63	0.370	50	20	0	0.1
NB-65	0.305	100	30	0	1
NB-66	0.262	80	30	0	1
NB-67	0.380	100	20	0	0.3
NB-68	0.241	100	20	0	0.1
NB-69	0.298	60	25	0	0.3
NB-70	0.198	0	5	0	0
NB-73	0.248	50	20	0	0.05
NB-74	0.418	80	30	0	0
NB-75	0.210	0	15	0	0

Table 4.6 Kubler index of first order illite peaks from x-ray diffraction patterns of all samples. The various alteration intensities are given. Note that the lowest FWHM value occurs in the decalcified samples where alteration is absent.



## CHAPTER 5

### DISCUSSION

#### Pressure Estimation

The trapping pressures of inclusions ( $P_t$ ) are estimated several ways. Pressure can be estimated from geologic information about the burial depths assuming hydrostatic or lithostatic pressure. Pressure is estimated from isochores when  $T_t$  is known. Isochores are calculated using MACFLINCOR, inputting  $T_m$  and  $T_h$  data, and gas analyses (Brown et al., 1995). However, MACFLINCOR does not allow input of all gaseous species measured by the quadrupole mass spectrometer, hence pressure estimates made with MACFLINCOR are low. The minimum  $P_t$  is most correctly estimated from the gas analyses,  $T_h$ , and salinity data. The assumption is that  $P_t$  is the sum of all the volatile inclusion species partial pressures calculated at  $T_t$  (calculated pressures are in Appendix G; the formulae for Henry's Law constants is in Appendix H):

$$P_t = P_{H_2O} + P_{CO_2} + P_{CH_4} + P_{N_2} + \dots$$

#### *Stage 1*

This calcite is unusual in that it hosts clathrate that melts as high as 23.3°C. This is used to estimate a minimum  $P_t$ . Clathrate is stable above 0°C provided a confining pressure exists because methane enters the ice "cage" and holds the ice structure together above normal melting temperatures of ice. Graphs from Katz et al. (1959) show that a

pure methane clathrate can exist at 23.3°C provided the pressure exceeds 5000 psi or 360 bar (equivalent to a lithostatic load of 1.3 km).

Using the sum of the partial pressures at  $T_h$  gives a total pressure of 1550 bars, equivalent to ~6 km depth if lithostatic conditions are assumed. Since boiling did not occur, 1550 bars is taken as a minimum pressure.

An alternative approach to estimating pressure is by geothermal gradient difference. Stage 1  $T_h$ 's are approximately 125°C above ambient conditions. If a geothermal gradient of 25°C/km is assumed, then rock temperatures of 150°C is reached at 5 km depth.

#### *Stage 2 white calcite*

Constraints on the pressure-temperature conditions for stage 2 calcite veins are complicated by fluid inclusion decrepitation. However, a measured maximum decrepitation temperature of 276°C places a lower bound on  $T_h$ . Isochores calculated using MACFLINCOR suggests a minimum  $P_t$  between 1200 and 1450 bars assuming  $P_t \geq 276^\circ\text{C}$  (see Fig. 5.1). This pressure corresponds to a lithostatic load of about 5 km.

#### *Stage 3 sericite-quartz-calcite*

The presence of Type 2 inclusions indicates fluid boiling, however there are no Type 1 inclusions with similar  $T_h$  values. Rather, a 100°C difference in the homogenization temperatures is measured between Type 1 and Type 2 fluid inclusions. Fluid inclusion observations and gas analysis indicate there is a range in  $\text{CO}_2/\text{H}_2\text{O}$  ratios in stage 3 Type 1 inclusions hosted in quartz. Fluid boiling occurs when  $P_{\text{H}_2\text{O}} + P_{\text{CO}_2} + P_{\text{CH}_4} + \dots$  exceed the

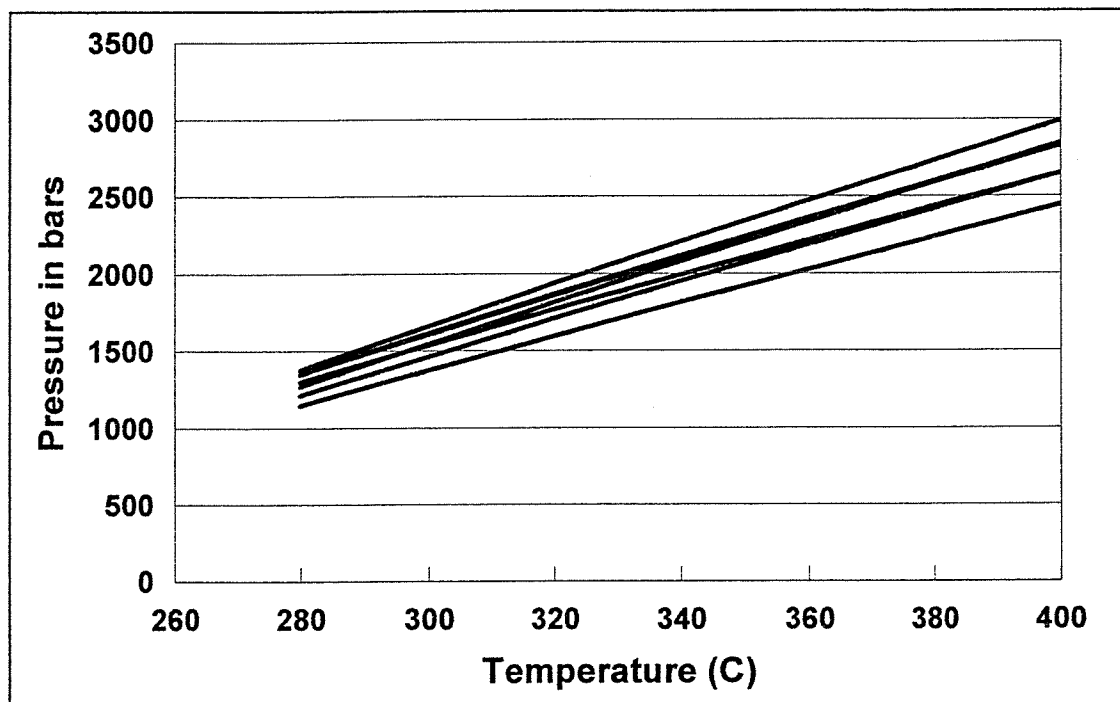


Figure 5.1 Isochore plot for stage 2 white calcite.

confining pressure ( $P_c$ ). Assuming a near constant  $P_t$  and  $T_t$ , boiling would occur when fluids were most charged with gaseous species. During times of low gas contents, fluid pressures would be  $<P_c$ , and  $T_h$  measurements will yield a temperature  $<T_t$ . Another possibility is that Type 2 inclusions reflect injection of a  $CO_2$ -dominated vapor into ore fluid. Some but not all of the  $CO_2$  dissolved in the ore fluids as the low density vapor phase moved quickly upward through the ore solution. To test the idea that Type 1 and Type 2 inclusions were trapped under similar P-T conditions, assume that Type 2 inclusions were trapped under boiling conditions when 2 phases, liquid and vapor were present, hence  $T_h = T_t$ . Hence,  $P_t$  and  $T_t$  can be estimated by the crossing isochore method when fluids of differing composition were trapped under similar P-T conditions. The similarity of Type 2 inclusion  $T_h$  values, and their occurrence together along fractures indicates Type 2 fluids existed during Pipeline mineralization, and are not a product of post-mineralization changes in fluid inclusions. Type 2 inclusions are not the product of pinching off. They show similar  $T_h$  values and all homogenize to vapor that does not agree with pinching off. Type 2 inclusions occur in all sections examined, and occur in clusters. Type 2 inclusion presence therefore suggests that for a short time during Pipeline mineralization,  $CO_2$  increased sufficiently to induce phase separation of a carbonic phase.

Gas-corrected isochores are calculated for stage 3 vein and ore quartz geothermometry data and the results are presented in Appendix G. Type 2 fluid inclusions have calculated homogenization pressures of 1910 to 2423 bar; most data points occur around 305°C and about 2000 bar pressure (Fig. 5.2). Assuming Type 2 inclusions were trapped during phase-separation conditions,  $T_h = T_t$ , and  $P_t$  can be calculated from either isochore calculation, or by the partial pressure method. MACFLINCOR calculations show Type 2

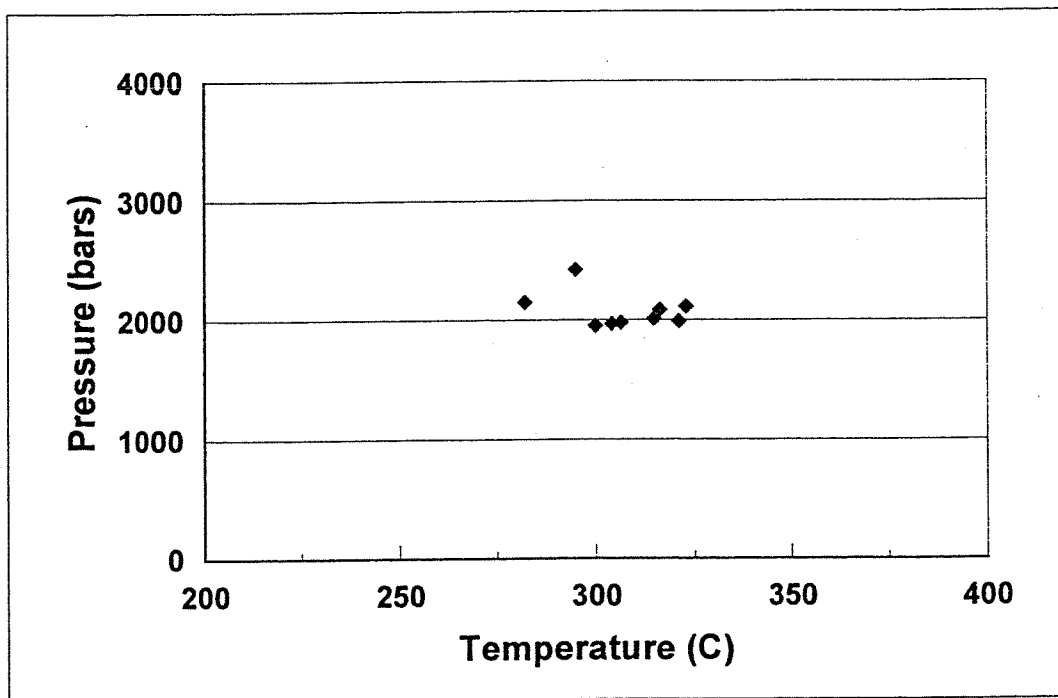


Figure 5.2 Homogenization conditions for all Type 2 inclusions hosted in quartz. Note that there is a general clustering of points in the temperature range 290° to 323°C and pressure range 1900 to 2200 bars.

inclusions comprise of about 0.71 to 0.75 mole fraction  $\text{CO}_2$ . Gas-corrected isochores of Type 1 inclusions intersect the zone defined by the Type 2 inclusions (Fig. 5.3). Hence, it shows that the assumption that Type 1 and Type 2 inclusions were trapped under similar P-T conditions is permissible. It follows then that  $T_h$  measured for most Type 1 inclusions are considerably less than  $T_t$ .

Stage 3 calcite gas-corrected isochores were calculated in order to show if calcite was formed under similar P-T conditions as quartz. Stage 3 calcite isochores do not intersect stage 3 vein and ore quartz gas-corrected isochores. For any given temperature,  $P_{t_{\text{calcite}}}$  is less than  $P_{t_{\text{qtz}}}$  (Fig. 5.4). The diagram shows a calcite  $P_t = \sim 1200$  bars if stage 3 calcite  $T_t$  was  $300^\circ\text{C}$ , the stage 3 quartz Type 2  $T_h$  values.

#### *Stage 5 calcite*

Stage 5 calcite pressure estimates are poorly constrained. The open-space filling and presence of calcareous sediment suggest that calcite was deposited under hydrostatic conditions. A depth of a few 100 m is possible for stage 5 calcite.

### **Fluid Inclusions**

#### *Stage 1 dark calcite*

Two fluid inclusion populations are hosted within the dark calcite veins. Microthermometry shows one population whose  $T_m$  is slightly below  $0^\circ\text{C}$  whereas a second population exhibits clathrate melting behavior above  $0^\circ\text{C}$ , indicating hydrocarbon species. The highest reported fluid inclusion clathrate melting temperature for a methane-

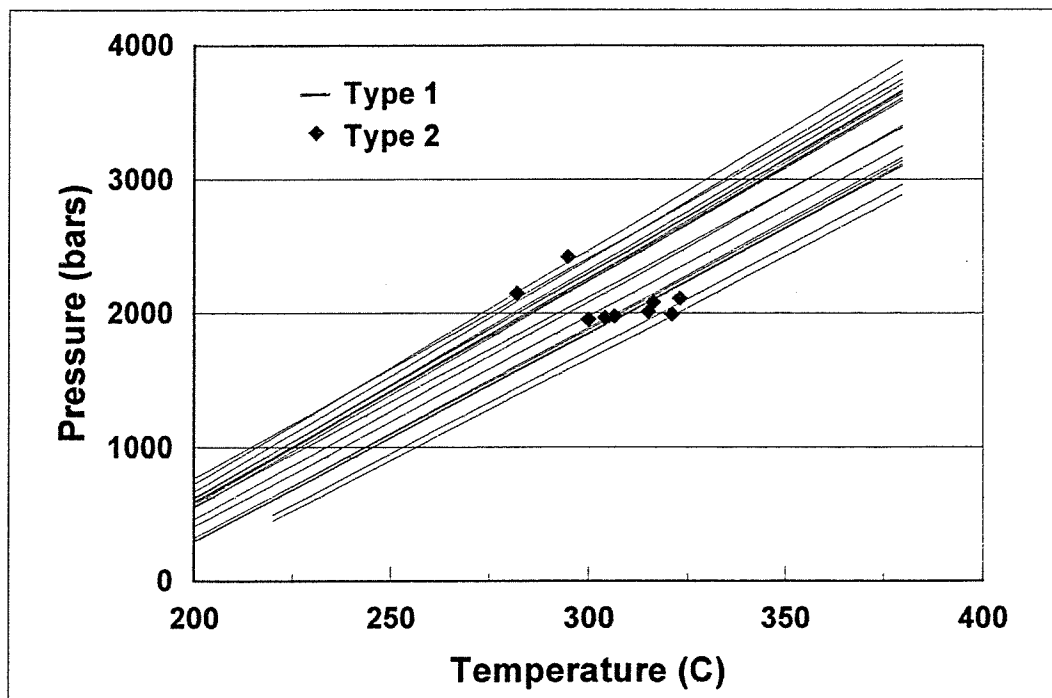


Figure 5.3 Comparison between stage 3 Type 1 isochores from sample NB-47 and all Type 2 inclusions showing that the Type 1 isochores intersect the zone in which Type 2 inclusions trapped.

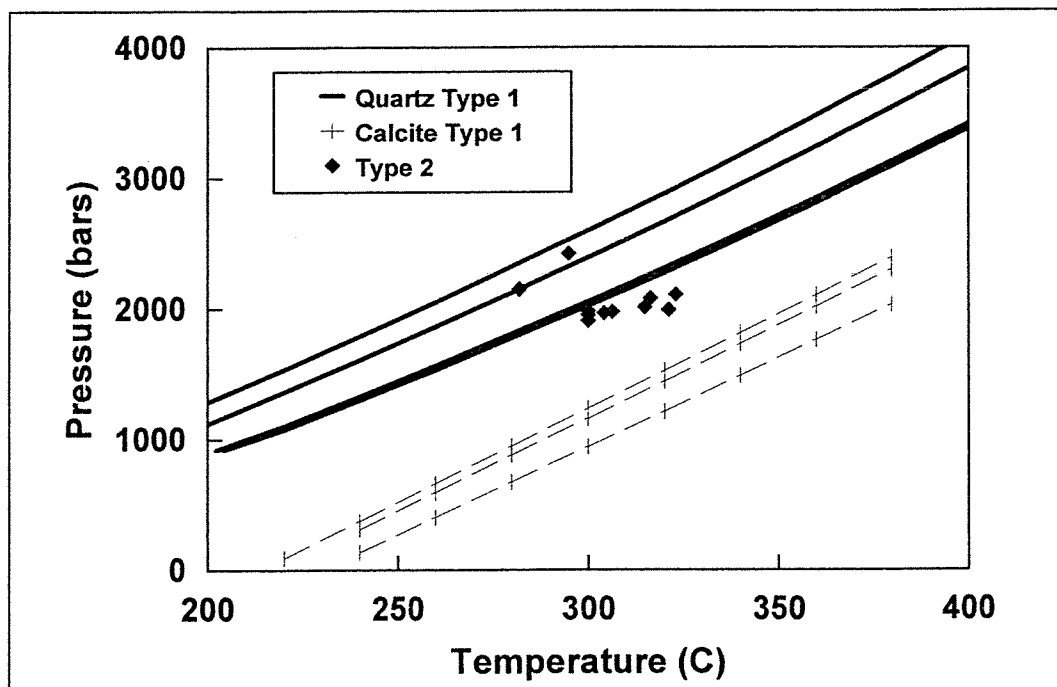


Figure 5.4 Isochore plot comparison between stage 3 quartz and calcite for the same sample, both have been corrected for the partial pressure of dissolved gases. For any given temperature, the pressure within the calcite inclusions is considerably lower.



bearing gas hydrate is 17°C (Yonaka, 1996) whereas my measurements are as high as 23.3°C. Gas analysis shows two populations of inclusions, one is methane-poor with  $\text{CO}_2/\text{CH}_4 > 2$  whereas the other population is methane-rich with  $\text{CO}_2/\text{CH}_4 < 2$  (Appendix C). It makes sense to correlate the methane-bearing clathrate inclusions identified by microthermometry with the methane-rich population recognized in the gas analysis data. Non-clathrate inclusions are correlated with the low  $\text{CH}_4$  gas population. The  $\text{N}_2/\text{Ar}$  vs.  $\text{CO}_2/\text{CH}_4$  plot (Fig. 4.20) shows a meteoric component. Inclusion volatiles with high  $\text{N}_2/\text{Ar}$  ratios and low  $\text{CO}_2/\text{CH}_4$  ratios explained by the breakdown of proteins to produce both  $\text{CH}_4$  and  $\text{N}_2$  (Norman et al., 1999) but these generally plot in the organic field. It is possible that  $\text{N}_2/\text{Ar}$  were higher in Early Mesozoic times when these inclusions were trapped. The  $\text{N}_2/\text{Ar}$  ratio of most inclusions based on present day  $\text{N}_2/\text{Ar}$  suggest a magmatic component to the fluids. But, the data could equally well represent a hyperbolic mixing curve between a  $\text{CH}_4\text{-N}_2$  rich pore fluid and a shallow meteoric water.

Calcite has reverse solubility, but is also deposited from hydrothermal solutions by boiling and loss of dissolved  $\text{CO}_2$  (Heinrich et al., 1989; Simmons, 1999). There is no evidence of boiling, therefore the best explanation is that calcite deposition is a consequence of heating. The most plausible explanation is that deposition of calcite resulted from downward penetrating cool groundwaters, however, saturation of vein fluids with calcite by addition of magmatic  $\text{CO}_2$  cannot be ruled out.

The lower  $\text{N}_2/\text{Ar}$  ratios in some inclusions agree with this interpretation. The hydrocarbon-rich aqueous and dark hydrocarbon-bearing inclusions are best explained as admixed pore hydrocarbon-rich fluids from the SRM. The Th of 145°C is above the maturation temperature of petroleum and well into the natural gas temperature window.

The suggestion of protein breakdown from gas data agrees with rising temperature.

A fracturing event allows downward flow of shallow ground water through the limestones and siltstones of the SRM. Cross cutting relationships and deformation of dark calcite veins indicate fracturing occurred before the Antler orogeny. From the estimated  $T_t$ , a minimum depth of this event is estimated at ~5 km assuming a geothermal gradient of 25°C/km and 25°C surface temperature.

### *Stage 2 white calcite*

Similar  $Th_{CO_2}$ , salinity and phase volume ratios for stage 2 inclusions indicate calcite deposition by a fluid with a chemistry remaining constant over time. Homogenization temperatures were not obtained for stage 2 calcite, but the highest measured decrepitation temperature of 276°C is a possible lower constraint on  $Th$ . However, calcite deforms easily, hence there is a possibility that stretching occurred in these high-pressured inclusions during measurement thus increasing  $Th$  values. Above 300°C, equal volumes of  $CO_2$  and  $H_2O$  are completely miscible in low salinity fluids (Bowers and Helgeson, 1983). The homogeneous nature of inclusions suggests that the chemistry is a miscible mixture of  $CO_2$  and  $H_2O$  controlled by equilibrium between fluids and wall rock, which suggests a temperature >300°C. The high density of the  $CO_2$  phase in these inclusions confirms that the stage 3 calcite developed under relatively high pressures. If calcite decrepitated before significant stretching occurs, isochores for the white calcite give a pressure of about 1.3 kbar at 276°C. Since  $Th$  is higher than the decrepitation temperature and most likely above 300°C, 1.5 kbar is taken to be a realistic minimum pressure. Therefore, a minimum lithostatic pressure corresponding to about

6 km depth existed during precipitation of the calcite. Data from the stage 3 mineralization gives a pressure of about 1.9 to 2.2 kbar, therefore, if this pressure is the load of upper plate rocks, then the isochore can be used to constrain temperature. By applying 1.9 to 2.2 kbar pressure to the isochore of white calcite, a corresponding trapping temperature of 320° to 340°C is determined.

The CO<sub>2</sub>/CH<sub>4</sub> vs. N<sub>2</sub>/Ar discrimination diagram (Fig. 4.20) shows the white calcite has a meteoric gas signature of a separated gas phase (Norman and Moore, 1997). It could well be that ground water N<sub>2</sub>/Ar ratios differed from the 32-54 ratio recorded today. This is consistent with the average fluid salinity of <1 eq. wt. % NaCl, of which a portion is dissolved CO<sub>2</sub>. There is no evidence to support fluid boiling, hence deposition of calcite is considered in response to an increase in fluid temperatures.

#### *Stage 3 quartz-sericite-calcite*

The data and isochore calculations indicate that Type 1 and Type 2 inclusions were derived from a fluid of variable CO<sub>2</sub> content and salinity at approximately 300°C and 2 kb. The range in observed Th values can be explained with the aid of Figure 5.6 that shows phase relationships in the CO<sub>2</sub>-NaCl-H<sub>2</sub>O system calculated for a salinity of 8 eq. wt. % NaCl. Figure 5.5 shows that phase separation (boiling) occurs at 300°C in fluids that have CO<sub>2</sub> >12 mol. %. Further it shows that inclusions trapped with less than 12 mol. % CO<sub>2</sub> will show a range in Th that will be proportional to amount of CO<sub>2</sub>. The gas analyses show aqueous inclusion CO<sub>2</sub> ranging up to 11.5 mol. % and Type 2 inclusions with about 89 mol. % CO<sub>2</sub>. Clathrate melting observations agree with a variable CO<sub>2</sub> content of inclusions. Hence, the data are consistent with a mineralizing fluid with

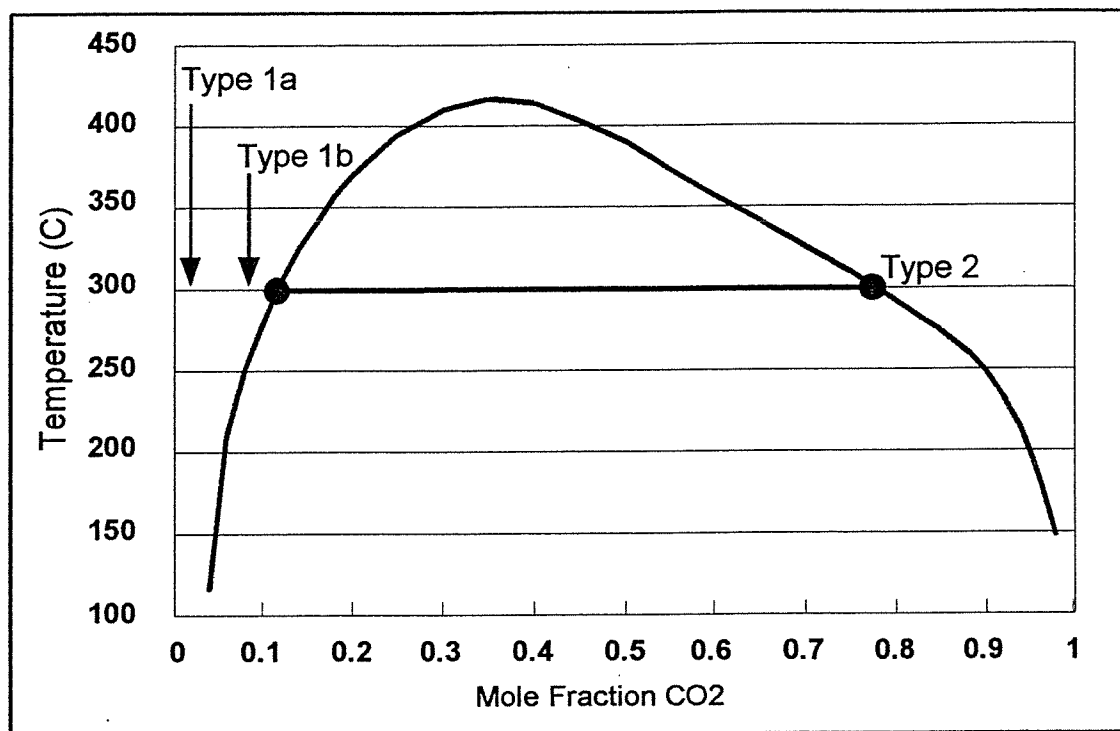


Figure 5.5 Immiscibility curve for brine (8 eq. wt. % NaCl) and CO<sub>2</sub> at 2000 bar. Type 1a inclusion CO<sub>2</sub> content is low and this group plots on the left of the diagram. Type 1b has more CO<sub>2</sub> and plots close to the solvus curve. Type 2 inclusion CO<sub>2</sub> content is high and this group plot on the right.

variable CO<sub>2</sub> content that boiled on rare occasions that resulted in trapping Type 2 inclusion fluids. As mentioned before, this may be the result of fluids with >12 mol. % CO<sub>2</sub> or admixing a CO<sub>2</sub>-rich vapor. The reason no Type 1 inclusions with Th ~300°C were measured could be due to chance, preferential trapping of Type 2 inclusion fluids, or that Type 1 inclusions trapped during boiling events were smaller in size, and hence overlooked.

Kuehn and Rose (1995) report CO<sub>2</sub>-vapor-filled inclusions in Carlin mineralization, similar to the Type 2, and they postulate that these CO<sub>2</sub>-rich inclusions are the result of a throttle-controlled change from lithostatic to hydrostatic pressures. I observed Type 2 inclusions in quartz veins several tens of meters below the ore zone and observed no increase in abundance of Type 2 inclusions in mineralized gold-bearing ore quartz, which follows from Kuehn and Rose's model. The data suggests that Pt does not change during quartz deposition. A pressure of about 2 kb can only be lithostatic for a hydrostatic pressure of 2 kb would require an unreasonable depth of mineralization. Hence, lithostatic or near lithostatic conditions prevailed during quartz deposition and silicification, which implies lithostatic conditions exist during gold mineralization.

The distribution of Th values can be explained by examination of a CO<sub>2</sub>-NaCl-H<sub>2</sub>O phase diagram (Fig. 5.6). The behavior of a Type 1 inclusions below Tt depends on the CO<sub>2</sub> content and is predictable. At Tt the inclusion pressure is Pt but as the inclusion cools, an inclusion with little CO<sub>2</sub> will follow P-T conditions corresponding to an isochore until the aqueous phase contracts sufficiently to develop a vapor bubble. Inclusions with more than about 3 mol. % CO<sub>2</sub>, which gas analysis indicates is most Type 1 inclusions and trapped at 300°C, will initially cool along a line defined by the isochore until the solvus is

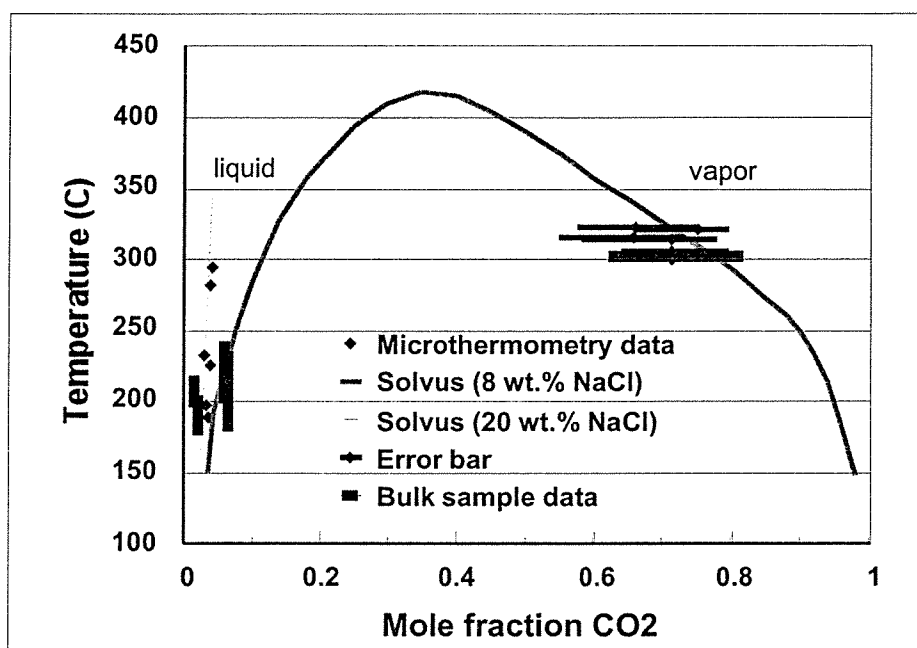


Figure 5.6 Plot of Th and CO<sub>2</sub> mole fraction determined from microthermometry for Type 1 (solid diamonds) and Type 2 (showing error bars). For bulk samples the Th range and gas analysis data is used to constrain a solid box to show the range for individual samples. Superimposed is the CO<sub>2</sub>-H<sub>2</sub>O-NaCl solvus curve calculated for 8 eq. wt. % NaCl (Bowers and Helgeson, 1985) and part of the solvus curve for 20 eq. wt. % NaCl (Takenouchi and Kennedy, 1965).

intersected. Thus, a spread of Th will reflect the CO<sub>2</sub> content and not necessarily Tt.

Plotting stage 3 data on a CO<sub>2</sub>-NaCl-H<sub>2</sub>O P-T solvus diagram shows that the distribution of Th measurements obtained is consistent with trapping temperatures of ~300°C and trapping pressures of ~2 kbar. Curves are plotted for the CO<sub>2</sub>-H<sub>2</sub>O-NaCl system at 8 eq. wt. % NaCl (Bowers and Helgeson, 1985) and 20 eq. wt. % NaCl (Takenouchi and Kennedy, 1965). Other gaseous species are ignored due to the lack of equations of state. Type 2 fluid inclusions cluster on the vapor side of the solvus curve indicating they represent a trapped vapor phase, as might be expected by boiling a fluid. Corresponding Type 1 inclusions with ~10 mol. % CO<sub>2</sub> were not observed on the left side of the solvus curve but are predicted. A plausible explanation is the “wetting” effect of non-aqueous phases causing more Type 2 inclusions to be trapped than Type 1. It follows that more observations might increase the chances of observing Type 1 inclusion whose composition plots to the solvus curve at 300°C. Alternatively, the solvus curve is affected by change of salinity, presence of other gases and change of pressure.

Quartz gas analysis data give N<sub>2</sub>/Ar ratios >500, indicating magmatic fluids (Fig. 4.21). The data supports a magmatic fluid source for Carlin-type deposits, originally proposed by Sillitoe and Bonham (1990).

Calcite isochores and calcite inclusion gas analyses are compatible with calcite mineralization occurring under different pressures than quartz. The calcite isochores do not intersect the P-T conditions measured for the stage 3 Type 2 inclusions, nor do they intersect stage 3 quartz Type 1 inclusion isochores. Therefore, deposition under lower pressures than prevalent during quartz mineralization is indicated, assuming Tt was the same or less. Gas analysis shows stage 3 calcite depositing fluids contain a shallow

meteoric component mixed with a magmatic fluid (Fig. 4.21). Entering stage 3 veins during lithostatic conditions is impossible for meteoric fluids because lithostatic pressures imply there are no fluid conduits to the water table. However, it is possible for meteoric fluids to migrate downwards into the deposit under less than lithostatic pressure. Meteoric fluids are expected to be saturated with calcite from contact with carbonate sediments. Deposition of calcite is explained by heating, as meteoric fluids descended, due to its reverse solubility. Veins with similar mineralogy are known to occur in other Carlin-type deposits (J. Cline, pers. comm.; Kuehn and Rose, 1995).

#### *Stage 5 calcite*

Stage 5 calcite has  $N_2/Ar$  ratios that are consistent with air saturated water ratios. Approximately equal  $CO_2/CH_4$  ratios are lower than meteoric waters and plots on a  $N_2/Ar$ - $CO_2/CH_4$  discrimination diagram in the evolved field. The increase in abundance of stage 5 calcite peripheral to the deposit suggests that a thermal source is responsible for circulating ground water during stage 5.

### **Clay Minerals**

The dominance of illite in rocks that display ore mineralization is attributed to hydrothermal alteration. This is supported by the correlation between illite peak FWHM and degree of alteration in comparison to unmineralized SRM. The dominance of the  $2M_1$  illite polytype also confirm mineralizing temperatures of 200° to 370°C (Lonker and Fitz Gerald, 1990; Weaver and Boekstra, 1984; and Yoder and Eugster, 1955).



Disappearance of kaolinite suggests that some illite formed at the expense of kaolinite. The indicated intergrown sericite and quartz suggests that illite in the most intensely mineralized area is of hydrothermal origin. Presence of illite inherited from SRM cannot be ruled out, however, the relationship between FWHM and alteration suggests that illite crystals grew during ore mineralization.

The presence of both illite and kaolinite in the fault gouges is attributable to incorporation of clay minerals from lithologies flanking the faults. Reaction of clay minerals to a hydrothermal fluid is ruled out because this would require an acid pH that is hard to explain in carbonate-rich terrain. Downward percolating waters along the fault that could alter illite to kaolinite is possible.

Based on electron microprobe images of stage 3 sericite, the material analyzed shows varying  $\text{SiO}_2$  content whereas the K/Al ratio remains relatively constant. The electron microprobe has the ability to resolve crystals greater than 3  $\mu\text{m}$ . However, the variability of  $\text{SiO}_2$  in the microprobe data (Table 4.5) is consistent with sericite and quartz intergrown on a micron or sub-micron scale. If the sericite comprised a mixed-layer clay or if a second discrete clay occurred, differences in the K/Al ratio would be expected. This is not true as only  $\text{SiO}_2$  varies. A plausible explanation is that fine-grained quartz occurs intergrown with the sericite.

## **Argon Geochronology**

### *Igneous rocks*

Argon ages obtained from minerals derived from intrusive rocks generally record

the time that the mineral closes to radiogenic argon loss. For biotites from relatively rapidly cooled rocks, the closure temperature is  $\sim 350^{\circ}\text{C}$  (Harrison et al., 1985).

K-feldspars commonly contain variable diffusion length scales (domains) due to their complex microstructures and thus have variable argon closure temperatures. The diffusion domains generally have closure temperatures that range from  $\sim 175^{\circ}$  to  $300^{\circ}\text{C}$  (Lovera et al., 1989). Sample 93271 biotite and K-feldspar yield analytically indistinguishable plateau ages, whereas there is a measurable discordance of  $\sim 0.8$  to  $1.5$  Ma for mineral pairs from Cortez dikes and JM-fine (Appendix F). Also, the JM-fine biotite plateau of  $36.28 \pm 0.12$  Ma is older than the essentially identical biotite ages from the other two Eocene dike samples. All three Eocene dike K-feldspars yield statistically different plateau ages, and the youngest K-feldspar comes from the Mill Canyon Eocene dike (JM-fine) and gives the oldest biotite age (Appendix F). The age discordance between mineral pairs and between similar minerals from different Eocene dike samples are linked to variations in closure temperatures and/or actual age differences of the samples. However, there is no simple cooling or intrusive history that explains all the age results from these samples. For instance, if the  $1.5$  Ma age discordance between biotite and K-feldspar from JM-fine is related to overall cooling from  $\sim 350^{\circ}$  to  $200^{\circ}\text{C}$  between  $36.2$  and  $34.7$  Ma, why does 93271 (South trench dike) yield concordant mineral ages? Additionally, if these rocks are emplaced at depths between  $\sim 1$  to  $2$  km, how can protracted cooling be explained? Answers could lie in the accuracy of the mineral ages or within the geological/thermal history. It is often observed that biotites yield ages older than coexisting sanidines from ash-flow tuffs and that the sanidines provide the most accurate age estimate. Perhaps the apparent discordance between the biotite and K-feldspar pairs for these samples is

attributed to inaccuracies in the biotite ages, thus making the K-feldspars the most reliable mineral for estimating the dike ages. Using the K-feldspar plateau ages indicates that the dikes were emplaced between 35.7 to 34.7 Ma. Alternatively, if the biotite ages are correct, the dike emplacement ages may be ~36.3 Ma and the K-feldspar ages represent cooling and/or partial resetting associated with post emplacement reheating associated with multiple heating events. The age of these Eocene rocks cannot be more precise, however, all results indicate that these rocks were intruded between 34.5 to 36.2 Ma.

The Mill Canyon stock (JM-coarse) sample has a biotite apparent age of  $152.24 \pm 0.33$  Ma. This age is interpreted to be the time of cooling through  $\sim 350^\circ\text{C}$  and suggests that it is derived from a Jurassic pluton. The K-feldspar has a much more complex age spectrum, but can be understood in terms of post-emplacement argon loss. The initial excess argon observed in the first few percent of argon released obscures the age of final argon loss, however, ages get as young as  $\sim 50$  Ma. Because this sample is spatially associated with JM-fine, an Eocene dike, it is suggested that the last time for argon loss from JM-coarse K-feldspar was  $\sim 35$  Ma.

During step-heating of K-feldspars for the generation of the age spectrum, diffusion coefficients are calculated based on the duration of the heating steps and the amount of released  $^{39}\text{Ar}$  (e.g., McDougall and Harrison, 1988). The diffusion coefficients are plotted on an Arrhenius diagram from which the argon kinetic parameters (activation energy, frequency factor) are obtained. These kinetic parameters are then used to model the argon retentivity of each diffusion domain and combined with the age spectrum to obtain a quantitative thermal history for the sample (Lovera et al., 1989). The thermal history is obtained by forward modeling the age spectrum, that is, by trial and error,

thermal histories are imposed upon the kinetic parameters until a calculated age spectrum matches that of the measured age spectrum. Results of multiple diffusion domain modeling conducted on JM-coarse K-feldspar are shown in Figure 5.7. The first models assume the pluton cooled quickly in the Jurassic and the K-feldspar only lost argon at ca. 35 Ma (Fig. 5.7). The calculated age spectra show that reconciling the measured age gradient between ca. 100 to 150 Ma is not possible without too much argon loss during the initial part of the spectrum. This suggests that the thermal history that produced the measured age gradient is more complex than this model.

Considering that many gold deposits in Nevada are associated with Cretaceous magmatic systems (e.g., Groff et al., 1997) thermal models incorporating reheating at ca. 100 Ma were tried. After numerous iterations, a good fit between the measured and modeled age spectra was obtained by using two short duration thermal events, one at ca. 110 and ca. 35 Ma (Fig. 5.8). The 110-Ma event serves to produce the age gradient from about 110 to 150 Ma, while the younger event causes the argon loss measured over the initial 10% of the spectrum. It is emphasized that other thermal models can also produce the measured spectrum. For instance, slow cooling throughout the Early Cretaceous could cause argon loss similar to a discrete event at 110 Ma. Also, the late Cretaceous ages may be related to argon loss associated with cooling during this time rather than an Eocene thermal event. Thus, the calculated models require some geological insight toward presenting a geologically relevant thermal history.

An Eocene event causing argon loss from the Mill Canyon stock K-feldspar is entirely plausible due to the spatial association with the Eocene JM-fine sample. The

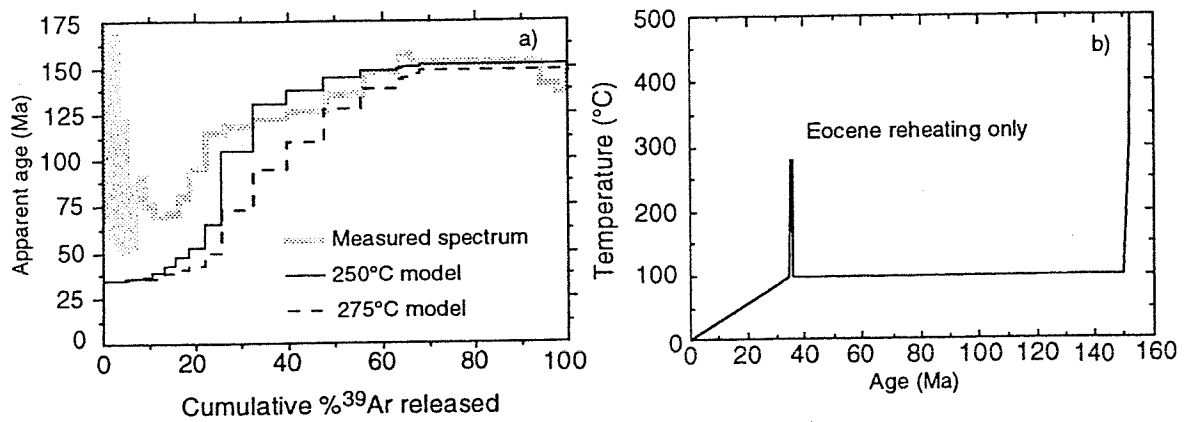


Figure 5.7 (a) Model and measured age spectra for JM-coarse K-feldspar, (b) thermal history. The poor fit between the measured and modeled spectra suggests a more complex thermal history is required to explain the age data.

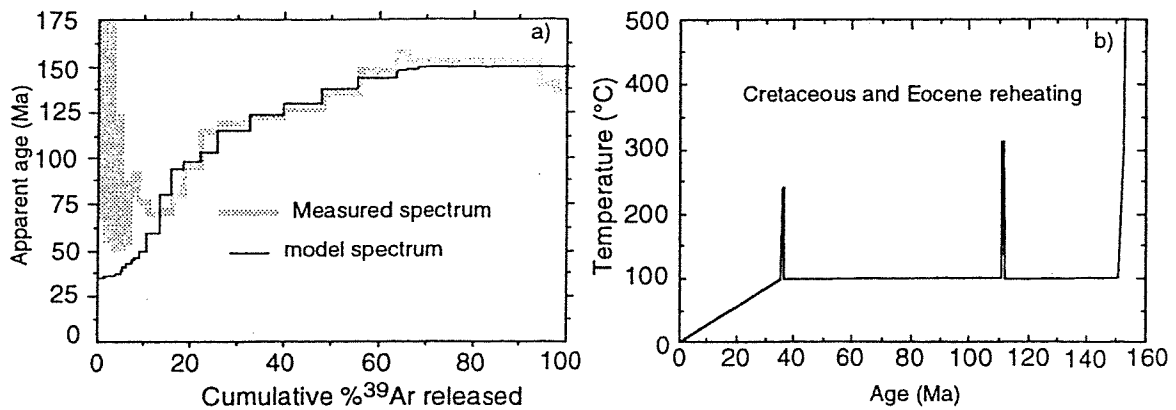


Figure 5.8 (a) Model and measured age spectra for JM-coarse K-feldspar, (b) thermal history. Using both Cretaceous and Eocene reheating events produces a calculated age spectrum which closely matches the measured spectrum.

Cretaceous event is more speculative which leads onto the discussion of the illite/sericite data.

### *Clay and sericite*

Despite the overall complexity of the illite and sericite spectra, recorded ages for large segments of the spectra are typically 90 to 110 Ma (Fig. 4.33). The old apparent ages observed in the high-temperature heating steps are interpreted to be related to incomplete degassing of inherited clay grains. Based on the age spectra alone, it is not possible to ascertain if the ca. 100 Ma ages are associated with new clay growth or if the detrital clays are heated sufficiently to cause nearly complete argon loss. However, mineral stability fields of illite and kaolinite, based on the  $K^+/H^+$  ratio, show that the fluids associated with the stage 3 veins and ore mineralization are more than capable of reacting with kaolinite to create fresh illite.

Dating of clay minerals from Carlin-type deposits have been largely unsuccessful (Arehart et al., 1993a; Folger et al., 1996). The Eocene hydrothermal event is regarded as an important gold epoch in Nevada (Teal and Jackson, 1997), and dating of adularia has provided convincing evidence for Eocene mineralization. However, in some deposits clay minerals are the only K-bearing minerals that can be used for dating by the  $^{40}\text{Ar}/^{39}\text{Ar}$  method. Two factors can lead to anomalously old  $^{40}\text{Ar}/^{39}\text{Ar}$  when analyzing clay. Inherited argon from nondegassed clay is observed in some age spectra. Second, clay minerals are very fine-grained, and variably crystalline, making recoil during irradiation a serious consideration. Retention of  $^{39}\text{Ar}$  in clay minerals is dependent upon the degree of crystallinity (Dong et al., 1995) with progressive  $^{39}\text{Ar}$  loss occurring in poorly crystalline

materials.

At Jerritt Canyon,  $^{40}\text{Ar}/^{39}\text{Ar}$  dating of diagenetic mica from altered and unaltered samples was unsuccessful in recording younger hydrothermal resetting events (Folger et al., 1996). The authors argue that the failure to measure younger apparent ages is because the hydrothermal temperatures were too low ( $120^\circ\text{-}260^\circ\text{C}$ ) or the duration of the heating interval too short to reset the isotopic system.

For stage 3 sericite (NB-102), inherited argon is not a problem due to its known hydrothermal origin at  $\sim 300^\circ\text{C}$ . Similarly, the hydrothermal origin of the sericite suggests that the material dated is well-crystallized and coarse-grained enough for recoil loss not to be a concern. Electron microprobe spot analyses show that the sericite has consistent K/Al ratios but that silicon varies (Table 4.5), implying that quartz is intergrown with the sericite. Microprobe data show a fine-grained sericite closely associated with quartz (Fig. 4.32). This being the case,  $^{39}\text{Ar}$  recoil from sericite into quartz explains the age spectrum (Fig. 4.33a). The last 20%  $^{39}\text{Ar}$  released coincides with a decrease in radiogenic yield and the lowest K/Ca ratio. The apparent drop in K/Ca is interpreted to result in differential recoil implantation of  $^{37}\text{Ar}$  and  $^{39}\text{Ar}$  into the intergrown quartz. Since the recoil distance for  $^{39}\text{Ar}_\text{K}$  is about 65% less than for  $^{37}\text{Ar}_\text{Ca}$ , it follows that the K/Ca ratio decreases if recoil occurred into quartz from sericite. Assuming the recoil of  $^{39}\text{Ar}$  out of the sample is negligible, the integrated age for sample NB-102 is the accepted age. In addition, the  $92.0 \pm 0.3$  Ma integrated age is within error of a  $92.8 \pm 1.0$  Ma K-Ar date reported for an alteration event in Gold Acres (Silberman and McKee, 1971). Therefore, the 92.0 Ma age is regarded as geologically meaningful.

The Pipeline illite samples dated give ages suggestive of Cretaceous mineralization.

The age spectra from the coarse- and fine- grained illite from sample NB-20 at Pipeline, are both discordant but have similar ages with many heating steps at ~100 Ma (Fig. 4.33). Sample NB-20 gives a Kubler Index of 0.341 and is regarded as well-crystalline, but according to the results of Dong et al. (1995), loss of  $^{39}\text{Ar}$  by recoil is still a consideration. Dong et al. (1995) provide a formula to calculate the amount of  $^{39}\text{Ar}$  loss due to recoil based on the illite crystallinity (Kubler Index), that being:

$$43.8 * (\Delta 2\theta) - 6.74$$

Applying a Kubler Index (measured as FWHM) of 0.341, the  $^{39}\text{Ar}$  loss is calculated at 8%. This would indicate that the age spectrum could not correspond to an Eocene clay which recoiled  $^{39}\text{Ar}$  to give an Early Cretaceous age. The integrated age of  $100.19 \pm 0.27$  Ma for fine-grained illite from NB-20 when corrected for 8%  $^{39}\text{Ar}$  recoil loss, yields an integrated age of ~92 Ma. This recalculated age is very similar to the integrated age from stage 3 hydrothermal vein sericite. Sample NB-19 has a FWHM of 0.362 which corresponds to 9%  $^{39}\text{Ar}$  recoil loss. The integrated age of this sample is 137.54 Ma which suggests that inherited argon could be a factor. Older ages (~300 Ma) at Jerritt Canyon are attributed to temperatures of 120°-260°C (Arehart et al., 1995) under which resetting failed to occur. However, hydrothermal temperatures at Pipeline were 300°-320°C. I attribute the ~50°C higher temperatures at Pipeline to be the reason for partial resetting of argon systematics in illite.

### *Summary*

The thermal history of the area is summarized as follows. Intrusion of the Mill Canyon stock occurred during the Jurassic and cooled to 350°C by  $152.2 \pm 0.3$  Ma. The



Gold Acres stock is probably part of the same intrusive body, but has been spatially separated by faulting that predates the Early Cretaceous vein set. Hydrothermal activity during the Early Cretaceous caused alteration in the Gold Acres deposit and the same fluids developed sericite-quartz-calcite veins in the Pipeline feeder zones along with alteration and mineralization in the Pipeline deposit. During the Eocene, extension allowed dikes to intrude the crust, provide heat and partially reset the K-feldspars within the Mill Canyon stock. Fluids penetrating existing faults caused partial resetting or growth of illite hosted in fault gouges. The Eocene event is significant elsewhere in Nevada (Groff et al., 1997; C. Henry, pers. comm.; J. Cline, pers. comm.; J. Muntean, pers. comm.; Hofstra et al., 1999), however, there is no evidence linking gold mineralization to a thermal event during the Eocene at Pipeline.

### Timing of Gold Mineralization

Despite the lack of adularia for  $^{40}\text{Ar}/^{39}\text{Ar}$  dating purposes, constraints can be put on the timing of gold mineralization. First, hydrothermal sericite dated at 92.0 Ma is paragenetically part of the quartz calcite veins that have pyrite-bearing and gold-bearing sidewalls. Fluid inclusion data from this vein set strongly supports more than two orders of magnitude reduction in  $\text{H}_2\text{S}$ , the key compound for gold transportation as a bisulfide complex. Second,  $^{40}\text{Ar}/^{39}\text{Ar}$  dating of illite collected from gold-bearing ore zones indicate either a resetting or new growth event during the Early Cretaceous (Fig. 4.33a and 4.33b). The intergrowth of Early Cretaceous illite and gold is recognized at Getchell (Cline et al., 2000) and although illite and gold intergrowth is reported at Pipeline (Foo et al., 1996), no

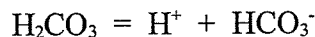
date is reported. Unlike northeastern Nevada where Eocene ages dominate reported gold mineralization (Hofstra et al., 1999), no evidence can be found at Pipeline to support mineral or gold deposition during the Eocene. Third, samples containing ore quartz (silicification) from the ore zones are gold-bearing.

### Geochemical Constraints

Calculations of pH were performed for the two stage 3 fluid inclusion end member salinities. The pH for the moderate salinity ( $\pm 8$  eq. wt. % NaCl) fluid is calculated from the dissociation of carbonic acid in brine of 8 wt. % NaCl. Carbon-dioxide amount is an average value taken from gas analysis. Activity coefficients are calculated from ionic strength (I) using the Debye-Hückel equation (Helgeson and Kirkham, 1974). The pH for the moderate salinity fluid is 4.66 and is calculated as follows:

Given:  $\text{CO}_2$  = 5.5 mole % or 2.91 Molar  
 NaCl = 8 eq. wt. % or 1.37 Molar  
 T = 300°C  
 P = 2000 bar  
 log K = -9.98338  
 $\gamma_{\text{HCO}_3^-}$  = 0.3045

Reaction:



$$m_{\text{CO}_2} = m_{\text{H}_2\text{CO}_3} + m_{\text{HCO}_3^-}$$

$$m_{\text{CO}_2} \cong m_{\text{H}_2\text{CO}_3}$$

$$\text{since } m_{\text{H}_2\text{CO}_3} \gg m_{\text{HCO}_3^-}$$

$$\begin{aligned} \log K &= -\text{pH} + \log \gamma_{\text{HCO}_3^-} + \log \text{HCO}_3^- - \log m_{\text{CO}_2} \\ \text{pH} &= -\log K + \log \gamma_{\text{HCO}_3^-} + \log \text{HCO}_3^- - \log m_{\text{CO}_2} \\ &= 9.98338 - 0.516 + \log \text{HCO}_3^- - \log 2.91 \end{aligned}$$

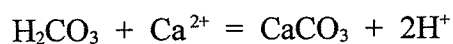
$$\begin{aligned} \text{Since} \quad & \text{H}^+ = \text{HCO}_3^- \\ \text{Then} \quad & \log \text{HCO}_3^- = -\text{pH} - \log \gamma_{\text{H}^+} \end{aligned}$$

$$\begin{aligned} 2 \text{ pH} &= 9.98338 - 0.516 - (-0.325) - 0.464 \\ \text{pH} &= 4.66 \end{aligned}$$

A different approach is taken for the hypersaline fluid and is based on the equilibrium between carbonic acid, calcium ions, calcite and pH. The  $\text{CO}_2$  value was obtained by averaging gas analyses,  $\text{Ca}^{++}$  is from fluid inclusion Tm data. Ionic strength is assumed to be = 4 based on salinity measurements and  $\gamma$  activity coefficients were determined using the Debye-Hückel equation.

$$\begin{aligned} \text{Given: CO}_2 &= 0.767 \text{ mol. \% or } 0.422 \text{ Molar} \\ \text{Ca} &= 1.01 \text{ Molar} \\ \text{T} &= 300^\circ\text{C} \\ \text{P} &= 2000 \text{ bar} \\ \log K &= -9.538 \\ \text{gamma}_{\text{Ca}^{++}} &= 0.0132 \\ \text{I} &= 4 \end{aligned}$$

Reaction:



$$\begin{aligned} \log K &= -2 \text{ pH} - \log a_{\text{Ca}^{2+}} - \log m_{\text{CO}_2} \\ 2 \text{ pH} &= -\log K - \log \gamma_{\text{Ca}^{2+}} - \log m_{\text{Ca}^{2+}} - \log m_{\text{CO}_2} \\ &= 9.538 - \log 0.0132 - \log 1.01 - \log 0.422 \\ &= 11.788 \end{aligned}$$

$$\text{pH} = 5.89$$

The hypothesis that acidic hydrothermal fluids react with the limestones in Carlin deposits to cause decalcification is proposed by Kuehn (1989) and Bakken (1990). I, therefore, propose that the moderate salinity, high- $\text{CO}_2$  fluid is the source fluid that entered the deposit and caused decarbonation. Calculations show that this fluid would dissolve about

1.35 moles of  $\text{CaCO}_3$  per kg of solution. This would increase fluid "salinity" to about 20 eq. wt. % NaCl, increasing  $\text{Ca}^{++}$  to about that of  $\text{Na}^+$ , increasing  $\text{HCO}_3^-$  in solution. This remarkably agrees with my data indicating the 15 to 25% salinity fluid that has  $\text{Ca} > \text{Na}$  and elevated  $\text{HCO}_3^-$ .

Gold solubility calculations were performed using thermodynamic data drawn from SUPCRT92 (Johnson et al., 1992) and Benning and Seward (1996). The logK value used to determine the ionization of metal gold to the  $\text{Au}^+$  state ( $\text{Au}^0 + \text{H}^+ = \text{Au}^+ + \frac{1}{2}\text{H}_2$ ) is taken from SUPCRT92. The solubility of the bisulfide species ( $\text{AuHS}^0$  and  $\text{Au}(\text{HS})_2^-$ ) is calculated using the formulae of Benning and Seward (1996). Gaseous species that participate in the reactions include  $\text{H}_2$  and  $\text{H}_2\text{S}$ . The fugacities of these gases are calculated knowing their concentration from the quadrupole analyses and calculating gas fugacities using Henry's Law gas constants (Appendix H). The activity coefficients are calculated as indicated above. I developed a spreadsheet to calculate gold solubility that considers all the above mentioned factors and gives the Au solubility for both  $\text{AuHS}^0$  and  $\text{Au}(\text{HS})_2^-$  species. The spreadsheet allows parameters such as pH, salinity, gas concentration, and temperature to be varied.

Taking the pH and salinity conditions established for stage 3 quartz samples, gold solubility was calculated for individual gas analyses because  $\text{H}_2$  and  $\text{H}_2\text{S}$  are the principle variables in calculating gold. Gold solubility for stage 3 quartz has two populations (Fig. 5.9). Samples with hypersaline inclusions (eg. NB-100) give  $< 2$  ppb solubility whereas the samples with about 8 eq. wt. % NaCl, give a range of 20 to  $> 500$  ppb gold solubility. The gold solubility in  $\sim 8$  eq. wt. % fluid is consistent with an ore fluid whereas the gold solubility in the more saline fluids is consistent with a spent fluid.

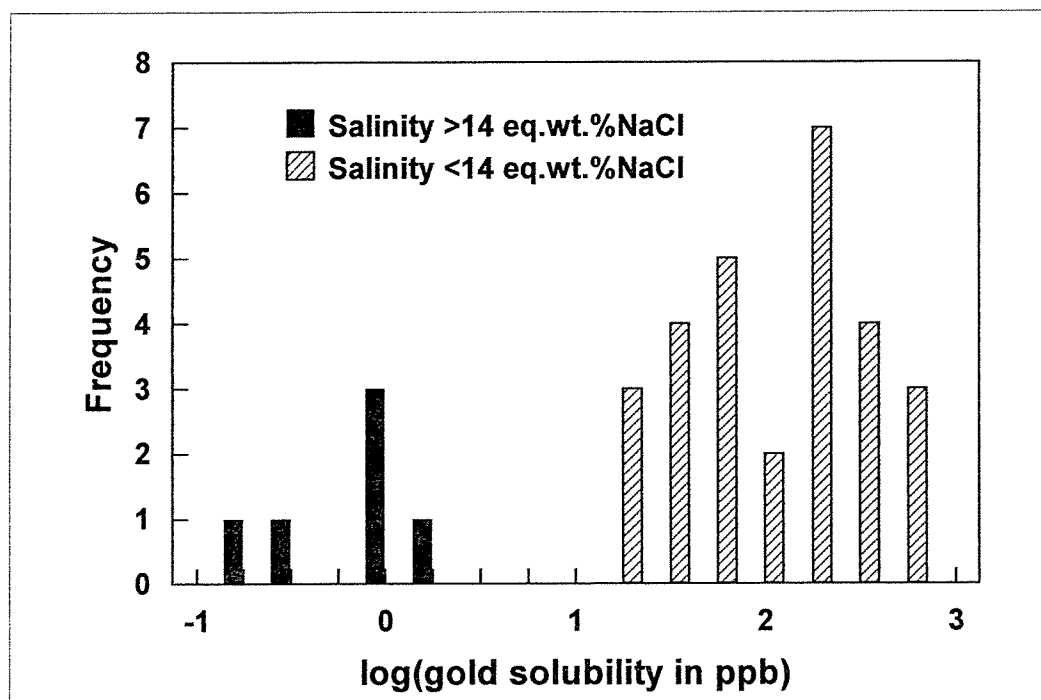


Figure 5.9 Histogram of calculated gold solubility for hypersaline (>14 eq. wt. % NaCl) and non-hypersaline (<14 eq. wt. % NaCl) stage 3 quartz inclusions. Solubility is calculated using the gas analysis of individual crushes and correcting for salinity.

Laboratory experiments (Seward, 1973) show that if all other factors, including  $a_{\text{H}_2\text{S}}$  is maintained constant and only temperature is varied, then a maximum gold solubility around 250°C occurs (Fig. 5.10). Trapping temperature is indicated to be about 300°C, therefore a decrease in fluid temperature cannot account for Pipeline gold mineralization. Loss of H<sub>2</sub>S by sulfidation reactions will result in gold deposition. Accepting that carbonic acid is responsible for decarbonation reactions, the strong linear relationship between fluid inclusion H<sub>2</sub>S and CO<sub>2</sub> indicates that gold at Pipeline was deposited during decarbonization, presumably by sulfidation occurring concurrently with wall-rock alteration. Analysis of SRM show a ready supply of available Fe.

I question the concept that  $a_{\text{H}_2\text{S}}$  is constant and that gold saturation occurs at 250°C. It is shown by Norman et al. (1997) that in hydrothermal systems the H<sub>2</sub>S content of a fluid is buffered by the assemblage pyrite-magnetite-pyrrhotite. The fugacity of H<sub>2</sub>S increases at higher temperatures. Unlike laboratory generated conditions, the  $a_{\text{H}_2\text{S}}$  of hydrothermal systems extends the gold solubility to higher temperatures. I calculated the  $a_{\text{H}_2\text{S}}$  at various temperatures along with the gold solubility buffered by pyrite-magnetite-pyrrhotite and take into account fugacities of gases and activities of ionic species. Figure 5.11 gives the gold solubility maxima around 350°C, maintaining constant pH = 4.66, H<sub>2</sub> = 0.0468 mol. %, ionic strength = 1.37. Assuming equilibrium of magnetite-pyrite-pyrrhotite or at least magnetite-pyrite, implies gold saturation can occur at temperatures below 350°C (in contrast to Fig. 5.10). However, since gold saturation occurs at 350°C then it follows that saturation at 300°C is more likely.

The H<sub>2</sub>S content of stage 3 quartz indicates a source at T > 300°C, and at mineralization temperature fluids had excess H<sub>2</sub>S. Data plot as expected from a

Original in 2nd person.

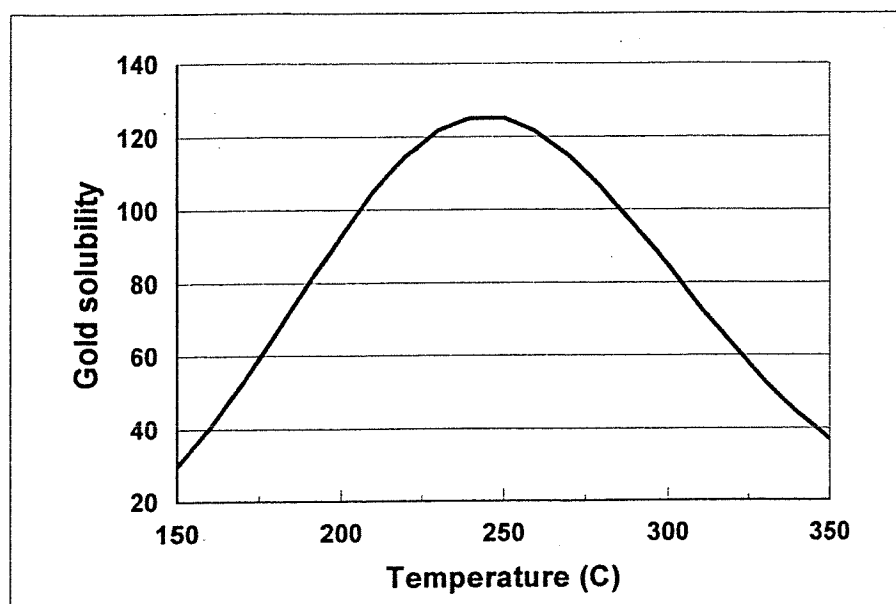


Figure 5.10 Theoretical gold solubility for the  $\text{Au}(\text{HS})^0$  complex at varying temperature based on constant salinity,  $\text{H}_2$ ,  $\text{H}_2\text{S}$  and pH. The chemistry is taken from sample NB-33 ;  $I = 1.37$ ,  $\text{H}_2 = 0.0468$  mol. %,  $\text{H}_2\text{S} = 0.0133$  mol. %. Note that the solubility maxima occurs around  $250^\circ\text{C}$ .

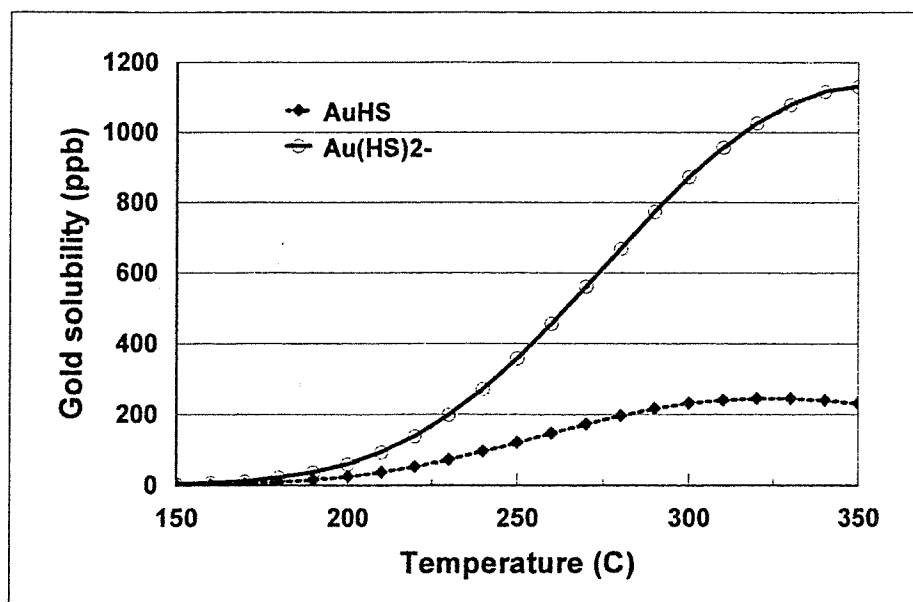


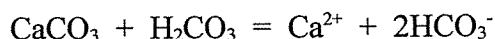
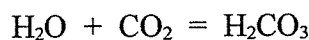
Figure 5.11 Theoretical gold solubility for the  $\text{Au}(\text{HS})^0$  and  $\text{Au}(\text{HS})_2^-$  complexes at varying temperature but constant salinity,  $\text{H}_2$  and pH (chemistry is based on sample NB-33;  $I = 1.37$ ,  $\text{H}_2 = 0.0468$  mol. %). The  $\text{H}_2\text{S}$  content is calculated as temperature varies by assuming that fluid  $\text{H}_2\text{S}$  is buffered by magnetite-pyrite-pyrrhotite and keeping  $\text{H}_2$  constant at 0.0468 mol. %. Note that maximum gold solubility is around  $350^\circ\text{C}$ .

sulfidation reaction between a hotter source that was in equilibrium with pyrite-magnetite coming into contact with cooler rocks.

### *Water-rock Ratios*

The term water-rock ratio is used to give the ratio between the mass of hydrothermal fluid that reacted with a unit mass of rock is calculated by two methods for Pipeline ore fluids.

*Consumption of CO<sub>2</sub>*: The calculations for the consumption of CO<sub>2</sub> is based on following reactions:



Applying these reactions, one mole of CO<sub>2</sub> is required to react with one mole of calcite. Gas data shows that the average CO<sub>2</sub> content before reaction is about 5.5 mole % and the CO<sub>2</sub> in >14 eq. wt. % NaCl inclusions is about 0.7 mole %. Assuming the higher salinity fluids represent spent solutions then this translates into consumption of 4.8 mole % CO<sub>2</sub> (ie., 2.67 moles CO<sub>2</sub> per kg of fluid). The SRM contains 80 % CaCO<sub>3</sub> (Gilluly and Masursky, 1965) or about 8 moles of calcite per kg of rock. The required minimum water-rock ratio for the decarbonization reaction is therefore  $8 / 2.67 \cong 3$ .

*Production of Ca<sup>++</sup> from acid attack on limestone*: Water-rock ratio is calculated a second way by assuming the spent fluids have about 25 eq. wt. % NaCl and a Ca/Na ratio of 1. Since fluid prior to decalcification had 8 eq. wt. % NaCl or 1.4M NaCl, and



assuming minimal  $\text{Ca}^{++}$ , then the spent fluid acquires about 1.4M  $\text{Ca}^{++}$ . The water to rock ratio is calculated by dividing the 8 moles of calcite in average SRM by the 1.4M  $\text{Ca}^{++}$  in solution giving a water to rock ratio of ~6. Both methods of calculation suggest water-rock ratios of Pipeline were low.

*Gold deposition:* Given a water-rock ratio of about 5, and assuming ore fluids were saturated in gold, the amounts of gold deposited by Pipeline fluids is calculated. Assuming an average gold concentration of 100 ppb based on calculations illustrated in Figure 5.9, each 1 kg of ore solution would deposit about 200  $\mu\text{g}$  gold. The amount of gold in 1 kg of rock would be 200  $\mu\text{g}$  \* 5 (W/R ratio) \* 10 (factor from decarbonization) = 10 mg/kg. The published grade for Pipeline is about 7 mg/kg. This calculation further enforces the general accuracy of the W/R calculation and the calculation of gold solubility.

### Source of Fluids

The fluid sources at Pipeline are meteoric fluids, evolved fluids and magmatic fluids. The  $\text{N}_2/\text{Ar}$  ratio of fluid inclusions indicate meteoric, evolved and minor magmatic fluids in all stages of calcite mineralization. Calcite depositing fluids typically have low amounts of dissolved solids and low  $\text{H}_2\text{S}$  contents. During both stage 1 and stage 2, higher  $\text{N}_2/\text{Ar}$  suggest the mineralizing event was intrusive driven. Gold mineralization at Pipeline is associated with a fluid that has  $\text{N}_2/\text{Ar} > 500$  indicating a strong magmatic component. These fluids have elevated salinity and  $\text{H}_2\text{S}$  and variable amounts of  $\text{CO}_2$ , high enough at times to boil. Only magmatic fluids reacted with wall rocks which parallels

our understanding of magmatic fluids that are expected to be out of equilibrium with cooler country rocks.

Stage 1 calcite shows crustal sources (Fig. 4.20), one with a meteoric component, an evolved fluid and possibly a magmatic component. Stage 2 calcite has a strong meteoric signature, but the  $N_2/Ar$  ratio is slightly elevated. Quartz from the stage 3 veins has a gas signature consistent with a magmatic fluid that has evolved by interaction with crustal rocks (Fig. 4.21). The reason for the scatter in Figure 4.21 is attributed to consumption of  $CO_2$  during decalcification that decreases the  $CO_2/CH_4$  ratio. Gas analyses from stage 3 quartz are consistent with the magmatic source model of Sillitoe and Bonham (1990) and Berger and Bagby (1991). Stage 3 calcite analyses indicate mixing between the fluid from which the quartz was deposited and air saturated water (Fig. 4.24). The stage 5 vuggy calcite has a strong evolved gas signature with no indication of a magmatic component.

### **Implications for this study on genetic models for Carlin-type deposits**

This study provides a consistent data set whereby field observations agree with fluid inclusion data and the chemical mass balance works. Several enigmatic aspects about Carlin-type deposits could be answered at Pipeline and include (1) the significance of carbonic fluid inclusions, (2) the hypersaline fluid inclusion chemistry and why they develop, (3) the source of gold mineralizing fluids, (4) P-T conditions during gold mineralization, (5) coeval gold mineralization and alteration, (6) an ore genesis mechanism that satisfies mass balance constraints, (7) low water-rock ratios, (8) localized alteration

Appendix 2

haloes, and (9) the spatial relationship of Carlin-type deposits to Cretaceous or Jurassic plutons.

Magmatic activity is seen as the driving force at Pipeline and supplier of ore fluids. This is indicated by (1)  $N_2/Ar$  ratios of source fluids, (2) dating that links gold mineralization to intrusive activity and alteration, (3) a special fluid that was out of equilibrium with country rock and had a special chemistry (elevated  $H_2S$  and  $CO_2$ ) not represented during other hydrothermal events, and (4) coincident with a zone of contact metamorphism around an intrusive body.

Fluid inclusion Th values  $\sim 200^\circ C$  for Type 1 inclusions are similar to other Carlin-type deposits. However, these inclusions require a large pressure correction as Tt is  $\sim 300^\circ C$ .

Carbonic fluid inclusions were reported at Carlin (Kuehn and Rose, 1995) but the presence of carbonic inclusions at Pipeline, both below and within ore zones, suggest that a pressure throttle did not exist. Changing  $CO_2$  content adequately explains the development of carbonic inclusions even though sporadic phase separation occurred. High  $CO_2$  is important for decalcification, the principle alteration style in Carlin-type deposits.

Low water-rock ratios are confirmed, implying limited alteration; this is compatible with limited fluids from a magmatic body. Limited fluid shows why significant amounts of gold are deposited despite no large scale meteoric water involvement. Mass balance calculations for gold deposition and decalcification are accounted for in a coeval event.

The oxidation event that replaced pyrite by Fe-oxides may not necessarily be supergene. Oxidation in Pipeline and other deposits could be magmatically driven during

the Eocene with oxidizing fluids migrating laterally rather than vertically.

Evidence to support Eocene gold mineralization is lacking at Pipeline, unlike deposits in Northeastern Nevada. Early Cretaceous gold mineralization at Pipeline is possibly an end-member example of Carlin-type deposits in the broader perspective. Cretaceous gold mineralization serves both to introduce gold and cause decalcification in one event. Eocene igneous activity was the driving mechanism behind circulating groundwater that caused oxidation of sulfide minerals, releasing gold. Gold was mobilized over short distances within Pipeline whereas in other deposits, circulating ground water leached gold from suitable host rocks and deposited gold in suitably prepared ground.

### **Genetic Model**

The stage 1 dark petroliferous calcite veins are precursors to gold mineralization. Stage 1 calcite was deposited in fractures within the Roberts Mountains Formation prior to the Antler Orogeny. Depth of formation is estimated at 5 km and about 150°C. Hydrocarbons present within the fluid inclusions were locally derived. Fluid movement could be related to a magmatic event.

West- over east-directed movement along the Roberts Mountains thrust during the Antler orogeny resulted in emplacement of Upper Plate rocks on top of Lower Plate rocks. Sympathetic shears developed in the SRM, close to and subparallel to the Roberts Mountains thrust. One of the shears broadened at what is now the Pipeline deposit. Immediately underlying the shear planes, stage 2 calcite stockwork deposited from

meteoric fluid that descended downward in newly-formed fractures, under P-T conditions exceeding 300°C at ~6 km depth.

Emplacement of the Mill Canyon and Gold Acres stocks as one intrusive body occurred during the Jurassic, ca. 152 Ma. Subsequent NNW-trending faulting, which is either Jurassic or Cretaceous in age, displaced the pluton along the Cortez - Pipeline fault to form two separate bodies.

At  $92.0 \pm 0.3$  Ma a second intrusive body was emplaced in the Gold Acres stock area. Hydrothermal fluids caused sericitic alteration in parts of the Gold Acres stock and fluids also reacted with calcareous country rock to form a skarn. The emplacement of the intrusive body caused tension in the country rock and opening of fractures up which hydrothermal fluids flowed. Stage 3 sericite and quartz were deposited on the sidewalls of the veins and limited sulfidation and gold mineralization occurred. The hydrothermal fluids entered the shear zones where permeability was highest following ground preparation during the Antler orogeny. Pressure-temperature conditions that existed were 300°C and 2000 bar lithostatic. Fluctuations of CO<sub>2</sub> content in the ore fluids caused minor fluid immiscibility. Decalcification reactions liberated Ca<sup>++</sup>, HCO<sub>3</sub><sup>-</sup> and minor Fe<sup>++</sup> ions increasing the ionic strength of the fluid and is reflected as an increase of salinity reported in eq. wt. % NaCl. The Fe<sup>++</sup> scavenged H<sub>2</sub>S in solution to form pyrite and in so doing dropped the solubility of gold as a bisulfide complex by two orders of magnitude. The mineralization model is summarized in Figure 5.12. Silicification occurred locally as a response to drop in temperature. Calculations give the mass of ore fluid to rock in the deposit at a maximum of 6:1. Toward the end of the event, fracturing extended outwards from the deposit. As the hydrothermal system collapsed, meteoric fluids under hydrostatic

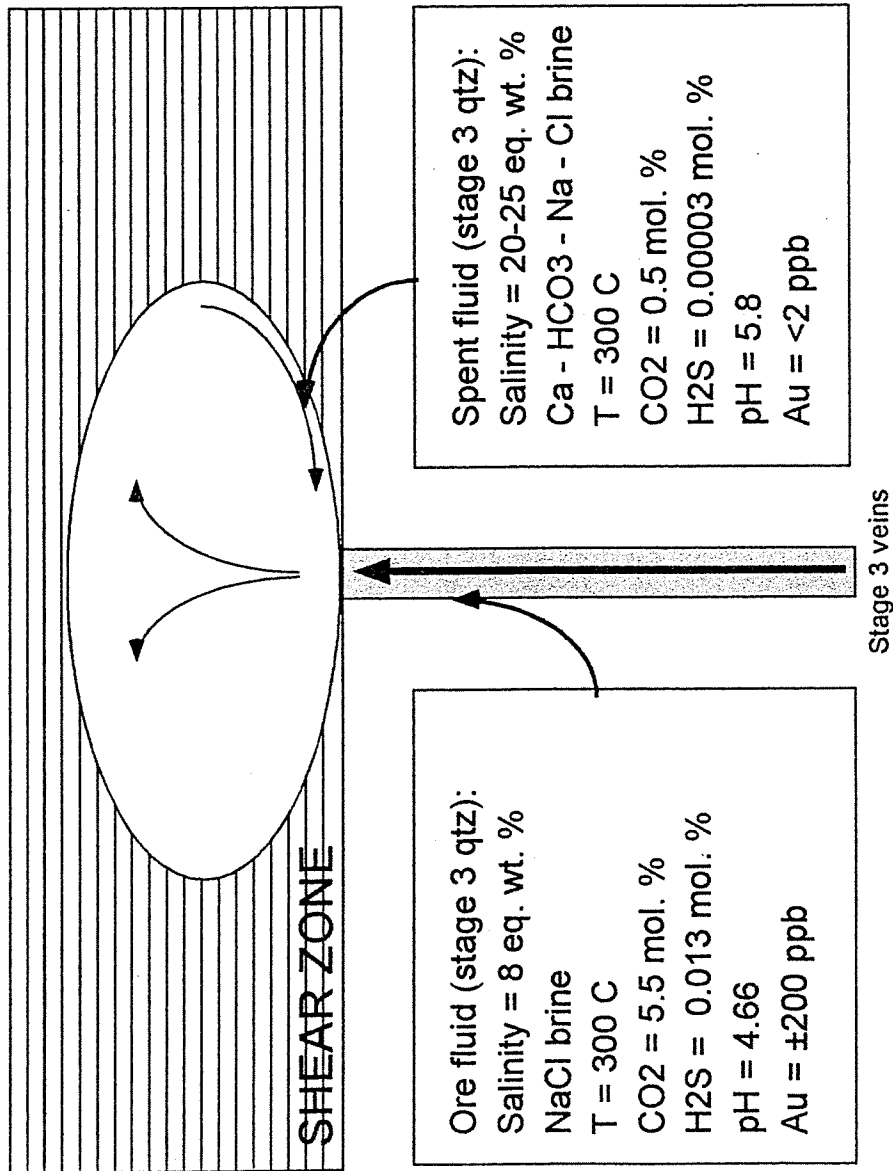


Figure 5.12 Schematic model for Pipeline gold mineralization during stage 3 showing the chemical differences between the ore fluid and the spent fluid.

conditions penetrated the country rock. Minor calcite was deposited from the fluids as they warmed up.

Stage 4 oxidation of the deposit occurred between 92 and 11 Ma, prior to development of stage 5 veins. Circulating meteoric water caused replacement of pyrite by Fe-oxides; acidic fluids were produced by the oxidation process and possibly induced further decalcification. Stage 3 calcite that may have been deposited in the deposit was destroyed. Oxidizing fluids did not penetrate above the shear zones to any extent and migration of oxidizing fluids appears to have been lateral rather than vertical. It is not known if this event was coeval with ~34-35 Ma dike emplacement in the region; the magmatic activity was potentially a heat source to drive circulating meteoric water.

Post-oxidation, stage 5 vuggy calcite was precipitated in open fractures that occur above, within, and below the deposit. During one precipitation cycle, a calcareous sediment was deposited. Drusey calcite subsequently covered this sediment.

Basin-and-Range extension at around 11 Ma tilted the deposit by about 15°. Pipeline was nearly exposed by erosion prior to 11 Ma but was buried by basin fill sediments as Crescent Valley formed.

CHAPTER 6  
CONCLUSION

My conclusions are summarized as follows:

- (1) The Pipeline deposit is the result of a single, Early Cretaceous, hydrothermal event, in which ore solutions dissolved calcite and deposited gold and pyrite. Field evidence does not exist which supports any other significant gold-bearing event. Calcite veining occurred during 2 events before stage 3 mineralization but were not gold-mineralizing events.
- (2) Gold mineralization occurs at  $\sim 300^{\circ}\text{C}$  at 2 kbar pressure under lithostatic conditions (an equivalent of  $\sim 8$  km depth).
- (3) Ore solutions with magmatic components, salinity about 8 eq. wt. % NaCl, and up to 8 mol. %  $\text{CO}_2$  migrated up subvertical fractures into the Pipeline structural zone. The slightly acidic ore fluids (pH  $\sim 4.66$ ) reacted with calcite in the Roberts Mountain Formation resulting in decalcification as the fluid mineralized and altered the Formation.
- (4) Gold deposition is the result of sulfidation. Iron released by decalcification reacted with  $\text{H}_2\text{S}$  to form pyrite, resulting in a breakdown of bisulfide-gold complexes, and gold deposition.
- (5) Mineralization occurs with no measurable change in fluid P or T, and mineralization resulted in spent ore solutions with up to 25 eq. wt. % NaCl salinity and  $>1.0$  Ca/Na ratios. Calcite removal resulted in volume loss, increasing insoluble components such as silt, pyrite and clay particles. Later, under non-lithostatic



pressures, near surface fluids enter fractures and deposit calcite.

- (6) The source fluids associated with gold mineralization have a distinctive gas signature i.e., a magmatic component and most likely originating from a skarn where the magmatic fluids reacted with carbonaceous calcareous rocks at  $\sim 400^{\circ}\text{C}$ . The ore fluids have greater than 3 mol.%  $\text{CO}_2$ ,  $\text{H}_2\text{S}$  in the order of 0.01 mol.%, 0.5 to  $\sim 1$  mol.%  $\text{CH}_4$ , and  $\text{N}_2/\text{Ar} > 500$ .
- (7) The  $\text{N}_2/\text{Ar}$  ratio of the ore fluid gas exceeds 500 that is consistent with a magmatic fluid component. Meteoric and evolved fluids are recognized by gas analysis and are associated with both calcite mineralization.
- (8) Timing, gas ratios, and fluid chemistry indicate gold mineralization was the product of magmatic activity which agrees with the Sillitoe and Bonham (1990) model that magmatic fluids are responsible for Carlin-type gold mineralization.
- (9) The process in which Type 2 ( $\text{CO}_2$ -dominated) inclusions form differs from the model proposed by Kuehn and Rose (1996). I see the process as a result of intermittent boiling in response to varying fluid  $\text{CO}_2$  contents. Type 2 inclusions form once the  $\text{CO}_2$ -brine solvus is reached. P-T conditions are unchanged.
- (10) Three thermal epochs occur. The first occurs at 152 Ma and is related to the intrusion of the Mill Canyon and Gold Acres stock. The second thermal epoch occurred about 92 Ma; stage 3 gold mineralization, and alteration of Gold Acres stock are within this time frame. The third thermal epoch is represented by dikes  $\sim 34$  to 35 Ma.
- (11) Dating of stage 3 vein sericite gives an integrated age of  $92.0 \pm 0.3$  Ma. Illite from ore zones give integrated ages that can be interpreted to be consistent with stage 3.

(12) Oxidation of the deposit occurs prior to Basin-and-Range extension and possibly during the Eocene.

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## APPENDIX A

## SAMPLE LIST

Sample #	Drillhole	Depth(ft)	Remarks
NB-1	DP-412	604.9	Dark calcite vein with banding.
NB-2	DP-413	867.5	Last crystallizing phase of stubby coxcomb clear calcite on top of rhombohedral calcite.
NB-3	DP-412	305	Botriodal calcite with earlier crystallized phase removed.
NB-4	DP-412	393.5	Clear and white calcite with small core of light brown colored calcite.
NB-5	DP-413	895.5	Quartz from qtz-carbonate vein.
NB-6	DP-412	929	Calcite (pale brown) on top of botrioidal Mn oxide which itself coats orange fine-grained calcite.
NB-7	DP-432	633.5	Buff carbonate sediment infilling vugs.
NB-8	DP-471	515.7	Euhedral barite occurring as thin tabular laths as late-stage vuggy infillings (thought to be supergene).
NB-9	DP-452	296.7	Quartz vein.
NB-10	DP-471	515.7	Barite. Vuggy infillings.
NB-11	DP-422	644.6	Calcite dogtooth spar (light brown color) from vug.
NB-12	Crescent pit		Calcite vein striking 155 degrees.
NB-13	DP-424	448	Calcite which postdates the tannish calcareous sediment.
NB-14	DP-472	450	Barite from vug.
NB-15			Southwest fault gouge zone collected 27' south of G14 on 4900 level. It trends N40E.
NB-16			N40E fault gouge zone (Fence Fault) collected at G20, 4900 level Stage 1.
NB-17			N40E fault gouge collected at G21, 4900 level Stage 1.
NB-18			N5W (fault gouge of Pipeline orientation collected at G8, 4860 level, CP.
NB-19	DP-476	880	Argillization which is superimposed upon silicification producing light fish-belly gray color.
NB-20	DP-98	486	30 percent argillization with laminae of hematite (0.3%).
NB-21	DP-76	584.3	
NB-22	DP-471	520	Tannish strongly argillized material.
NB-23	DP-468	343.5	
NB-30	DP-504	819	Porphyroblastic scapolite in fresh to slightly bleached host rock.
NB-31	DP-507	630.5	Breccia-filling which resembles concrete.

NB-32	DP-511	1200	Dark calcite vein (first calcite event).
NB-33	DP-511	1200	Younger qtz carbonate vein with initial euhedral qtz followed by pyrite, followed by infill of white calcite. Vein dips 75 degrees below horizontal.
NB-34	DP-98	655-660	White calcite vein with galena.
NB-35	DP-504	1105	Quartz carbonate vein in slightly sheared, moderately carbonaceous to fresh host rock. Quartz rim with calcite core.
NB-36	DP-504	1140	Quartz vein in slightly sheared moderately carbonaceous host rock.
NB-37	DP-504	1403.4	Quartz carbonate filled shear in fresh host rock.
NB-38	DP-507	746.1	Quartz carbonate vein whereby quartz appears to postdate the calcite; hosted within light tan moderately argillized SRM.
NB-39	DP-507	724	Calcite veins with tannish sediment filling coated by clear drusey calcite.
NB-40	DP-520	785.8	Gray mottled calcite vein hosted in tan weakly argillized SRM.
NB-41	DP-520	994.2	2" thick white quartz vein. Qtz appears to replace calcite.
NB-42	DP-520	784	Two white calcite veins.
NB-43	DP-521	912	Abundant dark calcite veins.
NB-44	DP-521	1002.8	Quartz carbonate vein with euhedral qtz grown from the sidewall and infilled by calcite.
NB-45	DP-521	1152	Quartz filled shear hosted by carbonaceous SRM.
NB-46	DP-525	1116.5	Dark calcite vein.
NB-47	DP-536	923.2	Quartz carbonate vein with euhedral qtz and core of white calcite.
NB-48	DP-532	903.8	Quartz carbonate vein with euhedral qtz and infill of calcite.
NB-49	DP-536	1097	Moderate silicification in strongly carbonaceous, microbrecciated, welded zone.
NB-50	DP-511	1286.2	Quartz filled shear hosted in strongly carbonaceous SRM.
NB-51	DP-532	1081	Framboidal pyrite in weakly carbonaceous SRM.
NB-52	DP-536	1124.5	Brecciation and microbrecciation in strongly carbonaceous SRM with breccia fill of sulphides almost totally replaced by goethite.
NB-53	DP-523	900	Goethitic fracture filling within microbrecciated host rock.
NB-54	DP-511	1354	Microbrecciation in strongly carbonaceous SRM within sheared interval.
NB-55	DP-532	1222.5	Microbrecciated shear zone with calcite microveining within carbonaceous SRM.

NB-56	DP-511	1313.7	Folded tiger stripe with replacement pyrite, hosted by moderately carbonaceous SRM.
NB-57	DP-104	599	Grayish tan, moderately to strongly argillized SRM.
NB-58	DP-113	476	Whiteish tan strongly argillized SRM with goethite fracture surfaces.
NB-59	DP-113	486	Off-white strongly sericitised, totally decalcified SRM.
NB-60	DP-435	585	Moderately hematitic, strongly argillized, sheared SRM.
NB-61	DP-507	736.3	Tannish vuggy sediment.
NB-62	DP-104	494.5	Grayish brownish tan moderately argillized SRM.
NB-63	DP-104	510-520	Moderately argillized SRM with goethite fracture coatings and Mn oxides.
NB-64	DP-104	520-530	Moderately argillized SRM with high Mn oxides.
NB-65	DP-104	577	Tan moderately argillized SRM.
NB-66	DP-104	681	Red moderately hematitic, moderately to strongly argillized SRM.
NB-67	DP-105	440	Weakly oxidised, moderately argillised SRM.
NB-68	DP-105	577	Weakly oxidised, moderately argillized SRM with high Mn oxide content.
NB-69	DP-111	680	Weakly hematitic, moderately to strongly argillized SRM.
NB-70	DP-111	825	Weakly argillized, limy calcareous siltstone below a shear zone.
NB-71	DP-111	849	Weakly hematitic, moderately argillized interbed within limy calcareous siltstone.
NB-72	DP-111	882	Weakly oxidized, moderately argillized SRM.
NB-73	DP-113	260	Moderately argillized SRM.
NB-74	DP-113	540	Brownish tan, moderately argillized SRM.
NB-75	DP-113	680	Brownish tan, moderately argillized SRM.
NB-76	DP-105	562	Quartz vein hosted in oxidised SRM (Qtz appears to postdate the oxidation).
NB-77	DP-495	710,4	7mm dark calcite vein hosted in grayish tan SRM.
NB-78	N25W		White calcite vein in Crescent pit.
NB-79	DP-428	424,5	White calcite from vug with Mn-oxide predating calcite and calcareous sediment postdating.
NB-80	DP-460	382	Quartz filling in vug.
NB-81	DP-412	1253	Quartz filled shear zone with stylolites.
NB-82	DP-511	1171,3	Fresh 1mm-sized pentagonal-dodecahedral pyrite in gray moderate to strongly argillised SRM.
NB-84	DP-532	1508,5	Light gray flame-like calcite veining which postdate stylolites hosted in SRM.
NB-85	DP-532	1508,5	Creamish white calcite vein which dips 60 from horizontal and crosscuts NB-84. Core of vein becomes more clearer.

NB-86	DP-532	1508,5	Slightly creamish white calcite vein which postdates NB-84 and NB-85 and is weakly vuggy. Mn-oxide coating formed on sidewall prior to calcite deposition.
NB-87	Pit		Off-white, totally decalcified, very strongly argillized SRM.
NB-88	DP-633	753,5'	Tannish, totally decalcified, porous, bleached SRM.
NB-89	DP-633	981,5'	Fresh, weakly carbonaceous, unaltered SRM.
NB-90	DP-633	955'	Recrystallized pyrite aggregate hosted in fresh SRM.
NB-91	DP-618	558,5'	Very strong limonite in very strongly argillized sheared zone.
NB-92	DP-618	551'	Very strong hematite with goethite and minor Mn in very strongly argillized shear zone.
NB-93	DP-618	555'	Very strong Mn oxides in very strongly argillized shear zone.
NB-94	DP-633	1054'	Microbreccia of silicified, weakly carbonaceous SRM filled in with darkish gray quartz. Quartz matrix is estimated at 70 percent.
NB-95	DP-602	360,5'	Quartz vein with oxidised pyrite. One crystal of stibnite occurs in a vug and paragenetically postdates the quartz.
NB-96	DP-603	437'	50 percent silicification of SRM.
NB-97	DP-616	688'	Very strong silicification in sheared zone. Silicification appears to postdate shearing.
NB-98	DP-602	365,5'	1" quartz vein parallel to bedding which has secondary calcite microveins. The sample infills a shear.
NB-99	DP-630	1385'	1" quartz vein dipping about 10 degrees to core axis and is probably related to the weak to moderate silicification in the hosting moderately carbonaceous SRM. Vein has 1mm quartz followed by 0,2mm chalcedony and then infilling by quartz.
NB-100	DP-632	855'	1" quartz carbonate vein dipping 45 degrees to core axis. Quartz is euhedral and primary.
NB-101	DP-633	1054'	Microbreccia with quartz matrix within weakly carbonaceous, silicified SRM.
NB-102	DP-641	915,5'	12 mm quartz chalcedony vein dipping 160 degrees and striking subparallel to bedding (dips opposite to bedding).
NB-103	DP-641	718,5'	4cm quartz vein dipping 150 degrees which has secondary calcite (look out for secondary FI).
NB-104	DP-641	778,5'	1" quartz carbonate vein dipping 150 degrees and comprises euhedral quartz and infilling of white calcite.

NB-105	DP-617	699,5'	15mm quartz carbonate vein dipping 130 degrees. The calcite has a slight orange stain.
NB-106	DP-640	865'	1" quartz carbonate vein (maybe same as NB-104)
NB-107	Pit 4440 level		Quartz vein with bladed quartz collected by TGT. Orientation of vein is N10W dip 81NE. Later infilling of openspace by orpiment and rare stibnite.
NB-108	DP-451	381'	Quartz vein with boxworks after sulphide minerals. Euhedral quartz occurs.
NB-109	Gold Acres		Mineralized quartz vein collected by Charles Tarnocai.
NB-110	Gold Acres		Mineralized quartz vein collected by Charles Tarnocai.
NB-111	DP-640	821,2'	A 4cm wide quartz-pyrite-carbonate vein dipping 30 degrees to core axis. Pyrite is zoned, occuring predominantly on one sidewall. Quartz paragenetically postdates pyrite whereas calcite postdates quartz.
NB-112	DP-640	803'	Almost black, moderately carbonaceous, laminated SRM with very sparse dust pyrite and about 5 percent fine crackle white calcite veins.

## Collar positions of the drillholes from which samples were collected

Drillhole	Easting	Northing	Elevation
DP-76	102436.65	59169.39	5058.08
DP-98	102450.19	59401.40	5059.38
DP-104	102641.23	59200.41	5050.53
DP-105	102839.40	59200.41	5044.43
DP-111	103041.18	59201.73	5048.57
DP-113	102241.59	59200.17	5064.03
DP-412	102910.33	57748.36	5024.11
DP-413	103151.26	57638.23	5019.45
DP-422	104631.59	56963.63	4991.09
DP-424	104427.01	56759.90	4989.37
DP-428	104422.42	56379.58	4982.26
DP-432	103656.88	56396.23	4990.21
DP-435	104046.73	59192.16	5043.23
DP-451	103004.44	54512.01	4970.81
DP-452	103105.20	54412.42	4967.25
DP-460	103488.94	54822.62	4964.92
DP-468	103558.91	55849.50	4985.87
DP-471	103347.12	55989.31	4992.23
DP-472	103157.33	55844.15	4995.50
DP-476	104300.29	59076.04	5039.64
DP-495	104735.33	56275.19	4976.61
DP-504	101838.83	58513.54	5077.18
DP-507	103735.74	58099.83	5026.23
DP-511	102529.98	58380.88	5047.24
DP-520	103020.63	57798.63	5020.61
DP-521	103125.16	57894.38	5018.18
DP-523	103313.88	57922.78	5012.57
DP-525	103517.53	57899.45	5014.06
DP-532	103920.39	57478.13	5008.06
DP-536	103415.82	57609.83	5011.13
DP-602	103996.40	55333.13	4965.02
DP-603	104078.70	55444.07	4966.58
DP-616	104036.50	56220.16	4982.40
DP-617	103777.90	56311.69	4993.43
DP-618	103563.40	56310.61	4989.62
DP-630	103315.60	57018.26	5006.60
DP-632	102445.30	56908.01	4798.04
DP-633	102316.60	57117.33	4797.95
DP-640	102285.42	58424.38	4740.00
DP-641	101971.06	58580.52	4780.00

## APPENDIX B

Sample	Mineral	Type	L+V=L			L+V=L		CO2 Vol. Fraction
			Th	Tm(ice)	Salinity	ThCO2	TmCO2	
NB-33	Quartz	primary	188.4	-5.4	8.41			
NB-33	Quartz	primary	179.4	-5.2	8.14			
NB-33	Quartz	primary	218.7					
NB-33	Quartz	primary	187.5					
NB-33	Quartz	primary	192.8					
NB-33	Quartz	primary	210.8					
NB-33	Quartz	primary	199.3					
NB-33	Quartz	primary	198.4					
NB-33	Quartz	secondary	>250			+17.8	-57.6	0.07
NB-33	Quartz	secondary	282.1	+4.7	9.44	+20.8		0.07
NB-33	Quartz	secondary	>295	+4.0	10.49	+27.5		0.07
NB-33	Quartz	primary	202.5	-4.9	7.73			
NB-33	Quartz	primary	204.5	-5.1	8			
NB-33	Calcite	primary	222.8	-1.8	3.06			
NB-33	Calcite	primary	218.7	-2	3.39			
NB-33	Calcite	primary	240	-2	3.39			
NB-33	Calcite	primary	235.3					

Sample	Mineral	Type	Th	Tm	Salinity
NB-47	Quartz	primary	172.8	-6.4	9.71
NB-47	Quartz	primary	181.7	-6.3	9.58
NB-47	Quartz	primary	175.6	-6.4	9.71
NB-47	Quartz	primary	174.9	-6.4	9.71
NB-47	Quartz	primary	178.2	-6.3	9.58
NB-47	Quartz	primary	180.6	-6.3	9.58
NB-47	Quartz	primary	202.1	-5.1	7.96
NB-47	Quartz	primary	203.9	-4.6	7.25
NB-47	Quartz	primary	179.2	-5	7.82
NB-47	Quartz	primary	177.2	-5.2	8.1
NB-47	Quartz	primary	178.8	-5.1	7.96
NB-47	Quartz	primary	179.6	-5.1	7.96
NB-47	Quartz	primary	186.2	-5.2	8.1
NB-47	Quartz	primary	173.5	-5.1	7.96
NB-47	Quartz	primary	175.5	-5.1	7.96
NB-47	Quartz	?	194.1	-4.9	7.68
NB-47	Quartz	?	195.6	-4.5	7.105
NB-47	Quartz	secondary	168.6	-3	4.86
NB-47	Quartz	?	188.9	-4	6.37
NB-47	Quartz	?	194	-4.4	6.96
NB-47	Quartz	?	195.3	-4.6	7.25
NB-47	Calcite	primary	176.8	-3.8	6.08
NB-47	Calcite	primary	168.4	-3	4.86
NB-47	Calcite	primary	168.7	-3.3	5.32
NB-47	Calcite	primary	169.2	-3	4.86
NB-47	Calcite	primary	167.4	-3.4	5.47
NB-47	Calcite	primary	155.2	-3	4.86
NB-47	Quartz	?	194	-4.4	6.96
NB-47	Quartz	?	195.3	-4.6	7.25
NB-47	Calcite	primary	176.8	-3.8	6.08
NB-47	Calcite	primary	168.4	-3	4.86
NB-47	Calcite	primary	168.7	-3.3	5.32



Sample	Mineral	Type	Th	Tm	Salinity			
NB-47	Calcite	primary	169.2	-3	4.86			
NB-47	Calcite	primary	167.4	-3.4	5.47			
NB-47	Calcite	primary	155.2	-3	4.86			
			Th(Celcius)	Tm(Celcius)	Salinity			
NB-99	Quartz	primary	235.4					
NB-99	Quartz	primary	220.3					
NB-99	Quartz	primary	242.3	-3.8	6.16			
NB-99	Quartz	primary	238.7					
NB-99	Quartz	primary	237.2	-5.6	8.68			
NB-99	Quartz	primary	217.1	-4.4	7.02			
NB-99	Quartz	primary	231.6					
NB-99	Quartz	primary	239.5					
NB-99	Quartz	primary	224.1	-4.2	6.74			
NB-99	Quartz	primary	228.2					
NB-99	Quartz	primary	220.6					
NB-99	Quartz	primary	199.3	-5.9	9.08			
NB-99	Quartz	primary	198	-5.2	8.14			
NB-99	Quartz	primary	206.3	-4.7	7.45			
NB-99	Quartz	primary	228.3					
NB-99	Quartz	primary	222.8	-3.5	5.71			Near edge
NB-99	Quartz	primary	203.5	-3.3	5.41			Near edge
NB-99	Quartz	primary	205.2	-4.3	6.88			Near edge
NB-99	Quartz	primary	216.9	-3.7	6.01			Near edge
NB-99	Quartz	primary	240.6	+5.8	6.88			Near edge
NB-99	Quartz	primary	218.5	+7.8	3.87			Near edge
NB-99	Quartz	primary	226	-4.9	7.73			Near edge
NB-99	Quartz	primary	204.1					At edge
NB-99	Quartz	primary	229.8	+4.8	8.28			At edge
NB-99	Quartz	primary	208.8	+7.3	4.65			At edge
NB-99	Quartz	primary	199.2					At edge
NB-99	Quartz	primary	193.5	+6.2	6.3			At edge
NB-99	Calcite	primary	142.2	+1.2				
NB-99	Calcite	primary	141.5	+0.8				
		Type	Th(Celcius)	Tm(Celcius)	Eq.wt.%NaC Lco2	Tm co2	Ca/Na	
NB-100	Quartz	Secondary	162	-11.4	15.37			
NB-100	Quartz	Secondary	165.1	-11.3	15.27			
NB-100	Quartz	Secondary	194.4	-11.9	15.86			
NB-100	Quartz	Secondary	171.9	-11.4	15.37			
NB-100	Quartz	Secondary	189.3	-12	15.96			
NB-100	Quartz	Secondary	181.4	-11.9	15.86	+16 to +18		
NB-100	Quartz	Primary	211.5	-21.1	23.11			
NB-100	Quartz	Primary	196.6	-19.4	21.96			
NB-100	Quartz	Primary	192.7	-26	25.66			1.4
NB-100	Quartz	Primary	218.5	-23.4				0.55
NB-100	Quartz	Primary	197.8	-23.7	24.5			0.65
NB-100	Quartz	Primary	207.4	-25.1	25.26			1.2

			Th	Tm(ice)	Salinity			
NB-102	Quartz	Primary	265.5	-4.9	7.73			
NB-102	Quartz	Primary	224.4	-4.9	7.73			
NB-102	Quartz	Primary	253.2	-4.6	7.31			
NB-102	Quartz	Primary	234.5	+5.4				
NB-102	Quartz	Primary	237.8	+7.5	ice metastability?			
NB-102	Quartz	Primary	215.4	>10	ice metastability?			
NB-102	Quartz	Primary	217.1	>10	ice metastability?			
NB-102	Quartz	Primary	213.8	+7.1	ice metastability?			
			L+V=L			L+V=L		
			Th	Tm(ice)	Salinity	ThCO2	TmCO2	CO2 Vol. Fraction
NB-104	Quartz		229.3					
NB-104	Quartz		>180	+7.9				
NB-104	Quartz		211.6	+7.1				
NB-104	Quartz		>200	+4.6				
NB-104	Quartz		196.5	-5.3	8.28			
NB-104	Quartz		204.6	-5.2	8.14			
NB-104	Quartz		198.1	-5.2	8.14			
NB-104	Quartz		223.6	+7.0	5.68			
NB-104	Quartz		>250			+23.4	-58.8	0.9
NB-104	Quartz		>300	+7.3	5.15	+19.6	-59.7	0.88
NB-104	Quartz		>300	+7.2	5.33	+20.4	-59.7	0.88
NB-104	Quartz		304.2	+7.6	4.62	+15.8	-57.7	0.88
NB-104	Quartz		306.4	+8.5	2.96	+17.8	-57.6	0.88
NB-104	Quartz		321.1	+8.2	3.52	+26.7	-58.2	0.9
NB-104	Quartz		323	+7.8	4.26	+23.2	-58.3	0.85
NB-104	Quartz		316.3	+8.2	3.52	+23.0	-58.2	0.85
NB-104	Quartz		314.9	+8.3	3.33	+23.4	-58.2	0.88
			Th	Tm(ice)	Salinity	ThCO2 to Liq		
NB-106	Quartz		206.9	-6.2	9.47			
NB-106	Quartz		211.8					
NB-106	Quartz		211.3					
NB-106	Quartz		187.9	-6.2	9.47			
NB-106	Quartz		191.3	-6.1	9.34			
NB-106	Quartz		>300	+7.6		+12.9		
NB-106	Quartz		197.8	-6	9.21			
NB-106	Quartz		190.7	-8.1	11.81			
NB-106	Quartz		179.5	-7.4	10.98			
NB-106	Quartz		181.3	-6.5	9.86			
NB-106	Quartz		195.9	-6.6	9.98			
NB-106	Quartz		204.2	-6.8	10.24			
NB-106	Calcite		204.7	0	ice metastability?			
NB-106	Calcite		172.8	-0.1	ice metastability?			
NB-106	Calcite		184.2	0	ice metastability?			

		L+V=L			L+V=L		CO2 Vol.
		Th	Tm(ice)	Salinity	ThCO2	TmCO2	Fraction
NB-107	Quartz	192.9	+7.3	5.154	23		0.05
NB-107	Quartz	233.1	+7.1	5.507	23		0.05
NB-107	Quartz	225.2	+7.2	5.331	23		0.05
NB-107	Quartz	224	+7.3	5.154	23		0.05
NB-107	Quartz	310	+7.2	5.331	24.1		0.4
NB-107	Quartz	310	+6.8	6.028	23.8		0.4
NB-107	Quartz	221.6	+7.1	5.507	23		0.05
NB-107	Quartz	310	+7.2	5.331	25.8		0.35
NB-107	Quartz	227.8	+7.4	4.976	26.8		0.07
NB-107	Quartz	220.1	+7.9	4.074	23		0.08
NB-107	Quartz	214.7	+7.8	4.256	23		0.07
NB-107	Quartz	210.5	+6.3	6.878	23		0.06
NB-107	Quartz	203.7	+7.9	4.074	23		0.06
NB-107	Quartz	227.9	+7.8	4.256	23		0.06
NB-107	Quartz	308.7	+7.3	5.154	24.9		0.45
NB-107	Quartz	312.8	+7.3	5.154	25.2		0.45
NB-107	Quartz	310.3	+7.3	5.154	23.8		0.5

		L+V=L			L+V=L		CO2 Vol.
		Th	Tm(ice)	Salinity	ThCO2	TmCO2	Fraction
NB-84	Calcite	>267	+9.6	0.825	+24		0.45
NB-84	Calcite	>267	+9.6	0.825	+23.2		0.5
NB-84	Calcite	>267			+23.4		0.5
NB-84	Calcite	>267			+23.2		0.55
NB-84	Calcite	>267			+25.5		0.55
NB-84	Calcite	>267			+25.4		0.45
NB-84	Calcite	>267			+25.3		0.5
NB-84	Calcite	>267	+10.1		+24.0	-61.6	0.45
NB-84	Calcite	>267	+11.5		+23.2		0.5
NB-84	Calcite	>267	+9.6	0.825	+23.4		0.5
NB-84	Calcite	>267			+23.2		0.55

		Th	Tm	Salinity	
NB-44	Quartz	primary	177.2	-7.2	10.73
NB-44	Quartz	primary	185	-5.8	8.95
NB-44	Quartz	primary	198	-5.7	8.81
NB-44	Quartz	primary	178.5	-5.5	8.55
NB-44	Quartz	primary	187.1	-5.5	8.55
NB-44	Quartz	primary	188.7	-6.1	9.34

		Th	Tm	Salinity
NB-1	Calcite		-0.4	
NB-1	Calcite	146.5	-1.2	
NB-1	Calcite	142.3	-1.1	
NB-1	Calcite	150.3	-0.6	
NB-1	Calcite	150.7	-0.8	
NB-1	Calcite	149.1	+1.8	
NB-1	Calcite	152	-0.4	
NB-1	Calcite	124.2	+2.9	
NB-1	Calcite	145.1	+12.9	
NB-1	Calcite	145.5	+21.1	
NB-1	Calcite	149	+23.3	

## APPENDIX C

Sample	Mineral	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-1	Calcite	5390A			0.32372	0	0.08936	97.4952	1.23136	0.02961	0.00068	0.00593	0.00442	0.80111	0.00018
NB-1	Calcite	5390B			0.19860	0	0.24266	97.6763	1.00020	0.03673	0.00078	0.0108	0.0074	0.80574	0.00066
NB-1	Calcite	5390C			0.23582	0.03744	0.20335	96.2122	0.46982	0.03568	0.00054	0.00728	0.00663	2.77804	0.00077
NB-1	Calcite	5390D			0.10213	0.03093	0.09922	95.0161	0.69156	0.04441	0.00602	0.01584	0.01461	3.94778	0.00843
NB-1	Calcite	5390E			0.36280	0	0.43028	93.7667	0.30190	0.02958	0.00496	0.00413	0.01092	5.07990	0.00063
NB-1	Calcite	5390G			0.12228	0.00665	0.09415	97.1353	0.22068	0.01686	0.00039	0.00224	0.00202	2.39477	0.000087
NB-1	Calcite	5390K			0.92900	0.00062	2.21812	95.4432	0.15589	0.00879	0.000078	0.00045	0.01888	1.21875	0.00027
NB-1	Calcite	5390L			0.58586	0.00034	1.73944	96.4221	0.11472	0.00795	0.000094	0.00045	0.0189	1.10570	0.00015
NB-1	Calcite	5390M			0.59875	0	1.98626	95.3099	0.20251	0.01218	0.00011	0.00034	0.0164	1.86724	0.000015
NB-1	Calcite	5390N			0.64801	0.00369	2.32866	95.4298	0.30637	0.01156	0.00015	0.00055	0.01703	1.24579	0.00011
NB-1	Calcite	5390O			0.83096	0.00499	1.96818	93.5757	0.20537	0.01241	0.00024	0.00056	0.01414	3.38072	0.00017
NB-7	Calc Sed	5745A	3914970	0.00596	0.00000	0.00136	0.00000	99.28357	0.49755	0.08691	0.00044	0.00596	0.00072	0.12347	0.00002
NB-7	Calc Sed	5745B	2179129	0.00548	0.00000	0.00146	0.02210	99.44859	0.37563	0.06481	0.00024	0.00548	0.00022	0.08138	0.00009
NB-7	Calc Sed	5745C	2059691	0.00691	0.00000	0.00258	0.08037	99.18751	0.51746	0.08055	0.00021	0.00691	0.00039	0.12400	0.00002
NB-7	Calc Sed	5745D	4159612	0.00909	0.00000	0.00130	0.22775	99.04573	0.45362	0.12999	0.00048	0.00909	0.00129	0.13069	0.00006
NB-7	Calc Sed	5745E	7386391	0.00692	0.00000	0.00111	0.18327	99.23124	0.38641	0.08646	0.00041	0.00692	0.00116	0.10300	0.00002
NB-7	Calc Sed	5745F	8903441	0.00620	0.00000	0.00111	0.13182	99.29899	0.36659	0.07835	0.00033	0.00620	0.00091	0.09567	0.00003
NB-7	Calc Sed	5745J	6536523	0.00605	0.00000	0.00035	0.10093	99.03522	0.63696	0.13154	0.00048	0.00905	0.00108	0.08439	0.00000
NB-10	Barite	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-10	Barite	5748A			0	0	0.00898	99.693	0.00636	0.0142	0.000167	0.00017	0.000188	0.277	0.000015
NB-10	Barite	5748B			0	0.00148	0.0353	99.736	0.104	0.0109	0.000199	0.000149	0.000294	0.205	0.000012
NB-10	Barite	5748C			0	0.000553	0.0342	99.546	0.00366	0.0104	0.000178	0.000011	0.000468	0.404	0.00002
NB-10	Barite	5748D			0	0.00247	0.0349	99.461	0	0.005573	0.000126	0.000011	0.000455	0.495	0.000029
NB-10	Barite	5748E			0	0.0041	0.102	99.368	0.0266	0.0199	0.000592	0.000251	0.00116	0.477	0.000097
NB-10	Barite	5748F			0	0.000787	0.0368	99.411	0.00601	0.0137	0.000169	0.000028	0.000535	0.531	0.000026
NB-10	Barite	5748G			0	0.00138	0.0469	99.473	0.008	0.016	0.000203	0.000028	0.000561	0.454	0.000039

	Crush	Counts	Ar max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-32	5848A	3660696	0.002979	0.015753	0.000227	0.225401	93.484450	0.960733	0.01002	0.001702	0.002979	0.008014	5.299741	0.000000
NB-32	5848B	2966724	0.002013	0.024688	0.000887	0.195842	96.006340	0.682456	0.00686	0.001185	0.002013	0.004875	3.081042	0.000000
NB-32	5848C	4879834	0.002927	0.000000	0.002543	0.185764	93.306340	0.989446	0.00651	0.001540	0.002927	0.008470	5.502327	0.000000
NB-32	5848D	1566848	0.002829	0.083008	0.000907	0.112740	95.659920	0.933299	0.022591	0.001741	0.002829	0.004816	3.199183	0.000000
NB-32	5848E	4204847	0.002802	0.000000	0.001081	0.153047	94.718470	0.935484	0.001820	0.001963	0.002802	0.006513	4.178830	0.000000
NB-32	5848F	4976033	0.004804	0.000000	0.002990	0.254422	89.386830	1.429271	0.022263	0.004001	0.004804	0.014108	8.902298	0.000017
NB-32	5848J	5248198	0.003236	0.000000	0.001454	0.192169	93.872180	1.216143	0.004813	0.001934	0.003236	0.007142	4.700921	0.000000
NB-32	5848K	9106990	0.003906	0.000000	0.001413	0.266619	92.055160	1.146448	0.000736	0.002541	0.003906	0.010518	6.512852	0.000014
NB-32	5848L	5466009	0.005161	0.000000	0.002037	0.255714	90.365880	1.434950	0.008786	0.002624	0.005161	0.011527	7.313306	0.000020
NB-32	5848M	6568289	0.003299	0.000000	0.000842	0.147167	95.135150	1.040955	0.004875	0.001255	0.003299	0.005856	3.660598	0.000001
NB-32	5848N	7915872	0.003546	0.000000	0.001295	0.175553	93.903750	1.192998	0.001798	0.001685	0.003546	0.007414	4.709964	0.000000
NB-32	5848O	9851422	0.003215	0.000000	0.001283	0.173974	94.351360	1.119840	0.002625	0.001337	0.003215	0.006816	4.339557	0.000000
NB-32	5848P	4866542	0.003486	0.000000	0.000830	0.297020	94.134900	1.187687	0.003095	0.001032	0.003486	0.007353	4.364590	0.000000
NB-32	5848Q	5659156	0.003955	0.000000	0.001422	0.317668	93.284680	1.269948	0.004845	0.001582	0.003955	0.008930	5.106990	0.000000
NB-36	5831A	13388400	0.000211	0.000000	0.000448	0.171363	98.019370	0.199747	0.000000	0.003361	0.000211	0.003206	1.602262	0.000026
NB-36	5831B	4769098	0.000225	0.038605	0.001069	0.281784	94.485210	0.056265	0.000000	0.008294	0.000225	0.009394	5.119340	0.000037
NB-36	5831C	3855259	0.000174	0.025215	0.000000	0.216828	95.443850	0.112557	0.000000	0.007858	0.000174	0.007256	4.186436	0.000000
NB-36	5831D	6310762	0.000053	0.000000	0.000771	0.200303	95.346900	0.141715	0.000000	0.009302	0.000053	0.006945	4.293973	0.000043
NB-36	5831E	9487064	0.000182	0.000000	0.000062	0.261061	95.004620	0.164915	0.000000	0.009158	0.000182	0.007582	4.552555	0.000041
NB-36	5831F	10030760	0.000195	0.000000	0.000143	0.222561	95.078510	0.175260	0.000000	0.008045	0.000195	0.008131	4.507300	0.000049
NB-36	5831J	3650279	0.000282	0.228558	0.000000	0.562108	94.545080	0.183968	0.000000	0.008257	0.000282	0.011735	4.40290	0.000000
NB-36	5831K	6676615	0.000210	0.054117	0.000000	0.387792	96.174320	0.080600	0.000000	0.008534	0.000210	0.008731	3.287914	0.000000
NB-36	5831L	15497420	0.000170	0.000000	0.000811	0.248982	96.525000	0.146570	0.000000	0.005605	0.000170	0.007083	3.065904	0.000043
NB-36	5831M	15090220	0.000137	0.000000	0.001476	0.216917	96.828950	0.145759	0.000000	0.005108	0.000137	0.005719	2.796031	0.000041
NB-36	5831N	9693801	0.000128	0.000452	0.000000	0.258923	97.010150	0.112259	0.000000	0.004980	0.000128	0.005325	2.607905	0.000000
NB-36	5831O	12888560	0.000145	0.000000	0.001430	0.213268	96.781370	0.117387	0.000000	0.004475	0.000145	0.006040	2.875999	0.000025
NB-36	5831P	9280945	0.000136	0.000000	0.000000	0.205482	96.669920	0.103302	0.000000	0.005177	0.000136	0.005548	2.991056	0.000022
NB-36	5831Q	9795414	0.000133	0.000000	0.000000	0.230537	96.896220	0.106405	0.000000	0.004344	0.000133	0.005558	2.756904	0.000022

Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-34	5746A	Calcite	0	0.000729	0.105	96.124	0.0541	0	0.000134	0.001632	0.0015	1.7	0.000029
NB-34	5746B	Calcite	0	0.00141	0.0796	97.921	0.051	0	0.00011	0.000544	0.00221	1.94	0.000022
NB-34	5746C	Calcite	0	0.00108	0.0796	97.378	0.0612	0	0.000088	0.0012	0.00204	2.455	0
NB-34	5746D	Calcite	0	0.000493	0.125	96.781	0.0619	0.00332	0.000151	0.000656	0.00385	3.02	0.000025
NB-34	5746E	Calcite	0	0.00107	0.078	97.941	0.0342	0	0.000055	0.000241	0.00215	1.943	0.000016
NB-34	5746F	Calcite	0	0.00128	0.0976	97.594	0.0717	0	0.000162	0.000938	0.00308	2.226	0.000018
NB-34	5746J	Calcite	0	0.000423	0.0936	97.146	0.0569	0	0.000084	0.000765	0.00288	2.696	0.000001
NB-34	5746K	Calcite	0	0	0.107	96.559	0.0474	0	0.000058	0.00062	0.00322	3.28	0.000012
NB-34	5746L	Calcite	0	0.000367	0.0851	97.426	0.0715	0	0.000088	0.000986	0.00254	2.41	0.000018
NB-34	5746M	Calcite	0	0.000433	0.0774	97.58	0.1	0	0.0001	0.00172	0.00246	2.23	0.000006
NB-34	5746N	Calcite	0	0.0002	0.0883	97.186	0.111	0	0.000118	0.00174	0.00295	2.6	0.000005
NB-34	5746P	Calcite	0	0.000453	0.0778	97.645	0.0629	0	0.000091	0.00078	0.00254	2.207	0.000021
NB-34	5746Q	Calcite	0	0.000286	0.0685	97.495	0.108	0	0.000115	0.00235	0.00197	2.31	0.000009
NB-34	5746R	Calcite	0	0.000383	0.0933	97.564	0.0638	0	0.000185	0.00123	0.00287	2.246	0.000028
NB-34	5746S	Calcite	0	0.000021	0.0973	97.462	0.077	0	0.000155	0.00103	0.00298	2.35	0.000036
NB-34	5746T	Calcite	0	0.000642	0.0783	97.89	0.0648	0	0.000114	0.000909	0.00222	1.957	0.000018
NB-34	5746U	Calcite	0	0.0011	0.112	96.918	0.1335	0	0.000227	0.00199	0.00354	2.81	0.000022
NB-34	5746V	Calcite	0	0.000908	0.132	96.294	0.118	0	0.000264	0.00202	0.00443	3.43	0.000025
Sample	Counts	Ar max	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
5661A	13353060	0.000960	1.682224	0.000043	0.228761	91.98646	0.190877	0.034814	0.010776	0.000960	0.010518	5.854364	0.000183
5661B	5961918	0.001596	0.026563	0.000000	0.171387	94.80742	0.166154	0.008587	0.006277	0.001596	0.006128	4.805873	0.000003
5661C	9718400	0.001527	0.000000	0.000000	0.156337	95.10228	0.157135	0.008977	0.007199	0.001527	0.005770	4.560764	0.000014
5661D	12199240	0.001096	0.000000	0.000000	0.131608	97.72803	0.122523	0.007539	0.003452	0.001096	0.002586	2.003143	0.000020
5661E	8292313	0.001023	0.017609	0.000000	0.198311	95.73127	0.128890	0.003678	0.006782	0.001023	0.004895	3.907521	0.000021
5661F	14221260	0.000873	0.000000	0.000370	0.236966	95.42583	0.160228	0.001607	0.007499	0.000873	0.006173	4.160423	0.000039
5661J	9866821	0.000898	0.000000	0.000000	0.287976	92.37776	0.157767	0.000000	0.012351	0.000898	0.009985	7.153229	0.000032
5661K	13690290	0.000855	0.000000	0.000093	0.251595	93.53843	0.163965	0.000000	0.008462	0.000855	0.009016	6.029544	0.000040
5661L	15707320	0.000917	0.000000	0.001865	0.392088	91.45277	0.154669	0.000000	0.012375	0.000917	0.014511	7.970525	0.000093
5661M	522755	0.001729	1.748810	0.000000	2.649343	68.79783	0.447177	0.002107	0.012718	0.001729	0.034082	26.306210	0.000000

	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	
NB-47	Quartz	6061A	2096815	0.0000719	0	0.0006045	0.1124231	97.63969	0.0442663	0	0.0024923	0.0000719	0.0029949	2.197497	0.0000332
NB-47	Quartz	6061B	1508904	0.0000637	0	0.0004052	0.1527035	97.76558	0.061164	0	0.0024467	0.0000637	0.0026549	2.015054	0
NB-47	Quartz	6061C	2543105	0.0000621	0	0.0009174	0.1508304	98.14724	0.0687116	0	0.0019482	0.0000621	0.0025863	1.627715	0.0000451
NB-47	Quartz	6061D	1021501	0.0001123	0	0.0028748	0.3119783	96.68582	0.0200555	0	0.0037005	0.0001123	0.0046796	2.970887	0
NB-47	Quartz	6061F	2170470	0.0000833	0	0.0015459	0.2298575	97.58023	0.0908486	0	0.0016636	0.0000833	0.0034689	2.092149	0.0001435
NB-47	Quartz	6061J	4165967	0.0000604	0	0.0012491	0.1122563	98.0655	0.085047	0	0.0020904	0.0000604	0.0025181	1.731254	0.0000838
NB-47	Quartz	6061K	1583162	0.0000822	0	0.0020006	0.1721286	97.20409	0.085643	0	0.0019777	0.0000822	0.0034269	2.530559	0.0001761
NB-47	Quartz	6061N	4480185	0.0000615	0	0.0016276	0.093094	98.15904	0.0947686	0	0.0020156	0.0000615	0.0025612	1.646809	0.0000701
NB-47	Quartz	6061O	5569970	0.000069	0	0.0017289	0.0890884	98.13785	0.0770375	0	0.002165	0.000069	0.0028753	1.689163	0.000103
	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	
NB-47	Calcite	6056B	10027390	0.000081	0	0.0045446	0.1008174	98.45542	0.0547837	0	0.0008853	0.000081	0.0033735	1.380039	0.0001432
NB-47	Calcite	6056C	8337252	0.0000524	0	0.0010801	0.0721521	98.60174	0.0366589	0	0.0004126	0.0000524	0.0021825	1.285745	0.0000307
NB-47	Calcite	6056D	7143973	0.0000728	0	0.0010631	0.0911884	98.04115	0.0183292	0	0.0007336	0.0000728	0.0030315	1.844469	0.0000285
NB-47	Calcite	6056E	7865752	0.0000437	0	0.0013314	0.0766649	98.74147	0.0092736	0	0.0003116	0.0000437	0.0018227	1.169096	0.0000285
NB-47	Calcite	6056F	11710710	0.0002412	0	0.0076716	0.1542457	97.05801	0.067039	0	0.0011686	0.0002412	0.0075656	2.703899	0.000151
NB-47	Calcite	6056J	10131690	0.0001526	0	0.0043493	0.1517741	98.99197	0.0904313	0	0.0008536	0.0001526	0.0063587	2.75413	0.0001477
NB-47	Calcite	6056K	9834060	0.0001312	0	0.0033394	0.1503735	97.26543	0.0547749	0	0.0007045	0.0001312	0.0054658	2.51983	0.0001
NB-47	Calcite	6056L	9187300	0.0001314	0	0.0014305	0.122768	96.87359	0.0593591	0	0.0005186	0.0001314	0.0054754	2.9368	0.0000503
NB-47	Calcite	6056M	9188462	0.0001193	0	0.001329	0.1063492	97.121	0.0546061	0	0.0004517	0.0001193	0.0049689	2.711232	0.0000633
NB-47	Calcite	6056N	8605552	0.0001196	0	0.0012388	0.1089512	97.04345	0.0506221	0	0.0004822	0.0001196	0.004985	2.790181	0.0000371
	Crush	Counts	Ar Min	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	
NB-78	Calcite	6057A	7385414	0.00149	0.00000	0.00112	0.04539	99.81807	0.10805	0.01411	0.00015	0.0000	0.01157	0.00004	
NB-78	Calcite	6057B	4742081	0.00668	0.00000	0.00138	0.03504	99.44621	0.40264	0.10132	0.00055	0.00668	0.00617	0.00002	
NB-78	Calcite	6057C	6877001	0.00373	0.00000	0.00038	0.02994	99.66788	0.23604	0.05781	0.00031	0.00373	0.00001	0.00001	
NB-78	Calcite	6057D	7679501	0.00143	0.00000	0.00078	0.03203	99.86224	0.08728	0.01455	0.00010	0.00143	0.0000	0.00002	
NB-78	Calcite	6057E	8066802	0.00073	0.00000	0.00080	0.04208	99.87890	0.06884	0.00635	0.00010	0.00073	0.00005	0.00004	
NB-78	Calcite	6057I	9207132	0.00211	0.00000	0.00168	0.06137	99.75428	0.15135	0.02486	0.00026	0.00211	0.00021	0.00006	
NB-78	Calcite	6057J	9636624	0.00091	0.00000	0.00208	0.07004	99.81428	0.09513	0.01287	0.00022	0.00091	0.00029	0.00006	
NB-78	Calcite	6057K	8292410	0.00121	0.00000	0.00099	0.03672	99.85226	0.09277	0.01362	0.00013	0.00121	0.00001	0.00002	

Sample	Counts	Ar max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-79	24007560	0.000797	0.051146	0.000733	0.147929	99.65356	0.135307	0.008137	0.000448	0.000797	0.000778	0.010770	0.000086
NB-79	27556970	0.002892	0.331062	0.015277	0.426138	98.71806	0.403896	0.032921	0.002504	0.002892	0.005085	0.061741	0.000415
NB-79	17151890	0.000429	0.000000	0.000000	0.040012	99.88842	0.064635	0.006435	0.000063	0.000429	0.000000	0.000000	0.000013
NB-79	22545540	0.001710	0.028444	0.000000	0.106354	99.62551	0.201776	0.030562	0.000369	0.001710	0.000265	0.004958	0.000052
NB-79	21486360	0.001285	0.017840	0.000067	0.102834	99.67937	0.150007	0.019984	0.000393	0.001285	0.000304	0.027877	0.000049
NB-79	23949310	0.001496	0.126572	0.000438	0.197899	99.41885	0.195949	0.020174	0.000661	0.001496	0.001167	0.036678	0.000112
NB-79	28327980	0.002602	0.304462	0.005571	0.404680	98.81334	0.381932	0.035786	0.002070	0.002602	0.003931	0.045277	0.000356
NB-79	27682080	0.001926	0.139242	0.000928	0.262123	99.28806	0.255940	0.026294	0.001215	0.001926	0.002178	0.021884	0.000207
NB-79	26994870	0.002489	0.214651	0.004850	0.306419	98.09888	0.302242	0.035283	0.001549	0.002489	0.002707	0.029671	0.000256
NB-79	22986630	0.001222	0.002113	0.000000	0.095569	98.71963	0.136953	0.020459	0.000306	0.001222	0.000267	0.023438	0.000045
Crush													
NB-80	Quartz		1.85	0	0.564	92.51	0.0357	0	0.0156	0.000613	0.00504	5.014	0.000299
NB-80	Quartz		0.031	0	0.66	92.213	0.241	0	0.00994	0.000497	0.00764	6.84	0.0002
NB-80	Quartz		0.276	0	0.694	91.232	0.128	0	0.0184	0.000329	0.0083	7.643	0.000251
NB-80	Quartz		0.037	0	0.534	93.526	0.24	0	0.0106	0.000271	0.00725	5.644	0.000166
NB-80	Quartz		0.011	0.000934	0.523	94.426	0.209	0	0.0155	0.000248	0.00635	4.807	0.000148
NB-80	Quartz		0.0597	0.00157	0.556	93.204	0.0813	0	0.0146	0.000049	0.0072	6.076	0.000162
NB-80	Quartz		0	0	0.388	94.792	0.288	0	0.00913	0.00022	0.0075	4.514	0.000127
NB-80	Quartz		0	0.000905	0.376	95.625	0.0532	0	0.00872	0.000121	0.00698	3.928	0.00007
NB-80	Quartz		0.0335	0.00116	0.283	93.727	0.104	0	0.0165	0.000061	0.0086	5.825	0.000116
NB-80	Quartz		0.0469	0.00276	0.38	93.093	0.177	0	0.0232	0.000051	0.01	6.266	0.000114
NB-80	Quartz		0	0.000164	0.339	95.291	0.219	0	0.00764	0.000045	0.00815	4.135	0.000063
NB-80	Quartz		0.0202	0.00195	0.354	94.677	0.177	0	0.00969	0.000003	0.00872	4.75	0.000096



	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-84	6492C			0.110461	0.006173	0.529836	29.05445	0.242463	0	0.003397	0.001099	0.178623	69.8735	0	H2O
NB-84	6492F			0.108977	0.008272	0.518926	33.25959	0.205817	0	0.002849	0.001957	0.165075	65.7284	0.000136	H2O
NB-84	6492H			0.10088	0.006429	0.485662	32.73355	0.350715	0	0.002511	0.002454	0.175187	66.1425	0.000101	H2O
NB-84	6492I			0.08007	0.003378	0.333934	49.12681	0.25939	0	0.002443	0.002175	0.149394	50.04222	0.000185	H2O
NB-84	6492J			0.082774	0.006913	0.41442	44.65445	0.369368	0	0.002718	0.003349	0.190073	54.27676	0.000185	H2O
NB-84	6492K			0.087398	0.005645	0.414445	42.68807	0.37018	0	0.002629	0.00307	0.18192	56.24643	0.000212	H2O
NB-84	6492L			0.091461	0.006877	0.48223	35.73901	0.38912	0	0.00283	0.003624	0.210096	63.07455	0.000206	H2O
NB-84	6492M			0.105916	0.008275	0.513276	27.17211	0.424925	0	0.003142	0.003311	0.216677	71.55214	0.000235	H2O
NB-84	6492N			0.088424	0.005396	0.446935	37.97552	0.398844	0	0.002646	0.003279	0.198903	60.87968	0.000372	H2O
NB-84	6492O			0.09816	0.006956	0.598017	23.33063	0.433216	0	0.001749	0.003143	0.205664	75.32231	0.00016	H2O
NB-84	6492P			0.087692	0.006668	0.505493	35.69197	0.469197	0.005099	0.002482	0.003557	0.229241	62.99816	0.000418	H2O
	Crush	Counts	Ar Max	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-85	6059A	15365470	0.001144	0.000000	0.004035	0.079509	99.834540	0.054835	0.008172	0.000541	0.001144	0.000465	0.016616	0.000147	CO2
NB-85	6059B	11439740	0.000086	0.000000	0.002217	0.049602	99.936460	0.003769	0.000000	0.000121	0.000086	0.000000	0.007683	0.000050	CO2
NB-85	6059C	10918630	0.000160	0.000000	0.001835	0.056395	99.920160	0.013300	0.000000	0.000120	0.000160	0.000000	0.007961	0.000054	
NB-85	6059D	13160050	0.000776	0.000000	0.004292	0.128243	99.764000	0.079896	0.000000	0.000738	0.000776	0.001418	0.020470	0.000178	
NB-85	6059E	13332010	0.000460	0.000000	0.004006	0.090609	99.854420	0.053867	0.000000	0.000469	0.000460	0.000782	0.015365	0.000130	
NB-85	6059J	11338890	0.000643	0.000000	0.002205	0.080630	99.847900	0.056562	0.000000	0.000301	0.000643	0.000546	0.011300	0.000106	
NB-85	6059K	11019190	0.000120	0.000000	0.002061	0.072288	99.877600	0.037301	0.000000	0.000218	0.000120	0.000311	0.010007	0.000085	
NB-85	6059L	10526690	0.000612	0.000000	0.001975	0.067477	99.880420	0.039779	0.000000	0.000166	0.000612	0.000233	0.009273	0.000071	
NB-85	6059M	11908440	0.000863	0.000000	0.004032	0.110244	99.796240	0.069877	0.000000	0.000527	0.000863	0.001076	0.016999	0.000158	
	Crush	Counts	Ar Min	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-86	6058A	2426384	0.00106	0.00000	0.00003	0.01623	99.88970	0.04297	0.00942	0.00003	0.00106	0.00000	0.04155	0.00000	
NB-86	6058B	2230480	0.00074	0.00000	0.00034	0.06705	99.83289	0.03325	0.00506	0.00000	0.00074	0.00026	0.06042	0.00000	
NB-86	6058C	4125322	0.00027	0.00000	0.00145	0.04013	99.89896	0.02859	0.00000	0.00001	0.00027	0.00008	0.03048	0.00002	
NB-86	6058D	6561870	0.00000	0.00000	0.00121	0.03849	99.91090	0.01335	0.00000	0.00006	0.00000	0.00005	0.03591	0.00002	Ar
NB-86	6058E	6162266	0.00076	0.00000	0.00182	0.02392	99.88219	0.04368	0.00968	0.00006	0.00076	0.00000	0.03767	0.00000	
NB-86	6058I	5980367	0.00001	0.00000	0.00019	0.04711	99.93385	0.00243	0.00000	0.00000	0.00000	0.00044	0.01598	0.00000	Ar

	Crush	Counts	Max.Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-95	Quartz	6213A	1054143	0.00147	0.00016	0.06433	97.10921	0.03321	0.01192	0.00034	0.00147	0.00386	2.77688	0.00002
NB-95	Quartz	6213B	2609008	0.00012	0.00110	0.07859	96.56620	0.00000	0.00000	0.00034	0.00012	0.00495	3.35882	0.00000
NB-95	Quartz	6213F	1519068	0.00011	0.00052	0.16914	96.95767	0.00000	0.00000	0.00018	0.00011	0.00454	2.86778	0.00016
NB-95	Quartz	6213G	3560079	0.00044	0.00092	0.18181	97.46474	0.00000	0.01282	0.00031	0.00044	0.00375	2.33510	0.00011
NB-95	Quartz	6213K	2143727	0.00037	0.00068	0.07426	96.77299	0.00000	0.00371	0.00031	0.00037	0.00403	3.14350	0.00013
NB-95	Quartz	6213L	1058250	0.00009	0.00022	0.09568	96.42011	0.00000	0.00000	0.00000	0.00009	0.00376	3.48010	0.00013
NB-95	Quartz	6213M	1381330	0.00008	0.00016	0.10631	97.02309	0.00000	0.00989	0.00019	0.00008	0.00324	2.85702	0.00010
NB-95	Quartz	6213N	2194647	0.00007	0.00063	0.06712	97.49698	0.00000	0.00000	0.00001	0.00007	0.00281	2.43236	0.00009
NB-95	Quartz	6213O	1003762	0.00010	0.00046	0.07895	96.43775	0.00000	0.00000	0.00019	0.00010	0.00403	3.47847	0.00015
NB-96	Silica	6250C	1675087	0.00302	0.00081	0.37486	97.06500	0.08843	0.03016	0.00071	0.00302	0.00476	2.43213	0.00011
NB-96	Silica	6250D	1339959	0.00006	0.00005	0.24926	98.89598	0.01172	0.00015	0.00003	0.00006	0.00157	0.84116	0.00002
NB-96	Silica	6250F	482840.8	0.00016	0.00000	0.58114	97.85554	0.05241	0.00044	0.00000	0.00016	0.00296	1.50728	0.00008
NB-96	Silica	6250G	681837.5	0.00009	0.00000	0.43796	97.43614	0.00000	0.00000	0.00021	0.00009	0.00370	2.11997	0.00002
NB-96	Silica	6250K	6012561	0.00089	0.00000	0.15626	98.32164	0.03496	0.00545	0.00013	0.00089	0.00127	0.47939	0.00003
NB-96	Silica	6250L	3123.061	0.02175	0.02472	49.20501	0.00000	2.37820	0.05295	0.00000	0.02175	0.90633	37.55245	0.00000
NB-97	Quartz	6214A	1540362	0.00045	0.00026	0.23269	97.71711	0.00139	0.00809	0.00016	0.00045	0.00309	2.03667	0.00007
NB-97	Quartz	6214B	907633.4	0.00126	0.00003	0.26498	98.06175	0.07107	0.01952	0.00009	0.00126	0.00280	1.57846	0.00005
NB-97	Quartz	6214C	3373780	0.00095	0.00121	0.29910	97.56363	0.04411	0.01832	0.00014	0.00095	0.00328	2.07516	0.00008
NB-97	Quartz	6214D	1580188	0.00039	0.00012	0.12715	97.71397	0.00000	0.00732	0.00008	0.00039	0.00256	2.14833	0.00006
NB-97	Quartz	6214	1361364	0.00006	0.00018	0.19549	97.03239	0.00000	0.00000	0.00017	0.00006	0.00345	2.76619	0.00009
NB-97	Quartz	6214F	958220.1	0.00008	0.00023	0.27454	97.15855	0.00000	0.00000	0.00008	0.00008	0.00339	2.56313	0.00009
NB-97	Quartz	6214G	515159	0.00033	0.00009	0.25016	97.30639	0.00000	0.00779	0.00018	0.00033	0.00288	2.43214	0.00005
NB-97	Quartz	6214K	917414.9	0.00008	0.00024	0.32032	97.57936	0.00722	0.00498	0.00000	0.00008	0.00318	2.08465	0.00005
NB-97	Quartz	6214L	1604874	0.00008	0.00020	0.19352	97.28046	0.00000	0.03543	0.00022	0.00008	0.00315	2.48696	0.00007
NB-97	Quartz	6214M	1535295	0.00006	0.00031	0.16995	97.66319	0.01437	0.00595	0.00002	0.00006	0.00270	2.14344	0.00007

	Crush	Counts	Max.Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-97	Quartz	6214A	1540362	0.00045	0.00026	0.23269	97.71711	0.00139	0.00809	0.00016	0.00045	0.00309	2.03667	0.00007	
NB-97	Quartz	6214B	907633.4	0.00126	0.00003	0.26498	98.06175	0.07107	0.01952	0.00009	0.00126	0.00280	1.57846	0.00005	
NB-97	Quartz	6214C	3373780	0.00095	0.00121	0.29910	97.56363	0.04411	0.01832	0.00014	0.00095	0.00328	2.07516	0.00008	
NB-97	Quartz	6214D	1580188	0.00039	0.00012	0.12715	97.71397	0.00000	0.00732	0.00008	0.00039	0.00256	2.14833	0.00006	N2
NB-97	Quartz	6214	1361364	0.00006	0.00018	0.19549	97.03239	0.00000	0.00000	0.00017	0.00006	0.00345	2.76619	0.00009	N2
NB-97	Quartz	6214F	958220.1	0.00008	0.00023	0.27454	97.15855	0.00000	0.00000	0.00008	0.00008	0.00339	2.56313	0.00009	N2
NB-97	Quartz	6214G	515159	0.00033	0.00009	0.25016	97.30639	0.00000	0.00779	0.00018	0.00033	0.00288	2.43214	0.00005	low,N2
NB-97	Quartz	6214K	917414.9	0.00008	0.00024	0.32032	97.57936	0.00722	0.00498	0.00000	0.00008	0.00318	2.08465	0.00005	
NB-97	Quartz	6214L	1604874	0.00008	0.00020	0.19352	97.28046	0.00000	0.03543	0.00022	0.00008	0.00315	2.48696	0.00007	N2
NB-97	Quartz	6214M	1535295	0.00006	0.00031	0.16995	97.66319	0.01437	0.00595	0.00002	0.00006	0.00270	2.14344	0.00007	

	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-99	Quartz	651796	0.00045	0.00000	0.00115	0.32595	92.92352	0.03106	0.00000	0.00085	0.00045	0.01058	6.70622	0.00019	
NB-99	Quartz	545883	0.00001	0.00000	0.00172	0.31282	92.65728	0.00000	0.00000	0.00195	0.00001	0.01194	7.01521	0.00027	
NB-99	Quartz	516277	0.00025	0.00000	0.00167	0.64047	93.77675	0.09080	0.00000	0.00092	0.00025	0.01031	5.47880	0.00028	
NB-99	Quartz	668262	0.00124	0.00000	0.00109	0.37563	95.11384	0.07623	0.00000	0.00062	0.00124	0.00934	4.42188	0.00013	
NB-99	Quartz	2851073	0.00218	0.00000	0.00248	0.24192	95.17368	0.03232	0.00150	0.00055	0.00218	0.00739	4.53778	0.00020	N2
NB-99	Quartz	1382007	0.00042	0.00000	0.00138	0.16769	94.00031	0.01815	0.00000	0.00127	0.00042	0.00903	5.80154	0.00023	
	Crush	Counts	Max. Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	
NB-100	Quartz	2065210	0.00001	0.00000	0.00111	0.71843	98.32487	0.06205	0.00000	0.00009	0.00001	0.00059	0.89280	0.00004	
NB-100	Quartz	665488.2	0.00004	0.02064	0.00084	1.20117	97.93796	0.11504	0.00000	0.00000	0.00004	0.00163	0.72254	0.00007	
NB-100	Quartz	1032062	0.00005	0.00000	0.00241	1.59640	97.20547	0.13474	0.00000	0.00000	0.00005	0.00199	1.05896	0.00004	
NB-100	Quartz	1286822	0.00003	0.00000	0.00141	1.00283	98.00095	0.13190	0.00000	0.00000	0.00003	0.00121	0.86167	0.00002	
NB-100	Quartz	3174728	0.00002	0.00000	0.00166	0.46714	98.52834	0.22188	0.00000	0.00000	0.00002	0.00196	0.77958	0.00002	
NB-100	Quartz	1120701	0.00002	0.00000	0.00061	1.00805	98.25744	0.19625	0.00000	0.00007	0.00002	0.00091	0.59664	0.00004	
NB-100	Quartz	1545827	0.00003	0.00000	0.00098	0.74929	98.37671	0.15531	0.00000	0.00000	0.00003	0.00139	0.71632	0.00001	
NB-100	Quartz	3317613	0.00026	0.00000	0.00076	0.83594	98.36558	0.16132	0.00000	0.00006	0.00026	0.00090	0.63517	0.00002	
NB-100	Quartz	1530231	0.00019	0.00000	0.00024	1.20135	97.92727	0.23794	0.00000	0.00008	0.00019	0.00102	0.63191	0.00000	
NB-100	Quartz	3736335	0.00016	0.00000	0.00095	0.88410	98.09772	0.11550	0.00000	0.00002	0.00016	0.00128	0.90023	0.00002	
NB-100	Quartz	3467158	0.00010	0.00000	0.00071	0.66874	98.53203	0.13344	0.00000	0.00001	0.00010	0.00134	0.64561	0.00002	
	Crush	Counts	Max. Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-100	Calcite	5686678	0.00041	0.00000	0.00125	0.14190	98.62723	0.05804	0.00000	0.00004	0.00041	0.00214	1.16894	0.00007	H2O, H2
NB-100	Calcite	6137726	0.00008	0.00000	0.00031	0.07543	98.91894	0.00000	0.00000	0.00001	0.00008	0.00139	1.00380	0.00005	
NB-100	Calcite	2451721	0.00031	0.00000	0.00000	0.05144	99.37001	0.01321	0.00000	0.00000	0.00031	0.00067	0.56434	0.00002	
NB-100	Calcite	7698231	0.00029	0.00000	0.00000	0.12696	99.30807	0.01348	0.00030	0.00000	0.00029	0.00069	0.55020	0.00001	
NB-100	Calcite	4810260	0.00035	0.00000	0.00000	0.28420	98.75375	0.01862	0.00000	0.00000	0.00035	0.00120	0.94185	0.00003	
NB-100	Calcite	8475448	0.00027	0.00000	0.00025	0.13216	99.12617	0.00970	0.00035	0.00000	0.00027	0.00090	0.73015	0.00003	
NB-100	Calcite	10898840	0.00011	0.00000	0.00034	0.07165	99.28859	0.01321	0.00000	0.00000	0.00011	0.00097	0.62510	0.00003	
NB-100	Calcite	10423720	0.00003	0.00000	0.00003	0.06933	99.14677	0.00571	0.00000	0.00002	0.00003	0.00119	0.77691	0.00004	

Crush	Counts	Max. Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-101 Quartz	6211A	1104967	0.00509	0.00000	0.20860	99.03116	0.29207	0.00000	0.00010	0.00509	0.00171	0.46301	0.00005	v.low
NB-101 Quartz	6211B	371256.7	0.01130	0.00000	0.19525	98.59070	0.54073	0.00906	0.00011	0.01130	0.00225	0.50566	0.00006	v.low
NB-101 Quartz	6211C	1506552	0.00385	0.00000	0.18470	99.02052	0.24958	0.00000	0.00006	0.00385	0.00190	0.53938	0.00003	v.low
NB-101 Quartz	6211D	688940.9	0.00734	0.00000	0.31858	98.42022	0.43682	0.00497	0.00000	0.00734	0.00275	0.79789	0.00006	v.low
NB-101 Quartz	6211E	1170819	0.00253	0.00012	0.18255	98.98097	0.13656	0.00000	0.00010	0.00253	0.00233	0.69474	0.00010	
NB-101 Quartz	6211F	1362152	0.00355	0.00000	0.10280	99.32558	0.18946	0.00020	0.00008	0.00355	0.00139	0.37792	0.00002	
NB-101 Quartz	6211J	1123529	0.00155	0.00000	0.15401	99.44701	0.11233	0.00000	0.00000	0.00155	0.00222	0.28286	0.00002	
NB-101 Quartz	6211K	904615.5	0.00635	0.00000	0.26443	99.08123	0.29564	0.00000	0.00000	0.00635	0.00276	0.35060	0.00000	
NB-101 Quartz	6211L	699766.3	0.00230	0.00000	0.26876	99.15573	0.13719	0.00000	0.00000	0.00230	0.00269	0.43332	0.00002	
NB-101 Quartz	6211M	729406.5	0.00341	0.00000	0.24802	98.99156	0.21237	0.00000	0.00000	0.00341	0.00191	0.53073	0.00000	
NB-101 Quartz	6211N	813691.9	0.00219	0.00000	0.23816	99.06855	0.14213	0.00000	0.00000	0.00219	0.00238	0.54858	0.00000	
NB-101 Quartz	6211O	840129.7	0.00282	0.00000	0.22596	98.99679	0.15942	0.00000	0.00000	0.00282	0.00289	0.61210	0.00004	
Crush	Counts	Max. Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-103 Quartz	6249A	200127.4	0.00005	0.00000	0.57486	97.94026	0.15538	0.00000	0.00110	0.00005	0.00194	1.32646	0.00000	low
NB-103 Quartz	6249B	4941354	0.00002	0.00152	0.41415	98.80122	0.21377	0.00000	0.00111	0.00002	0.00287	0.56521	0.00015	CH4, CO2
NB-103 Quartz	6249C	1173384	0.00010	0.00070	0.88735	96.71080	0.11750	0.00000	0.00340	0.00010	0.00427	2.47593	0.00006	
NB-103 Quartz	6249D	4170253	0.00005	0.00142	0.81569	96.55255	0.18889	0.00000	0.00264	0.00005	0.00532	2.43330	0.00013	
NB-103 Quartz	6249E	489206.4	0.00011	0.00000	1.05883	96.58871	0.22052	0.00000	0.00203	0.00011	0.00440	2.12540	0.00011	v.low
NB-103 Quartz	6249F	1521147	0.00004	0.00000	0.24724	99.01335	0.05447	0.00000	0.00064	0.00004	0.00152	0.68275	0.00005	
NB-103 Quartz	6249G	2112687	0.00018	0.00156	1.27478	95.73946	0.27579	0.00000	0.00274	0.00018	0.00742	2.69789	0.00018	
NB-103 Quartz	6249J	879303.9	0.00011	0.00000	0.73303	96.78619	0.19011	0.00000	0.00127	0.00011	0.00450	2.28478	0.00013	v.low
NB-103 Quartz	6249K	905473.7	0.00010	0.00023	0.71103	97.08931	0.17855	0.00000	0.00178	0.00010	0.00418	2.01484	0.00008	v.low
NB-103 Quartz	6249L	940702.6	0.00011	0.00035	0.85467	96.73643	0.20789	0.00000	0.00150	0.00011	0.00462	2.19441	0.00012	

Crush	Counts	Ar max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-104 Quartz	6428C	1754199	0.001538	0.001874	1.001931	87.004550	0.000000	0.000000	0.005538	0.001538	0.013268	11.971250	0.000039	N2
NB-104 Quartz	6428D	925850.8	0.000640	0.001829	1.105392	89.427210	0.000000	0.000000	0.005141	0.000640	0.009901	9.449888	0.000000	N2
NB-104 Quartz	6428E	1511005	0.001207	0.001197	1.114775	89.883150	0.000000	0.000000	0.003223	0.001207	0.008760	8.987660	0.000017	N2
NB-104 Quartz	6428F	1540030	0.001251	0.001712	1.136998	90.014150	0.000000	0.000000	0.001984	0.001251	0.007951	8.835995	0.000000	N2
NB-104 Quartz	6428G	2764011	0.000987	0.001378	1.136540	92.747290	0.000000	0.000000	0.001736	0.000987	0.006182	6.105889	0.000004	N2
NB-104 Quartz	6428N	3863585	0.001176	0.001007	0.898000	93.566710	0.000000	0.000954	0.000610	0.001176	0.005534	5.525978	0.000025	N2
NB-104 Quartz	6428O	1521158	0.001351	0.001536	1.209754	90.256720	0.000000	0.003569	0.001382	0.001351	0.007759	8.517919	0.000000	N2
NB-104 Quartz	6428P	1044577	0.001571	0.001945	1.108470	87.308460	0.000000	0.000000	0.001707	0.001571	0.010053	11.567800	0.000000	N2
Crush	Counts	Ar max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-104 Calcite	6430A	785410.4	0.000005	0.000000	0.102539	98.909500	0.000000	0.000000	0.000000	0.000005	0.001135	0.986816	0.000012	
NB-104 Calcite	6430B	538771.7	0.0000341	0.0000097	0.327185	98.682010	0.013781	0.000000	0.000000	0.000341	0.003499	0.973085	0.000000	
NB-104 Calcite	6430C	419819.2	0.000407	0.000000	0.018351	99.368100	0.017705	0.000230	0.000000	0.000407	0.000370	0.594841	0.000000	CH4, CO2
NB-104 Calcite	6430D	2524585	0.000372	0.000463	0.060753	99.406040	0.008358	0.000000	0.000000	0.000372	0.000867	0.523112	0.000029	strong,CO2
NB-104 Calcite	6430E	4440892	0.000997	0.000680	0.011735	99.574490	0.042580	0.010313	0.000062	0.000997	0.000328	0.358794	0.000011	low
NB-104 Calcite	6430F	988764.8	0.000461	0.000002	0.004133	99.851460	0.016063	0.003328	0.000160	0.000461	0.000244	0.324145	0.000000	
NB-104 Calcite	6430G	6083811	0.001024	0.000000	0.001771	0.024563	99.447840	0.091508	0.000119	0.001024	0.001074	0.426471	0.000061	CH4,CO2
NB-104 Calcite	6430H	9239875	0.000284	0.000000	0.000251	0.004111	99.759120	0.006522	0.001983	0.000284	0.000173	0.227558	0.000003	
NB-104 Calcite	6430I	*****	0.000275	0.000000	0.000920	0.032587	99.708360	0.016414	0.000176	0.000275	0.000377	0.239145	0.000057	
NB-104 Calcite	6430J	4516559	0.000288	0.000000	0.017709	99.495360	0.006632	0.001070	0.000002	0.000288	0.000363	0.478565	0.000011	
NB-104 Calcite	6430K	7364627	0.000275	0.000000	0.000022	0.011594	99.526670	0.007345	0.000000	0.000275	0.000352	0.452558	0.000013	
NB-104 Calcite	6430L	*****	0.000216	0.000000	0.000116	0.024316	99.486620	0.002982	0.000046	0.000216	0.000449	0.485219	0.000025	
NB-104 Calcite	6430M	*****	0.000361	0.000000	0.000513	0.018937	99.561720	0.019213	0.000061	0.000361	0.000359	0.397086	0.000030	

Crush	Counts	Max. Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-107 Quartz	735832.6	0.00029	0.00000	0.00163	0.21868	95.52840	0.21131	0.00000	0.00138	0.00029	0.01195	4.02532	0.00134	
NB-107 Quartz	5549299	0.00020	0.00000	0.00071	0.14868	95.41310	0.20247	0.00000	0.00079	0.00020	0.00822	4.22581	0.00022	
NB-107 Quartz	7571808	0.00034	0.00000	0.00220	0.16175	96.33165	0.48191	0.00000	0.00152	0.00034	0.01456	3.00641	0.00021	
NB-107 Quartz	4702521	0.00019	0.00000	0.00009	0.12389	94.21039	0.03460	0.00000	0.00083	0.00019	0.00783	5.62233	0.00004	
NB-107 Quartz	8867061	0.00024	0.00000	0.00175	0.13284	94.33173	0.05452	0.00000	0.00064	0.00024	0.00985	5.46861	0.00006	
NB-107 Quartz	9679538	0.00007	0.00000	0.00164	0.13459	94.59941	0.05568	0.00000	0.00137	0.00007	0.01062	5.19656	0.00006	
NB-107 Quartz	3837124	0.00021	0.00000	0.00084	0.13518	93.64553	0.05601	0.00000	0.00062	0.00021	0.00860	6.15314	0.00009	
NB-107 Quartz	2682901	0.00021	0.00000	0.00047	0.20268	93.39180	0.05861	0.00000	0.00071	0.00021	0.00860	6.33710	0.00003	
NB-107 Quartz	3787845	0.00017	0.00000	0.00049	0.09653	94.38718	0.02784	0.00000	0.00047	0.00017	0.00719	5.48027	0.00003	
NB-107 Quartz	3798337	0.00021	0.00000	0.00035	0.12948	93.57909	0.02175	0.00000	0.00094	0.00021	0.00855	6.25981	0.00004	
NB-107 Quartz	2820668	0.00021	0.00000	0.00066	0.14880	92.40850	0.03046	0.00000	0.00065	0.00021	0.00880	7.40410	0.00004	
NB-107 Quartz	7099338	0.00021	0.00000	0.00135	0.13405	94.25304	0.06170	0.00000	0.00059	0.00021	0.00873	5.54050	0.00003	
Crush	Counts	Max. Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-108 Quartz	1765782	0.00001	0.00000	0.00075	0.11389	99.45970	0.21236	0.00000	0.00000	0.00001	0.00022	0.21309	0.00000	
NB-108 Quartz	1042204	0.00005	0.00000	0.00072	0.18243	98.73631	0.19226	0.00000	0.00020	0.00005	0.00229	0.88573	0.00004	CH4
NB-108 Quartz	3607321	0.00005	0.00000	0.00188	0.32752	99.12994	0.09599	0.00000	0.00044	0.00005	0.00211	0.44208	0.00005	CO2
NB-108 Quartz	1378197	0.00011	0.00000	0.00059	0.40216	98.76000	0.07206	0.00000	0.00015	0.00011	0.00441	0.76052	0.00010	
NB-108 Quartz	1090154	0.00005	0.00000	0.00002	0.43940	98.78320	0.10075	0.00000	0.00000	0.00005	0.00224	0.67536	0.00003	
NB-108 Quartz	854680.8	0.00009	0.00000	0.00003	0.71008	98.75185	0.16884	0.00000	0.00001	0.00009	0.00357	0.36557	0.00005	
NB-108 Quartz	1025691	0.00009	0.00000	0.00005	0.68164	98.84555	0.15530	0.00000	0.00000	0.00009	0.00391	0.31354	0.00001	
NB-108 Quartz	516465.4	0.00028	0.03151	0.00000	0.81436	98.75181	0.16650	0.00000	0.00000	0.00028	0.01186	0.22390	0.00007	
NB-108 Quartz	731511.4	0.00034	0.02076	0.00007	0.86609	98.64111	0.17281	0.00000	0.00009	0.00034	0.01418	0.28487	0.00003	
NB-108 Quartz	2067356	0.00005	0.00000	0.00053	0.58967	98.97416	0.18035	0.00000	0.00003	0.00005	0.00228	0.25294	0.00005	
NB-108 Quartz	5015312	0.00004	0.00000	0.00060	0.39361	98.99125	0.16798	0.00000	0.00017	0.00004	0.00159	0.44477	0.00004	

	Crush	Counts	Max.Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2	Problem
NB-109	Quartz	105467.9	0.00117	1.58862	0.00114	0.92499	89.27659	0.09163	0.00000	0.00208	0.00017	0.00693	8.11786	0.00018	
NB-109	Quartz	1087376	0.00015	0.00000	0.00021	0.32666	98.19670	0.03440	0.00000	0.00013	0.00015	0.00278	1.43891	0.00006	
NB-109	Quartz	1078297	0.00037	0.00000	0.00241	0.67149	90.88541	0.00000	0.00000	0.00022	0.00037	0.01551	8.42464	0.00033	v.Low
NB-109	Quartz	73510.05	0.00023	0.76706	0.00134	0.86000	92.32441	0.18747	0.00000	0.00000	0.00023	0.00974	5.82998	0.00000	
NB-109	Quartz	106862.2	0.00325	0.45454	0.00000	1.49042	92.04359	0.19224	0.00000	0.00000	0.00325	0.01601	5.79982	0.00014	v.Low
NB-109	Quartz	5540874	0.00004	0.00000	0.00278	0.38822	98.86997	0.17116	0.00000	0.00000	0.00004	0.00180	0.56602	0.00003	H2,CH4,H2C
NB-109	Quartz	1110376	0.00018	0.00000	0.00175	1.02873	94.49899	0.16997	0.00000	0.00000	0.00018	0.00760	4.29281	0.00015	
NB-109	Quartz	418749.2	0.00023	0.06225	0.00122	1.08189	95.79124	0.13892	0.00000	0.00000	0.00023	0.00952	2.91476	0.00009	
NB-109	Quartz	3027328	0.00009	0.00000	0.00236	0.56799	98.02115	0.19972	0.00000	0.00000	0.00009	0.00367	1.20504	0.00007	CH4
NB-109	Quartz	3206894	0.00018	0.00000	0.00201	0.15550	93.90902	0.08541	0.00000	0.00070	0.00018	0.01309	5.83384	0.00026	N2
NB-109	Quartz	1780039	0.00037	0.00000	0.00209	0.25222	90.22281	0.02765	0.00000	0.00048	0.00037	0.01531	9.47940	0.00002	
NB-109	Quartz	829630.9	0.00046	0.00000	0.00276	0.42974	86.84009	0.00793	0.00000	0.00062	0.00046	0.01927	12.69959	0.00000	
NB-109	Quartz	94230.18	0.00110	0.24360	0.00413	1.39441	89.79996	0.00000	0.00000	0.00033	0.00110	0.04592	28.51164	0.00000	Low
NB-110	Quartz	194658.1	0.00020	0.38296	0.00000	0.90896	96.41021	0.01678	0.00000	0.00033	0.00020	0.00824	2.27251	0.00000	
NB-110	Quartz	345681.1	0.00016	0.13112	0.00000	0.36784	97.14555	0.00000	0.00000	0.00000	0.00016	0.00652	2.34896	0.00002	
NB-110	Quartz	1693117	0.00028	0.00000	0.00354	0.28732	97.57693	0.56592	0.00000	0.00089	0.00028	0.01178	1.55332	0.00029	N2,CO2
NB-110	Quartz	1322854	0.00019	0.00000	0.00101	0.27086	95.43567	0.00554	0.00000	0.00055	0.00019	0.00771	4.27851	0.00015	
NB-110	Quartz	70441.4	0.00180	0.75119	0.00000	1.51561	88.15727	0.10286	0.00000	0.00108	0.00180	0.02058	9.44924	0.00036	
NB-110	Quartz	392827.8	0.00022	0.04600	0.00000	0.78718	94.99339	0.16521	0.00000	0.00026	0.00022	0.00906	3.99879	0.00013	
NB-110	Quartz	350918	0.00028	0.02127	0.00128	0.91271	92.58945	0.08308	0.00000	0.00000	0.00028	0.01182	6.38611	0.00027	
NB-110	Quartz	422850.6	0.00061	0.00000	0.00331	1.24041	84.41102	0.00000	0.00000	0.00069	0.00061	0.02555	14.31844	0.00058	N2
NB-110	Quartz	615208.7	0.00044	0.00000	0.00236	0.63690	89.53461	0.00000	0.00000	0.00031	0.00044	0.01829	9.80711	0.00040	N2
NB-111	Pyrite	849680.3	0.00024	0.00000	0.00000	0.03260	98.83224	0.08934	0.00000	0.00009	0.00024	0.00117	1.04425	0.00009	
NB-111	Pyrite	609390.8	0.00052	0.00000	0.00000	0.04056	98.26064	0.02824	0.00000	0.00008	0.00052	0.00006	0.66988	0.00000	
NB-111	Pyrite	3506683	0.00049	0.00000	0.00000	0.05278	97.81666	0.14092	0.00000	0.00011	0.00049	0.00345	1.98555	0.00004	
NB-111	Pyrite	3750622	0.00032	0.00000	0.00000	0.06025	98.06673	0.24168	0.00000	0.00009	0.00032	0.00302	1.62786	0.00004	

	Crush	Counts	Max. Ar	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
DP-624 549'														
DP-624 5 Calcite	6218A	2637950	0.00061	0.00000	0.00000	0.00500	99.95068	0.02809	0.00733	0.00005	0.00061	0.00002	0.00821	0.00000
DP-624 5 Calcite	6218B	4265408	0.00051	0.00000	0.00000	0.00727	99.95833	0.02101	0.00449	0.00001	0.00051	0.00000	0.00838	0.00000
DP-624 5 Calcite	6218C	7598424	0.00038	0.00000	0.00124	0.00836	99.96114	0.01767	0.00222	0.00000	0.00038	0.00000	0.00900	0.00000
DP-624 5 Calcite	6218E	9382940	0.00034	0.00000	0.00071	0.01046	99.96053	0.01571	0.00361	0.00002	0.00034	0.00001	0.00861	0.00000
DP-624 5 Calcite	6218F	12715780	0.00025	0.00000	0.00133	0.00720	99.97270	0.01147	0.00326	0.00003	0.00025	0.00002	0.00374	0.00000
DP-624 5 Calcite	6218I	3909535	0.00011	0.00000	0.00000	0.01485	99.95980	0.00517	0.00073	0.00002	0.00011	0.00003	0.01927	0.00000
	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-4 Calcite	"5391A			0.02481	0.08885	0.26179	97.2355	1.36029	0.25232	0.00109	0.11459	0.19215	0.19328	0.14664
NB-4 Calcite	"5391B			0.52223	0	0.47595	98.5601	0.20244	0.01415	0.02045	0.00709	0.01754	0.14353	0.0065
NB-4 Calcite	"5391C			0.43474	0	0.32661	98.6625	0.27085	0.04656	0.00714	0.00543	0.00667	0.22927	0.00144
NB-4 Calcite	"5391D			0.15035	0	0.14122	99.2272	0.28005	0.04808	0.0051	0.00474	0.0034	0.1308	0.00122
NB-4 Calcite	"5391E			0.4324	0.04474	0.22082	98.9573	0.13132	0.05598	0.00243	0.0015	0.00414	0.14564	0.00047
NB-4 Calcite	"5391F			0.72365	0.14958	0.58104	98.0155	0.2714	0.03465	0.02551	0.00951	0.02319	0.14304	0.00949
NB-4 Calcite	"5391J			0.27618	0	0.15471	99.3008	0.10502	0.04085	0.00157	0.0013	0.0025	0.1143	0.00029
NB-4 Calcite	"5391K			0.17459	0.02134	0.13185	99.5424	0.04508	0.01313	0.00127	0.00067	0.00194	0.06607	0.00024
NB-4 Calcite	"5391L			0.43654	0	0.36641	98.8877	0.13817	0.01962	0.00861	0.00279	0.00771	0.12536	0.00215
NB-4 Calcite	"5391M			0.30485	0.04017	0.24297	99.1664	0.09421	0.0225	0.00296	0.00134	0.00383	0.11745	0.00059
NB-4 Calcite	"5391N			0.32102	0.04063	0.21264	99.1684	0.08937	0.0237	0.00267	0.00131	0.00365	0.13344	0.00052
	Crush	Counts	Ar Max.	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-45 Quartz	5873B			0.879	0.000433	1.886	91.928	0.306	0	0.00756	0.000709	0.0296	4.963	0.000139
NB-45 Quartz	5873C			0.302	0.00457	1.018	91.819	0.0583	0	0.00347	0.00014	0.0287	6.765	0.000098
NB-45 Quartz	5873D			0.327	0.00377	1.17	93.385	0.208	0	0.00426	0.00534	0.0388	4.84	0.00004
NB-45 Quartz	5873E			0.93	0.00341	1.989	91.752	0.528	0	0.00529	0.00568	0.0287	4.76	0.000041
NB-45 Quartz	5873F			0.772	0.00403	1.805	93.281	0.1815	0	0.00377	0.0067	0.0377	3.904	0.000049
NB-45 Quartz	5873G			0.282	0.00333	0.828	93.628	0.308	0	0.0027	0.00358	0.0213	4.92	0.000062
NB-45 Quartz	5873K			0.097	0.00132	0.872	94.157	0.288	0	0.0022	0.00508	0.0328	4.543	0.000022



Sample	H2	He	CH4	H2O	N2	O2	H2S	Ar	CnHm	CO2	SO2
NB-33 Quartz	0.04007	0	1.0585	92.1513	0.273	0	0.01078	0.001224	0.0126	6.4406	0.000064
NB-33 Quartz	0.11	0	0.69849	95.1225	0.127227	0	0.004524	0.000202	0.007926	3.9288	0
NB-33 Quartz	0.1963	0	0.5756	96.9341	0.1003	0	0.003572	0.000177	0.005756	2.1813	0.000021
NB-33 Quartz	0.03756	0.001353	0.8897	93.2174	0.1467	0	0.006761	0.000064	0.011978	5.667	0.000056
NB-33 Quartz	0.26294	0	0.9989	94.8633	0.11388	0	0.004963	0.000279	0.0116	3.7385	0.000023
NB-33 Quartz	0.03701	0.000334	1.038	92.2921	0.20973	0	0.01868	0.000085	0.012587	6.3879	0.000057
NB-33 Quartz	0.060166	0	0.918156	94.4357	0.18667	0	0.005465	0.000118	0.0107	4.3759	0.000041
NB-33 Quartz	0.08587	0.001095	1.0492	92.8296	0.1703	0	0.006119	0.00003	0.013167	5.84	0.000054
NB-33 Quartz	0.031713	0	0.8714	93.4297	0.17365	0	0.00857	0.000501	0.010287	5.466	0.000043
NB-33 Quartz	0.03757	0.003073	1.6103	86.7862	0.23298	0	0.008747	0.000513	0.021385	11.298	0.000072
NB-33 Quartz	0.042226	0.001011	1.365	90.5725	0.28916	0	0.008318	0.000414	0.016812	7.6767	0.000036
NB-33 Quartz	0.124645	0	1.16731	94.6775	0.1851	0	0.006306	0.000332	0.007854	3.82423	0.000011
NB-33 Quartz	0.040523	0.000746	1.28937	93.0304	0.2745	0	0.006485	0.000684	0.01002	5.3568	0.000032
NB-33 Calcite	0	0.000069	0.0689	99.443	0.0422	0	0.000183	0.000791	0.000814	0.44	0
NB-33 Calcite	0	0	0.112	99.442	0.0271	0	0.00041	0.00015	0.000942	0.417	0.000032
NB-33 Calcite	0	0	0.133	99.38	0.033	0	0.000499		0.000994	0.452	0.000039
NB-33 Calcite	0	0	0.11	99.243	0.0247	0	0.000351	0.000266	0.00113	0.62	0.000007
NB-33 Calcite	0	0.000304	0.133	98.998	0.0213	0	0.000508	0.000201	0.00148	0.844	0
NB-33 Calcite	0	0	0.118	99.24	0.0249	0	0.000298	0.000087	0.00112	0.615	0.000007
NB-33 Calcite	0	0	0.0898	99.212	0.0245	0	0.000226	0.000366	0.00102	0.669	0.000003
NB-33 Calcite	0	0.000109	0.099	99.217	0.0247	0	0.00023	0.000243	0.00108	0.657	0.000004
NB-33 Calcite	0	0.00131	0.111	99.29	0.0361	0	0.0003	0.00024	0.00117	0.559	0.000014
NB-33 Calcite	0	0.000024	0.114	99.148	0.0262	0	0.000229	0.000207	0.001317	0.71	0.000007
NB-33 Calcite	0	0.000019	0.0827	99.518	0.0386	0	0.000123	0.000523	0.000558	0.356	0.000003
NB-33 Calcite	0	0.000368	0.122	99.26	0.0468	0	0.000206	0.000635	0.000893	0.566	0.000004

## APPENDIX D

Sample	NB-99	NB-100	NB-102	NB-103	NB-107
Na	0.96	3.38	0.87	1.24	1.05
K	0.9	0.85	0.9	0.3	0.5
Ca	4.2	5.2	0.8	0.7	0.4
Cl	1.44	8.76	0.77	2.16	1.87
F	0.16	0.14	0.18	0.14	0.12
Br	0.01	0.04	<0.01	0.02	0.01
SO <sub>4</sub> <sup>2-</sup>	1.92	1.53	0.62	0	0

Results of bulk ion leach with results reported in ppm. Cations are analyzed by AA whereas anions are analyzed by ion chromatography.

## APPENDIX E

**Sample preparation and irradiation:**

Mineral separate obtained with standard heavy liquid and magnetic techniques. Clays obtained via floatation methods. Samples were irradiated in machined Al discs at the Univ. of Michigan Ford Reactor along with neutron flux monitor Fish Canyon Tuff sanidine, (FC-1) with an assigned age of 27.84 Ma (Deino and Potts, 1990), relative to Mmhb-1 at 520.4 Ma (Samson and Alexander, 1987).

**Instrumentation:**

Mass Analyzer Products 215-50 mass spectrometer on line with automated all-metal extraction system.

Mo double-vacuum resistance furnace:

All samples step-heated.

Reactive gases removed by reaction with 3 SAES GP-50 getters, 2 operated at  $-450^{\circ}\text{C}$  and 1 at  $20^{\circ}\text{C}$ . Gas also exposed to a W filament operated at  $-2000^{\circ}\text{C}$ .

**Analytical parameters:**

NM-64 data: Irradiation duration 24 hours

Electron multiplier sensitivity averaged  $1.0 \times 10^{-16}$  moles/pA.

Total furnace system blanks plus backgrounds were about:

1500, 10, 3, 11,  $11 \times 10^{-18}$  moles at masses 40, 39, 38, 37, and 36, respectively for temperatures  $<1300^{\circ}\text{C}$ .

$(^{40}\text{Ar}/^{39}\text{Ar})_k = 0.025 \pm 0.005$ ;  $(^{36}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00026 \pm 0.00002$ ; and  $(^{39}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00065 \pm 0.00005$ .

NM-80 data: Irradiation duration 24 hours

Electron multiplier sensitivity averaged  $1.0 \times 10^{-16}$  moles/pA.

Total furnace system blanks plus backgrounds were about:

1450, 20, 2, 1,  $5 \times 10^{-18}$  moles at masses 40, 39, 38, 37, and 36, respectively for temperatures  $<1300^{\circ}\text{C}$ .

$(^{40}\text{Ar}/^{39}\text{Ar})_k = 0.021 \pm 0.002$ ;  $(^{36}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00026 \pm 0.00002$ ; and  $(^{39}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00065 \pm 0.00005$ .

NM-95 data: Irradiation duration 24 hours

Electron multiplier sensitivity averaged  $1.0 \times 10^{-16}$  moles/pA.

Total furnace system blanks plus backgrounds were about:

700, 8, 0.5, 4,  $5 \times 10^{-18}$  moles at masses 40, 39, 38, 37, and 36, respectively for temperatures  $<1300^{\circ}\text{C}$ .

$(^{40}\text{Ar}/^{39}\text{Ar})_k = 0.024 \pm 0.002$ ;  $(^{36}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00028 \pm 0.000005$ ; and  $(^{39}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00078 \pm 0.00003$ .

NM-100 data: Irradiation duration 50 hours

Electron multiplier sensitivity averaged  $1.0 \times 10^{-16}$  moles/pA.

Total furnace system blanks plus backgrounds were about:

1000, 10, 1, 0.5,  $3 \times 10^{-18}$  moles at masses 40, 39, 38, 37, and 36, respectively for temperatures  $<1300^{\circ}\text{C}$ .

$(^{40}\text{Ar}/^{39}\text{Ar})_k = 0.0275 \pm 0.0001$ ;  $(^{36}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00028 \pm 0.000003$ ; and  $(^{39}\text{Ar}/^{39}\text{Ar})_{ca} = 0.00076 \pm 0.00002$ .

J-factors determined to a precision of  $\pm 0.1\%$  by  $\text{CO}_2$  laser-fusion of 4 single crystals from each of 4 or 6 radial positions around the irradiation tray.

Correction factors for interfering nuclear reactions were determined using K-glass and  $\text{CaF}_2$  and are as follows:

**Age calculations:**

Total gas ages and errors calculated by weighting individual steps by the fraction of  $^{39}\text{Ar}$  released.

Plateau ages calculated for the indicated steps by weighting each step by the inverse of the variance.

Plateau age errors calculated using the method of (Taylor, 1982).

MSWD values are calculated for n-1 degrees of freedom for plateau ages.

If the MSWD is outside the 95% confidence window (cf. Mahon, 1996; Table 1), the error is multiplied by the square root of the MSWD.

Isochron data regressed using York (1969) method.

Decay constants and isotopic abundances after Steiger and Jäger (1977).

All final errors reported at  $\pm 2\sigma$ , unless otherwise noted.

## APPENDIX F

ID	Temp (°C)	<sup>40</sup> Ar/ <sup>39</sup> Ar	<sup>37</sup> Ar/ <sup>39</sup> Ar	<sup>36</sup> Ar/ <sup>39</sup> Ar (x 10 <sup>-3</sup> )	<sup>39</sup> Ar <sub>K</sub> (x 10 <sup>-16</sup> mol)	K/Ca	<sup>40</sup> Ar* (%)	<sup>39</sup> Ar (%)	Age (Ma)	±1σ (Ma)
<b>Cortez Biotite, wt. = 0.93 mg, J=0.0034332, NM-64, Lab#=7709-01</b>										
A	600	25.89	0.0387	82.27	15.8	13.2	6.0	1.9	9.6	3.0
B	750	9.400	0.0170	14.41	74.7	29.9	54.4	10.6	31.42	0.60
C	850	7.385	0.0100	4.956	123	51.0	79.8	25.0	36.16	0.34
D	920	7.090	0.0083	4.065	104	61.6	82.7	37.1	35.96	0.37
E	1000	7.134	0.0093	4.324	235	54.9	81.7	64.6	35.76	0.20
F	1075	6.454	0.0075	2.126	230	68.1	89.9	91.5	35.58	0.19
G	1110	7.238	0.0287	3.968	33.0	17.8	83.5	95.4	37.0	1.1
H	1180	9.782	0.3364	11.99	12.5	1.5	63.8	96.8	38.3	2.8
I	1210	7.338	0.4471	3.830	27.2	1.1	84.7	100.0	38.1	1.3
<b>total gas age</b>			n=9		855	51.8			<b>35.09</b>	<b>0.88*</b>
<b>plateau</b>			MSWD=1.31	n=7	steps C-I	764	54.7	89.4	<b>35.80</b>	<b>0.24*</b>
<b>NB-20 Fine Illite, wt. = 3.95 mg, J=0.0034782, NM-64, Lab#=7672-01</b>										
B	500	5.426	0.0228	3.388	59.8	22.4	81.1	1.8	27.41	0.61
C	550	13.93	0.0220	1.964	139	23.2	95.7	6.1	81.73	0.30
E	625	14.49	0.1031	0.6720	377	4.9	98.5	17.8	87.41	0.21
F	650	15.32	0.0855	0.3578	356	6.0	99.2	28.8	92.90	0.22
G	675	16.15	0.0779	0.2538	606	6.6	99.4	47.4	98.03	0.23
H	700	16.95	0.0919	0.2286	749	5.6	99.5	70.5	102.87	0.22
I	730	17.33	0.0976	0.2807	669	5.2	99.4	91.2	105.00	0.23
J	760	18.12	0.0589	0.4635	111	8.7	99.1	94.6	109.36	0.39
K	800	22.15	0.0473	0.9291	117	10.8	98.7	98.2	132.16	0.40
L	850	37.14	0.1254	3.260	28.2	4.1	97.4	99.1	213.8	1.3
M	950	42.56	0.2413	7.092	16.3	2.1	95.1	99.6	237.6	2.1
N	1250	23.39	0.4009	14.46	14.1	1.3	81.8	100.0	116.2	2.4
<b>total gas age</b>			n=12		3243	7.0			<b>100.19</b>	<b>0.27</b>
<b>NB-20 Coarse Illite, wt. 3.52 mg, J=0.0034500, NM-64, Lab#=7674-01</b>										
B	500	9.379	0.0120	3.018	85.7	42.5	90.2	2.8	52.66	0.43
C	550	15.46	0.0109	1.554	108	46.7	96.9	6.3	92.15	0.36
D	600	14.75	0.0104	0.4704	203	49.1	98.9	12.9	89.84	0.27
E	625	15.62	0.0107	0.4446	288	47.5	99.0	22.3	95.10	0.25
F	650	16.04	0.0104	0.2153	406	49.1	99.5	35.4	98.01	0.22
G	675	16.36	0.0099	0.1624	532	51.3	99.6	52.7	100.05	0.24
H	700	16.84	0.0093	0.2020	576	54.9	99.5	71.4	102.83	0.23
I	730	17.59	0.0090	0.1848	542	56.8	99.6	89.0	107.31	0.24
J	760	20.85	0.0094	0.4129	220	54.5	99.3	96.1	126.21	0.32
K	800	29.05	0.0093	0.5130	49.4	54.7	99.4	97.8	173.66	0.75
L	850	49.10	0.0138	2.013	51.0	37.1	98.7	99.4	282.75	0.95
M	950	86.03	0.0271	8.198	12.0	18.9	97.2	99.8	463.0	3.1
N	1250	24.53	0.0735	43.72	6.25	6.9	47.3	100.0	71.8	5.7
<b>total gas age</b>			n=13		3079	51.6			<b>106.28</b>	<b>0.60*</b>

ID	Temp (°C)	$^{40}\text{Ar}/^{39}\text{Ar}$	$^{37}\text{Ar}/^{39}\text{Ar}$	$^{36}\text{Ar}/^{39}\text{Ar}$ ( $\times 10^{-3}$ )	$^{39}\text{Ar}_K$ ( $\times 10^{-16}$ mol)	K/Ca	$^{40}\text{Ar}^*$ (%)	$^{39}\text{Ar}$ (%)	Age (Ma)	$\pm 1\sigma$ (Ma)
<b>NB-19 Illite, wt.= 4.07 mg, J=0.0034297, NM-64, Lab#=7676-01</b>										
B	500	8.202	0.0326	8.626	83.7	15.6	68.6	3.8	34.50	0.48
C	550	12.70	0.0291	3.831	140	17.5	90.9	10.1	70.04	0.31
D	600	13.59	0.0194	-4.4523	5.44	26.4	109.5	10.4	89.8	5.8
E	625	17.95	0.0276	0.8412	468	18.5	98.5	31.6	106.21	0.23
F	650	19.99	0.0272	0.4759	298	18.7	99.2	45.0	118.71	0.28
G	675	21.61	0.0267	0.4778	322	19.1	99.2	59.6	128.05	0.29
H	700	24.71	0.0258	0.5383	279	19.8	99.3	72.3	145.73	0.35
I	730	30.20	0.0250	0.6925	232	20.4	99.2	82.8	176.54	0.49
J	760	37.36	0.0251	0.9964	143	20.3	99.2	89.2	215.75	0.49
K	800	42.99	0.0261	1.366	60.2	19.5	99.0	92.0	245.84	0.77
L	850	52.59	0.0292	1.424	82.8	17.5	99.2	95.7	296.84	0.76
M	950	53.42	0.0448	5.091	37.2	11.4	97.1	97.4	295.5	1.2
N	1250	5.126	0.0700	3.327	57.5	7.3	80.4	100.0	25.34	0.61
<b>total gas age</b>			n=13		2209	18.5			<b>137.54</b>	<b>0.78*</b>
<b>Cortez K-feldspar, wt. = 0.88 mg, J=0.0034276, NM-64, Lab#=7705-01</b>										
C	800	10.63	0.0058	16.45	164	88.4	54.0	8.2	35.19	0.43
E	900	6.960	0.0103	7.218	10.0	49.8	69.0	8.7	29.5	3.8
F	900	6.975	0.0059	4.619	26.3	85.8	80.1	10.0	34.2	1.4
G	1000	6.217	0.0045	1.896	52.3	113.1	90.6	12.6	34.50	0.74
H	1100	6.008	0.0050	1.031	145	101.4	94.5	19.9	34.78	0.28
I	1200	6.028	0.0050	1.113	288	101.8	94.1	34.2	34.75	0.17
J	1250	5.827	0.0047	0.3657	304	109.2	97.7	49.4	34.87	0.15
K	1300	5.869	0.0048	0.4003	292	107.2	97.6	63.9	35.06	0.16
L	1350	6.011	0.0046	0.7785	175	111.9	95.8	72.7	35.25	0.23
M	1400	6.000	0.0046	0.7441	195	111.2	95.9	82.4	35.24	0.22
N	1750	6.391	0.0050	2.338	352	101.4	88.8	100.0	34.76	0.16
<b>total gas age</b>			n=11		2003	104.1			<b>34.91</b>	<b>0.50*</b>
<b>plateau</b>			MSWD=0.93	n=11	steps C-N	2003		100.0	<b>34.93</b>	<b>0.13*</b>
<b>NB-59 Illite, wt. = 10.64 mg, J=0.0037063, NM-80, Lab#=8602-01</b>										
B	500	6.986	0.0055	3.780	89.6	92.7	83.7	1.8	38.69	0.17
C	550	17.14	0.0062	2.269	87.5	81.7	96.0	3.6	106.77	0.20
D	600	14.43	0.0074	1.240	34.7	68.9	97.3	4.3	91.51	0.28
E	625	15.41	0.0049	0.7376	308	103.8	98.5	10.5	98.71	0.19
F	650	16.01	0.0063	0.6135	409	80.7	80.7	18.7	102.74	0.18
G	675	16.36	0.0061	0.5560	558	84.3	98.9	30.0	105.05	0.18
H	700	16.71	0.0047	0.5889	681	108.8	98.8	43.7	107.20	0.27
I	740	17.21	0.0042	0.6749	993	120.1	98.7	63.7	110.20	0.21
J	780	19.88	0.0040	0.8429	882	127.8	98.6	81.4	126.56	0.29
K	800	28.88	0.0042	1.836	361	121.6	98.0	88.7	180.03	0.33
L	850	47.04	0.0043	2.302	242	118.6	98.5	93.6	285.94	0.58
M	900	72.48	0.0065	3.489	101	78.1	98.5	95.6	423.72	0.79
N	1000	64.71	0.0486	4.012	80.6	10.5	98.1	97.3	381.35	0.72
O	1650	5.729	0.0191	4.769	136	26.7	75.1	100.0	28.53	0.16
<b>total gas age</b>			n=14		4965	104.9			<b>131.52</b>	<b>0.54*</b>

ID	Temp (°C)	<sup>40</sup> Ar/ <sup>39</sup> Ar	<sup>37</sup> Ar/ <sup>39</sup> Ar	<sup>36</sup> Ar/ <sup>39</sup> Ar (x 10 <sup>-3</sup> )	<sup>39</sup> Ar <sub>K</sub> (x 10 <sup>-16</sup> mol)	K/Ca	<sup>40</sup> Ar* (%)	<sup>39</sup> Ar (%)	Age (Ma)	±1σ (Ma)
<b>93271 K-feldspar, wt. = 6.97 mg, J=0.0039260, NM-95, Lab#=9577-01</b>										
A	700	8.384	0.0222	11.18	104	23.0	60.3	1.3	35.48	0.47
B	800	5.263	0.0125	0.4233	317	40.9	97.2	5.4	35.87	0.13
C	900	5.170	0.0097	0.2097	651	52.4	98.4	13.7	35.658	0.090
D	1000	5.149	0.0085	0.1580	1217	59.7	98.6	29.3	35.623	0.074
E	1100	5.138	0.0081	0.1011	1590	63.0	99.0	49.6	35.658	0.073
F	1200	5.155	0.0078	0.1150	1303	65.4	98.9	66.3	35.752	0.069
G	1250	5.146	0.0069	0.0412	1876	73.9	99.3	90.3	35.836	0.073
H	1300	5.137	0.0082	0.0648	758	61.9	99.2	100.0	35.729	0.078
<b>total gas age</b>			n=8		7815	63.1			<b>35.72</b>	<b>0.16*</b>
<b>plateau</b>			n=8	steps A-H	7815	63.1		100.0	<b>35.72</b>	<b>0.06*</b>
<b>93271 Biotite, wt. = 8.35 mg, J=0.003911, NM-95, Lab#=9576-01</b>										
A	650	32.68	0.0674	103.6	126	7.6	6.3	1.6	14.5	1.1
B	750	7.611	0.0254	9.468	483	20.1	62.9	7.8	33.49	0.17
C	830	5.493	0.0070	1.182	972	72.4	93.2	20.1	35.767	0.079
D	900	5.352	0.0060	0.6091	1122	85.2	96.2	34.4	35.966	0.075
E	970	5.403	0.0078	0.8376	935	65.4	95.0	46.3	35.848	0.080
F	1050	5.408	0.0124	0.7288	1149	41.0	95.6	61.0	36.111	0.071
G	1120	5.305	0.0214	0.5701	2200	23.9	96.4	89.0	35.724	0.073
H	1180	5.305	0.3993	0.7169	571	1.3	96.2	96.3	35.656	0.093
I	1240	5.406	0.6488	0.8043	257	0.79	96.2	99.6	36.32	0.15
J	1350	6.463	0.1303	3.989	35.2	3.9	81.6	100.0	36.81	0.92
<b>total gas age</b>			n=10		7849	43.1			<b>35.38</b>	<b>0.22*</b>
<b>plateau</b>			MSWD=4.93**	n=8	steps C-J	7240	45.3	92.2	<b>35.88</b>	<b>0.14*</b>
<b>NB-102 Sericite, wt. 5.71 mg, J=0.0039223, NM-95, Lab#=9574-01</b>										
A	600	25.59	0.0288	33.45	62.6	17.7	61.3	11.9	107.71	0.84
B	630	16.64	0.0190	2.594	68.8	26.9	95.3	25.0	108.79	0.53
C	660	15.96	0.0131	0.8573	54.3	39.0	98.3	35.4	107.68	0.63
D	690	15.47	0.0095	0.8151	35.0	53.5	98.3	42.0	104.50	0.94
E	720	15.05	0.0108	0.8740	63.5	47.4	98.1	54.1	101.56	0.55
F	750	14.64	0.0170	1.100	56.9	30.1	97.6	65.0	98.38	0.62
G	780	14.15	0.0256	0.8151	51.3	20.0	98.1	74.7	95.70	0.68
H	810	13.77	0.0349	0.8174	33.5	14.6	98.1	81.1	93.1	1.0
I	840	13.28	0.0415	0.9153	13.7	12.3	97.8	83.7	89.7	2.5
J	870	12.92	0.0547	0.0123	9.17	9.3	99.8	85.5	89.0	3.7
K	900	11.90	0.0578	0.4717	5.23	8.8	98.7	86.5	81.2	6.5
L	1000	9.373	0.0765	3.602	9.60	6.7	88.5	88.3	57.7	3.6
M	1100	6.075	0.0932	5.187	12.8	5.5	74.5	90.7	31.7	2.8
N	1200	4.227	0.0856	6.170	10.7	6.0	56.5	92.8	16.8	3.4
O	1300	4.426	0.0954	10.26	12.5	5.4	31.1	95.2	9.7	3.0
P	1650	11.76	0.1630	25.52	25.4	3.1	35.8	100.0	29.5	1.6
<b>total gas age</b>			n=16		525	26.3			92.0	1.1

ID	Temp (°C)	$^{40}\text{Ar}/^{39}\text{Ar}$	$^{37}\text{Ar}/^{39}\text{Ar}$	$^{36}\text{Ar}/^{39}\text{Ar}$ ( $\times 10^{-3}$ )	$^{39}\text{Ar}_K$ ( $\times 10^{-16}$ mol)	K/Ca	$^{40}\text{Ar}^*$ (%)	$^{39}\text{Ar}$ (%)	Age (Ma)	$\pm 1\sigma$ (Ma)
<b>JM-coarse Biotite, wt. 2.77 mg, J=0.0078027, NM-100, Lab#=9912-01</b>										
B	680	13.54	0.1147	10.63	117	4.4	76.7	2.2	140.5	1.3
C	750	11.86	0.0146	1.862	441	35.0	95.1	10.6	152.17	0.48
D	820	11.43	0.0035	0.3904	1168	147.6	98.8	32.7	152.30	0.47
E	900	11.40	0.0050	0.2238	946	103.0	99.2	50.6	152.59	0.39
F	950	11.43	0.0176	0.3452	363	28.9	98.9	57.5	152.44	0.43
G	1025	11.34	0.0298	0.3961	576	17.1	98.7	68.4	151.19	0.38
H	1200	11.43	0.0581	0.3363	1475	8.8	98.9	96.4	152.56	0.39
I	1300	12.89	0.7204	5.296	192	0.71	88.1	100.0	153.30	0.73
total gas age			n=8		5278	60.5			152.08	0.95*
plateau		MSWD=1.91	n=7	steps C-I	5161	61.8		97.8	152.24	0.33*
<b>JM-fine Biotite, wt. = 3.41 mg, J=0.0076919, NM-100, Lab#=9914-01</b>										
A	600	9.180	0.0178	21.72	182	28.7	29.8	2.5	37.57	0.94
B	680	4.965	0.0074	6.569	221	69.3	60.4	5.6	41.12	0.61
C	750	3.351	0.0018	1.463	563	281.7	86.3	13.3	39.69	0.24
D	820	2.872	0.0011	0.3869	777	463.4	95.1	24.1	37.50	0.17
E	900	2.724	0.0010	0.2206	979	528.8	96.6	37.6	36.15	0.16
F	950	2.766	0.0010	0.2928	632	530.9	95.9	46.3	36.44	0.20
G	1025	2.749	0.0011	0.2833	1319	474.7	96.0	64.5	36.24	0.12
H	1200	2.753	0.0032	0.2893	2226	161.2	95.9	95.3	36.272	0.094
I	1300	3.207	0.0124	1.668	343	41.1	83.8	100.0	36.91	0.36
total gas age			n=9		7242	330.2			36.87	0.38*
plateau		MSWD=1.12	n=5	steps E-I	5500	336.8		75.9	36.28	0.12*

ID	Temp (°C)	$^{40}\text{Ar}/^{39}\text{Ar}$	$^{37}\text{Ar}/^{39}\text{Ar}$	$^{36}\text{Ar}/^{39}\text{Ar}$ ( $\times 10^{-3}$ )	$^{39}\text{Ar}_k$ ( $\times 10^{-16}$ mol)	K/Ca	$^{40}\text{Ar}^*$ (%)	$^{39}\text{Ar}$ (%)	Age (Ma)	$\pm 1\sigma$ (Ma)
<b>JM-coarse K-feldspar, wt. = 14.24 mg, J=0.0077880, NM-100, Lab#=9913-01</b>										
A	450	312.0	0.0345	28.99	51.8	14.8	97.2	0.2	2188.1	3.8
B	450	7.912	0.0093	2.521	13.6	55.1	90.2	0.3	97.6	2.2
C	500	18.30	0.0155	1.543	61.8	33.0	97.4	0.6	234.49	0.74
D	500	5.459	0.0149	1.099	41.2	34.2	93.6	0.7	70.38	0.82
E	550	34.39	0.0161	1.996	190	31.8	98.2	1.6	421.30	0.85
F	550	4.466	0.0350	1.236	85.8	14.6	91.3	1.9	56.37	0.28
G	600	16.01	0.0416	1.356	238	12.3	97.3	3.0	206.66	0.42
H	600	4.046	0.0615	1.058	121	8.3	91.7	3.5	51.41	0.26
I	650	9.282	0.0631	0.8432	246	8.1	97.1	4.5	122.36	0.27
J	650	4.076	0.0739	0.9930	151	6.9	92.3	5.2	52.09	0.22
K	700	6.622	0.0724	0.6828	257	7.0	96.6	6.3	87.73	0.21
L	700	4.281	0.0707	0.8728	172	7.2	93.5	7.0	55.36	0.19
M	750	6.240	0.0671	0.9878	110	7.6	95.0	7.5	81.40	0.29
N	800	6.905	0.0705	0.5824	299	7.2	97.2	8.8	91.91	0.22
O	850	5.730	0.0615	0.3675	443	8.3	97.7	10.7	77.00	0.18
P	900	5.242	0.0677	0.3073	561	7.5	97.8	13.2	70.67	0.16
Q	950	6.134	0.0769	2.920	612	6.6	85.6	15.8	72.30	0.23
R	1000	6.161	0.0702	0.7217	640	7.3	96.2	18.6	81.40	0.19
S	1050	7.148	0.0494	0.3319	721	10.3	98.3	21.7	96.11	0.23
T	1100	8.676	0.0282	0.3747	908	18.1	98.4	25.6	116.17	0.27
U	1100	8.951	0.0172	0.4027	1483	29.7	98.4	32.0	119.66	0.26
V	1100	9.257	0.0144	0.4799	1721	35.4	98.2	39.5	123.39	0.26
W	1100	9.638	0.0147	0.7734	1886	34.8	97.4	47.7	127.24	0.27
X	1100	10.40	0.0158	0.9366	1833	32.3	97.1	55.6	136.61	0.37
Y	1100	11.44	0.0175	1.469	1816	29.1	96.0	63.5	148.01	0.29
Z	1230	11.90	0.0247	0.4127	649	20.7	98.8	66.3	158.00	0.32
ZA	1280	11.49	0.0191	0.2172	1969	26.7	99.2	74.8	153.50	0.51
ZB	1330	11.42	0.0116	0.1393	4440	44.0	99.4	94.0	152.86	0.37
ZC	1430	10.58	0.1661	0.4387	871	3.1	98.6	97.8	140.98	0.31
ZD	1530	10.43	0.1460	0.7142	449	3.5	97.8	99.7	137.93	0.33
ZE	1650	14.11	0.1750	9.826	63.6	2.9	79.3	100.0	150.84	0.72
<b>total gas age</b>			n=31		23101	26.6			<b>136.37</b>	<b>0.65*</b>



ID	Temp (°C)	$^{40}\text{Ar}/^{39}\text{Ar}$	$^{37}\text{Ar}/^{39}\text{Ar}$	$^{36}\text{Ar}/^{39}\text{Ar}$ (x 10 <sup>-3</sup> )	$^{39}\text{Ar}_K$ (x 10 <sup>-16</sup> mol)	K/Ca	$^{40}\text{Ar}^*$ (%)	$^{39}\text{Ar}$ (%)	Age (Ma)	$\pm 1\sigma$ (Ma)
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**JM-fine K-feldspar, wt. = 9.73 mg, J=0.0076364, NM-100, Lab#=9915-01**

A	550	10.91	0.0584	24.38	32.5	8.7	33.8	0.1	50.1	1.7
B	550	4.009	0.0446	3.615	13.3	11.4	72.8	0.2	39.7	1.9
C	600	3.187	0.0493	0.6886	17.5	10.3	92.9	0.3	40.3	1.4
D	600	3.195	0.0489	1.581	30.1	10.4	84.6	0.4	36.88	0.89
E	650	3.352	0.0496	3.578	14.7	10.3	67.8	0.5	31.0	1.7
F	750	2.672	0.0170	0.3439	245.8	30.0	95.2	1.6	34.72	0.13
G	850	2.611	0.0070	0.1484	722.0	72.7	97.3	4.8	34.654	0.087
H	950	2.597	0.0061	0.0558	1493	84.2	98.3	11.6	34.839	0.074
I	1025	2.584	0.0059	0.0497	1800	86.6	98.4	19.7	34.685	0.088
J	1100	2.586	0.0057	0.0454	2434	90.3	98.4	30.6	34.726	0.082
K	1150	2.586	0.0056	0.0981	1569	91.1	97.8	37.7	34.519	0.074
L	1200	2.578	0.0056	0.0587	1952	91.2	98.3	46.4	34.571	0.071
M	1250	2.584	0.0055	0.0381	3010	93.3	98.5	60.0	34.738	0.078
N	1350	2.600	0.0054	0.0218	6412	94.8	98.7	88.8	35.011	0.076
O	1600	2.676	0.0058	0.1642	2485	87.7	97.2	100.0	35.471	0.081
<b>total gas age</b>			n=15		22232	89.5			<b>34.90</b>	<b>0.17*</b>
<b>plateau</b>	MSWD=1.12		n=7	steps F-L	10216	86.3		46.7	<b>34.66</b>	<b>0.12*</b>

**Notes:**

Isotopic ratios corrected for blank, radioactive decay, and mass discrimination, not corrected for interfering reactions.

Individual analyses show analytical error only; total gas age error includes error in J and irradiation parameters.

n= number of heating steps

K/Ca = molar ratio calculated from reactor produced  $^{39}\text{Ar}_K$  and  $^{37}\text{Ar}_{Ca}$ .

\* 2 $\sigma$  error

Sample	Mineral	Lab #	Plateau age		Plateau		Steps (Plateau)	Isochron age		$^{40}\text{Ar}/^{36}\text{Ar}_i$		Steps (Isochron)	Isochron MSWD
			(Ma)	(Ma)	Error (Ma)	MSWD		(Ma)	Error (Ma)	325	Error		
Cortez	Biotite	7709	35.8	0.24	1.31	C-I	35.17	0.76	325	34	C-I	1.01	
Cortez	K-feldspar	7705	34.93	0.13	0.93	C-N	34.92	0.15	296.2	8.8	C-N	1.16	
93271	Biotite	9576	35.88	0.14	4.93*	C-I	35.83	0.59	310	35	C-I	8.78*	
93271	K-feldspar	9577	35.72	0.06	1.04	A-H	35.72	0.08	293	12	A-H	1.38	
JM-fine	Biotite	9914	36.28	0.12	1.12	E-I	36.12	0.22	332	42	E-I	0.32	
JM-fine	K-feldspar	9915	34.66	0.06	1.98	F-L	34.67	0.11	290	58	F-L	2.88	
JM-fine	K-feldspar	9915	-	-	-	M-O	34.78	0.47	603	100	M-O	11.1*	
JM-coarse	Biotite	9912	152.2	0.33	1.91	C-I	152.1	0.46	310	22	C-I	2.19	
JM-coarse	K-feldspar	9913	-	-	-	-	-	-	-	-	-	-	

All errors  $2\sigma$

\* MSWD outside 95% confidence level, error multiplied by square root MSWD

## APPENDIX G

## ISOCHORES CALCULATIONS THAT TAKE GAS CONTENT INTO ACCOUNT

## H2O-CO2-NaCl

Stack	Sample	Inclusion	Length	Width		
NB107	NB107	1				
T	P (Bowers & Helgeson)					
192.9	609		Tm clath	7.3	CO2 Den	0.22
200	642		Th CO2 L-V	23	CO2 MV	199.67
220	1190		Th to	vapor	Aqueous Den	1.031
240	1726		CO2 VolFrac	0.05	Molal NaCl	0.93
260	2250		T of Estim	23	Wt% NaCl	5.154
280	2763		Th Total	192.9	X(NaCl)	0.016
300	3268		L-V	L	Bulk XH2O	0.979
320	3765				Bulk XCO2	0.005
340	4255				Bulk XNaCl	0.016
360	4738		Th	P @ Th	Bulk Den	0.991
380	5215		192.9	609	Bulk MV	18.98
400	5687					
NB107	NB107	2				
T	P (Bowers & Helgeson)					
			Tm clath	7.1	CO2 Den	0.22
233	1544		Th CO2 L-V	23	CO2 MV	199.67
240	1730		Th to	vapor	Aqueous Den	1.034
260	2251		CO2 VolFrac	0.05	Molal NaCl	0.997
280	2763		T of Estim	23	Wt% NaCl	5.507
300	3266		Th Total	233.1	X(NaCl)	0.018
320	3761		L-V	L	Bulk XH2O	0.978
340	4250				Bulk XCO2	0.005
360	4732				Bulk XNaCl	0.018
380	5209		Th	P @ Th	Bulk Den	0.993
400	5680		233.1	1544	Bulk MV	18.977
NB107	NB107	3				
T	P (Bowers & Helgeson)					
			Tm clath	7.2	CO2 Den	0.22
225.2	1323		Th CO2 L-V	23	CO2 MV	199.67
240	1720		Th to	vapor	Aqueous Den	1.034
260	2242		CO2 VolFrac	0.05	Molal NaCl	0.997
280	2754		T of Estim	23	Wt% NaCl	5.507
300	3257		Th Total	225.2	X(NaCl)	0.018
320	3752		L-V	L	Bulk XH2O	0.978
340	4241				Bulk XCO2	0.005
360	4723				Bulk XNaCl	0.018
380	5199		Th	P @ Th	Bulk Den	0.993
400	5671		225.2	1323	Bulk MV	18.977
NB107	NB107	4				
T	P (Bowers & Helgeson)					
			Tm clath	7.3	CO2 Den	0.22
224	1293		Th CO2 L-V	23	CO2 MV	199.67
240	1726		Th to	vapor	Aqueous Den	1.031
260	2250		CO2 VolFrac	0.05	Molal NaCl	0.93
280	2763		T of Estim	23	Wt% NaCl	5.154
300	3268		Th Total	224	X(NaCl)	0.016
320	3765		L-V	L	Bulk XH2O	0.979
340	4255				Bulk XCO2	0.005
360	4738				Bulk XNaCl	0.016
380	5215		Th	P @ Th	Bulk Den	0.991
400	5687		224	1293	Bulk MV	18.98

NB107		NB107		10					
T	P (Bowers & Helgeson)								
220.1	649	Tm clath	7.9	CO2 Den	0.22				
240	1154	Th CO2 L-V	23	CO2 MV	199.67				
260	1646	Th to	vapor	Aqueous Den	1.023				
280	2126	CO2 VolFrac	0.08	Molal NaCl	0.727				
300	2597	T of Estim	23	Wt% NaCl	4.074				
320	3058	Th Total	220.1	X(NaCl)	0.013				
340	3512	L-V	L	Bulk XH2O	0.979				
360	3958			Bulk XCO2	0.008				
380	4399			Bulk XNaCl	0.013				
400	4833	Th	P @ Th	Bulk Den	0.958				
		220.1	649	Bulk MV	19.55				
NB107		NB107		11					
T	P (Bowers & Helgeson)								
214.7	677	Tm clath	7.8	CO2 Den	0.22				
220	819	Th CO2 L-V	23	CO2 MV	199.67				
240	1337	Th to	vapor	Aqueous Den	1.024				
260	1841	CO2 VolFrac	0.07	Molal NaCl	0.761				
280	2334	T of Estim	23	Wt% NaCl	4.256				
300	2817	Th Total	214.7	X(NaCl)	0.014				
320	3291	L-V	L	Bulk XH2O	0.98				
340	3757			Bulk XCO2	0.007				
360	4217			Bulk XNaCl	0.013				
380	4670	Th	P @ Th	Bulk Den	0.968				
400	5117	214.7	677	Bulk MV	19.358				
NB107		NB107		12					
T	P (Bowers & Helgeson)								
210.5	721	Tm clath	6.3	CO2 Den	0.22				
220	962	Th CO2 L-V	23	CO2 MV	199.67				
240	1456	Th to	vapor	Aqueous Den	1.045				
260	1943	CO2 VolFrac	0.06	Molal NaCl	1.264				
280	2424	T of Estim	23	Wt% NaCl	6.878				
300	2899	Th Total	210.5	X(NaCl)	0.022				
320	3368	L-V	L	Bulk XH2O	0.972				
340	3831			Bulk XCO2	0.006				
360	4290			Bulk XNaCl	0.022				
380	4744	Th	P @ Th	Bulk Den	0.995				
400	5193	210.5	721	Bulk MV	19.149				
NB107		NB107		13					
T	P (Bowers & Helgeson)								
203.7	561	Tm clath	7.9	CO2 Den	0.22				
220	1009	Th CO2 L-V	23	CO2 MV	199.67				
240	1544	Th to	vapor	Aqueous Den	1.023				
260	2066	CO2 VolFrac	0.06	Molal NaCl	0.727				
280	2575	T of Estim	23	Wt% NaCl	4.074				
300	3074	Th Total	203.7	X(NaCl)	0.013				
320	3564	L-V	L	Bulk XH2O	0.981				
340	4046			Bulk XCO2	0.006				
360	4521			Bulk XNaCl	0.013				
380	4989	Th	P @ Th	Bulk Den	0.974				
400	5451	203.7	561	Bulk MV	19.174				

NB107		NB107		5			
T	P (Bowers & Helgeson)						
		Tm clath	7.2	CO2 Den	0.725		
		Th CO2 L-V	24.1	CO2 MV	60.733		
300	1746	Th to	liquid	Aqueous Den	1.032		
310	1892	CO2 VolFrac	0.4	Molal NaCl	0.964		
320	2038	T of Estim	24.1	Wt% NaCl	5.331		
340	2326	Th Total	310	X(NaCl)	0.017		
360	2612	L-V	L	Bulk XH2O	0.82		
380	2894			Bulk XCO2	0.166		
400	3173			Bulk XNaCl	0.014		
420	3448	Th	P @ Th	Bulk Den	0.909		
440	3719	310	1892	Bulk MV	25.191		

NB107		NB107		6			
T	P (Bowers & Helgeson)						
		Tm clath	6.8	CO2 Den	0.729		
		Th CO2 L-V	23.8	CO2 MV	60.387		
300	1766	Th to	liquid	Aqueous Den	1.038		
310	1911.5	CO2 VolFrac	0.4	Molal NaCl	1.098		
320	2057	T of Estim	23.8	Wt% NaCl	6.028		
340	2346	Th Total	310	X(NaCl)	0.019		
360	2632	L-V	L	Bulk XH2O	0.817		
380	2915			Bulk XCO2	0.167		
400	3195			Bulk XNaCl	0.016		
420	3471	Th	P @ Th	Bulk Den	0.914		
440	3743	310	1911.5	Bulk MV	25.159		

NB107		NB107		7			
T	P (Bowers & Helgeson)						
		Tm clath	7.1	CO2 Den	0.22		
221.6	1241	Th CO2 L-V	23	CO2 MV	199.67		
240	1730	Th to	vapor	Aqueous Den	1.034		
260	2251	CO2 VolFrac	0.05	Molal NaCl	0.997		
280	2763	T of Estim	23	Wt% NaCl	5.507		
300	3266	Th Total	221.6	X(NaCl)	0.018		
320	3761	L-V	L	Bulk XH2O	0.978		
340	4250			Bulk XCO2	0.005		
360	4732			Bulk XNaCl	0.018		
380	5209	Th	P @ Th	Bulk Den	0.993		
400	5680	221.6	1241	Bulk MV	18.977		

NB107		NB107		9			
T	P (Bowers & Helgeson)						
		Tm clath	7.4	CO2 Den	0.268		
227.8	1047	Th CO2 L-V	26.8	CO2 MV	164.472		
240	1361	Th to	vapor	Aqueous Den	1.029		
260	1859	CO2 VolFrac	0.07	Molal NaCl	0.896		
280	2346	T of Estim	26.8	Wt% NaCl	4.976		
300	2825	Th Total	227.8	X(NaCl)	0.016		
320	3296	L-V	L	Bulk XH2O	0.976		
340	3759			Bulk XCO2	0.008		
360	4217			Bulk XNaCl	0.016		
380	4668	Th	P @ Th	Bulk Den	0.975		
400	5114	227.8	1047	Bulk MV	19.343		



H<sub>2</sub>O-NaCl-[KCl]

Stack	Sample	Inclusion			
NB-33	NB-33			1	
T	P (Bodnar & Vityk)	P(gases)	P(Total)		
	188.4	8			Tm ice -5.4
	200	206	911	1117	Th L-V 188.4
	220	549	811	1360	Th to L
	240	891	714	1605	Molal NaCl 1.56
	260	1233	625	1858	Wt% NaCl 8.38
	280	1575	546	2121	X(NaCl) 0.03
	300	1917	471	2388	Crit.Temp. 451
	320	2259	405	2664	Crit.Press. 426
	340	2601	348	2949	Bulk Den 0.942
	360	2943	297	3240	Bulk MV 20.4
	380	3285	253	3538	
	400	3627	215	3842	

NB-33	NB-33	Inclusion			
NB-33	NB-33			2	
T	P (Bodnar & Vityk)	P(gases)	P(Total)		
	179.4	7			Tm ice -5.2
	180	18			Th L-V 179.4
	200	369	911	1280	Th to L
	220	720	811	1531	Molal NaCl 1.51
	240	1071	714	1785	Wt% NaCl 8.1
	260	1423	625	2048	X(NaCl) 0.03
	280	1774	546	2320	Crit.Temp. 449
	300	2125	471	2596	Crit.Press. 419
	320	2476	405	2881	Bulk Den 0.948
	340	2828	348	3176	Bulk MV 20.27
	360	3179	297	3476	
	380	3530	253	3783	
	400	3882	215	4097	

NB-33	NB-33	Inclusion			
NB-33	NB-33			-4.9	
T	P (Bodnar & Vityk)	P(gases)	P(Total)		
	202.5	9	911	920	Tm ice -4.9
	220	291	811	1102	Th L-V 202.5
	240	614	714	1328	Th to L
	260	937	625	1562	Molal NaCl 1.42
	280	1259	546	1805	Wt% NaCl 7.68
	300	1582	471	2053	X(NaCl) 0.02
	320	1905	405	2310	Crit.Temp. 445
	340	2227	348	2575	Crit.Press. 408
	360	2550	297	2847	Bulk Den 0.925
	380	2873	253	3126	Bulk MV 20.36
	400	3196	215	3411	

NB-33	NB-33	Inclusion			
NB-33	NB-33			8	
T	P (Bodnar & Vityk)	P(gases)	P(Total)		
	204.5	10	911	921	Tm ice -5.1
	220	259	811	1070	Th L-V 204.5
	240	581	714	1295	Th to L
	260	902	625	1527	Molal NaCl 1.48
	280	1224	546	1770	Wt% NaCl 7.96
	300	1546	471	2017	X(NaCl) 0.03
	320	1867	405	2272	Crit.Temp. 448
	340	2189	348	2537	Crit.Press. 415
	360	2510	297	2807	Bulk Den 0.925
	380	2832	253	3085	Bulk MV 20.79

NB-33		NB33 CALCITE		9			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	222.8	14				Tm ice	-1.8
	240	263	51	314		Th L-V	222.8
	260	552	44	596		Th to	L
	280	841	37	878		Molal NaCl	0.52
	300	1130	31	1161		Wt% NaCl	2.96
	320	1419	26	1445		X(NaCl)	0.01
	340	1709	22	1731		Crit.Temp.	401
	360	1998	18	2016		Crit.Press.	288
	380	2287	15	2302		Bulk Den	0.862
	400	2576				Bulk MV	21.37

NB-33		NB33 CALCITE		10			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	218.7	13				Tm ice	-2
	220	32	59	91		Th L-V	218.7
	240	326	51	377		Th to	L
	260	619	44	663		Molal NaCl	0.58
	280	913	37	950		Wt% NaCl	3.28
	300	1207	31	1238		X(NaCl)	0.01
	320	1500	26	1526		Crit.Temp.	404
	340	1794	22	1816		Crit.Press.	296
	360	2087	18	2105		Bulk Den	0.871
	380	2381	15	2396		Bulk MV	21.16

NB-33		NB33 CALCITE		11			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	235.3	18				Tm ice	-2
	240	83	51	134		Th L-V	235.3
	260	359	44	403		Th to	L
	280	636	37	673		Molal NaCl	0.58
	300	912	31	943		Wt% NaCl	3.28
	320	1189	26	1215		X(NaCl)	0.01
	340	1465	22	1487		Crit.Temp.	404
	360	1742	18	1760		Crit.Press.	296
	380	2018	15	2033		Bulk Den	0.848
	400	2295				Bulk MV	21.72

H2O-NaCl-[KCl]		Sample		Inclusion			
Stack		NB-47		1			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	195.6	9				Tm ice	-4.5
	200	81	214	295		Th L-V	195.6
	220	409	195	604		Th to	L
	240	737	176	913		Molal NaCl	1.31
	260	1065	158	1223		Wt% NaCl	7.11
	280	1393	141	1534		X(NaCl)	0.02
	300	1722	124	1846		Crit.Temp.	440
	320	2050	109	2159		Crit.Press.	393
	340	2378	95	2473		Bulk Den	0.927
	360	2706	83	2789		Bulk MV	20.3
	380	3034	71	3105			
	400	3362					



NB47		NB-47					
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	168.6	6				Tm ice	-3
	180	204				Th L-V	168.6
	200	551	214	765		Th to	L
	220	898	195	1093		Molal NaCl	0.87
	240	1246	176	1422		Wt% NaCl	4.86
	260	1593	158	1751		X(NaCl)	0.02
	280	1940	141	2081		Crit.Temp.	419
	300	2287	124	2411		Crit.Press.	336
	320	2634	109	2743		Bulk Den	0.936
	340	2982	95	3077		Bulk MV	20.11
	360	3329	83	3412			
	380	3676	71	3747			
	400	4023					
NB47		NB-47					
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	188.9	8				Tm ice	-4
	200	192	214	406		Th L-V	188.9
	220	525	195	720		Th to	L
	240	857	176	1033		Molal NaCl	1.16
	260	1190	158	1348		Wt% NaCl	6.37
	280	1522	141	1663		X(NaCl)	0.02
	300	1854	124	1978		Crit.Temp.	433
	320	2187	109	2296		Crit.Press.	375
	340	2519	95	2614		Bulk Den	0.928
	360	2851	83	2934		Bulk MV	20.28
	380	3184	71	3255			
	400	3516					
NB47		NB-47					
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	194	8				Tm ice	-4.4
	200	107	214	321		Th L-V	194
	220	436	195	631		Th to	L
	240	765	176	941		Molal NaCl	1.28
	260	1094	158	1252		Wt% NaCl	6.96
	280	1424	141	1565		X(NaCl)	0.02
	300	1753	124	1877		Crit.Temp.	439
	320	2082	109	2191		Crit.Press.	390
	340	2411	95	2506		Bulk Den	0.928
	360	2740	83	2823		Bulk MV	20.29
	380	3070	71	3141			
	400	3399					
NB47		NB-47					
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	195.3	9				Tm ice	-4.6
	200	86	214	300		Th L-V	195.3
	220	415	195	610		Th to	L
	240	744	176	920		Molal NaCl	1.34
	260	1073	158	1231		Wt% NaCl	7.25
	280	1402	141	1543		X(NaCl)	0.02
	300	1731	124	1855		Crit.Temp.	441
	320	2060	109	2169		Crit.Press.	397
	340	2389	95	2484		Bulk Den	0.929
	360	2718	83	2801		Bulk MV	20.27
	380	3047	71	3118			
	400	3376					

NB47		NB-47		6			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	178.8	7				Tm ice	-5.1
	180	28				Th L-V	178.8
	200	379	214	593		Th to	L
	220	731	195	926		Molal NaCl	1.48
	240	1082	176	1258		Wt% NaCl	7.96
	260	1433	158	1591		X(NaCl)	0.03
	280	1784	141	1925		Crit.Temp.	448
	300	2136	124	2260		Crit.Press.	415
	320	2487	109	2596		Bulk Den	0.948
	340	2838	95	2933		Bulk MV	20.28
	360	3189	83	3272			
	380	3541	71	3612			
	400	3892					

NB47		NB-47		7			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	177.2	7				Tm ice	-5.1
	180	56				Th L-V	177.2
	200	410	214	624		Th to	L
	220	763	195	958		Molal NaCl	1.48
	240	1116	176	1292		Wt% NaCl	7.96
	260	1469	158	1627		X(NaCl)	0.03
	280	1822	141	1963		Crit.Temp.	448
	300	2175	124	2299		Crit.Press.	415
	320	2528	109	2637		Bulk Den	0.949
	340	2881	95	2976		Bulk MV	20.26
	360	3234	83	3317			
	380	3588	71	3659			
	400	3941					

NB47		NB-47		8			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	179.6	7				Tm ice	
	180	14				Th L-V	179.6
	200	344	214	558		Th to	L
	220	675	195	870		Molal NaCl	0
	240	1006	176	1182		Wt% NaCl	0
	260	1337	158	1495		X(NaCl)	0
	280	1668	141	1809		Crit.Temp.	374
	300	1999	124	2123		Crit.Press.	218
	320	2330	109	2439		Bulk Den	0.891
	340	2660	95	2755		Bulk MV	20.22
	360	2991	83	3074			
	380	3322	71	3393			
	400	3653					

NB47		NB-47		9			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	186.2	8				Tm ice	-5.2
	200	245	214	459		Th L-V	186.2
	220	588	195	783		Th to	L
	240	931	176	1107		Molal NaCl	1.51
	260	1275	158	1433		Wt% NaCl	8.1
	280	1618	141	1759		X(NaCl)	0.03
	300	1961	124	2085		Crit.Temp.	449
	320	2305	109	2414		Crit.Press.	419
	340	2648	95	2743		Bulk Den	0.943
	360	2991	83	3074		Bulk MV	20.4
	380	3335	71	3406			
	400	3678					

NB47	NB-47		14			
T	P (Bodnar & Vityk)	P(gases)	P(Total)			
	194.1	8			Tm ice	-4.9
	200	106	214	320	Th L-V	194.1
	220	438	195	633	Th to	L
	240	770	176	946	Molal NaCl	1.42
	260	1103	158	1261	Wt% NaCl	7.68
	280	1435	141	1576	X(NaCl)	0.02
	300	1767	124	1891	Crit.Temp.	445
	320	2099	109	2208	Crit.Press.	408
	340	2432	95	2527	Bulk Den	0.933
	360	2764	83	2847	Bulk MV	20.18
	380	3096	71	3167		
	400	3428				

NB47	NB-47		15			
T	P (Bodnar & Vityk)	P(gases)	P(Total)			
	172.8	6			Tm ice	-6.4
	180	139			Th L-V	172.8
	200	507	214	721	Th to	L
	220	875	195	1070	Molal NaCl	1.84
	240	1244	176	1420	Wt% NaCl	9.71
	260	1612	158	1770	X(NaCl)	0.03
	280	1980	141	2121	Crit.Temp.	463
	300	2348	124	2472	Crit.Press.	459
	320	2717	109	2826	Bulk Den	0.964
	340	3085	95	3180	Bulk MV	19.94
	360	3453	83	3536		
	380	3822	71	3893		
	400	4190				

NB47	NB-47		16			
T	P (Bodnar & Vityk)	P(gases)	P(Total)			
	181.7	7			Tm ice	-6.3
	200	333	214	547	Th L-V	181.7
	220	690	195	885	Th to	L
	240	1046	176	1222	Molal NaCl	1.81
	260	1402	158	1560	Wt% NaCl	9.58
	280	1759	141	1900	X(NaCl)	0.03
	300	2115	124	2239	Crit.Temp.	462
	320	2472	109	2581	Crit.Press.	456
	340	2828	95	2923	Bulk Den	0.956
	360	3185	83	3268	Bulk MV	20.11
	380	3541	71	3612		
	400	3897				

NB47	NB-47		17			
T	P (Bodnar & Vityk)	P(gases)	P(Total)			
	175.6	7			Tm ice	-6.4
	180	87			Th L-V	175.6
	200	452	214	666	Th to	L
	220	817	195	1012	Molal NaCl	1.84
	240	1182	176	1358	Wt% NaCl	9.71
	260	1546	158	1704	X(NaCl)	0.03
	280	1911	141	2052	Crit.Temp.	463
	300	2276	124	2400	Crit.Press.	459
	320	2641	109	2750	Bulk Den	0.962
	340	3005	95	3100	Bulk MV	19.99
	360	3370	83	3453		
	380	3735	71	3806		
	400	4100				

NB47		NB-47		18			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	178.2	7				Tm ice	-6.3
	180	39				Th L-V	178.2
	200	400	214	614		Th to	L
	220	761	195	956		Molal NaCl	1.81
	240	1122	176	1298		Wt% NaCl	9.58
	260	1483	158	1641		X(NaCl)	0.03
	280	1843	141	1984		Crit.Temp.	462
	300	2204	124	2328		Crit.Press.	456
	320	2565	109	2674		Bulk Den	0.959
	340	2926	95	3021		Bulk MV	20.05
	360	3287	83	3370			
	380	3647	71	3718			
	400	4008					

NB47		NB-47		19			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	180.6	7				Tm ice	-6.3
	200	354	214	568		Th L-V	180.6
	220	712	195	907		Th to	L
	240	1070	176	1246		Molal NaCl	1.81
	260	1427	158	1585		Wt% NaCl	9.58
	280	1785	141	1926		X(NaCl)	0.03
	300	2143	124	2267		Crit.Temp.	462
	320	2501	109	2610		Crit.Press.	456
	340	2859	95	2954		Bulk Den	0.957
	360	3216	83	3299		Bulk MV	20.09
	380	3574	71	3645			
	400	3932					

NB47		NB-47		20			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	202.1	9				Tm ice	-5.1
	220	299	195	494		Th L-V	202.1
	240	624	176	800		Th to	L
	260	948	158	1106		Molal NaCl	1.48
	280	1272	141	1413		Wt% NaCl	7.96
	300	1596	124	1720		X(NaCl)	0.03
	320	1921	109	2030		Crit.Temp.	448
	340	2245	95	2340		Crit.Press.	415
	360	2569	83	2652		Bulk Den	0.927
	380	2894	71	2965		Bulk MV	20.74
	400	3218					

NB47		NB-47		22			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	204.8	10				Tm ice	-5
	220	254	195	449		Th L-V	204.8
	240	574	176	750		Th to	L
	260	895	158	1053		Molal NaCl	1.45
	280	1216	141	1357		Wt% NaCl	7.82
	300	1536	124	1660		X(NaCl)	0.03
	320	1857	109	1966		Crit.Temp.	446
	340	2178	95	2273		Crit.Press.	411
	360	2498	83	2581		Bulk Den	0.924
	380	2819	71	2890		Bulk MV	20.82
	400	3140					

NB47		NB-47		23			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	179.2	7				Tm ice	-5
	180	21				Th L-V	179.2
	200	371	214	585		Th to	L
	220	721	195	916		Molal NaCl	1.45
	240	1071	176	1247		Wt% NaCl	7.82
	260	1421	158	1579		X(NaCl)	0.03
	280	1771	141	1912		Crit.Temp.	446
	300	2121	124	2245		Crit.Press.	411
	320	2471	109	2580		Bulk Den	0.947
	340	2821	95	2916		Bulk MV	20.31
	360	3171	83	3254			
	380	3521	71	3592			
	400	3871					

NB47		NB-47		24			
T	P (Bodnar & Vityk)	P(gases)	P(Total)				
	177.2	7				Tm ice	-5.2
	180	57				Th L-V	177.2
	200	410	214	624		Th to	L
	220	764	195	959		Molal NaCl	1.51
	240	1118	176	1294		Wt% NaCl	8.1
	260	1472	158	1630		X(NaCl)	0.03
	280	1826	141	1967		Crit.Temp.	449
	300	2180	124	2304		Crit.Press.	419
	320	2534	109	2643		Bulk Den	0.95
	340	2887	95	2982		Bulk MV	20.23
	360	3241	83	3324			
	380	3595	71	3666			
	400	3949					

H2O-NaCl-[KCl]		Stack		Sample		Inclusion	
T	P (Bodnar & Vityk)						
	196.5	9					6
	200	67	1124	1191		Tm ice	-5.3
	220	399	1000	1399		Th L-V	196.5
	240	731	883	1614		Th to	L
	260	1063	776	1839		Molal NaCl	1.54
	280	1395	679	2074		Wt% NaCl	8.24
	300	1727	592	2319		X(NaCl)	0.03
	320	2059	513	2572		Crit.Temp.	450
	340	2391	443	2834		Crit.Press.	422
	360	2723	381	3104		Bulk Den	0.935
	380	3055	326	3381		Bulk MV	20.57
	400	3387					

104w		NB-104		7			
T	P (Bodnar & Vityk)						
	204.6	10				Tm ice	-5.2
	220	258	1000	1258		Th L-V	204.6
	240	580	883	1463		Th to	L
	260	902	776	1678		Molal NaCl	1.51
	280	1224	679	1903		Wt% NaCl	8.1
	300	1546	592	2138		X(NaCl)	0.03
	320	1868	513	2381		Crit.Temp.	449
	340	2190	443	2633		Crit.Press.	419
	360	2512	381	2893		Bulk Den	0.926
	380	2834	326	3160		Bulk MV	20.76

104w	NB-104		8			
T	P (Bodnar & Vityk)					
	198.1	9			Tm ice	-5.2
	200	40	1124	1164	Th L-V	198.1
	220	370	1000	1370	Th to	L
	240	699	883	1582	Molal NaCl	1.51
	260	1029	776	1805	Wt% NaCl	8.1
	280	1358	679	2037	X(NaCl)	0.03
	300	1688	592	2280	Crit.Temp.	449
	320	2017	513	2530	Crit.Press.	419
	340	2347	443	2790	Bulk Den	0.932
	360	2676	381	3057	Bulk MV	20.63
	380	3006	326	3332		
NB99	NB99		1			
T	P (Bodnar & Vityk)					
	242.3	21			Tm ice	-3.8
	260	264			Th L-V	242.3
	280	538			Th to	L
	300	812			Molal NaCl	1.11
	320	1086			Wt% NaCl	6.08
	340	1360			X(NaCl)	0.02
	360	1634			Crit.Temp.	430
	380	1908			Crit.Press.	367
	400	2182			Bulk Den	0.867
	420	2456			Bulk MV	21.72
NB99	NB99		2			
T	P (Bodnar & Vityk)					
	237.2	19			Tm ice	-5.6
	240	59			Th L-V	237.2
	260	346			Th to	L
	280	634			Molal NaCl	1.62
	300	921			Wt% NaCl	8.65
	320	1208			X(NaCl)	0.03
	340	1495			Crit.Temp.	454
	360	1783			Crit.Press.	432
	380	2070			Bulk Den	0.897
	400	2357			Bulk MV	21.45
NB99	NB99		3			
T	P (Bodnar & Vityk)					
	217.1	12			Tm ice	-4.4
	220	56			Th L-V	217.1
	240	360			Th to	L
	260	664			Molal NaCl	1.28
	280	967			Wt% NaCl	6.96
	300	1271			X(NaCl)	0.02
	320	1575			Crit.Temp.	439
	340	1879			Crit.Press.	390
	360	2182			Bulk Den	0.904
	380	2486			Bulk MV	20.82
NB99	NB99		4			
T	P (Bodnar & Vityk)					
	224.1	14			Tm ice	-4.2
	240	249			Th L-V	224.1
	260	544			Th to	L
	280	839			Molal NaCl	1.22
	300	1134			Wt% NaCl	6.67
	320	1430			X(NaCl)	0.02
	340	1725			Crit.Temp.	436
	360	2020			Crit.Press.	382
	380	2315			Bulk Den	0.894
	400	2610			Bulk MV	21.06

NB99		NB99		5		
T	P (Bodnar & Vityk)					
	199.3		9		Tm ice	-5.9
	200		21		Th L-V	199.3
	220		353		Th to	L
	240		685		Molal NaCl	1.7
	260		1018		Wt% NaCl	9.05
	280		1350		X(NaCl)	0.03
	300		1683		Crit.Temp.	458
	320		2015		Crit.Press.	442
	340		2347		Bulk Den	0.938
	360		2680		Bulk MV	20.51
	380		3012			
	400		3345			
	420		3677			

NB99		NB99		6		
T	P (Bodnar & Vityk)					
	198		9		Tm ice	-5.2
	200		42		Th L-V	198
	220		372		Th to	L
	240		701		Molal NaCl	1.51
	260		1031		Wt% NaCl	8.1
	280		1360		X(NaCl)	0.03
	300		1690		Crit.Temp.	449
	320		2020		Crit.Press.	419
	340		2349		Bulk Den	0.932
	360		2679		Bulk MV	20.63
	380		3009			
	400		3338			
	420		3668			

NB99		NB99		7		
T	P (Bodnar & Vityk)					
	206.3		10		Tm ice	-4.7
	220		227		Th L-V	206.3
	240		545		Th to	L
	260		862		Molal NaCl	1.37
	280		1179		Wt% NaCl	7.39
	300		1496		X(NaCl)	0.02
	320		1814		Crit.Temp.	442
	340		2131		Crit.Press.	401
	360		2448		Bulk Den	0.919
	380		2765		Bulk MV	20.48
	400		3083			
	420		3400			

NB99		NB99		8		
T	P (Bodnar & Vityk)					
	222.8		14		Tm ice	-3.5
	240		267		Th L-V	222.8
	260		560		Th to	L
	280		854		Molal NaCl	1.02
	300		1148		Wt% NaCl	5.62
	320		1441		X(NaCl)	0.02
	340		1735		Crit.Temp.	426
	360		2029		Crit.Press.	355
	380		2322		Bulk Den	0.887
	400		2616		Bulk MV	21.23

NB99	NB99	9		
T	P (Bodnar & Vityk)			
	203.5	10	Tm ice	-3.3
	220	268	Th L-V	203.5
	240	581	Th to	L
	260	895	Molal NaCl	0.96
	280	1208	Wt% NaCl	5.32
	300	1521	X(NaCl)	0.02
	320	1834	Crit.Temp.	423
	340	2147	Crit.Press.	348
	360	2460	Bulk Den	0.906
	380	2774	Bulk MV	20.79
NB99	NB99	10		
T	P (Bodnar & Vityk)			
	205.2	10	Tm ice	-4.3
	220	244	Th L-V	205.2
	240	560	Th to	L
	260	877	Molal NaCl	1.25
	280	1193	Wt% NaCl	6.81
	300	1509	X(NaCl)	0.02
	320	1825	Crit.Temp.	437
	340	2142	Crit.Press.	386
	360	2458	Bulk Den	0.916
	380	2774	Bulk MV	20.56
NB99	NB99	11		
T	P (Bodnar & Vityk)			
	216.9	12	Tm ice	-3.7
	220	59	Th L-V	216.9
	240	359	Th to	L
	260	660	Molal NaCl	1.08
	280	961	Wt% NaCl	5.93
	300	1262	X(NaCl)	0.02
	320	1562	Crit.Temp.	429
	340	1863	Crit.Press.	363
	360	2164	Bulk Den	0.896
	380	2465	Bulk MV	21.01
NB99	NB99	12		
T	P (Bodnar & Vityk)			
	226	15	Tm ice	-4.9
	240	222	Th L-V	226
	260	519	Th to	L
	280	815	Molal NaCl	1.42
	300	1112	Wt% NaCl	7.68
	320	1408	X(NaCl)	0.02
	340	1704	Crit.Temp.	445
	360	2001	Crit.Press.	408
	380	2297	Bulk Den	0.901
	400	2594	Bulk MV	20.9



## APPENDIX H

Formulae for the salinity and temperature correction of Henry's Law Constants as supplied by Drummond (1981). These formulae are valid for 0 - 6 molal solutions in the temperature range of 25 - 400°C, pressures up to 500 bar and 3 mole percent of gas.

All determinations of fugacity is in the following form:

$$\text{fugacity} = K_H * X$$

where  $K_H$  is the value for Henry's Law constants and X is the molar concentration of the gas.

H<sub>2</sub>

$$\ln K_H = A + BT + C/T + DT^2 + Em$$

T = Temperature in Kelvin

m = NaCl molality

A = 5.91

B = 0.01632

C = -340.0

D = -2.769 x 10<sup>-5</sup>

E = 0.2021

CO<sub>2</sub>

$$\ln K_H = A + BT + CX + D/T + E/X + FXT + GX/T + HT/X$$

T = Temperature in Kelvin

X = NaCl molality + 1.0

A = 20.244

B = -0.016323

C = -1.0312

D = -3629.7

E = 0.4445

F = 0.0012806

G = 255.9

H = -0.001606

CH<sub>4</sub>

$$\ln K_H = A + BP + CT + DX + E/T + F/X + G/P + HP/X + IP/T + JTX$$

- P = CH<sub>4</sub> pressure in atm.  
 T = Temperature in Kelvin  
 X = NaCl molality + 1.0  
 A = 26.187  
 B = 0.0013647  
 C = -0.026991  
 D = 0.1169  
 E = -3380.7  
 F = -0.2409  
 G = -0.2779  
 H = 0.0001919  
 I = -0.1428  
 J = 0.0002778

H<sub>2</sub>S

$$\ln K_H = A + BT + CX + D/T + E/X + FXT + GX/T + HT/X$$

- T = Temperature in Kelvin  
 X = NaCl molality + 1.0  
 A = 11.416  
 B = -0.007013  
 C = 0.2905  
 D = -2067.7  
 E = 0.5705  
 F = -0.0001574  
 G = -46.2  
 H = -0.001777

The following calculations for Henry's Law constants, applied to simple apolar gases, is taken from Prini and Crovetto (1989) and are valid from ambient temperatures to the T<sub>max</sub> show.

Formulae take the form of:

$$\ln K_H = A_1 + A_2 \cdot 10^3/T + A_3 \cdot 10^6/T^2 + A_4 \cdot 10^9/T^3 + A_5 \cdot 10^{12}/T^4$$

System	A <sub>1</sub>	A <sub>2</sub>	A <sub>3</sub>	A <sub>4</sub>	A <sub>5</sub>	σ	T <sub>max</sub> (K)
He-H <sub>2</sub> O	-7.1725	5.9734	-0.9038			5.9	588.7
Ne-H <sub>2</sub> O	-5.9825	5.5176	-0.8886			3.2	543.4
Ar-H <sub>2</sub> O	-7.8972	7.0178	-1.2649			2.7	568.4
Kr-H <sub>2</sub> O	-7.5642	6.8773	-1.3047			2.9	525.6
Xe-H <sub>2</sub> O	-9.3604	7.9654	-1.5167			12.9	574.8
O <sub>2</sub> -H <sub>2</sub> O	-15.9766	15.7951	-4.3331	0.3502		5.0	616.0
CH <sub>4</sub> -H <sub>2</sub> O	-18.5223	17.7956	-4.8318	0.3856		3.3	633.0
H <sub>2</sub> -H <sub>2</sub> O	-46.0050	64.8729	32.9118	7.6094	-0.6673	10.8	636.0
N <sub>2</sub> -H <sub>2</sub> O	-55.5386	77.9340	-13.9781	9.2813	-0.8226	8.9	636.0

Above 573 K and up to the critical temperature, T<sub>cl</sub>, the following formulae are better suited:

$$\ln K_H = (B_0/T) \cdot (T_{cl} - T) \cdot \ln((T_{cl} - T)/T_{cl}) + \sum_{i=0}^n (B_{i+1})/T^i (1000)^i$$

where B<sub>0</sub> has a value between 0 and -4, usually -1.

System	B <sub>1</sub>	B <sub>2</sub>	B <sub>3</sub>	B <sub>4</sub>	B <sub>5</sub>	σ
He-H <sub>2</sub> O	-6.4859	5.2327	-0.8086			6.5
Ne-H <sub>2</sub> O	-5.3238	4.7936	-0.7959			2.1
Ar-H <sub>2</sub> O	-7.1874	6.2632	-1.1676			1.5
Kr-H <sub>2</sub> O	-7.0173	6.2204	-1.2220			4.0
Xe-H <sub>2</sub> O	-8.7307	7.2588	-1.4265			11.8
O <sub>2</sub> -H <sub>2</sub> O	-13.3190	12.8557	-3.4516	0.2592		4.7
CH <sub>4</sub> -H <sub>2</sub> O	-15.5767	14.5624	-3.8519	0.2838		2.5
C <sub>2</sub> H <sub>6</sub> -H <sub>2</sub> O	-20.6180	19.3949	-5.2453	0.3956		2.7
H <sub>2</sub> -H <sub>2</sub> O	-38.4512	53.4846	-27.4317	6.3522	-0.5590	10.6
N <sub>2</sub> -H <sub>2</sub> O	-47.7453	66.7623	-34.2820	7.9705	-0.7094	8.4